

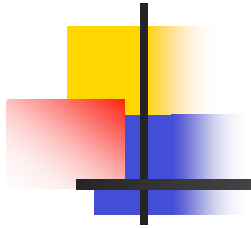
Cost effective electronics for LAr and photo-detectors readout

S. Centro (ICARUS Collaboration)

Università di Padova / INFN Padova

European Strategy for Future Neutrino Physics

CERN, 1-3 October 2009

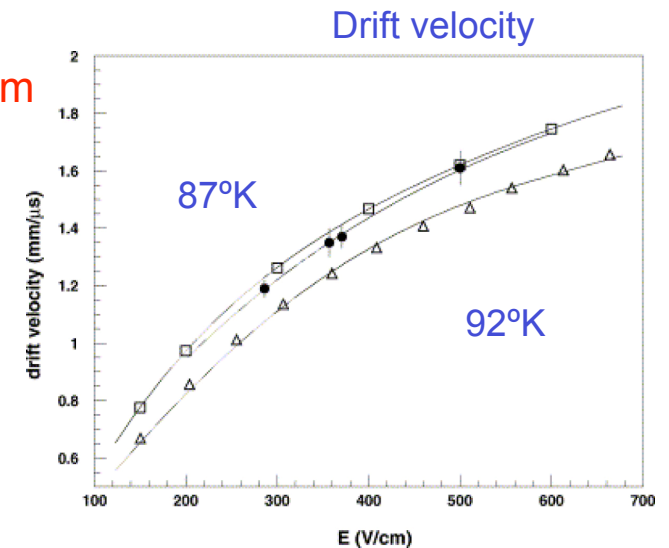
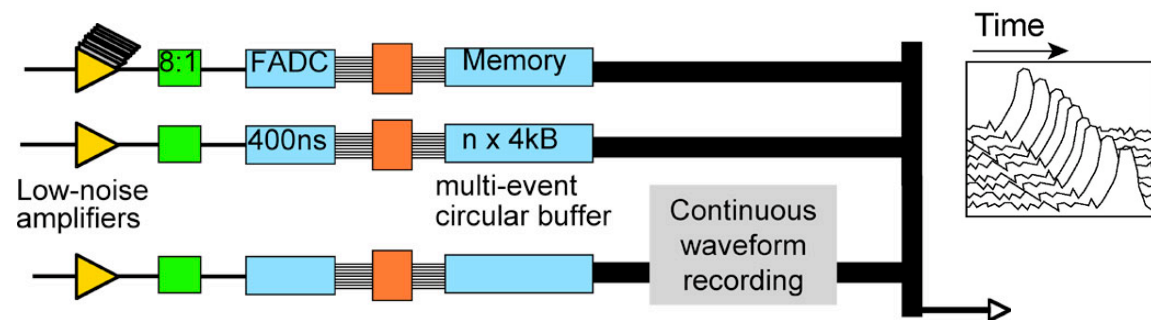
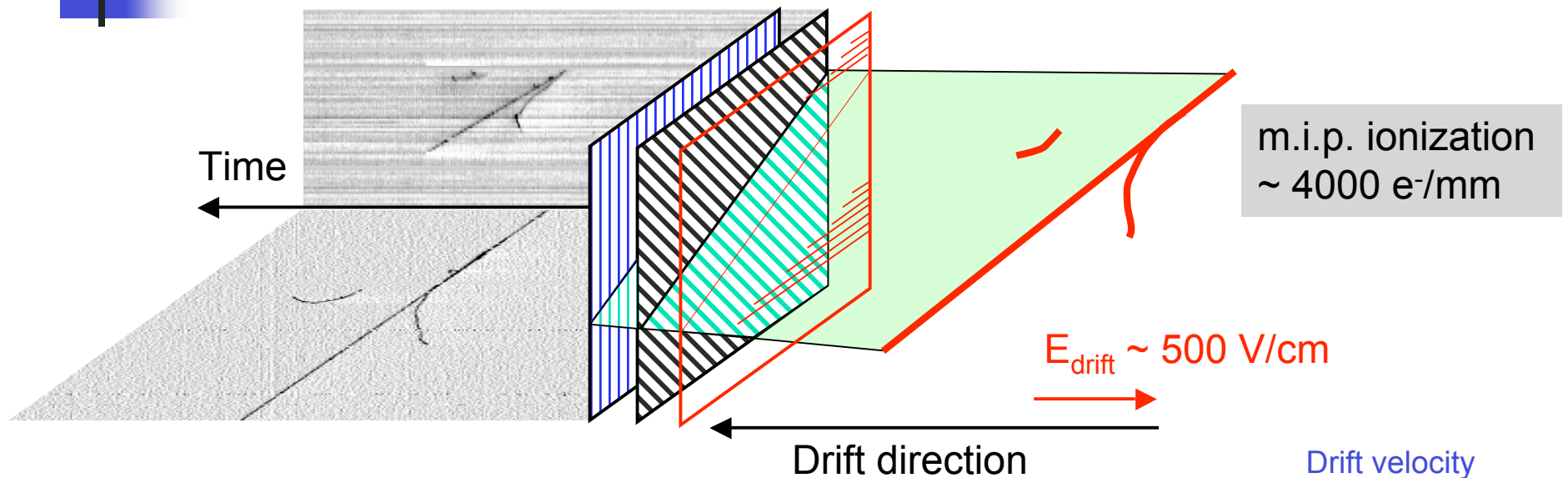


Outline

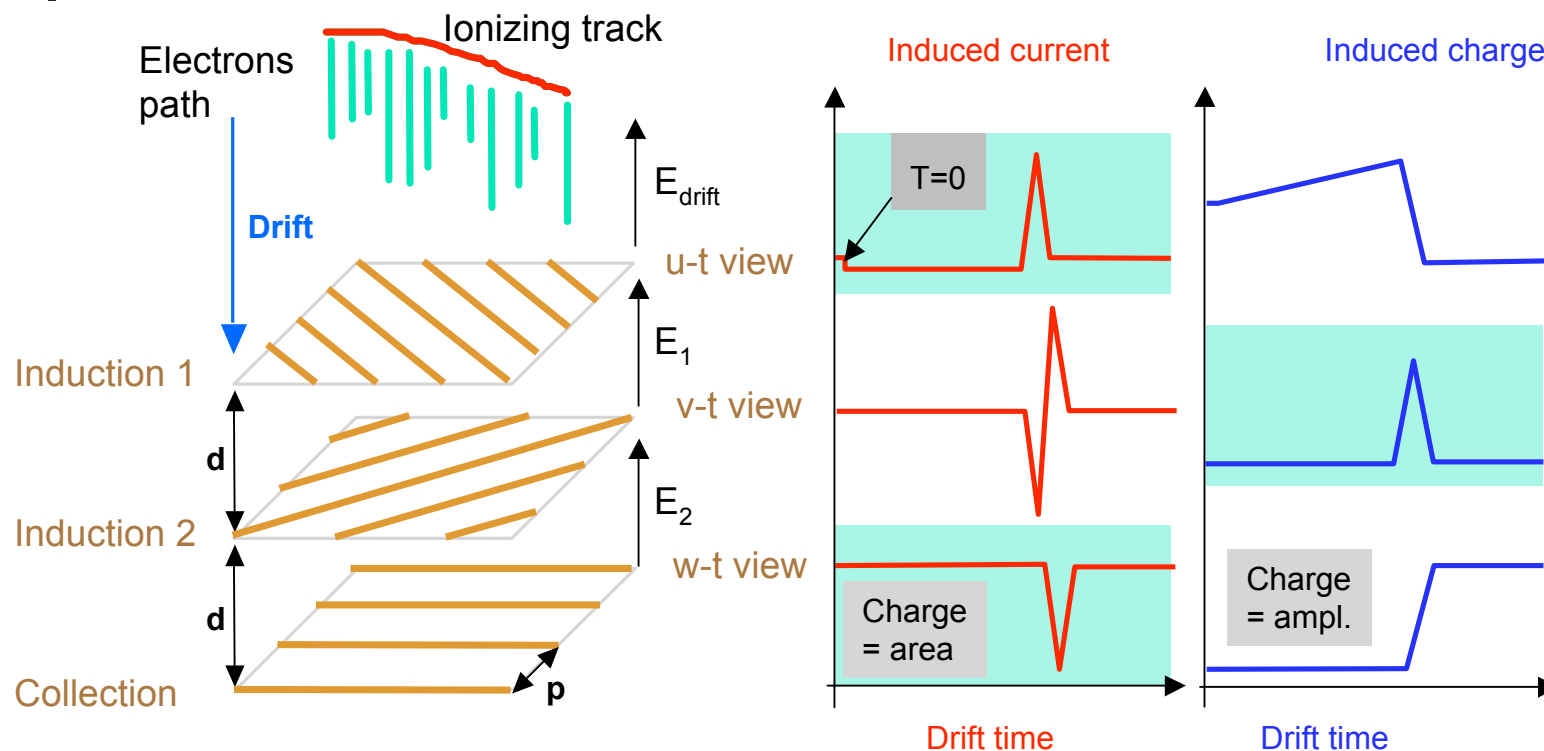
- Charge signals from *liquid* Argon TPC
 - Characteristics and critical issues
 - A proven architecture
 - Toward updated schemes

- Light signals from *liquid & gaseous* Argon
 - Characteristics and critical issues
 - Basic DAQ architecture

The ICARUS-like read-out



The induction/collection signals

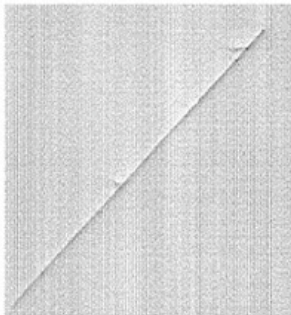


- ICARUS T600: three wire planes (pitch 3mm, separation 3mm)

$E_{\text{drift}} = 500 \text{ V/cm}$
 Mip signal $\sim 12000 \text{ e}^-$ (inc. recombination)
 Electron drift velocity $\sim 1.5 \text{ mm}/\mu\text{s}$
 Typical grid transit time $\sim 2\text{-}3 \mu\text{s}$

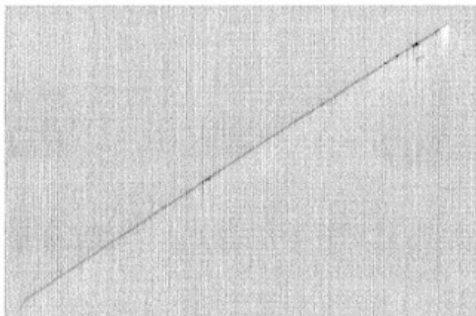
Induction signals require different treatment, but proper filtering makes the signal shape very much the same.

Induction-1

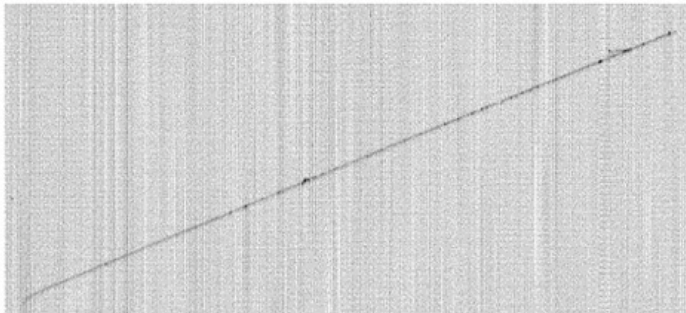


Passing through muon with θ -ray emission.

Induction-2

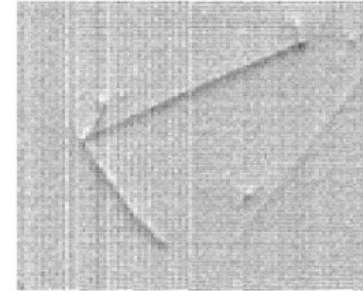


Collection

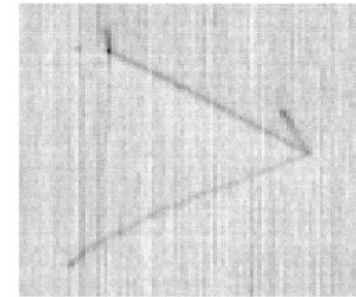


Low-multiplicity hadron interaction

Induction-1



Induction-2



Collection

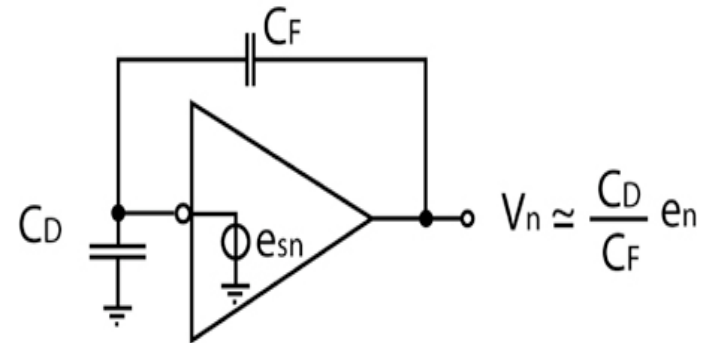


Drift time vertical
Wires horizontal

Preamplifier for LAr TPC

- Need of very low noise amplifier:
 - No amplification around sense wires
Collected charge $\sim 10^4$ electrons/mip
 - Large input capacitance (C_D)
 - Wires (20 pF/m)* + cables (50 pF/m)
 - In T600 $C_D \sim 300\text{-}400\text{pF}$
 - Serial noise (proportional to C_D)
dominates over parallel noise
(proportional only to signal bandwidth)
 - High trans-conductance (g_m) input devices
are required to ensure acceptable Signal-to-
Noise level ($S/N \geq 10$)

* 3mm wire pitch



$$e_{sn}^2 \propto \frac{1}{g_m} T$$



Choice of the active input device

- Bipolar transistors
 - $g_m \approx 400\text{mS}$ @ $I_c \approx 10\text{ mA}$ (Amplification **merit factor** $g_m \cdot Z_{out} \approx 10^5$)
 - BUT: **parallel noise** density $\approx 2\text{ pA} / \sqrt{\text{Hz}}$ **too high** (with a typical LAr signal bandwidth of $\sim 1\text{ MHz}$ gives **unacceptable noise contribution**)
- jFET
 - Good $g_m \approx 40\text{mS}$ @ $I_{ds} \approx 10\text{ mA}$ (Amplif. **merit factor** $g_m \cdot Z_{out} \approx 10^4$)
 - **negligible parallel noise** density $\approx 0.001\text{ pA} / \sqrt{\text{Hz}}$
- VLSI-CMOS
 - Lower g_m , (Amplif. **merit factor** $g_m \cdot Z_{out} \approx 10^3$)

jFET was the ICARUS choice :
charge sensitive preamplifier with high g_m **2-jFET input stage**

The ICARUS T600 preamplifier

■ Custom IC in BiCMOS technology

- Classical **unfolded** cascode integrator
- External input stage jFET's
 - Two IF4500 (Interfet) or BF861/2/3 (Philips) in parallel to increase g_m (50-60 mS)
- External feedback network
 - Allow sensitivity and decay time optimization
 - High value f.b. resistor ($100M\Omega$) reduce parallel noise

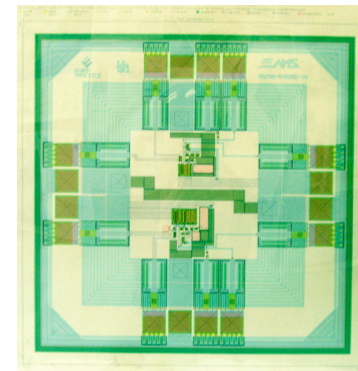
■ Two channels per IC

- symmetrical layout guarantees identical electrical behavior

Two versions:

“quasi-current” mode: $R_f C_f \approx 1.6\mu s$ (collection + first induction)

“quasi-charge” mode: $R_f C_f \approx 30\mu s$ (mid induction)



Sensitivity ≈ 6 mV/fC

Dynamic range > 200 fC

Linearity $< 0.5\%$ @ full scale

Gain 6.5 ± 0.5 mV/fC,

Gain uniformity $< 3\%$

E.N.C. $\approx (350 + 2.5 \times C_D)$ el ≈ 1200 el. @ 400pF

Power consumption ≈ 40 mW

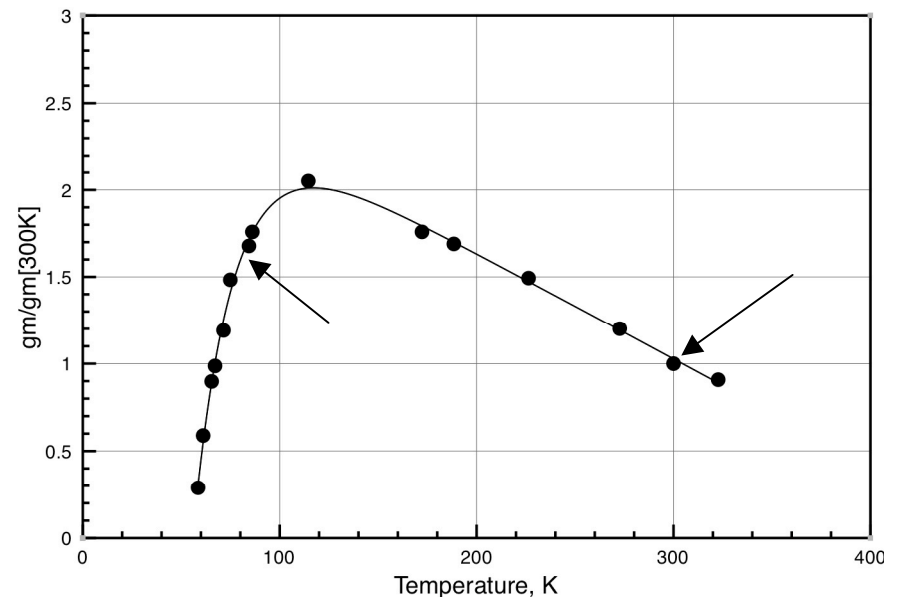
1LSB = 1 mV

Electronics in LAr ?

Deeply investigated within ICARUS collaboration (since 1988)

- Limited choice of active devices working at LAr temperature
 - GaS-jFET (High Electron Mobility Transistor technology)
 - Silicon jFET (High Resistive Substrate technology)
 - CMOS very low temp. **now** available but...
 - **Issues:**
 - Better S/N due to improved g_m at cryogenic temperature
 - Reliability at LAr temperature
 - Availability on the market

U310 jFET

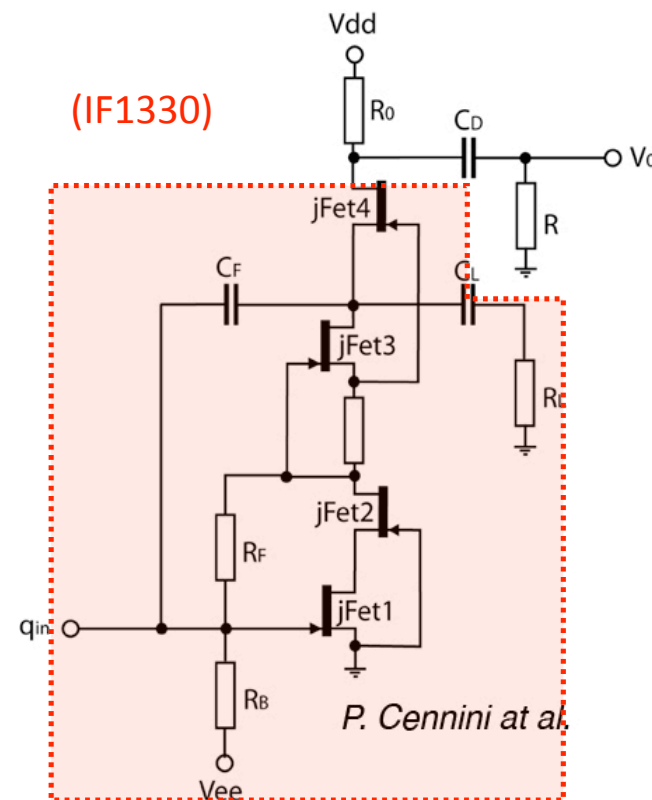


The TOTEM architecture

- Charge Integrator made on Thick Film Hybrid technology with discrete jFET only
 - Minimum active and passive components
 - Ability to drive long transmission line
 - Reduced power consumption
 - Minimum cable connections
 - Current signal from Positive Power Supply
 - Common Negative polarization
- Characteristics
 - Optimized for low detector capacitance

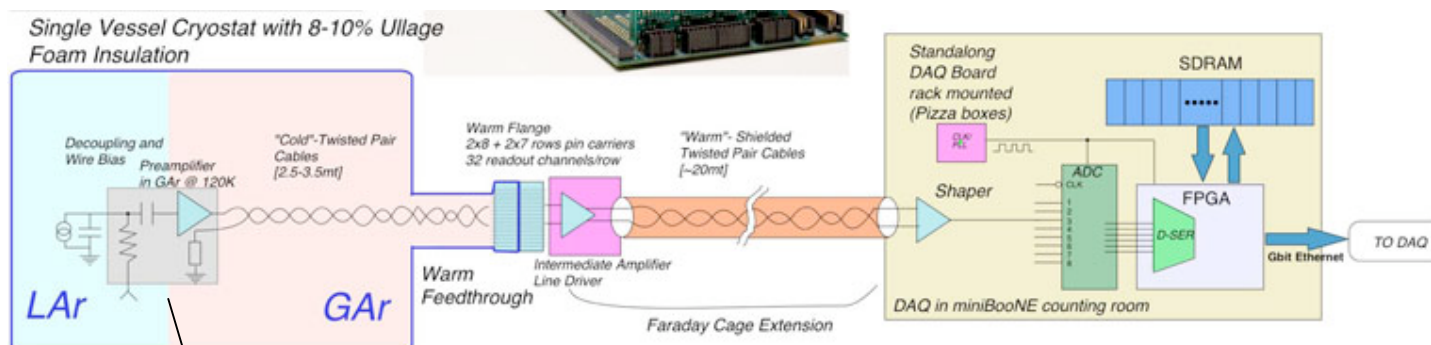
Sensitivity $\approx 0.45 \text{ mV/fC}$ ($0.9 \text{ }\mu\text{A/fC}$)
 Dynamic range $\pm 1.5 \text{ pC}$
 Linearity $< 0.5\%$ @ full scale
 Input impedance $\approx 420 \text{ }\Omega$
 Input capacitance $\approx 20 \text{ pF}$
 E.N.C. $\approx (390 + 7 \times C_D) \text{ eI}$
 Power consumption $\approx 11 \text{ mW}$

$$V_0 = \frac{R_0}{R_L} * \frac{q_{in}}{C_F}$$



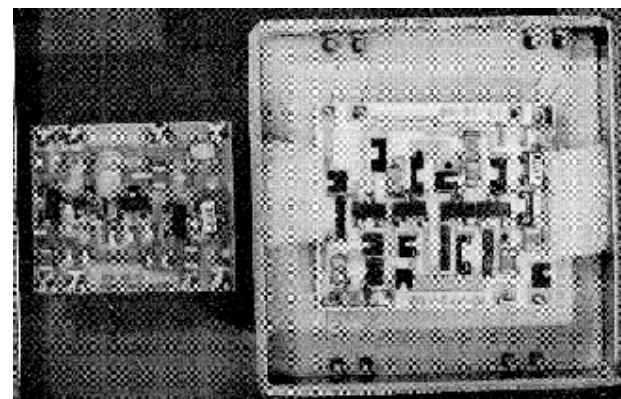
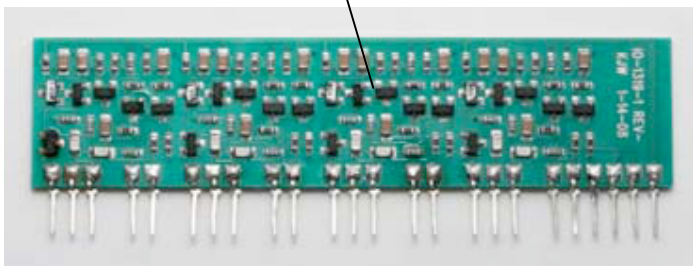
MicroBooNE: cryogenic front-end

Electronics chain



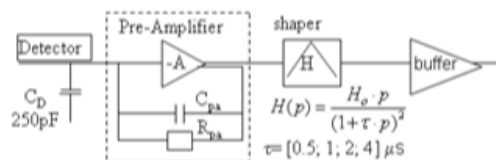
Several years of experience in
NA-34 & NA-48

JFet discrete amplifier



Step 2) (2008) on the basis of the experience acquired during the first phase, new version (TOPEST) integrating also the shaper+buffer, 8 channels + single components for characterization.

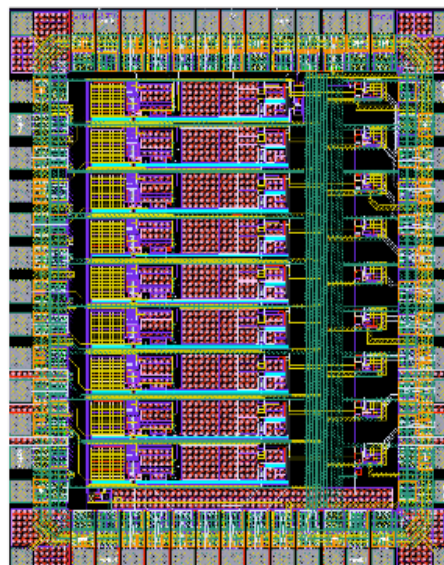
Received at the end of July 2008. Tests at IPNL. Typical total gain 7.5 mV/fC, 40 mip dynamic range.



- selectable:
feedback capacitance (500 fF-1 pf)
feedback resistor (2 - 10 MΩ)
- selectable shaping times (0.5 - 4 μs range)
- power switching on-off

Step 3) (End 2008), detector tests 64 channels:

study noise vs track reconstruction as a function of angles and shaping times



Private communication:

$$g_m = 117 \text{ mS}$$

$$i_d = 8.655 \text{ mA}$$

$$W_{\text{tot}} = 8100 \mu\text{W}$$

$$L = 0.35 \mu$$

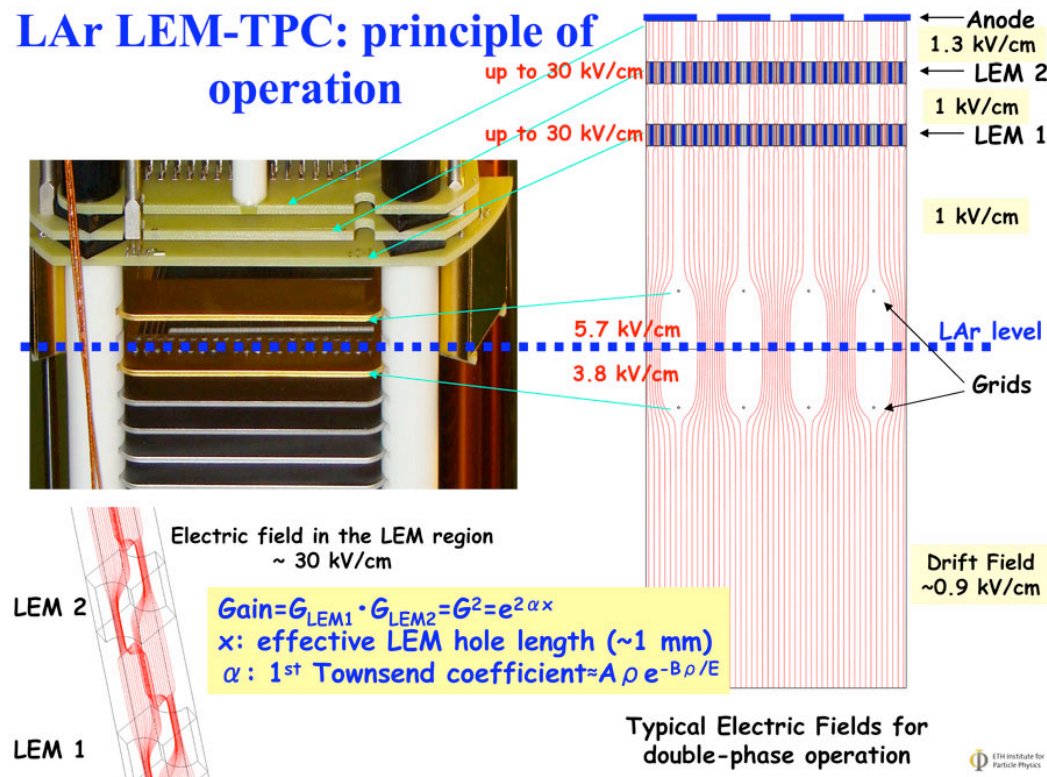
$$g = 10 \text{ (gates)}$$

Noise=1000e
@ Cd 250pF
??

Double phase Ar detectors

Double phase detectors enhance charge generated in liquid.

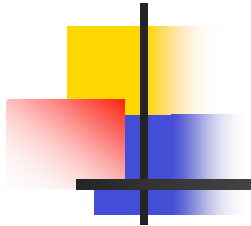
LAr LEM-TPC: principle of operation



Similar signal shape

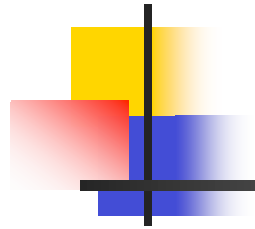
S/N intrinsically higher

Previous issues also apply



Pro & Contra cold amps

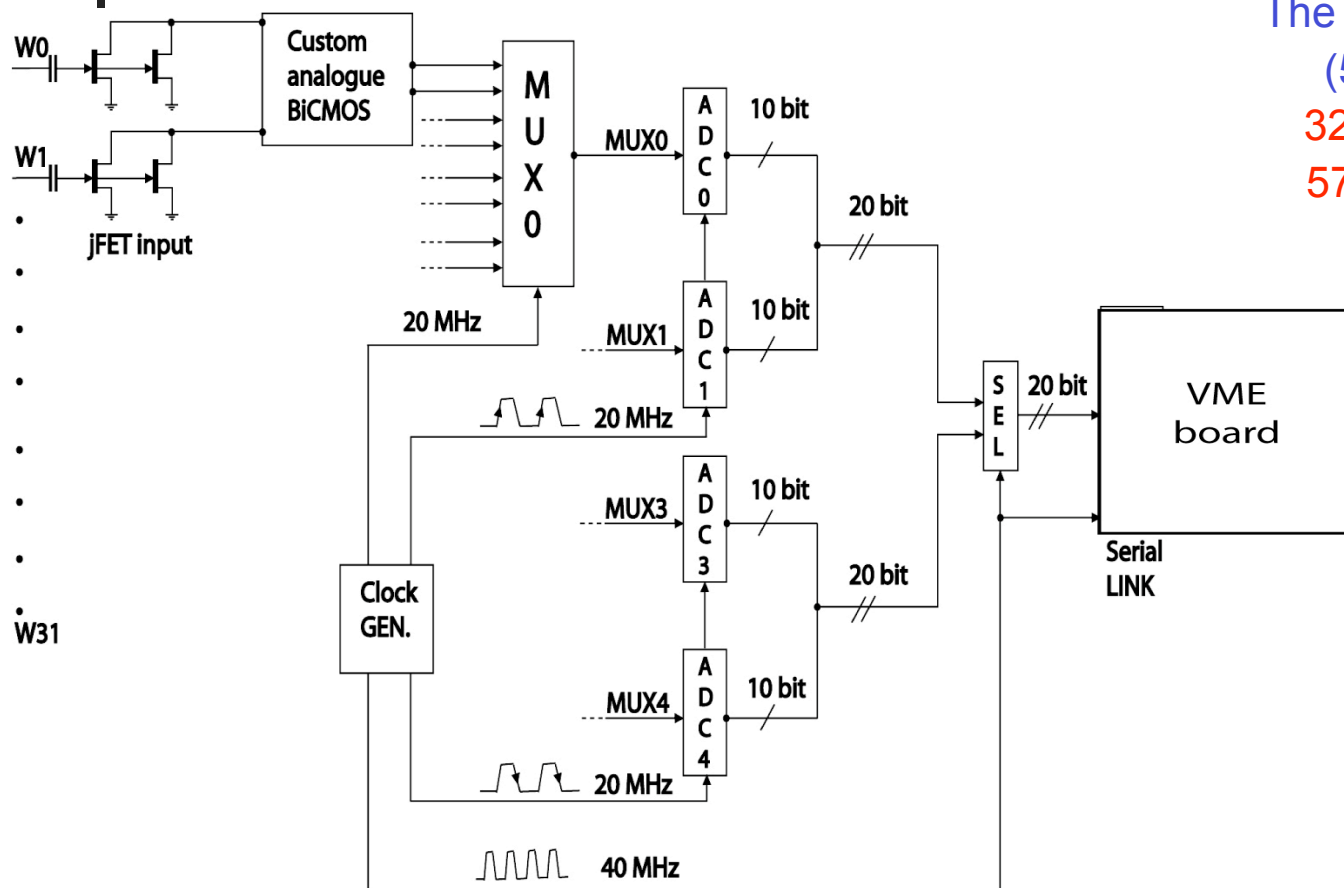
- Advantages
 - Reduction of input capacitance due to cable absence
 - Reduction of micro-phonic noise (detector = Faraday cage)
 - Improvement of S/N [~ 2.4] due the **combined effect** of lower [~ 1.9] Johnson noise and higher [~ 1.26] g_m @ 86°K
- Disadvantages
 - Inaccessibility during detector operation
 - Need of careful selection of components, extensive burn-in and temperature cycles before installation to minimize components failure
 - Design architecture and technology restricted by limited choice of active components
 - Limit on power dissipation ($< 100 \text{ mW/cm}^2$ to avoid LAr boil-off)



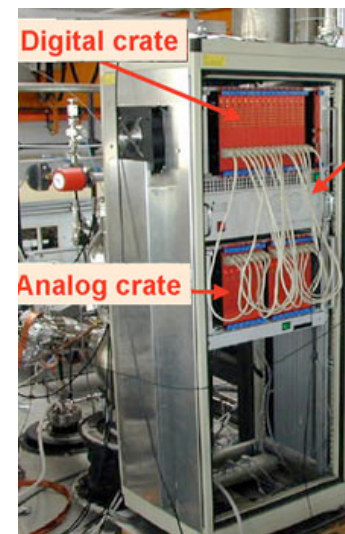
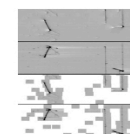
The ICARUS T600 experience

- **Analogue front-end** followed by a multiplexed **ADC** ($1\text{LSB} \cong 1000e^-$) whose output is stored in RAM: **waveform recorder**.
- Digital VME module performs local storage, **hit finding** and **factor 4 data compression** (*recent improvement*).

T600 DAQ block diagram



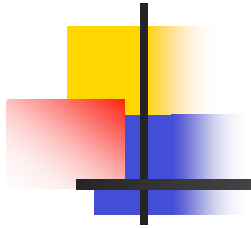
The T600 DAQ system
 (5·10⁴ channels)
 32 channels/board
 576 channels/rack





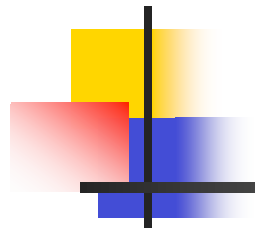
Signals and noise in **large** TPC

- In a multi-kton TPC we can foresee wires with a pitch larger than the **3mm** used in the T600
 - The adoption of **6mm** pitch for a large TPC seems reasonable and
 - A realistic capacitance value for 10m electrode wires, 6mm pitch, and average 8m of cable is $\sim 600pF$ (cfr.: 300-400pF in the T600)
- It follows that the Signal to Noise Ratio should be very similar to that of the T600.
 - **Hence a completely new design of the analogue front-end would hardly improve the performance**




AD conversion


- **Serial ADC** are **now** preferable over Flash ADC.
 - To reach the 3MHz sampling rate, AD must be clocked at 48MHz .
 - Mini Small Outline Package (MSOP) smaller than $5 \times 5 \text{ mm}^2$. Many house **2 or even 4 channels**. **Competitive in price and power consumption.**
- We can assume a resolution of 10bit but 12bit ADCs are also available at reasonable cost. More components available soon.



Available Serial ADC



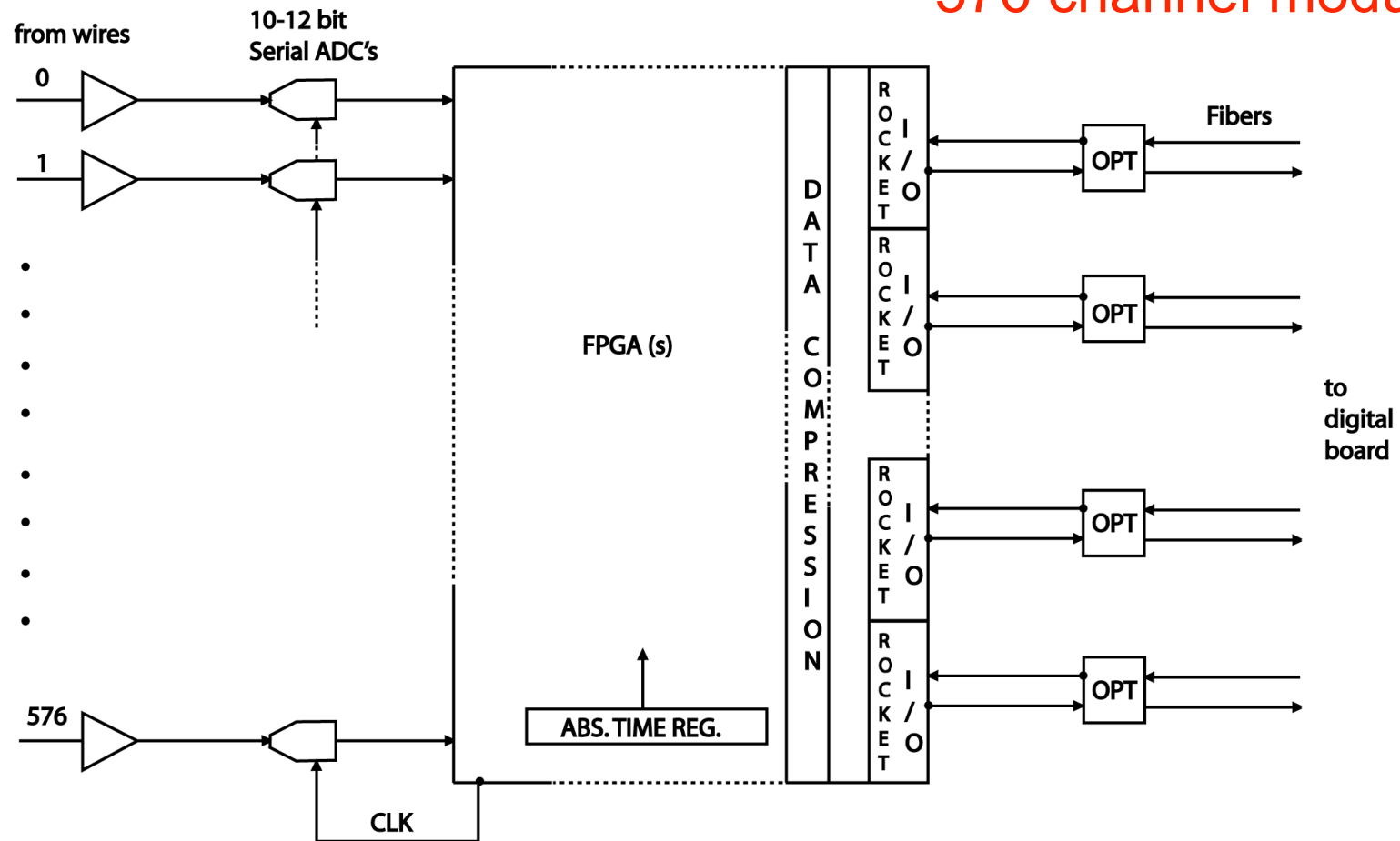
Manufacturer	Res	Part. Num.	Freq. <i>MHz</i>	Power mW typ.	Supply	Cost \$ 1000 pcs
Analog Devices	10	AD7273	3	11.4	2.35 – 3.6	3.75
Analog Devices	10	AD7277	3	10.5	2.35 – 3.6	3.60
Maxim	10	MAX1334	4.5	40	5, 3.3	NA
Maxim	10	MAX1335	4	40	3.3	NA
Analog Devices	12	AD7274	3	11.4	2.35 – 3.6	3.75
Analog Devices	12	AD7276	3	10.5	2.35 – 3.6	4.0 – 6.25
Linear Technology	12	LTC1403-1	2.8	14	2.7 – 3.3	4.00
Maxim	12	MAX1332	3	38	5, 3.3	NA
Linear Technology	14	LTC1403A-1	2.8	14	2.7 – 3.3	7.00
Analog Devices	16	AD7621	3	86	2.5	29.95



The frequency given in the table refers to the sampling rate.

Compact architecture

576 channel module



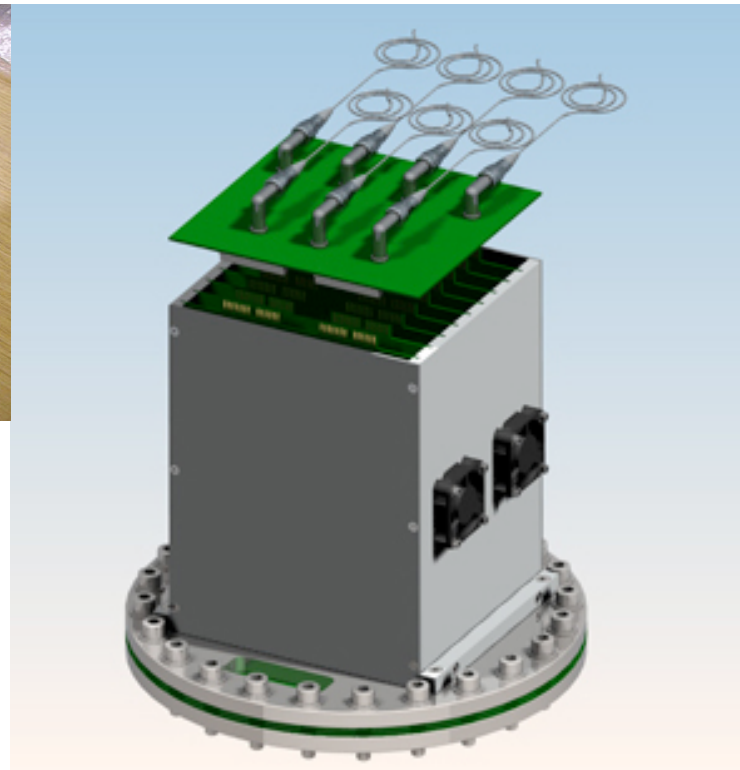
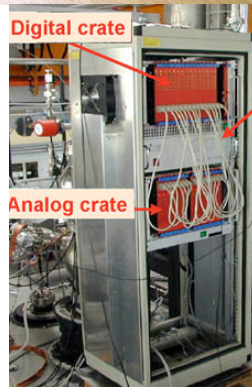
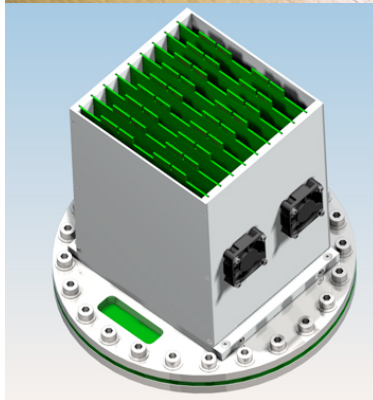
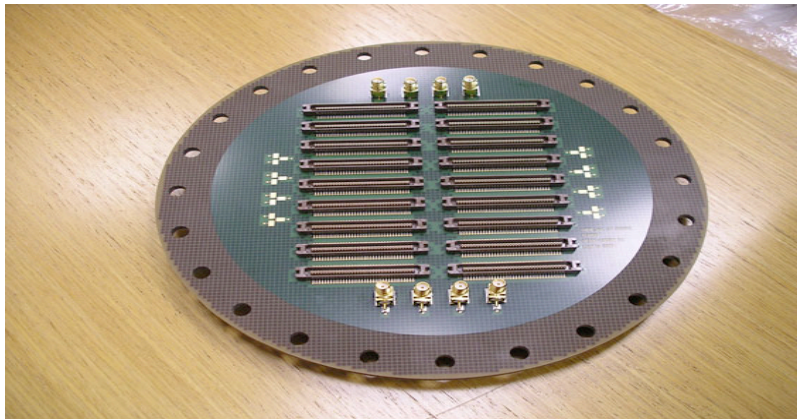


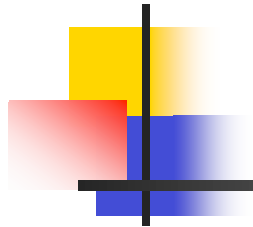
New data distribution

- A set of a few FPGA for 576 channels (one flange) will be used to handle, filter, and organize the serial information provided by the serial ADC's.
- Assuming a sampling frequency of 1.5Mhz, 10bit ADC's we need to transmit ~8 Gbit/s, (including error correction redundancy).
- Optical links with 1.5Gbit/s data rates are standards and can be driven by suitable interfaces available on FPGA from different vendors.
- **Six optical links could serve all the channels of one module (576) and convey also extra information as absolute time.**
- The architecture of the DAQ system can be enhanced through the adoption of a modern switched I/O allowing the parallelization of the serial data flows.

New electronics layout

- The whole electronics of ~600 channels can be hosted in a compact crate (~12 liter volume) incorporating the feed-through flange that forms a sort of backplane.
- External cables will be essentially eliminated.





Conclusions on charge read-out

- The ICARUS DAQ **basic** architecture is well suited even for larger size LAr-TPC (*single phase*);
- Similar structures adopted by other projects. Differences limited to the front-end choice: **cold versus warm.**
- Main upgrades concern:
 - More compact version of the front-end amplifier
 - Adoption of high frequency serial ADCs
 - **Housing and integration electronics on detector**
 - Optical links for Gbit/s transmission rate

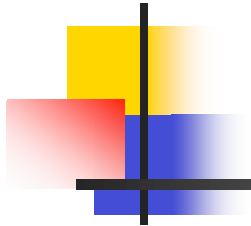


Photo-detectors readout

Ionization in **liquid** Argon (LAr) is accompanied by **scintillation light emission**.

The two processes are **complementary** through recombination and their relative weight depends on the strength of **the electric field** and **dE/dx**.

Electron and photon yield similar ($Y_{\text{ion}} = \sim 2.9 \cdot 10^4 \text{ e}^-/\text{MeV}$, $Y_{\text{ph}} = \sim 2.4 \cdot 10^4 \text{ } \gamma/\text{MeV}$ @ 500v/cm for *mip*).

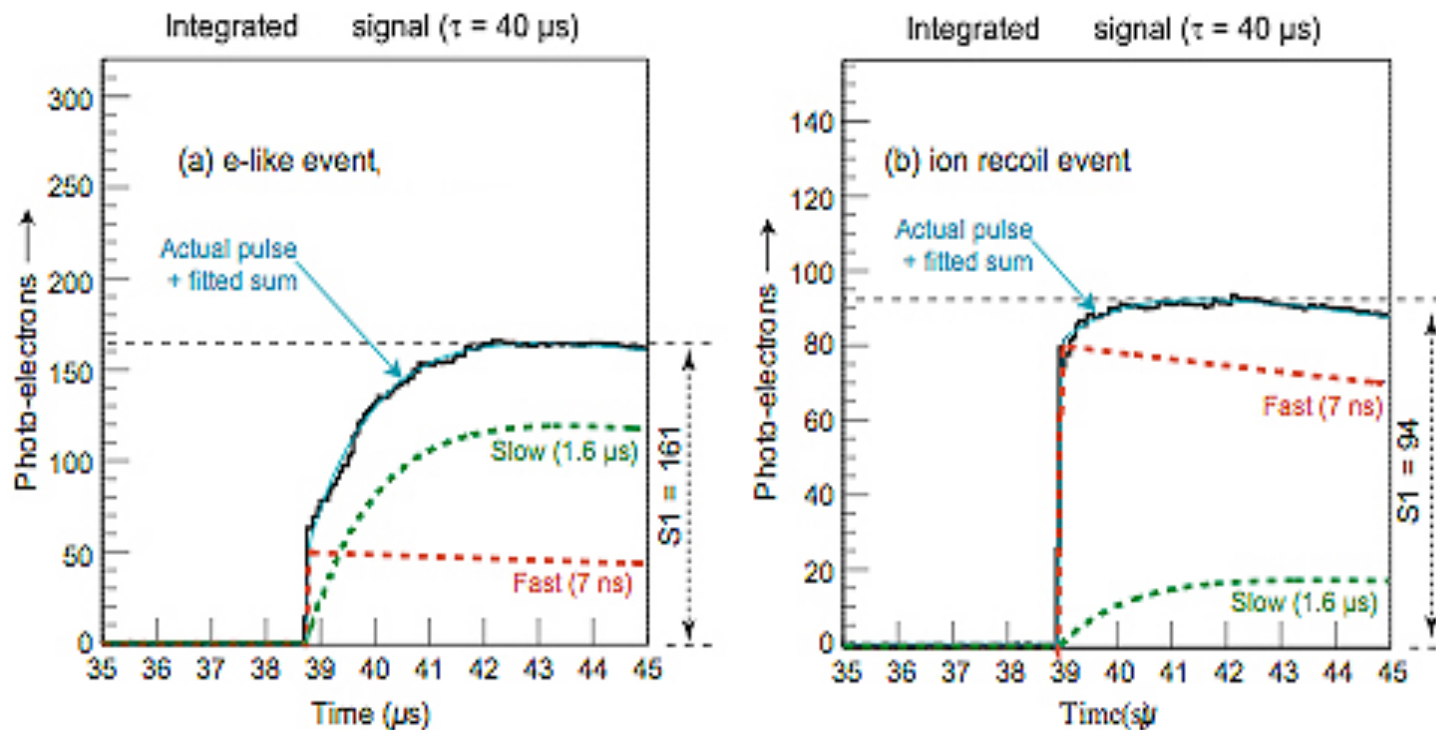
Light is emitted at 128nm (detection generally through wave-shifting) with **two-component** exponential decay ($\tau_s \sim 6 \text{ ns}$ and $\tau_L \sim 1.5 \text{ } \mu\text{s}$).

Prompt light signal typically used for **trigger** (eg. Icarus) or for **calorimetry/particle identification** (eg. WArP).

Example of light coll. in WArP

mip: ~25% of light **short time** constant ~75% **long time** constant.

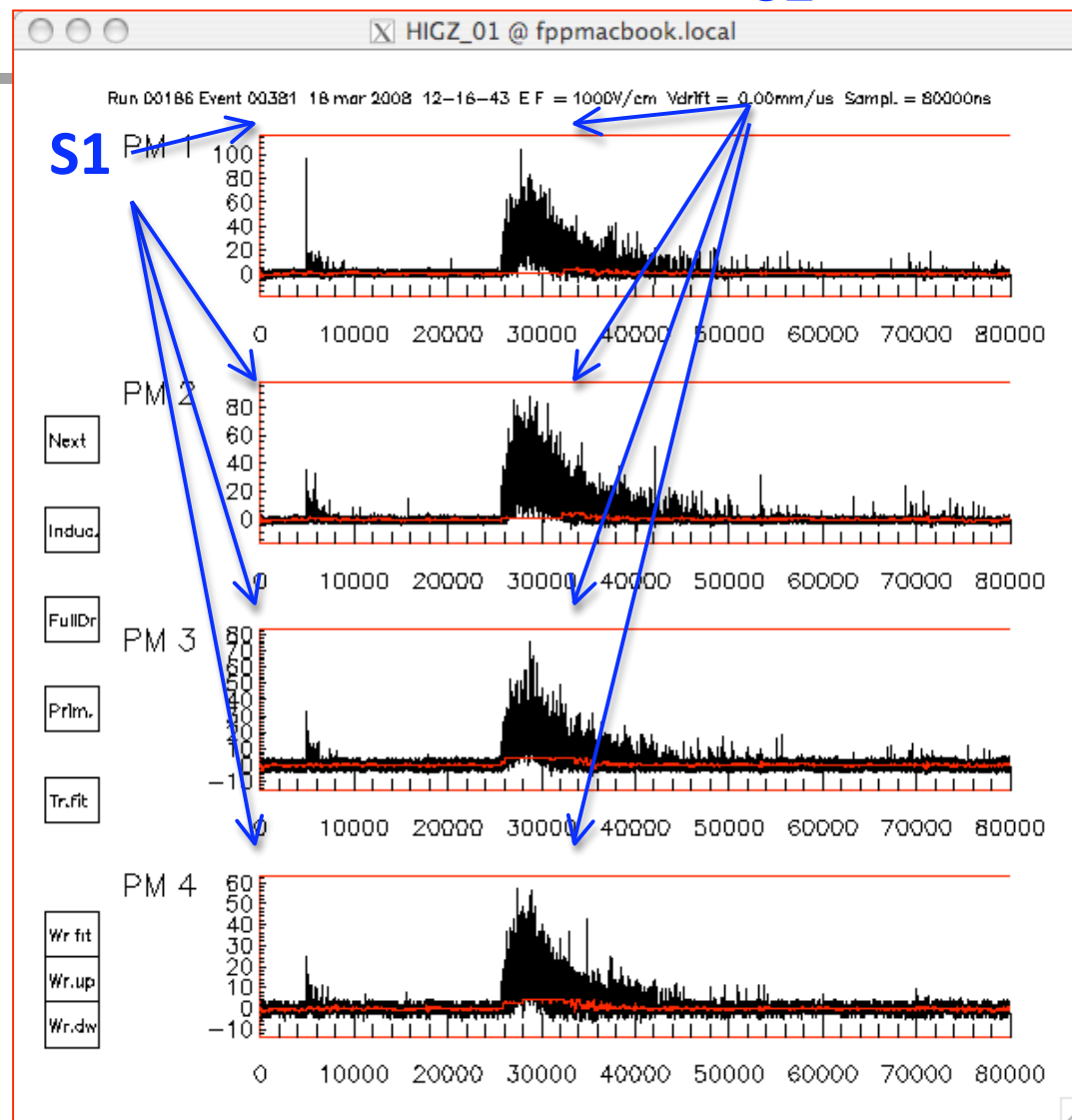
recoil: ~75% of light **short time** constant ~25% **long time** constant.

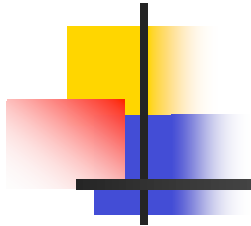


Double phase signals

S2

- S1 primary scintillation.
- S2 scintillation in gas phase proportional to extracted ionization electrons.
- Ionization electrons identified individually.
- Efficient alternative to direct charge measurement for tiny signals (few electrons)
- S1 and S2 have similar characteristics.





Conclusion

Waveform recording based on **high performance** (expensive) commercial solution ($\geq 1\text{GHz}$ - $\geq 8\text{bit}$, multi buffering) is well suited for signals provided by PMTs in single and double phase Ar detectors, allowing full measurement of the signal structure.

Investment required:

for low cost waveform recorders for experiments requiring high number of channels;

for **on line data reduction, signal recognition, and trigger pre-processing** through high speed FPGAs.

Also **onto detector integration** would be a benefit (see first part).