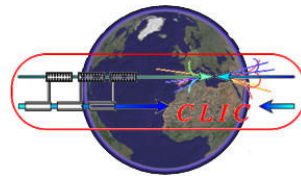


# COOLING & VENTILATION FOR THE DRIVE BEAM TUNNEL

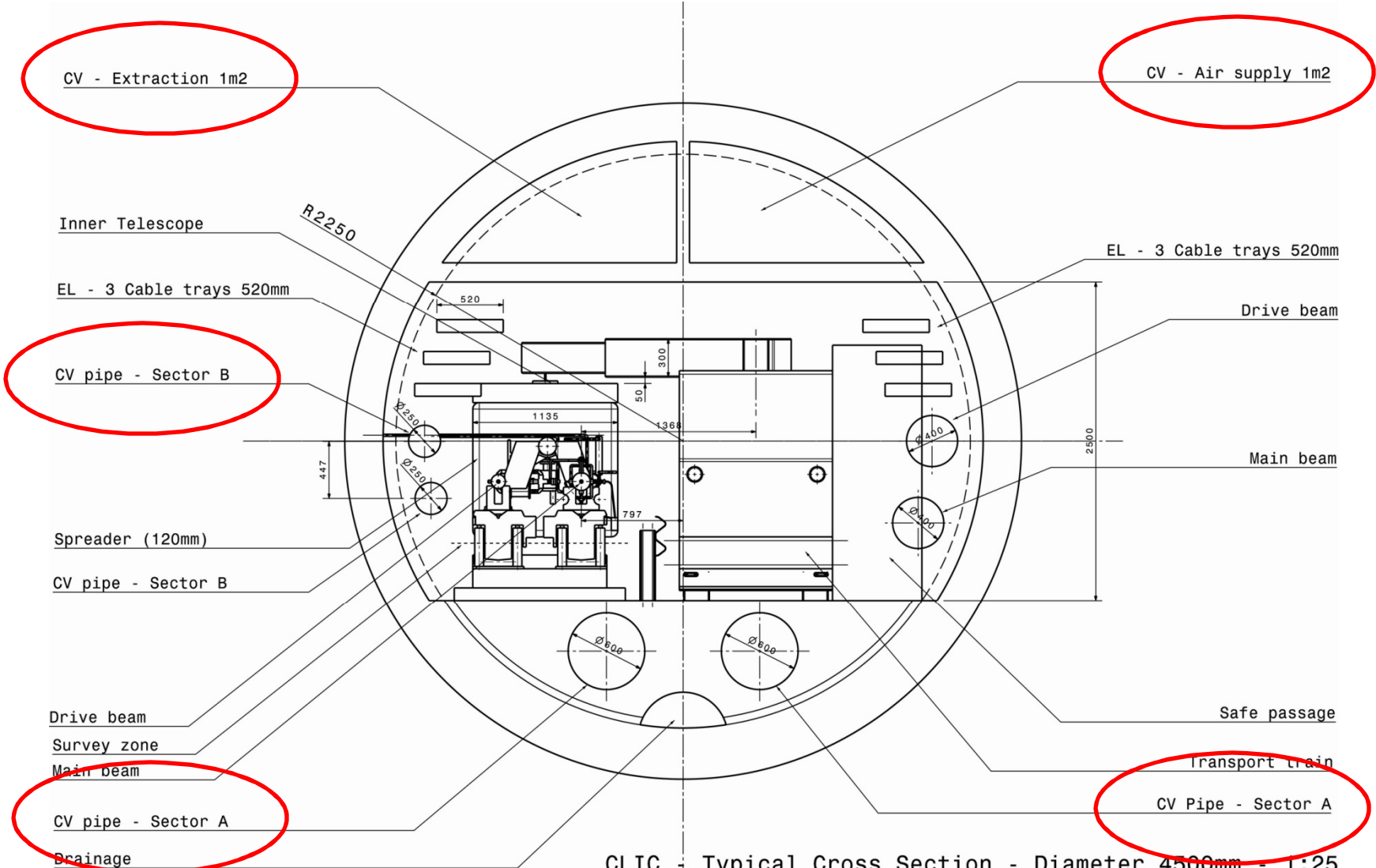




# Agenda

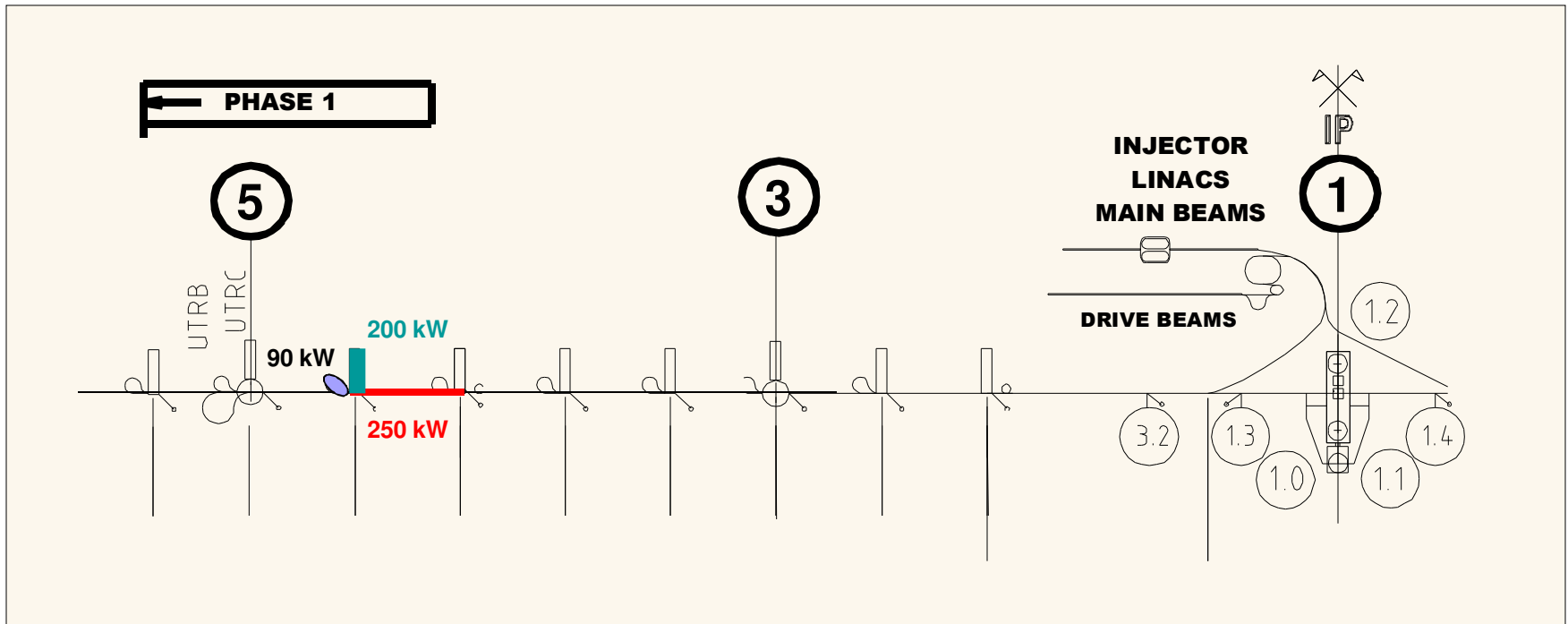
- Tunnel cross section
- Ventilation:
  - main parameters
  - improvements, pending issue
  - proposed solution
- Cooling:
  - main parameters
  - proposed solution
  - pending issues

# Tunnel cross section



# Ventilation main parameters: heat dissipation in the air

Drive Beam sector = 250 kW  
 UTRA cavern = 200 kW  
 Loop = 90 kW



Heat dissipation in the tunnel:  
 250 kW / DB sector  
 1250 kW between two shafts

Heat dissipation in the Loops & UTRA:  
 290 kW / DB sector  
 1450 kW between two shafts



# Ventilation working parameters:

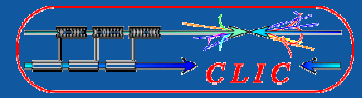
Cooling power: 1250 kW

Delta T: 20 °C → 17-37 °C

Flow rate: **180'000 m<sup>3</sup>/h**

• If  $v = 12 \text{ m/s} \rightarrow$  Cross section:  $4.1 \text{ m}^2$

• If cross section  $1.2 \text{ m}^2 \rightarrow v = 41 \text{ m/s}$



a) Reduce the cooling power removed by air

- Cross section ducts:  $1.2 \text{ m}^2$
- Flow rate:  $52'000 \text{ m}^3/\text{h}$
- Cooling power:  $360 \text{ kW}$

b) Using pre-alignment shafts for ventilation shall allow a reduction in the dimensions of AHU on surface

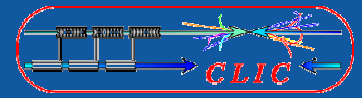


## c) Validate the delta temperature

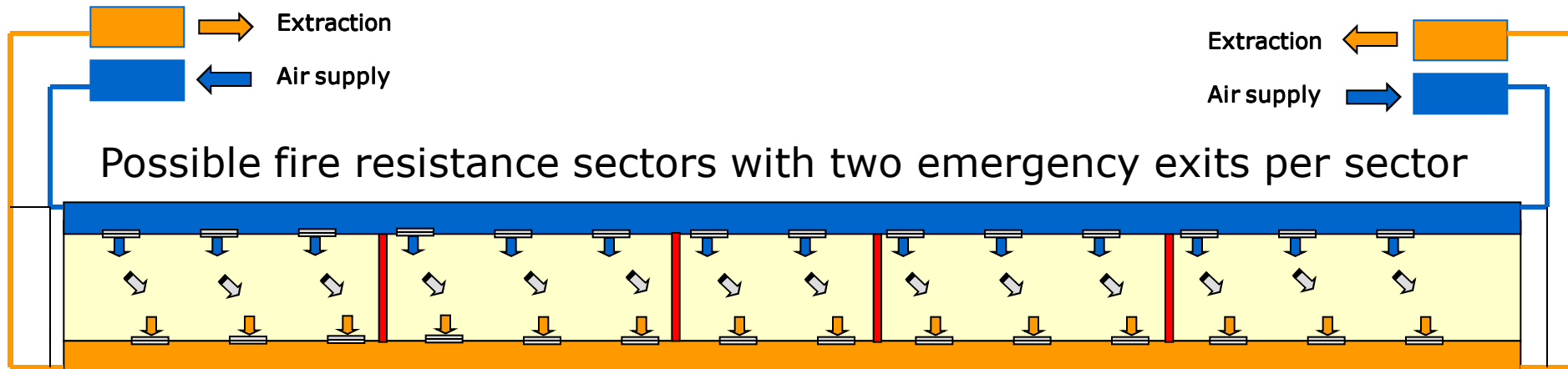
- Supply and extraction temperatures are average values at louvers position.
- Effective temperatures close to equipment are related to the heat load in each component and local air speed: **HOT SPOTS**
- Define the maximum acceptable temperature for equipment



# Proposed solution



## Semi transversal principle



Optimisation of the air flow rate  
Low air speed in the tunnel  
Optimisation of the gradient temperature  
Reversible and redundant operation possible  
Energy recovery possible, recycling of air

SHAFT  
POINT



1 Smoke extraction trap  
per sector



NEXT  
SHAFT  
POINT

1 supply and extraction  
grille per 30 mtrs.

# Water cooling main parameters



	<b>User</b>	<b>Power [MW]</b>	<b>Delta T [°C]</b>	<b>Flow rate [m3/h]</b>
Circuit A Demineralized water	Modules	70	27-45	3'350
Circuit B Demineralized water	UTRA, UTRC, loop, beam dump	15	27-52	516
Circuit C Raw water	Fire fighting	n.a.	n.a.	35
Circuit D Compressed air	Regulation	n.a.	n.a.	760
Drain system	Pumps in each UTRA; raised in each shaft			

# Water cooling main parameters

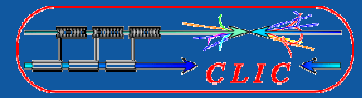


## WITH EXISTING CROSS SECTION

	Flow rate [m <sup>3</sup> /h]	ND	Pressure loss [bars/km]
Circuit A Demineralized water	3'350	600	~ 1.13
Circuit B Demineralized water	516	300	~ 0.8

Impossible to regulate the pressure at each delivery point for modules with such a pressure difference along the supply pipe

# Possible solutions



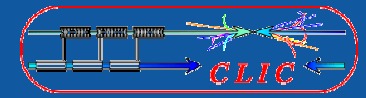
- Use of booster pumps along the tunnel to have lower working pressure,
- Increase of pipes diameters:
  - ND600 → ND800
  - ND300 → ND400
- Use of cooling towers every 4.4 km,
- Doubling the circuits to reduce the flow rate and working pressures.

# Pending issues



- Space needed in the cross section to pass from ND600 to delivery point (ND50? T.b.c.)
- Temperatures are at outlet of cooling station: stability in length still to be analysed
- Stability of temperature in time: local heating.
- Cooling with water from lake: reduce inlet temperature

# Conclusions



<b>AIR</b>	<ul style="list-style-type: none"><li>- Thermal charges removed by air to be confirmed</li><li>- Validate working temperatures for air</li></ul>
<b>WATER</b>	<ul style="list-style-type: none"><li>- Pressure loss on cooling circuit to be reduced;</li><li>- Temperature stability in time and length</li><li>- Study of connection between main collector and cooling pipe for module</li></ul>
	<ul style="list-style-type: none"><li>- Ratio air/water heat dissipation confirmed?</li><li>- Evaluate the impact on tunnel cross section</li><li>- All this figures require the use of non standard manufacturing, tooling and equipment: increase of costs.</li></ul>

Still to be discussed: heat dissipations in Exp. Caverns, LINACS etc.....