

# RF Characterization of Superconducting Samples

Sebastian Keckert

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[G. Ciovati et. al., APL 104, 092601]

## Detailed understanding of cavity loss mechanisms

- Bulk Niobium  
surface treatments, N-doping/infusion
- Thin films  
Nb/Cu, Nb<sub>3</sub>Sn, Multilayer, ...

How does an ideal tool look?

(without going through the hassle of building an entire cavity)

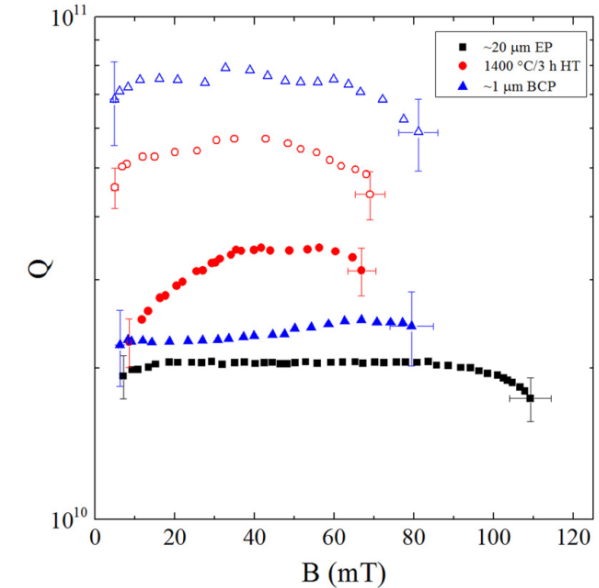
→ Measure RF surface resistance

- $\omega$ ,  $B_{RF}$ ,  $T$
- High resolution:  $Q_0 \approx 3 \cdot 10^{11} \leftrightarrow R_S \approx 1 \text{ n}\Omega$

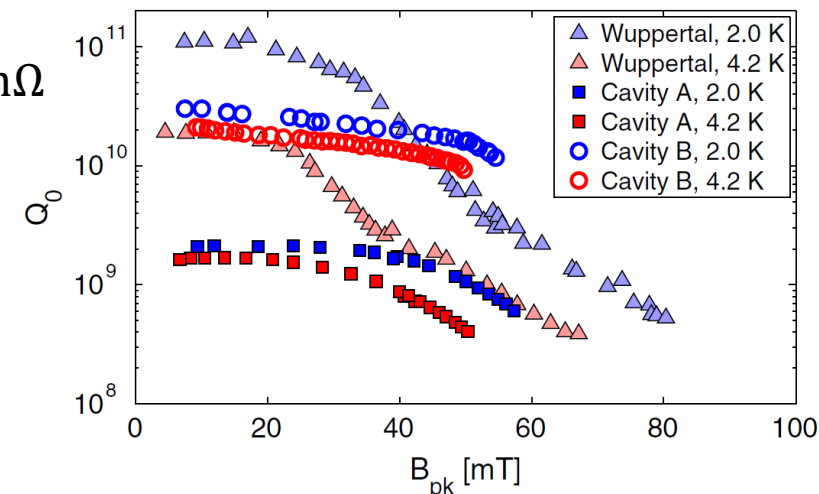
→ Characterize SC properties

- RF penetration depth,  $B_C$ , m.f.p.
- Flux trapping, cooling conditions

→ Small samples, easy to change



[S. Posen, M. Liepe, PRSTAB 17, 112001]



## Characterization Test Facility implemented at HZB

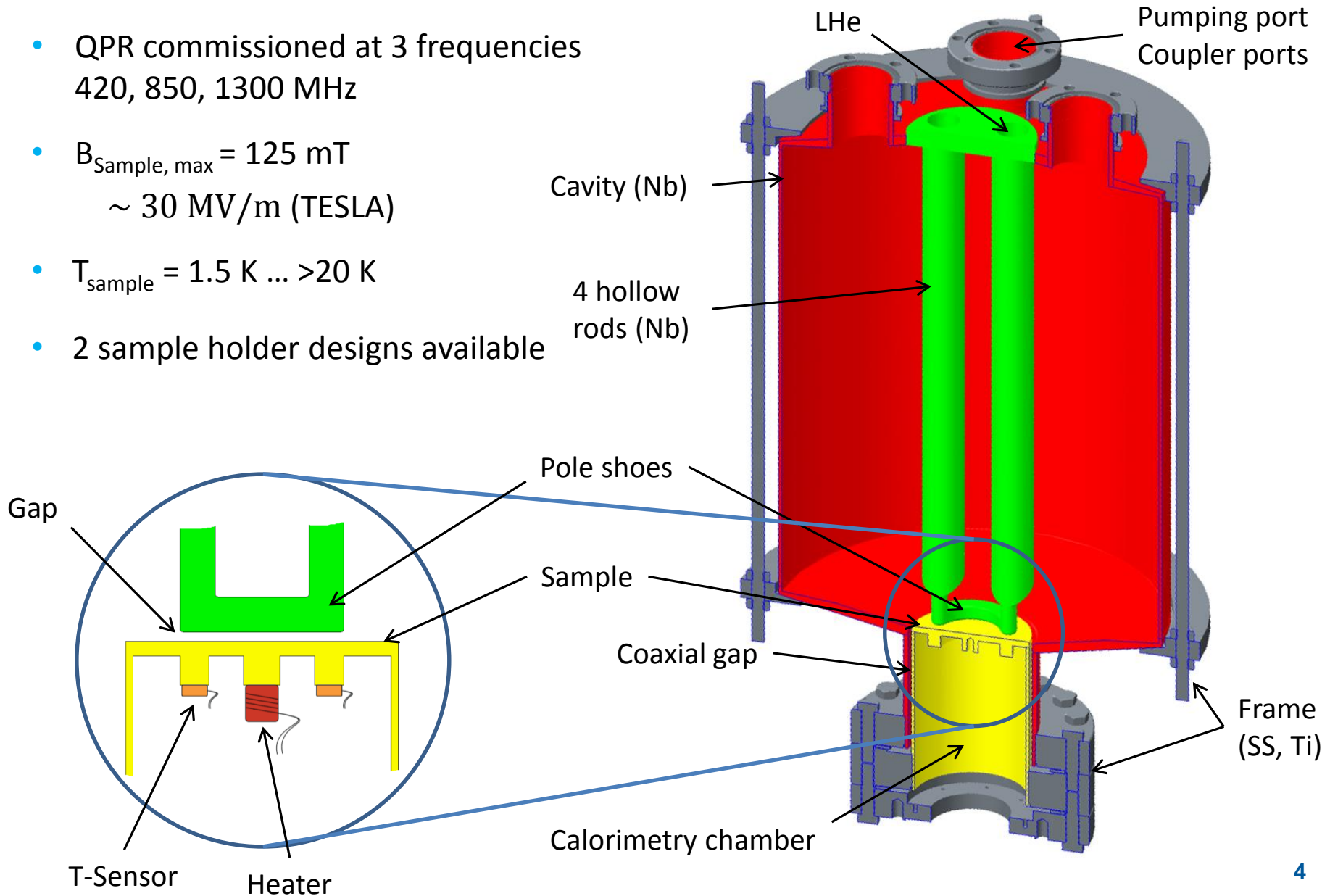
- October 2015: Milestone 78 fulfilled
- PhD thesis of Raphael Kleindienst
- Successful commissioning runs
- Sample development

## Characterization Test Facility implemented at HZB

- October 2015: Milestone 78 fulfilled
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  - Successful commissioning runs
  - Sample development
  
  - This talk: Further characterization methods
    - Trapped magnetic flux
    - Penetration depth
    - RF critical field
- to be continued in the framework of ARIES

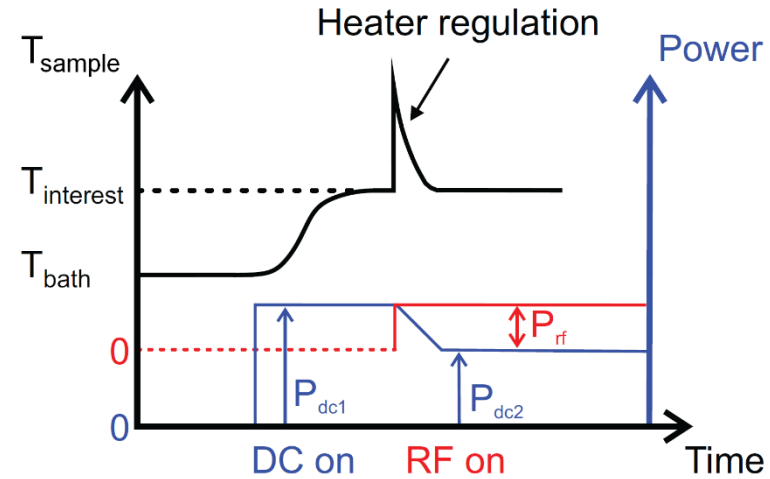
# The Quadrupole Resonator (QPR)

- QPR commissioned at 3 frequencies  
420, 850, 1300 MHz
- $B_{\text{Sample, max}} = 125 \text{ mT}$   
 $\sim 30 \text{ MV/m (TESLA)}$
- $T_{\text{sample}} = 1.5 \text{ K} \dots >20 \text{ K}$
- 2 sample holder designs available



$$P_{RF, diss} = \frac{1}{2} \iint_{sample} R_S |\vec{H}|^2 dS = R_S \frac{\omega U}{G} = P_{DC,1} - P_{DC,2}$$

$$\Rightarrow R_S = \frac{G}{\omega U} (P_{DC,1} - P_{DC,2}) = c(\omega) \cdot \frac{P_{DC,1} - P_{DC,2}}{P_{RF pickup}}$$



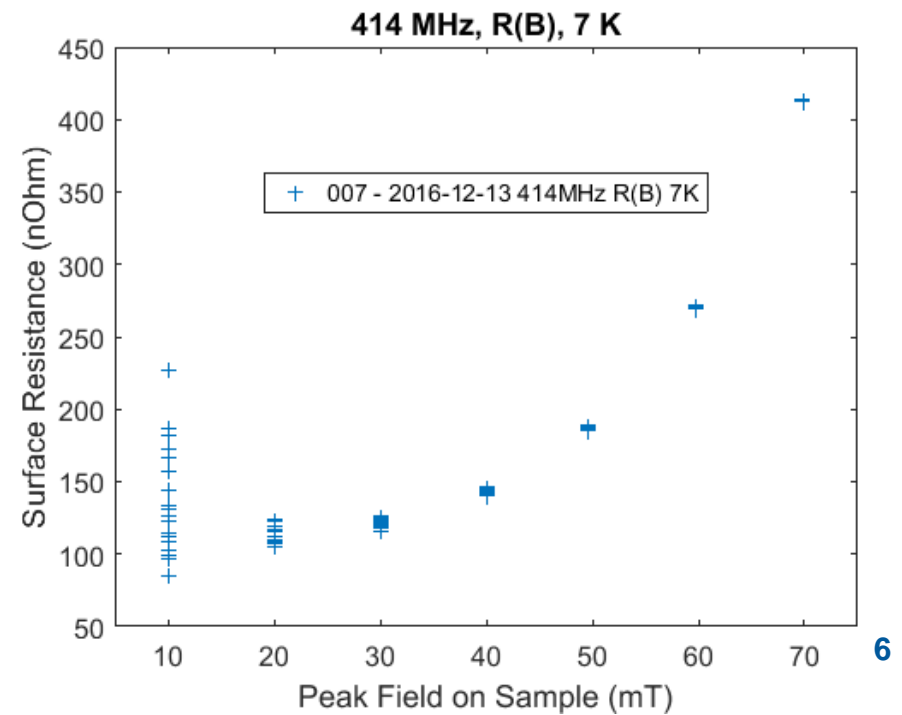
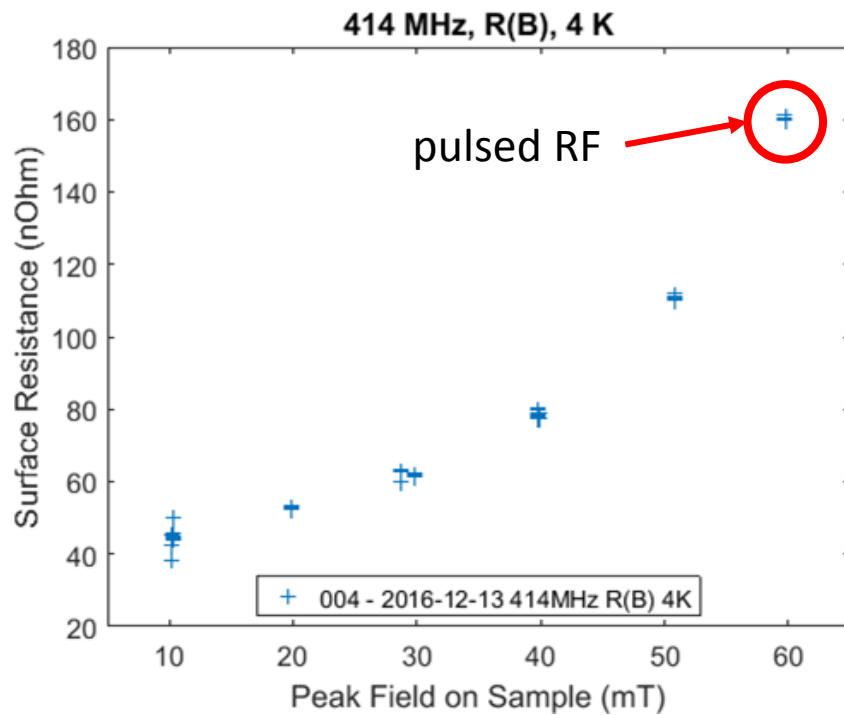
- Temperature resolution: 0.1 mK (calibrated cernox sensors)
- Surface resistance limit:  $\Delta P_{DC} \geq 1 \%$  and  $B_{RF} \leq 125$  mT

Sample temperature	Reference power	$R_S$ resolution limit
1.9 K	2.4 mW	0.006 n $\Omega$
2 K	4.6 mW	0.011 n $\Omega$
4 K	83 mW	0.2 n $\Omega$
7 K	375 mW	0.9 n $\Omega$

# Resolution & measurement limits

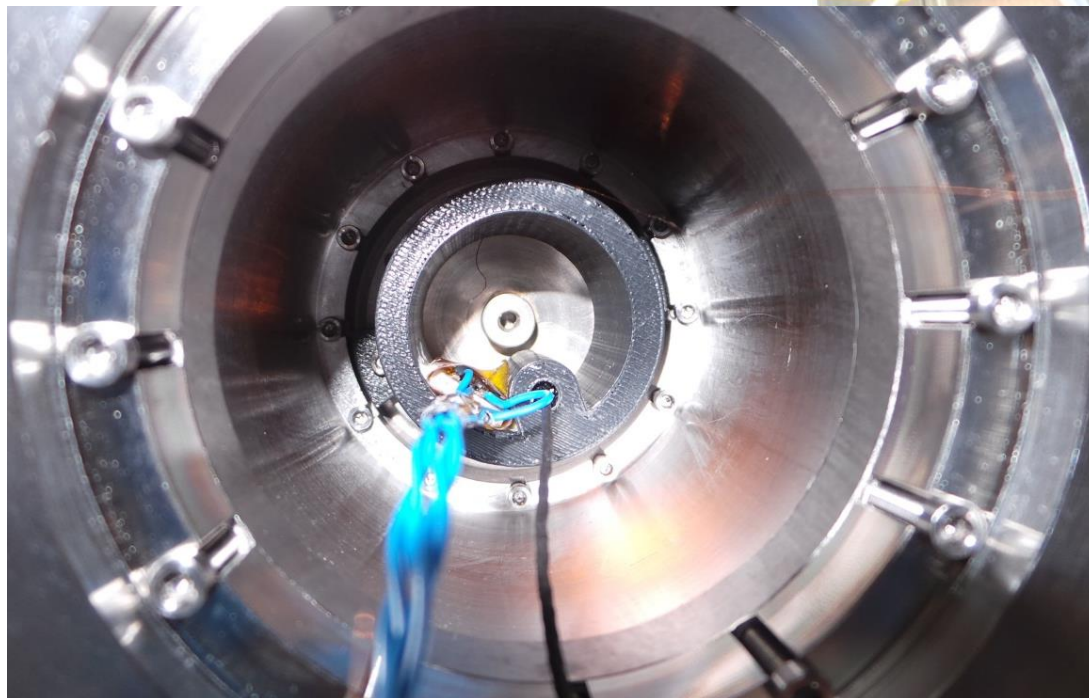
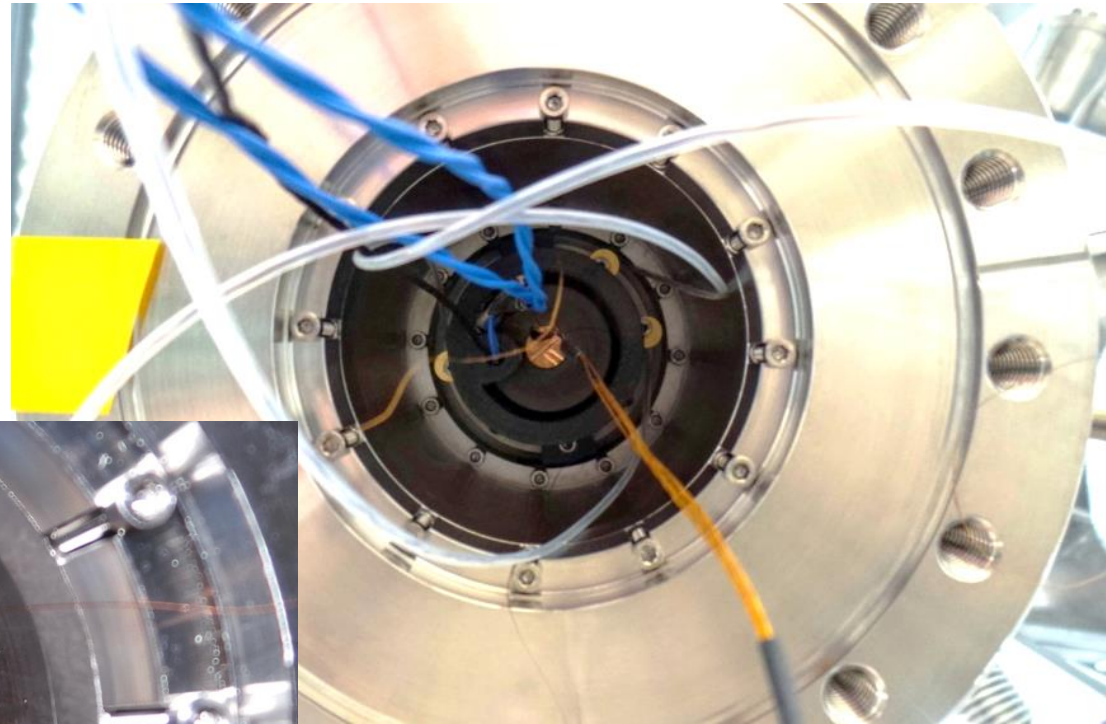
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# Trapped magnetic flux

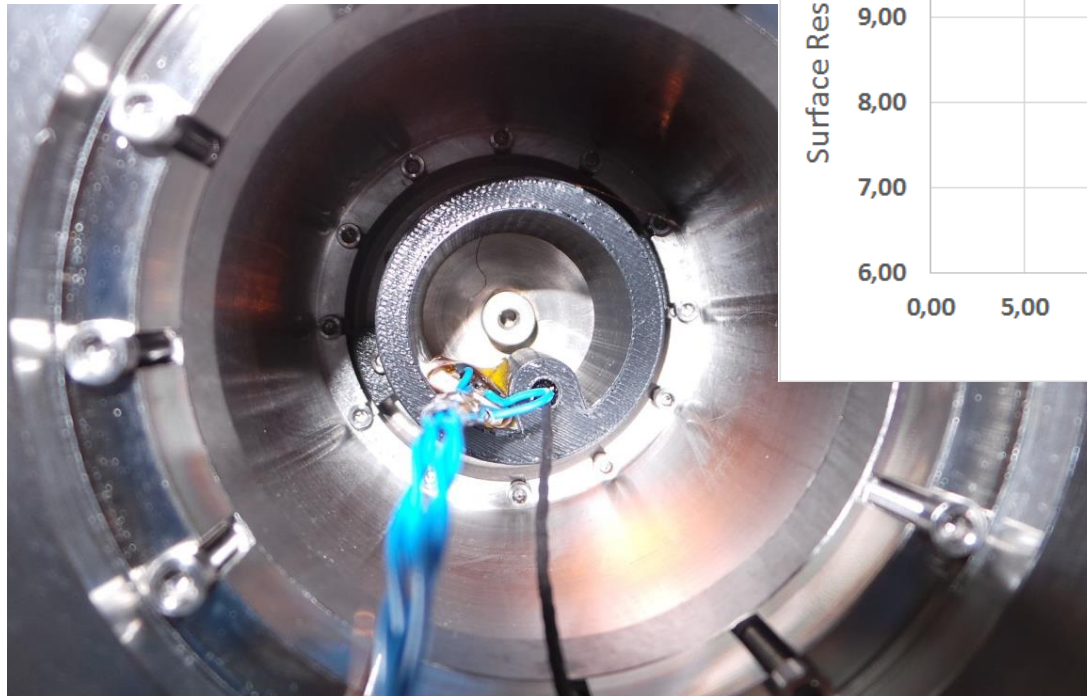
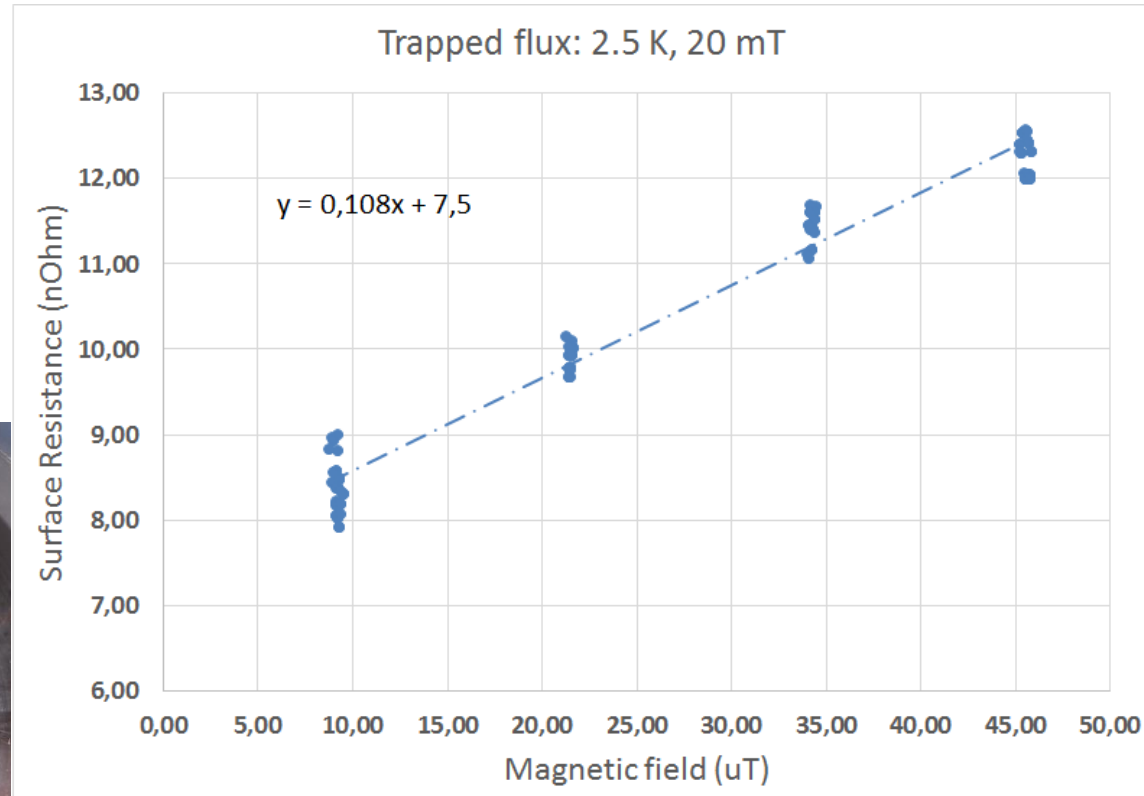
- Coil installed below sample
- Flux gate probe measures applied and trapped flux





# Trapped magnetic flux

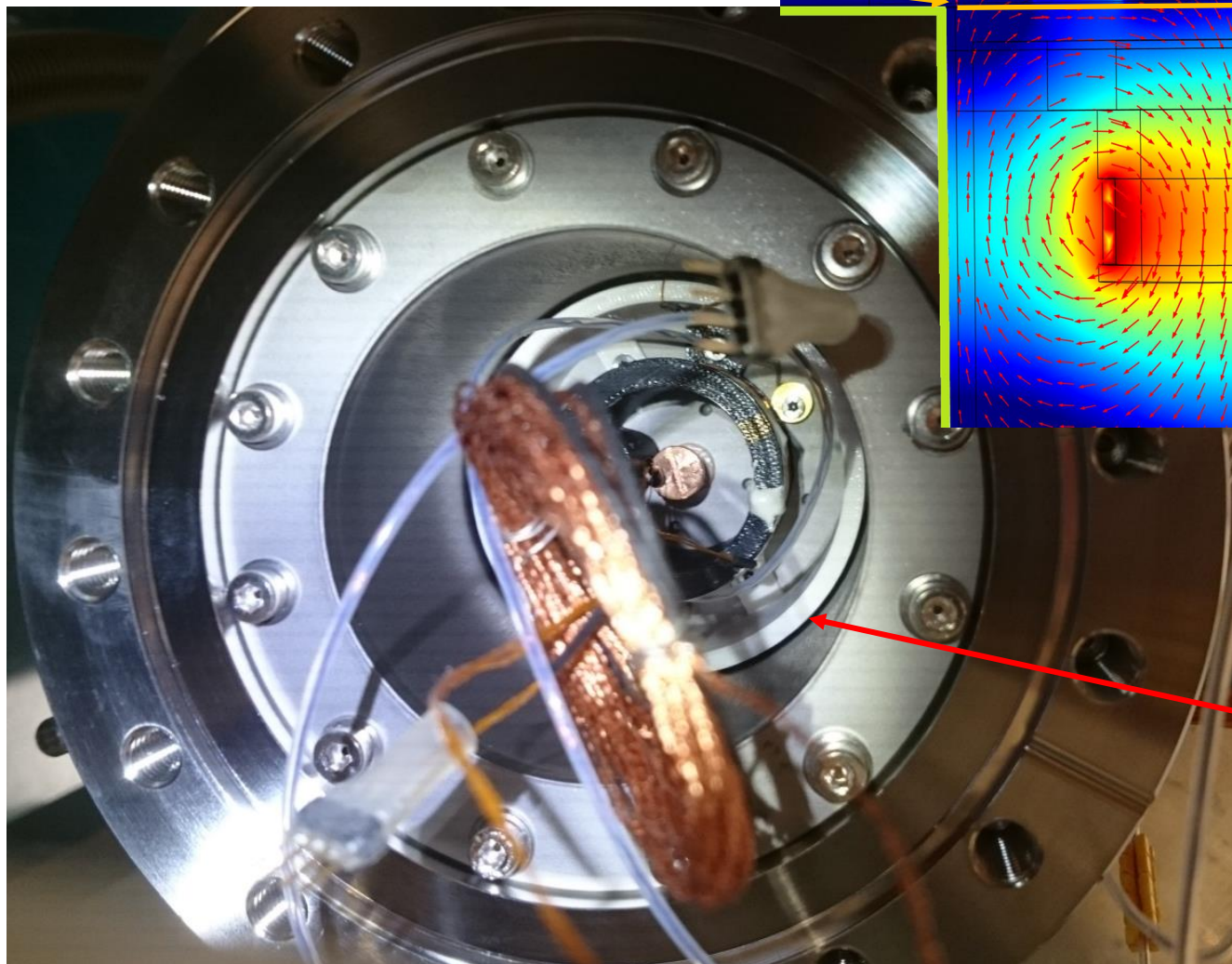
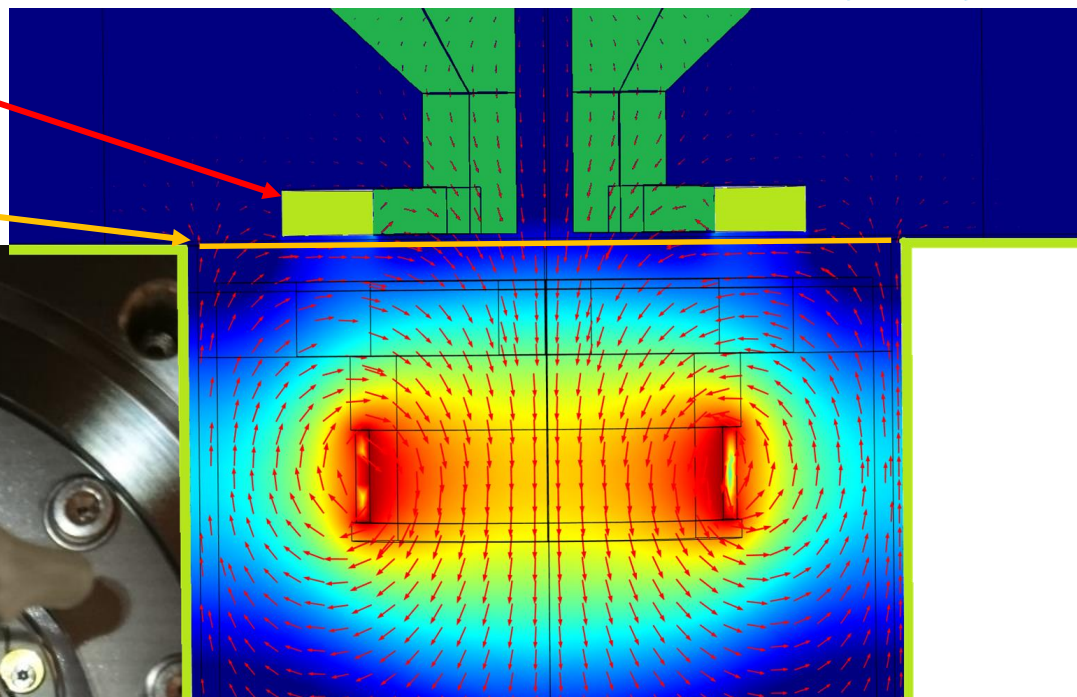
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# Trapped magnetic flux

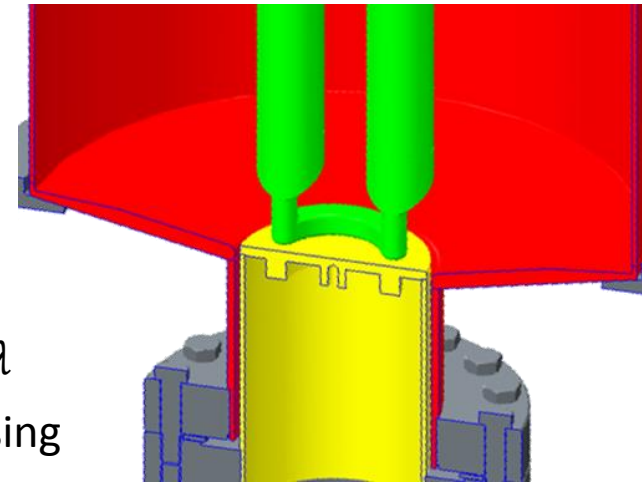
QPR pole shoes (SC!)

RF surface



2nd coil with  
reversed field

- $\lambda(T) = \frac{\lambda_0}{\sqrt{1 - \left(\frac{T}{T_c}\right)^4}}$
- Slater's Theorem:  $\frac{\Delta f}{f} = \frac{\frac{1}{4} \int_V^{V+\Delta V} (\epsilon_0 |E|^2 - \mu_0 |H|^2) dV}{U}$   
 Electric penetration contribution negligible,  $dV = dA d\lambda$   
 → increasing volume of resonator → frequency decreasing



- $\lambda(T) - \lambda_0 = \Delta\lambda = -\frac{G_{\text{sample}}}{\pi\mu_0 f^2} \Delta f$
- mean free path from  $\lambda(0 \text{ K}) = \lambda_0$   
 $\lambda_0(l) = \lambda_L \sqrt{1 + \frac{\pi\xi_0}{2l}}$
- $RRR \approx \frac{l [\text{nm}]}{2.7}$

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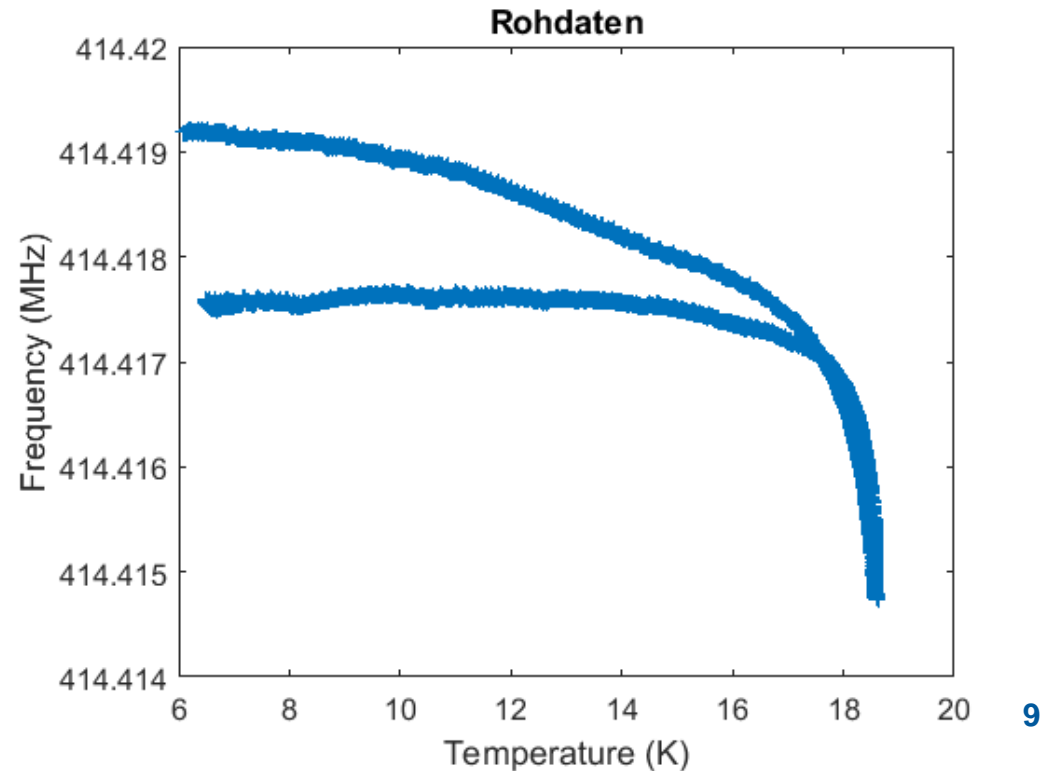
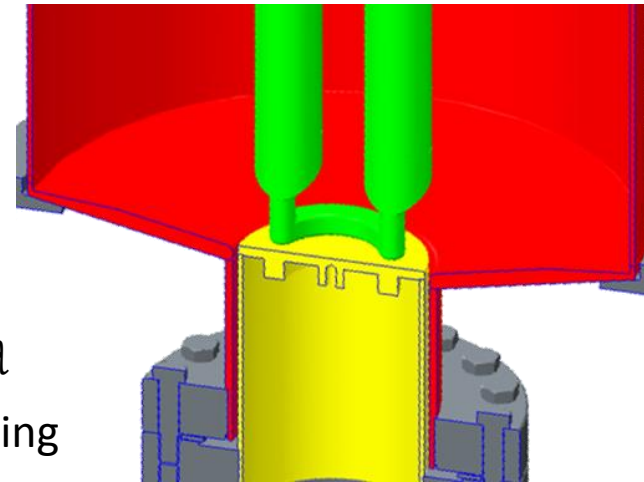
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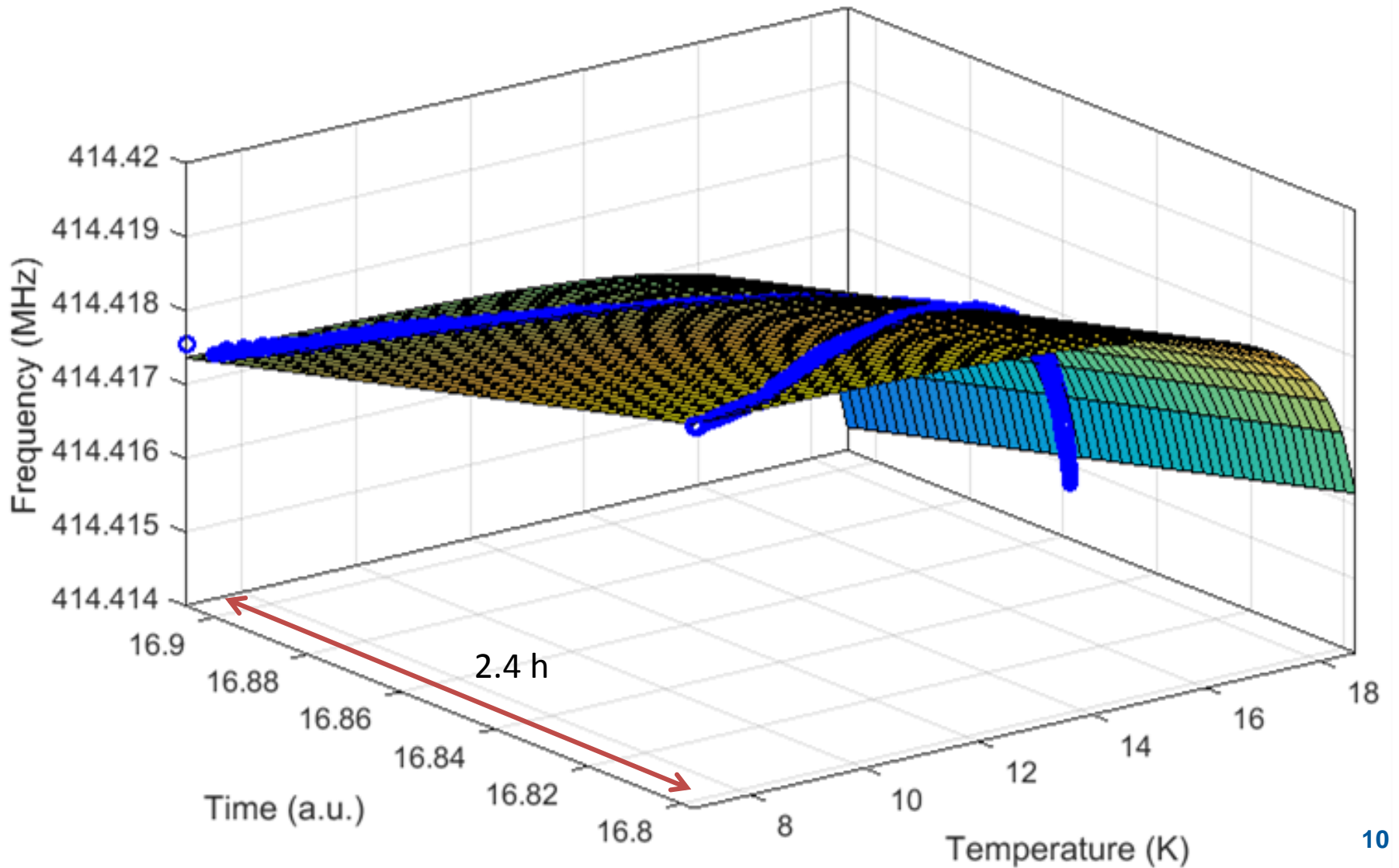
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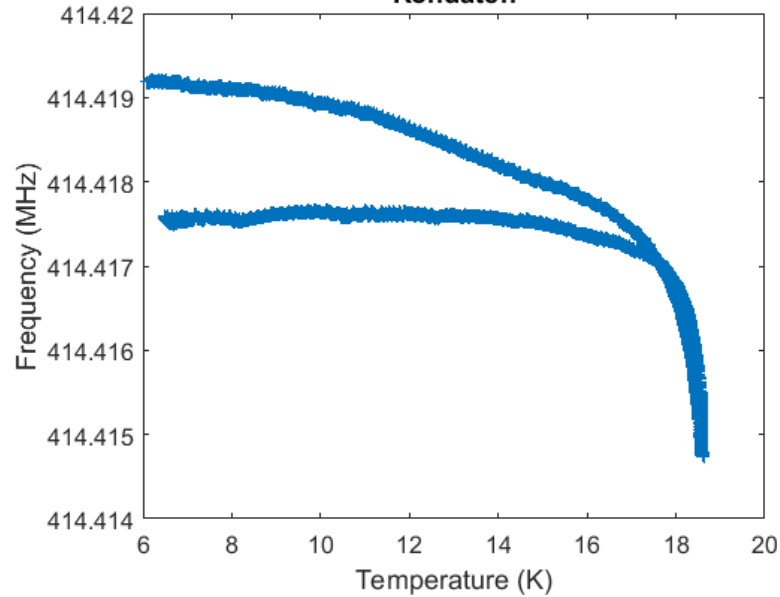
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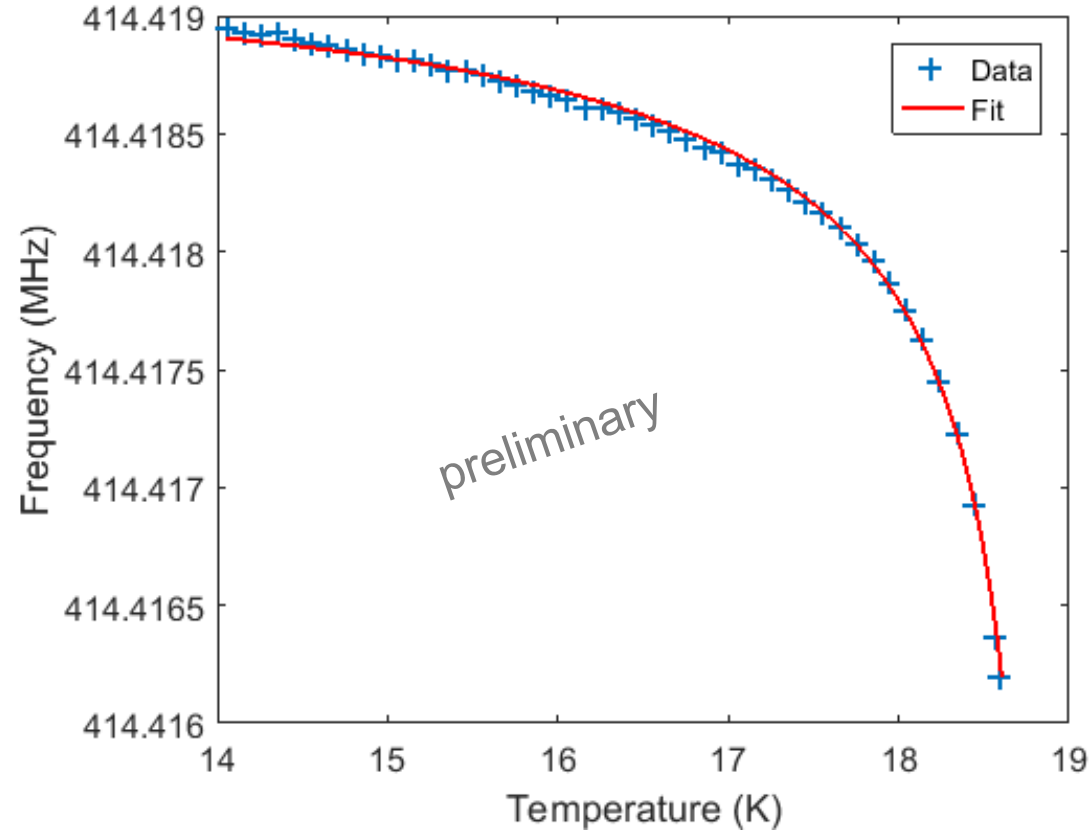
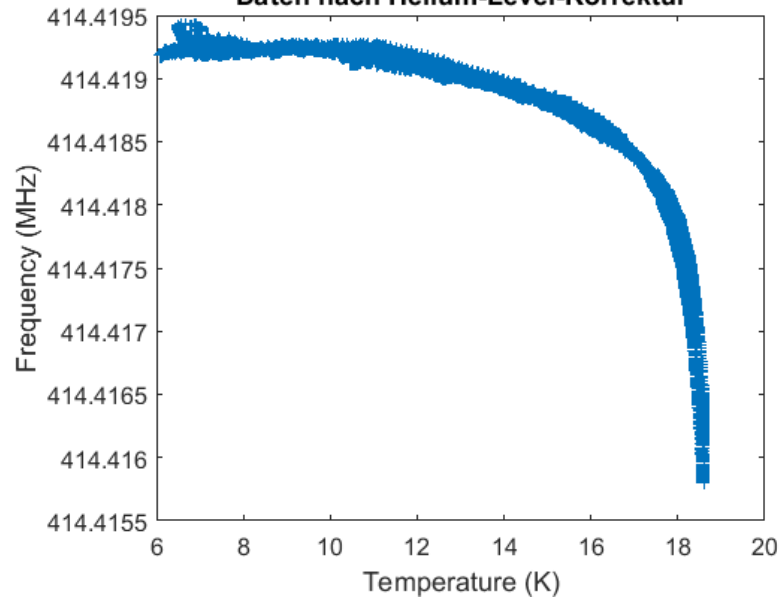
- Decreasing helium level  $\rightarrow$  linear drift of frequency



Rohdaten



Daten nach Helium-Level-Korrektur

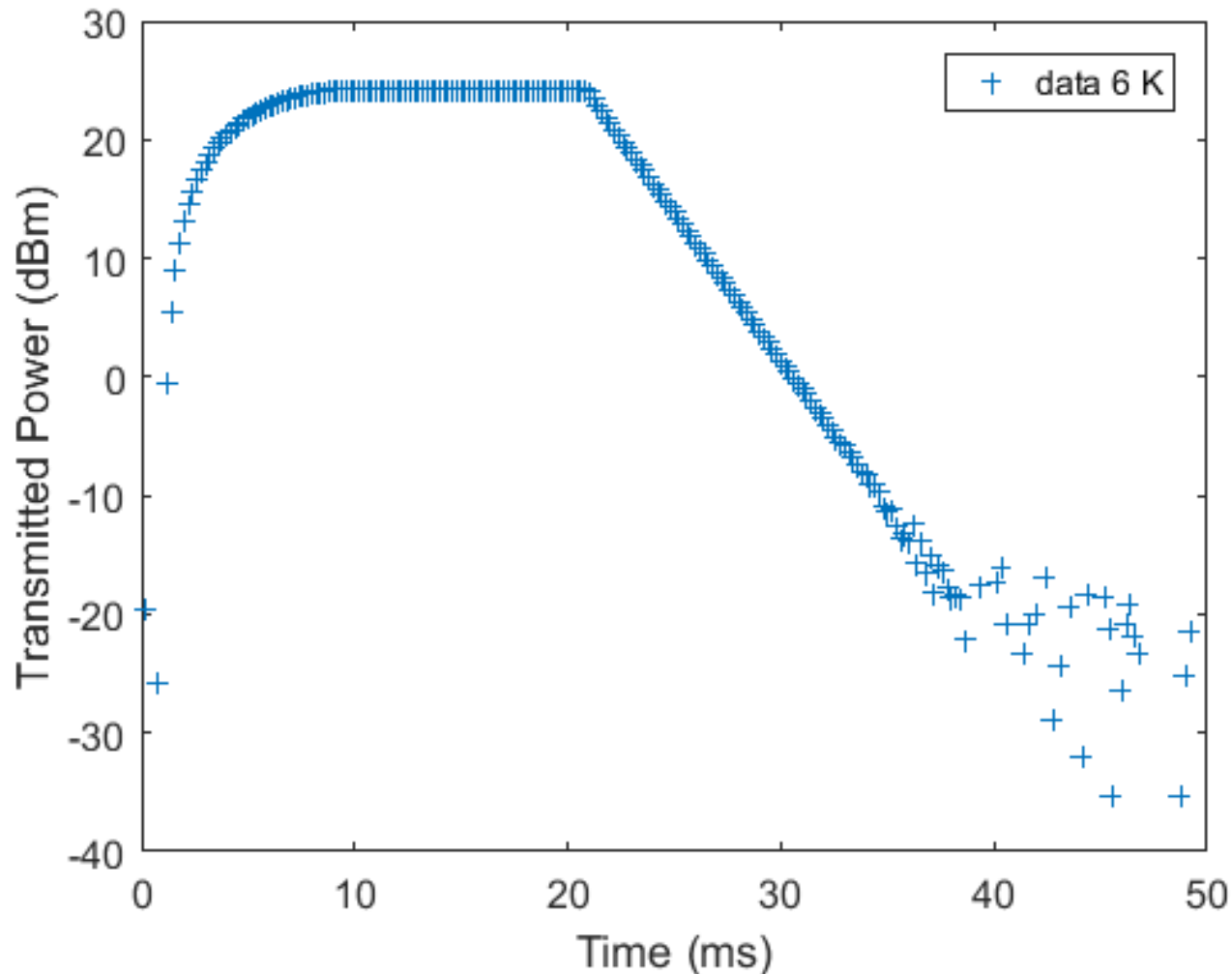


Nb<sub>3</sub>Sn sample (provided by Cornell)

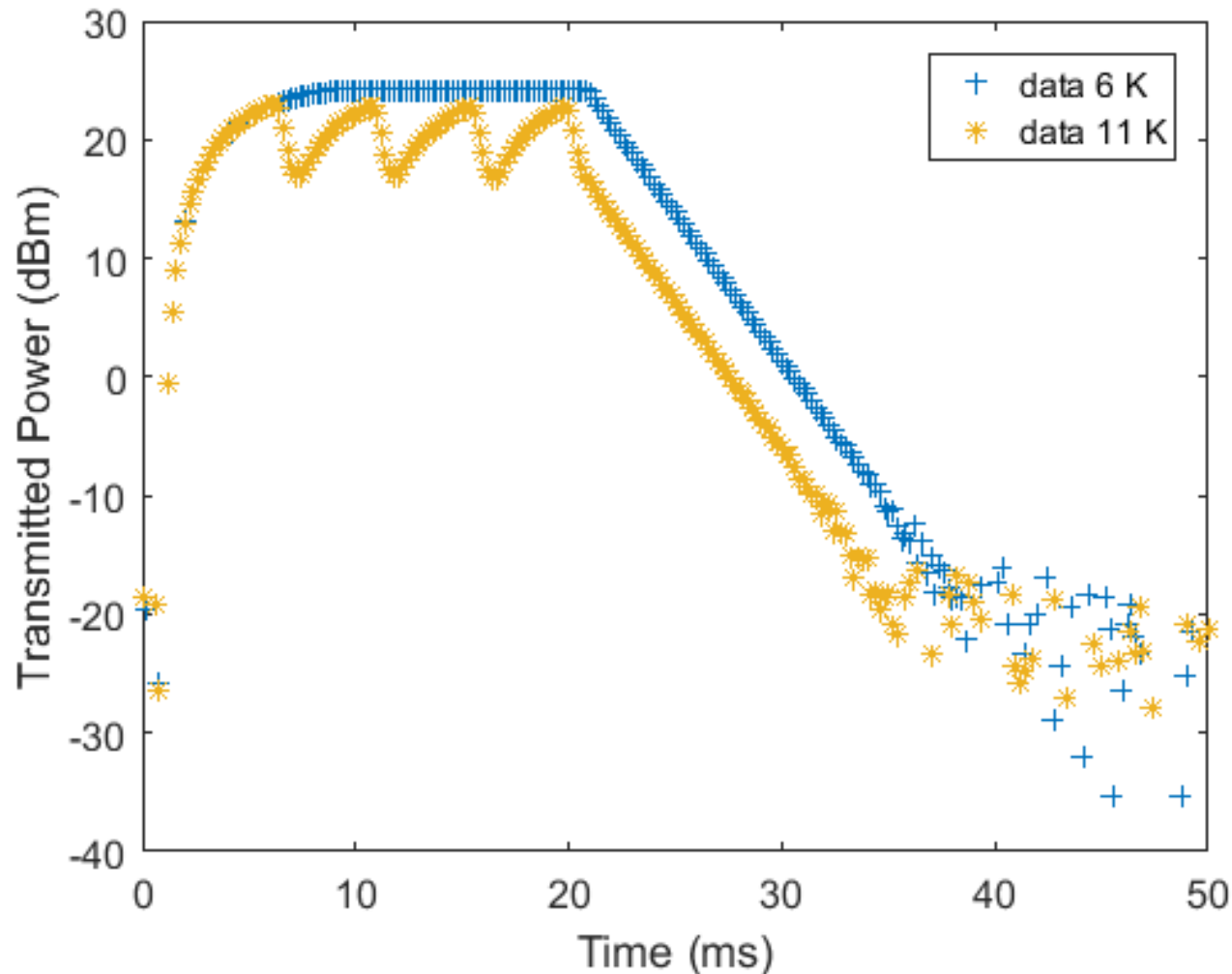
$$\lambda_L = 90 \text{ nm}$$

$$\lambda_0 \approx 140 \text{ nm (from fit)}$$

- $B_c(T) = B_{c,0} \cdot \left(1 - \left(\frac{T}{T_c}\right)^2\right)$
- Single short pulse of RF power  $\rightarrow$  sample quenches

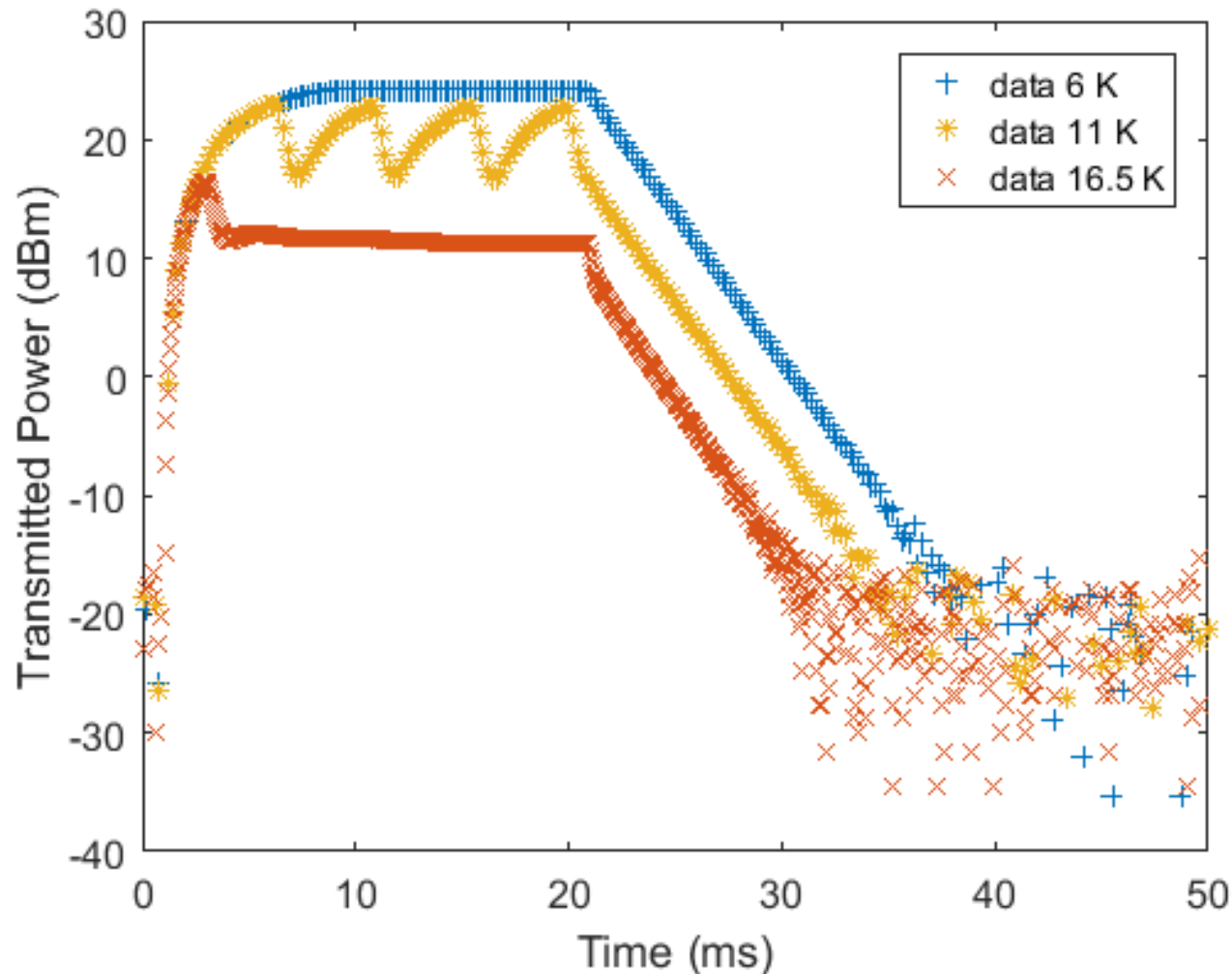


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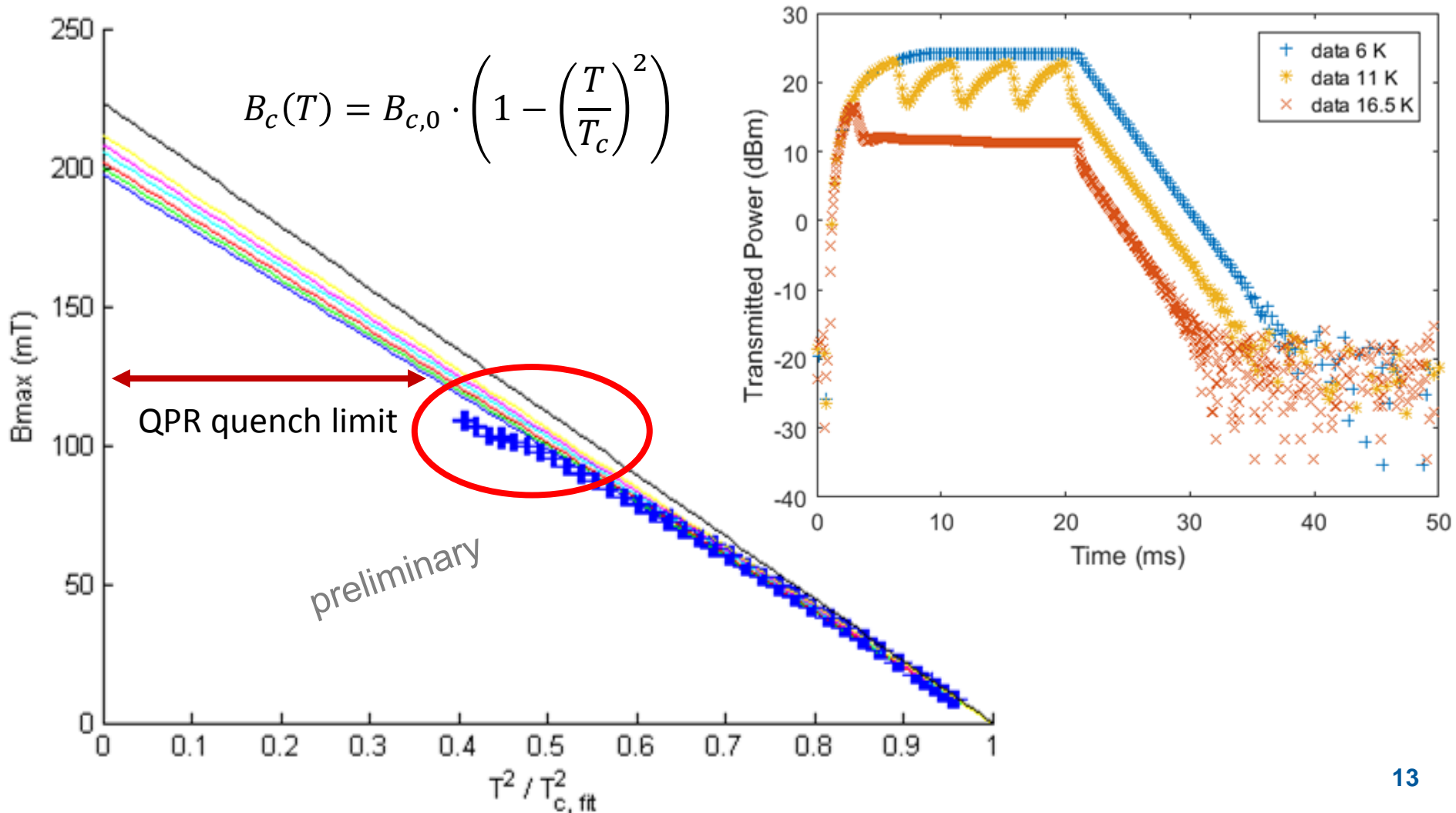




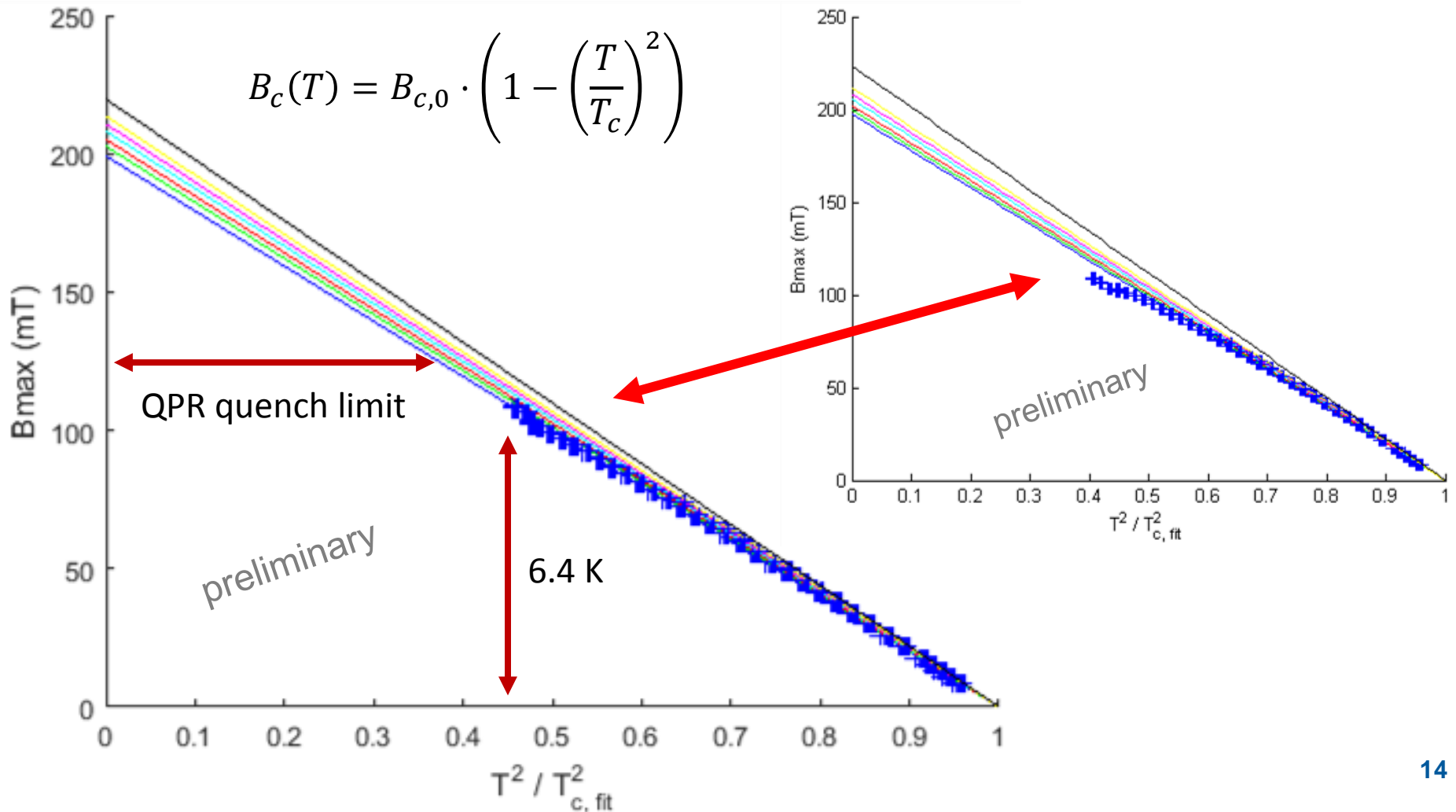
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- N-doped Nb sample (provided by Jefferson Lab)
- Significant RF heating at lower temperatures



- Significant RF heating at lower temperatures → correction applied to data
- N-doped Nb sample (provided by Jefferson Lab)  
→ no reduction of quench field observed



- QPR commissioned at 420, 850, 1300 MHz
  - Quench limit at 125 mT
- Automated penetration depth measurement
- Single pulse critical field measurement
- Work ongoing on trapped magnetic flux

**Thank you for your attention!**



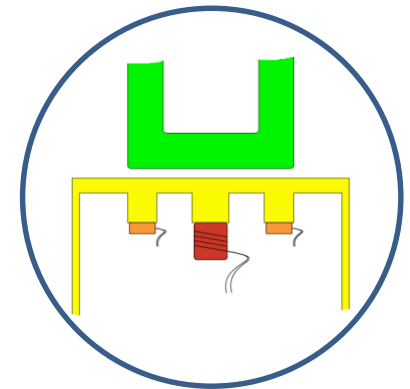
EuCARD-2 is co-funded by the partners  
and the European Commission under  
Capacities 7th Framework Programme,  
Grant Agreement 312453



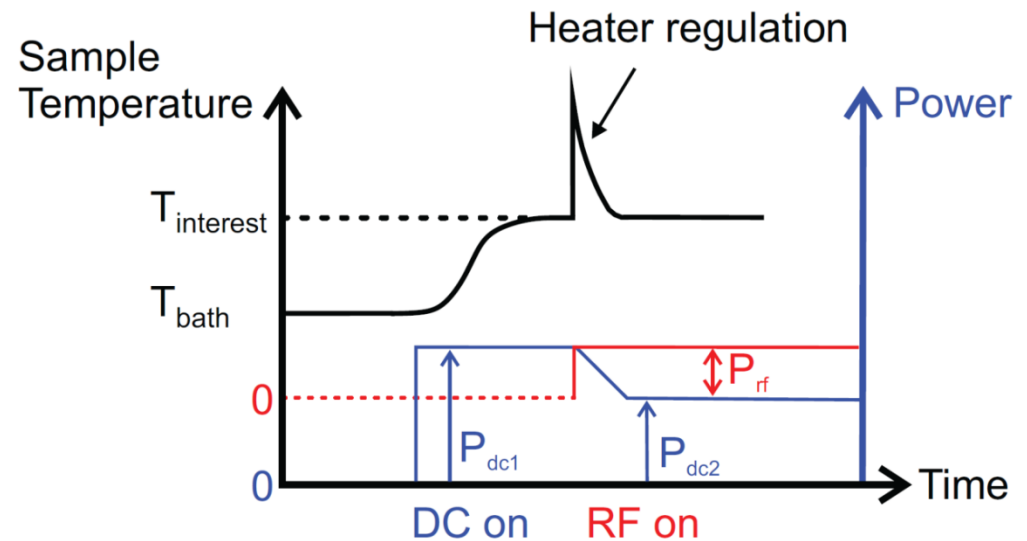


## RF-DC compensation technique

- High precision: calorimetric measurement
  - Resolution: sub-nΩ
- Wide temperature range:  $T_{min} = T_{LHe}$ ,  $T_{max} > 20 K$
- Operating at low frequency (420 MHz)
  - Low BCS resistance  $\rightarrow$  sensitivity to  $R_{res}$



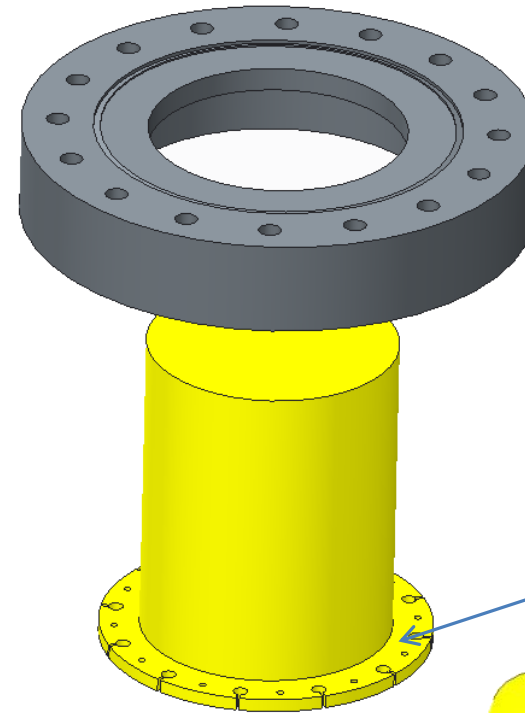
$$\begin{aligned}
 P_{RF} &= \frac{1}{2} \iint_{sample} R_S |\vec{H}|^2 dS \\
 &= R_S \frac{\omega U}{G} \\
 &= P_{DC,1} - P_{DC,2} \\
 \Rightarrow R_S &= \frac{G}{\omega U} (P_{DC,1} - P_{DC,2}) \\
 &= c(\omega) \cdot \frac{P_{DC,1} - P_{DC,2}}{P_{RF \text{ pickup}}}
 \end{aligned}$$



[S. Aull, „High Resolution Surface Resistance Studies“, SRF 2013]

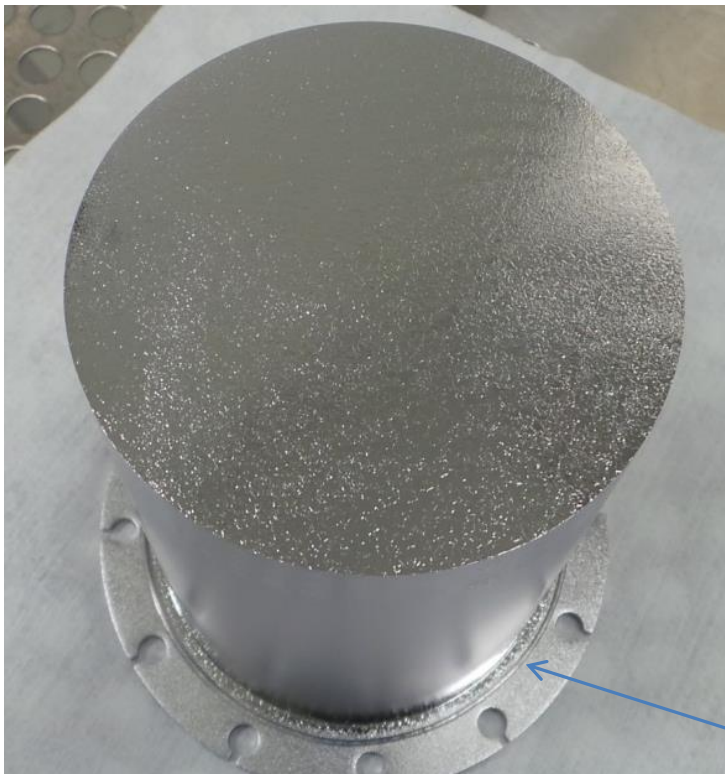
# Alternative calorimetry chamber

- Pure Nb sample  
→ high temperature treatments possible
  - baking, doping, coating
- UHV tight system  
→ Indium wire gasket reproducible
- Height adjustment possible  
→ compatible to CERN QPR



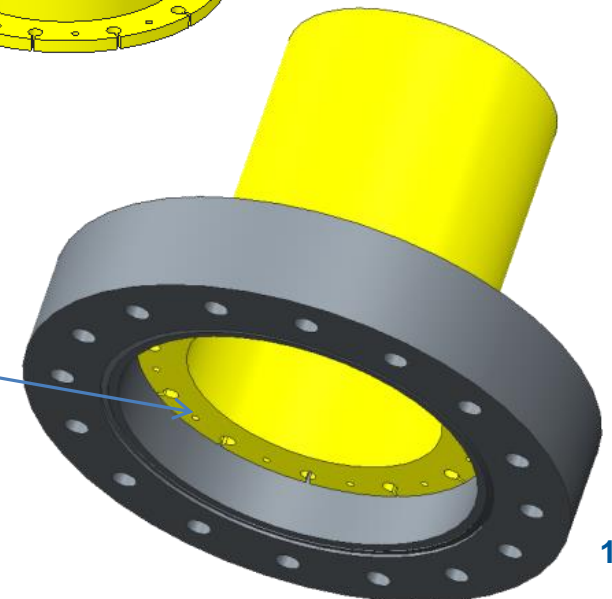
Double sided  
CF100 flange

Indium wire



Indium wire

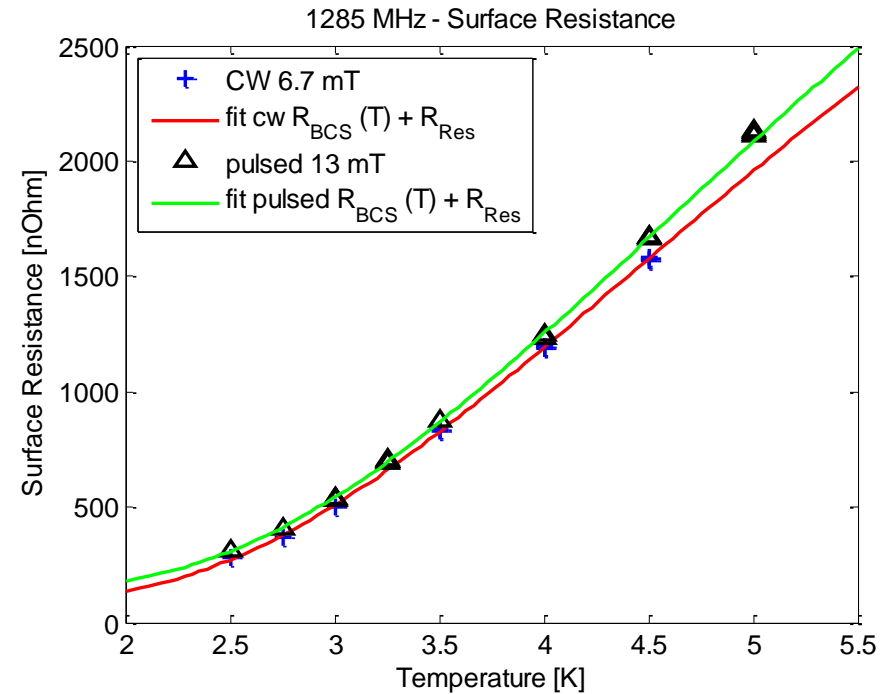
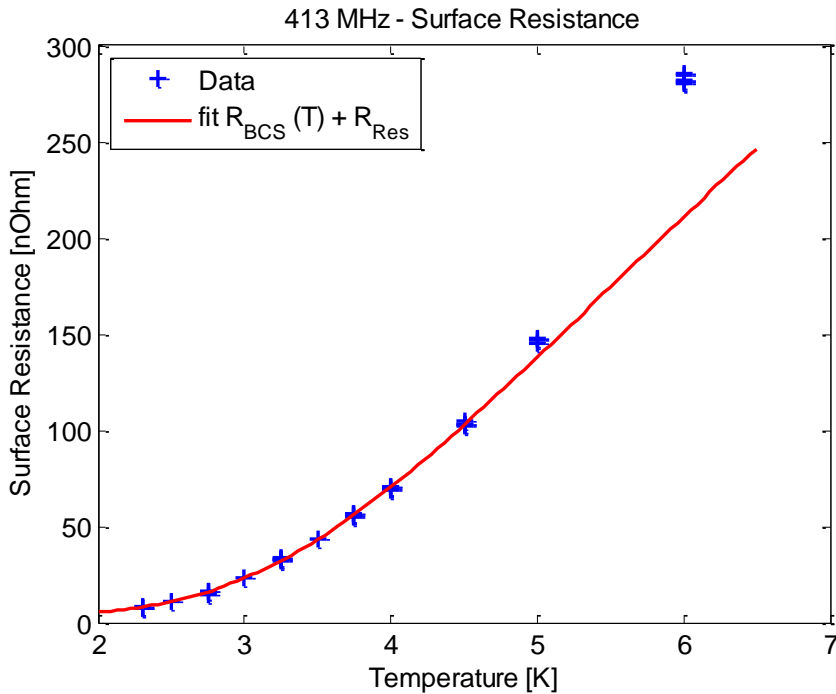
additional  
T-sensors





# Commissioning of alt. calorimetry chamber

$$R_S = R_{BCS} + R_{res} = \frac{A\omega^2}{T} \exp\left(-b \frac{T_C}{T}\right) + R_{res}$$



	413 MHz 16 mT, cw	1285 MHz 6.7 mT, cw	1285 MHz 13 mT, 30% DF
$A \left[ \frac{\mu\Omega \text{ K}}{(\text{GHz})^2} \right]$	$4.1 \pm 0.2$	$2.86 \pm 0.13$	$3.37 \pm 0.15$
$b$	$2.01 \pm 0.03$	$1.62 \pm 0.03$	$1.68 \pm 0.03$
$R_{res} [\text{n}\Omega]$	$4.3 \pm 0.5$	$83 \pm 12$	$136 \pm 12$

# Alternative calorimetry chamber

