

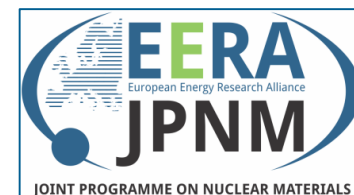


MAX Phases for Gen-IV Lead Fast Reactors (LFRs)

Dr. Konstantina Lambrinou

The 5th Huddersfield Annual Accelerator Symposium:
Announcing the **UK National Ion Beam Centre**

Buckley Lecture Theatre, U Huddersfield, 21/04/2017



- Introduction
 - Starting R&D Point: MYRRHA
 - Envisaged Applications for MYRRHA & Gen-IV LFRs
 - Why MAX Phases for MYRRHA & Gen-IV LFRs?
- MAX Phase Synthesis: Application-Driven
 - Phase Purity: Zr-Al-C System vs. (Zr,Nb)-(Al,Sn)-C System
 - Oxidation Resistance: (Zr,Ti)-Al-C System
 - Mechanical Properties: (Nb,Zr)-Al-C System
- MAX Phase Compatibility with Liquid LBE
 - Compatibility with Static LBE
 - Compatibility with Fast-Flowing LBE
- Mechanical Properties of MAX Phases
- Exploratory Ion Irradiation of $(\text{Nb}_{0.85}, \text{Zr}_{0.15})_4\text{AlC}_3$
- Conclusions

MAX Phase R&D Starting Point: MYRRHA

Accelerator

(600 MeV - 4 mA proton)

Reactor

- Subcritical or Critical modes
- 65 to 100 MWth



MYRRHA Stainless Steels

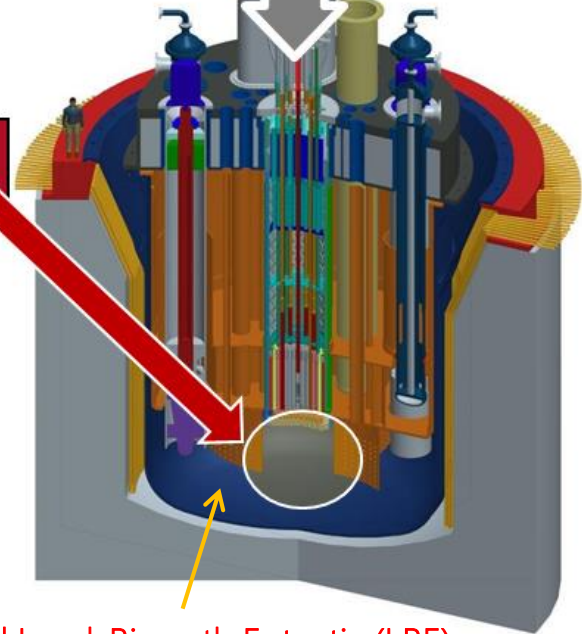
- 316L: structural steel
- DIN 1.4970: fuel cladding steel

Spallation Source

Fast
Neutron
Source

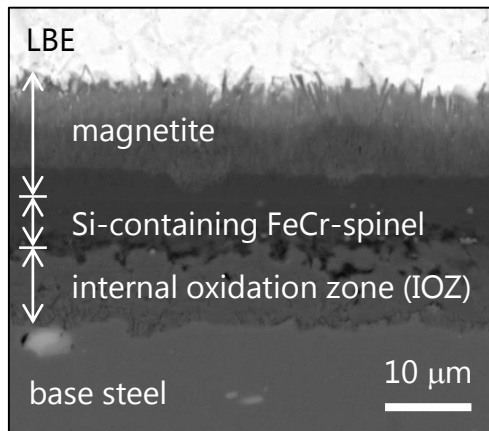
Multipurpose
Flexible
Irradiation
Facility

Liquid Lead-Bismuth Eutectic (LBE)
Primary Coolant



Basic Liquid Metal Corrosion (LMC) Mechanisms

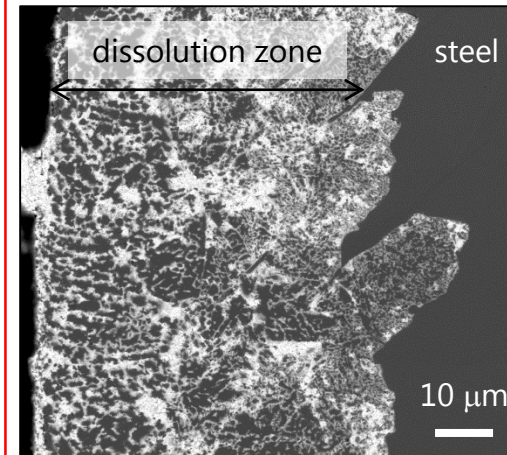
1. Oxidation



- Multi-layered oxide scales form in contact with O-containing LBE on steel surface
- If protective at service conditions, oxide scales minimize further attack of steel by LBE

EP-823: 490°C, 5016 h, oxygen saturation, **static LBE**
(K. Lambrinou, SCK•CEN)

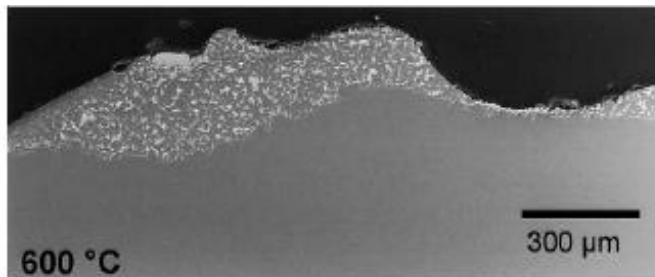
2. Dissolution



- Loss of steel alloying elements (Ni, Mn, Cr)
- LBE penetration
- Ferritization of dissolution zone due to loss of austenite stabilizers (Ni, Mn)

316L: 500°C, 3282 h, $7.5 \times 10^{-13} < [\text{O}] \text{ (mass\%)} < 2.8 \times 10^{-8}$,
static LBE (K. Lambrinou, SCK•CEN)

3. Erosion



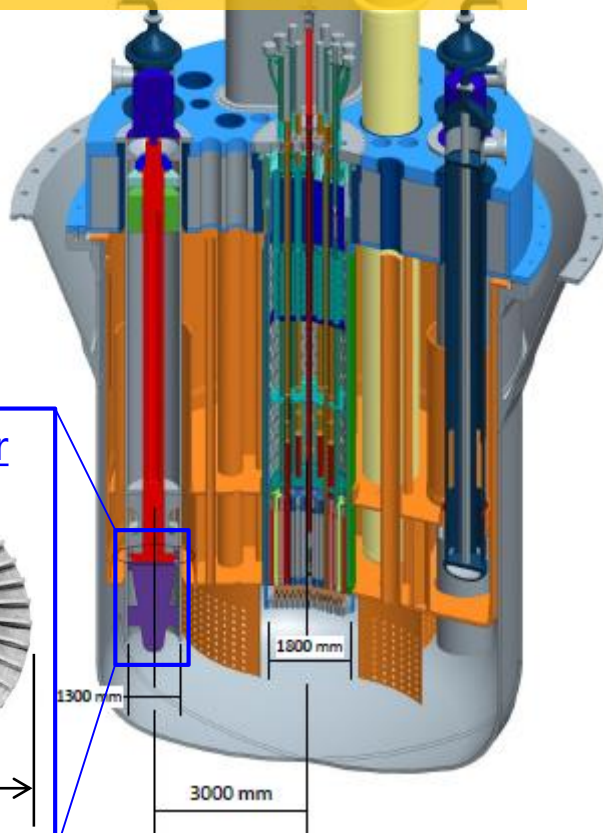
- Severe material loss & compromise of structural integrity
- Observed at high LBE flow velocities, two-phase flow, and sites of flow diversion

316L: 600°C, 2000 h, $[\text{O}] \approx 10^{-6}$ mass%, **flowing LBE** ($v \approx 2$ m/s)
(Müller et al., *Journal Nuclear Materials* **301** (2002) 40-46)

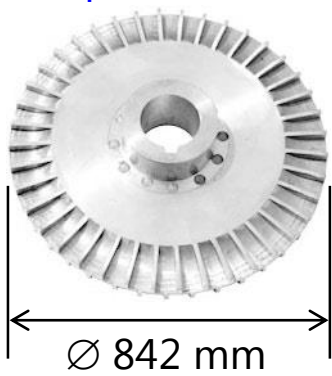
Envisaged Applications for MYRRHA & Gen-IV LFRs

MYRRHA Pump Impeller Service Conditions:

- $T \approx 270^\circ\text{C}$ ($T \approx 480^\circ\text{C}$ in Gen-IV LFRs)
- High LBE flow velocity ($v \approx 10\text{-}20\text{ m/s}$)
- LBE [O] $\approx 10^{-6}$ mass%
- Low fast neutron dose ($< 1\text{ dpa}$)



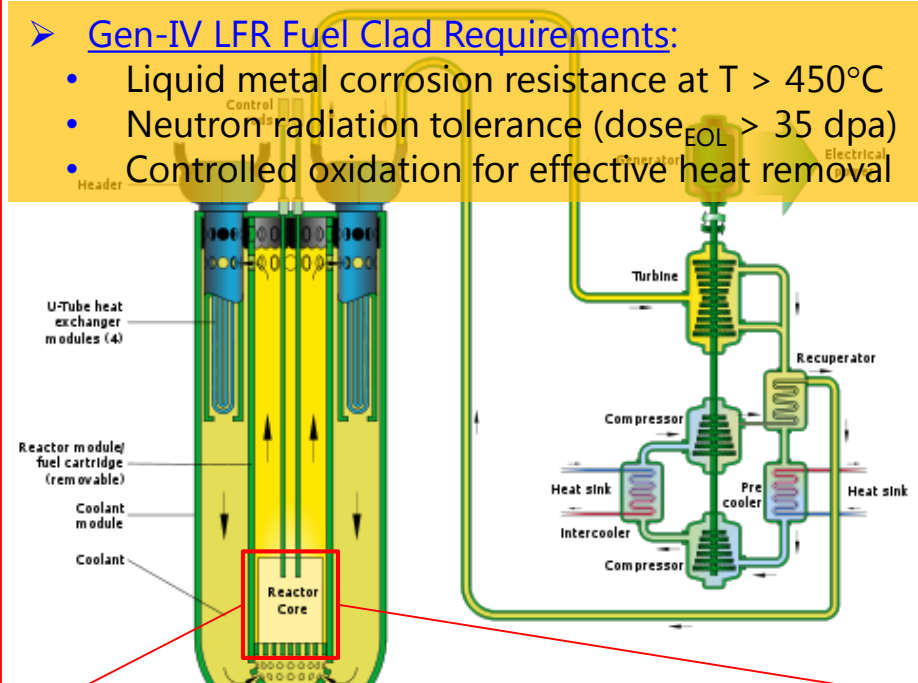
Impeller Rotor



Gen-IV LFR Fuel Cladding Materials

Gen-IV LFR Fuel Clad Requirements:

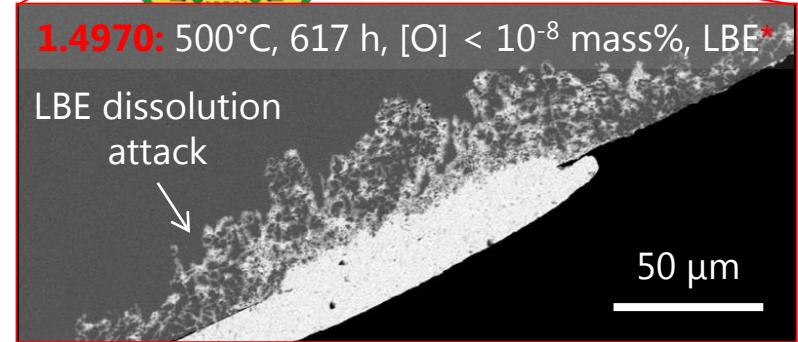
- Liquid metal corrosion resistance at $T > 450^\circ\text{C}$
- Neutron radiation tolerance (dose_{EOL} $> 35\text{ dpa}$)
- Controlled oxidation for effective heat removal



1.4970: 500°C , 617 h, [O] $< 10^{-8}$ mass%, LBE*

LBE dissolution attack

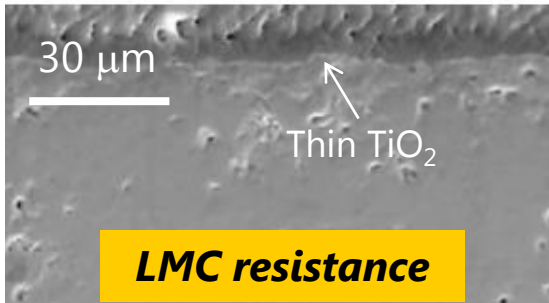
50 μm





Why MAX Phases for MYRRHA & Gen-IV LFRs?

- **MAX Phases:** unique combination of physical, chemical, mechanical properties, e.g., LMC resistance, machinability, damage tolerance, irradiation tolerance, ...



Ti₃SiC₂: 650°C, 3000 h,
[O] ≈ 10⁻⁸ mass%, static LBE

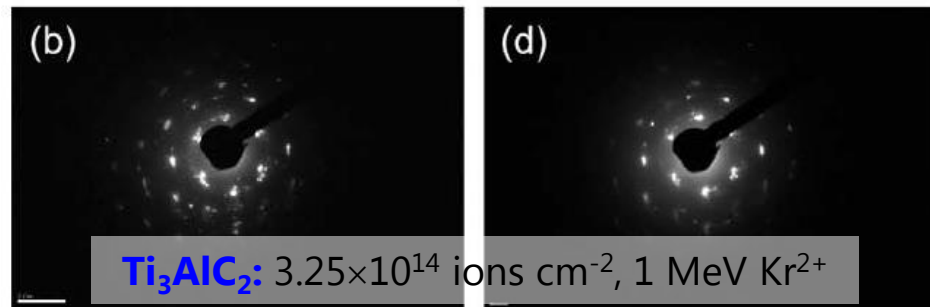
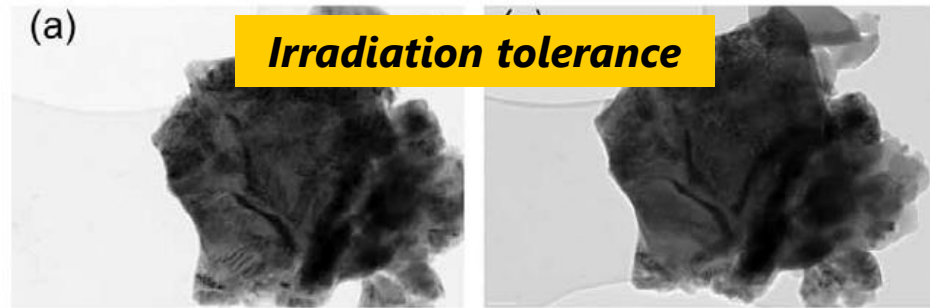
(A. Heinzl et al., *Journal of Nuclear Materials* **392** (2009) 255-258)



(M.W. Barsoum & M. Radovic,
Annu. Rev. Mater. Res. **41**
(2011) 195-227)

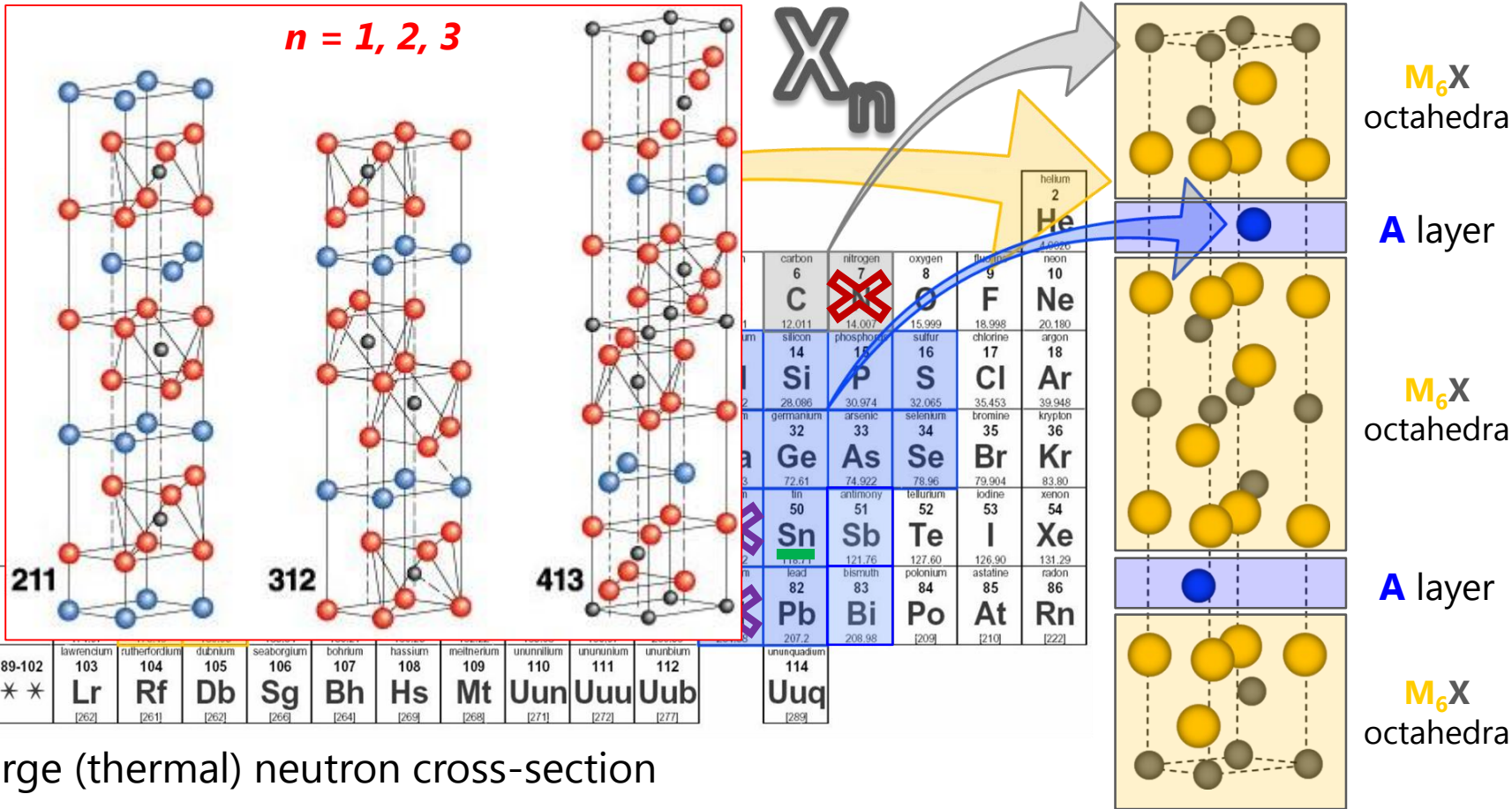


(M.W. Barsoum & M. Radovic,
Annu. Rev. Mater. Res. **41** (2011) 195-227)







(K.R. Whittle et al., *Acta Materialia* **58** (2010) 4362-4368)

MAX ($M_{n+1}AX_n$) Phases: Elemental Preselection

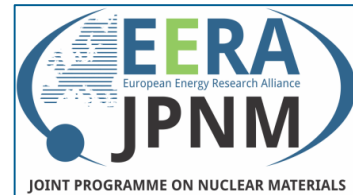
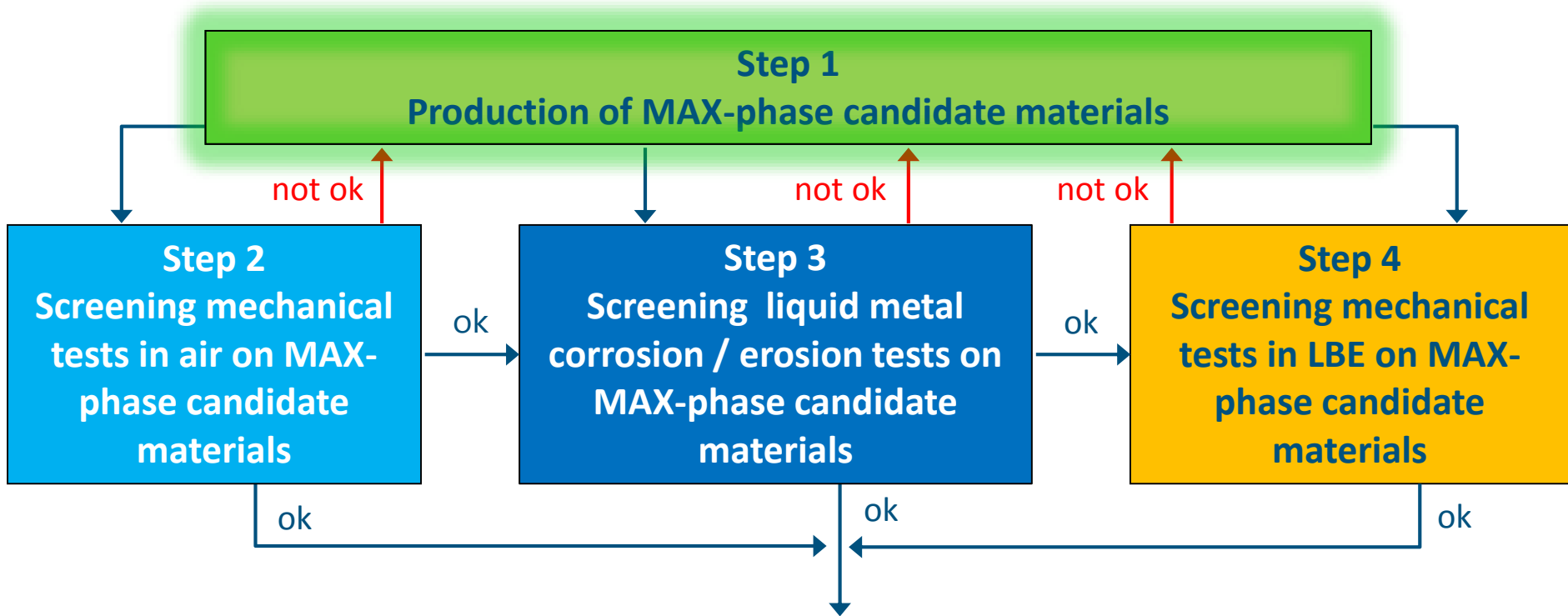


hydrogen 1 H 1.0079	beryllium 4 Be 9.0122											helium 2 He 4.0026	
lithium 3 Li 6.941	magnesium 12 Mg 24.305											neon 10 Ne 20.180	
sodium 11 Na 22.990	calcium 20 Ca 40.078											argon 18 Ar 39.948	
potassium 19 K 39.098	strontium 38 Sr 87.62											krypton 36 Kr 83.80	
rubidium 37 Rb 85.468	barium 56 Ba 137.33											xenon 54 Xe 131.29	
caesium 55 Cs 132.91	radium 88 Ra [226]	89-102 **	lawrencium 103 Lr [262]	rutherfordium 104 Rf [261]	dubnium 105 Db [262]	seaborgium 106 Sg [266]	bohrium 107 Bh [264]	hassium 108 Hs [269]	meitnerium 109 Mt [268]	ununnitium 110 Uun [271]	ununium 111 Uuu [272]	ununbium 112 Uub [277]	ununquadium 114 Uuq [289]
carbon 6 C 12.011	nitrogen 7 N 14.007	oxygen 8 O 15.999	fluorine 9 F 18.998	silicon 14 Si 28.086	phosphorus 15 P 30.974	sulfur 16 S 32.065	chlorine 17 Cl 35.453	argon 18 Ar 39.948	germanium 32 Ge 72.61	arsenic 33 As 74.922	selenium 34 Se 78.96	bromine 35 Br 79.904	krypton 36 Kr 83.80
boron 5 B 10.811	aluminum 13 Al 26.981	nitrogen 7 N 14.007	oxygen 8 O 15.999	silicon 14 Si 28.086	phosphorus 15 P 30.974	sulfur 16 S 32.065	chlorine 17 Cl 35.453	argon 18 Ar 39.948	germanium 32 Ge 72.61	arsenic 33 As 74.922	selenium 34 Se 78.96	bromine 35 Br 79.904	krypton 36 Kr 83.80
tin 50 Sn 118.710	antimony 51 Sb 121.76	tellurium 52 Te 127.60	iodine 53 I 126.90	lead 82 Pb 207.2	bismuth 83 Bi 208.98	polonium 84 Po [209]	astatine 85 At [210]	radon 86 Rn [222]	tin 50 Sn 118.710	antimony 51 Sb 121.76	tellurium 52 Te 127.60	iodine 53 I 126.90	radon 86 Rn [222]

-  Large (thermal) neutron cross-section
-  Long-lived isotope ^{14}C
-  Alloying elements in commercial clads (zircalloys/15-15Ti stainless steels)
-  System of interest: **Zr-Al-C** and **solid solutions thereof (+Nb, Ti, Cr, Sn, ...)**

Laminated crystal structure

MAX Phase R&D: Approach, Challenges, Achievements



STEP 1

Synthesis: Zr-Al-C System

- Discovery (synthesis) of MAX phases in the Zr-Al-C system!
- Synthesis facilitated by the use of finer starting powders (ZrH_2 , Al & C)
- Production of phase-pure Zr-based MAX phases proved challenging

Zr_3AlC_2

Space group

$P6_3/mmc$ (194)

a (Å)

3.33308(6)

c (Å)

19.9507(3)

Zr_2AlC

Space group

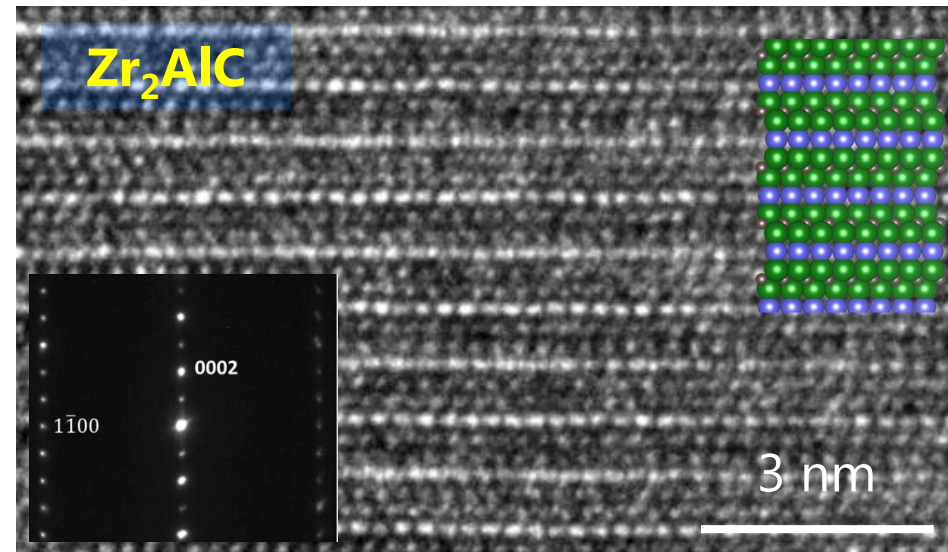
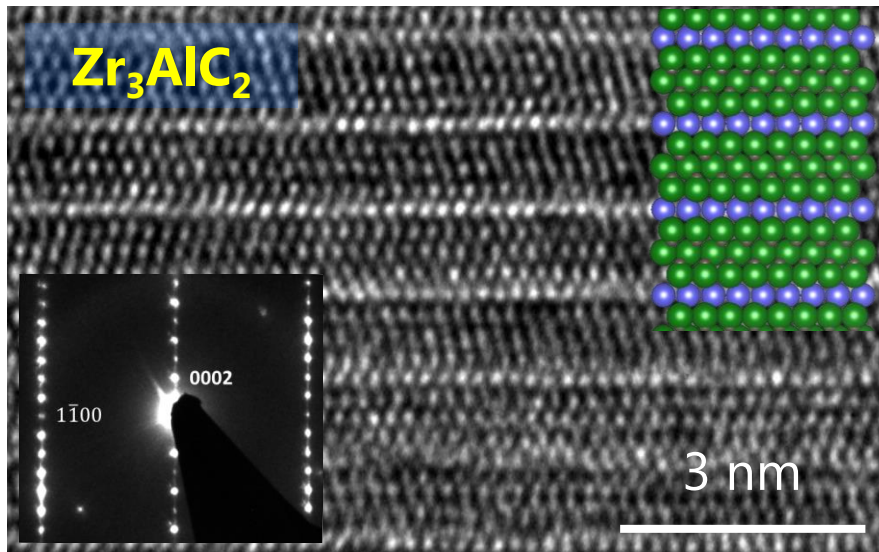
$P6_3/mmc$ (194)

a (Å)

3.3237(2)

c (Å)

14.5705(4)



(T. Lapauw et al., *J. Eur. Ceram. Soc.* **36** (2016) 943–947)

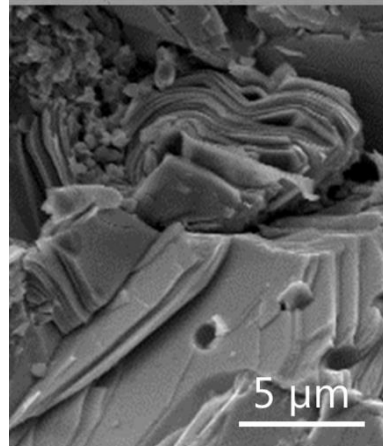
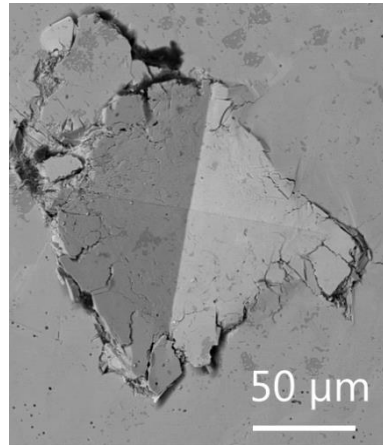
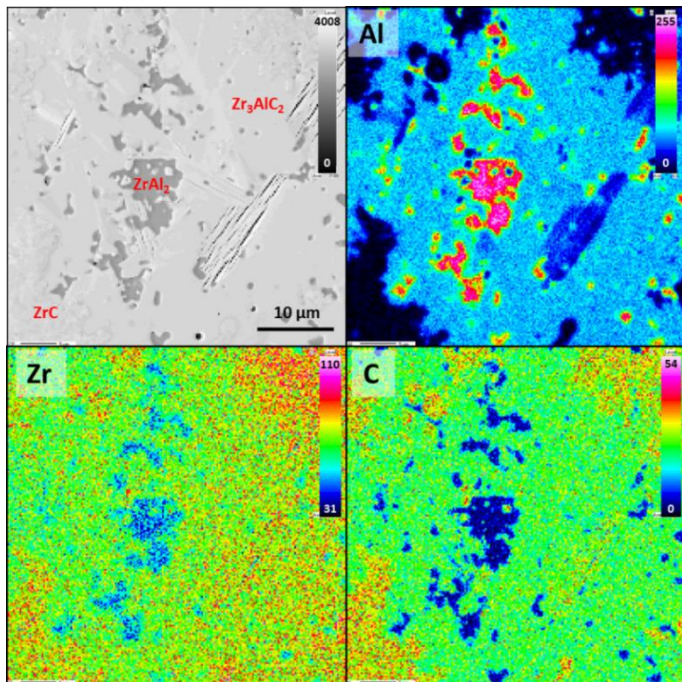
(T. Lapauw et al., *J. Eur. Ceram. Soc.* **36** (2016) 1847–1853)

STEP 1

Zr-Al-C System Challenge: Phase Purity

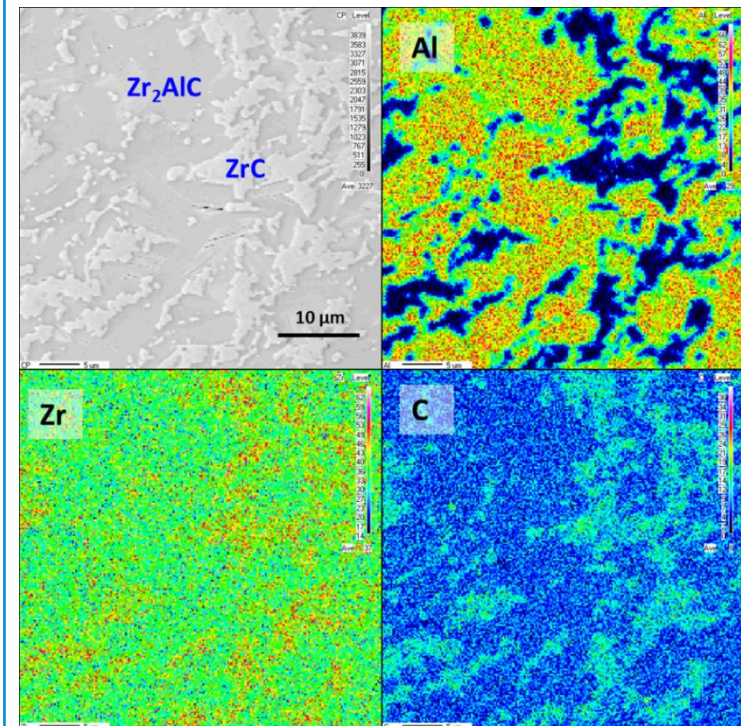
Starting ratio: $\text{Zr:Al:C} = 51.0 : 15.9 : 33.1$

Phase	Weight%
Zr_3AlC_2	59(1)
ZrC	35(1)
ZrAl_2	6(1)



$\text{Zr:Al:C} = 50 : 20 : 30$

Phase	Weight%
Zr_2AlC	67(1)
ZrC	33(1)



- **Phase purity:** minimises differences in swelling, corrosion behaviour, etc.
- Synthesis of $(\text{M},\text{M}')_{n+1}(\text{A},\text{A}')\text{X}_n$ solid solutions to increase phase purity!

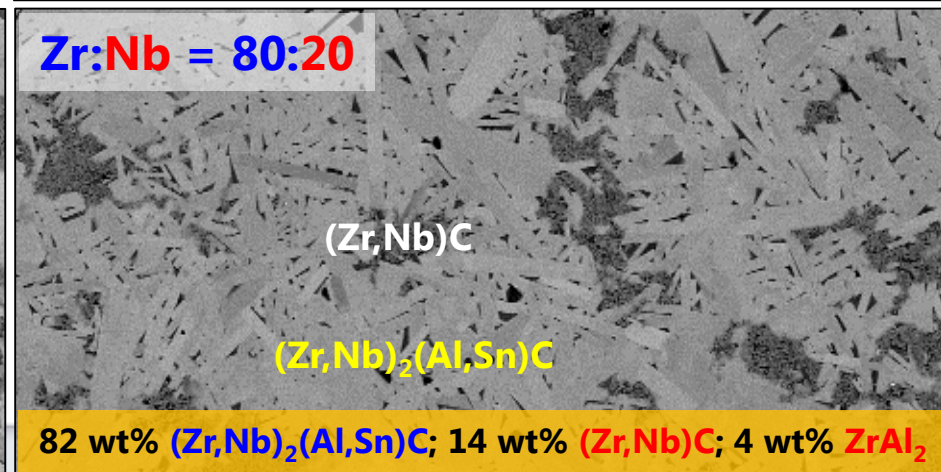
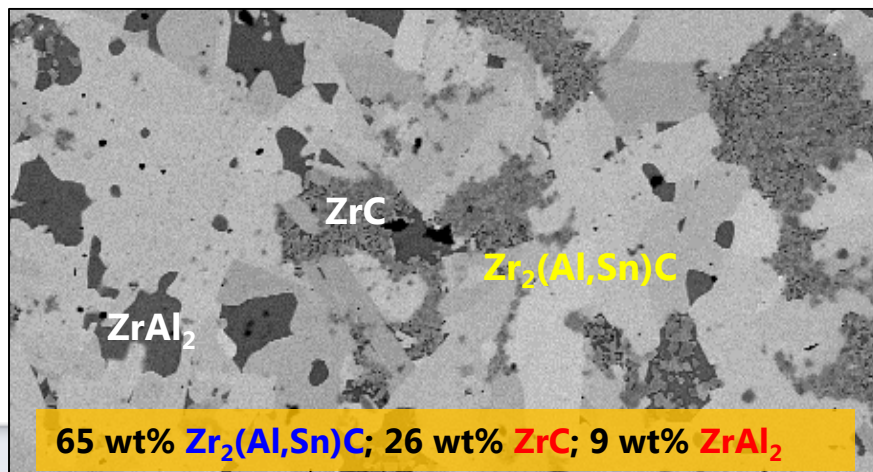
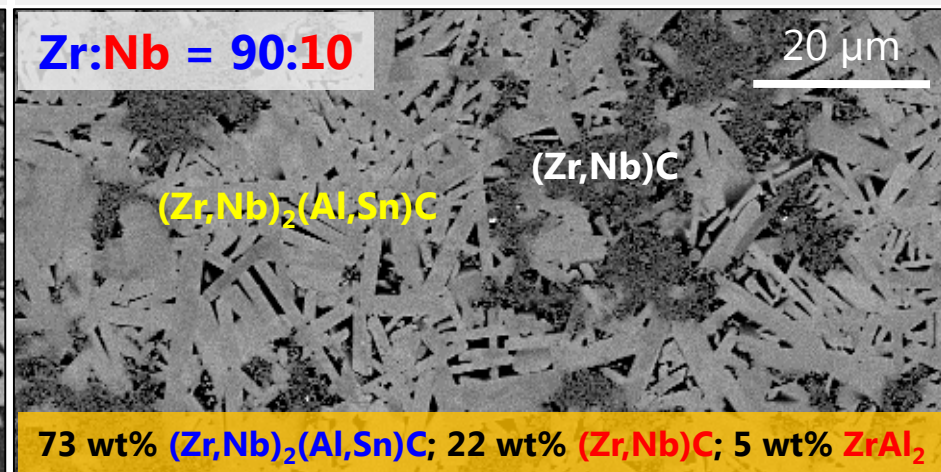
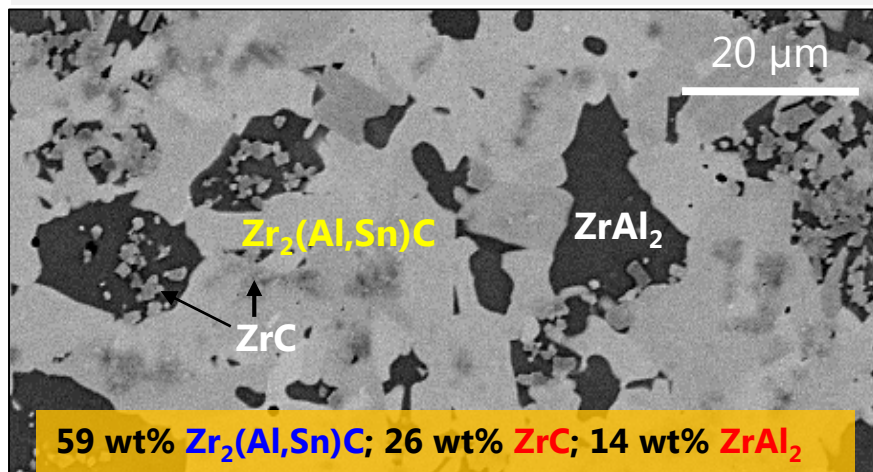
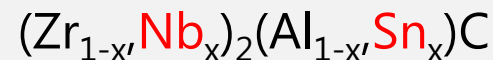
STEP 1

High Phase Purity: (Zr,Nb)-(Al,Sn)-C SS

- Best Zr₂AlC-based material contained 67 wt% Zr₂AlC & 33 wt% ZrC

Sn was selected as most promising alloying A-element in Zr₂(Al_{1-x}A_x)C

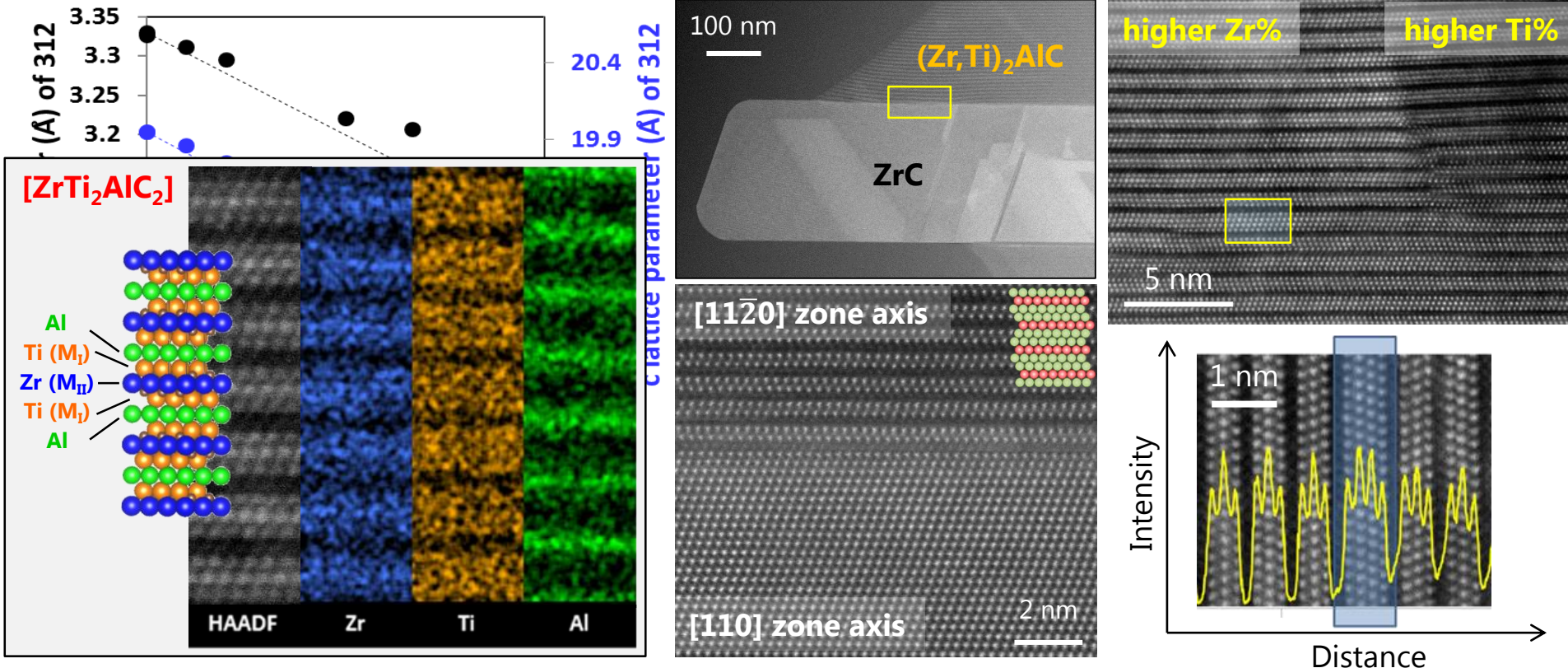
Solid solution on both M and A sites:



STEP 1

Oxidation Resistance: (Zr,Ti)-Al-C SS

- Investigation of **Ti** solubility in $Zr_{n+1}AlC_n$ by *reactive hot pressing*
 - Solid solubility over the entire compositional range for both 211 & 312
 - **Atomic ordering** in both 312 & 413 stackings: Ti on M_I site & Zr on M_{II} site
 - Non phase-pure MAX phase ceramics (Zr_2Al_3 , $ZrAl_3$, $(Zr,Ti)C$)



STEP 1

Mechanical Properties: (Nb,Zr)-Al-C SS

Property

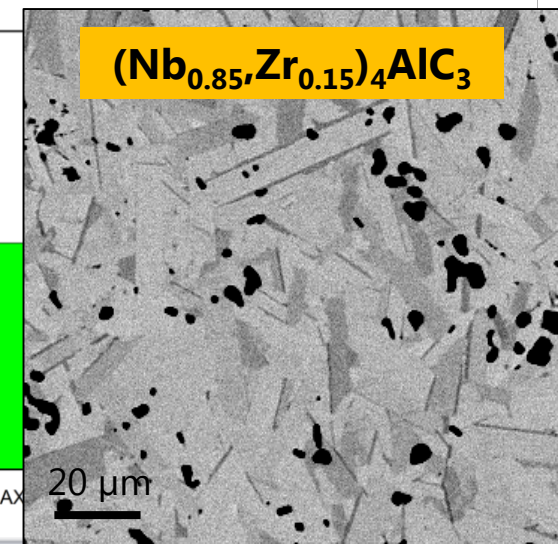
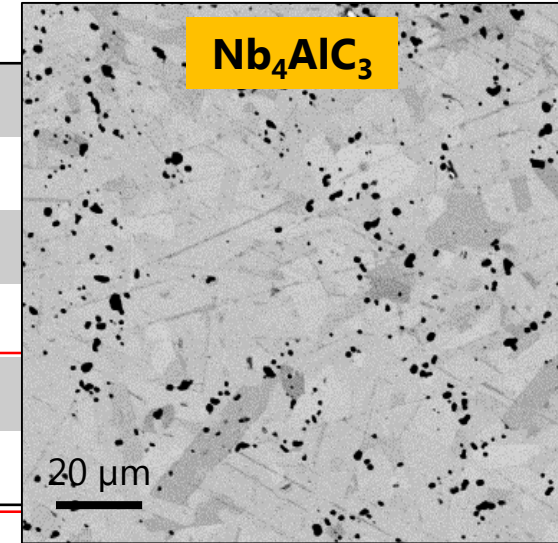
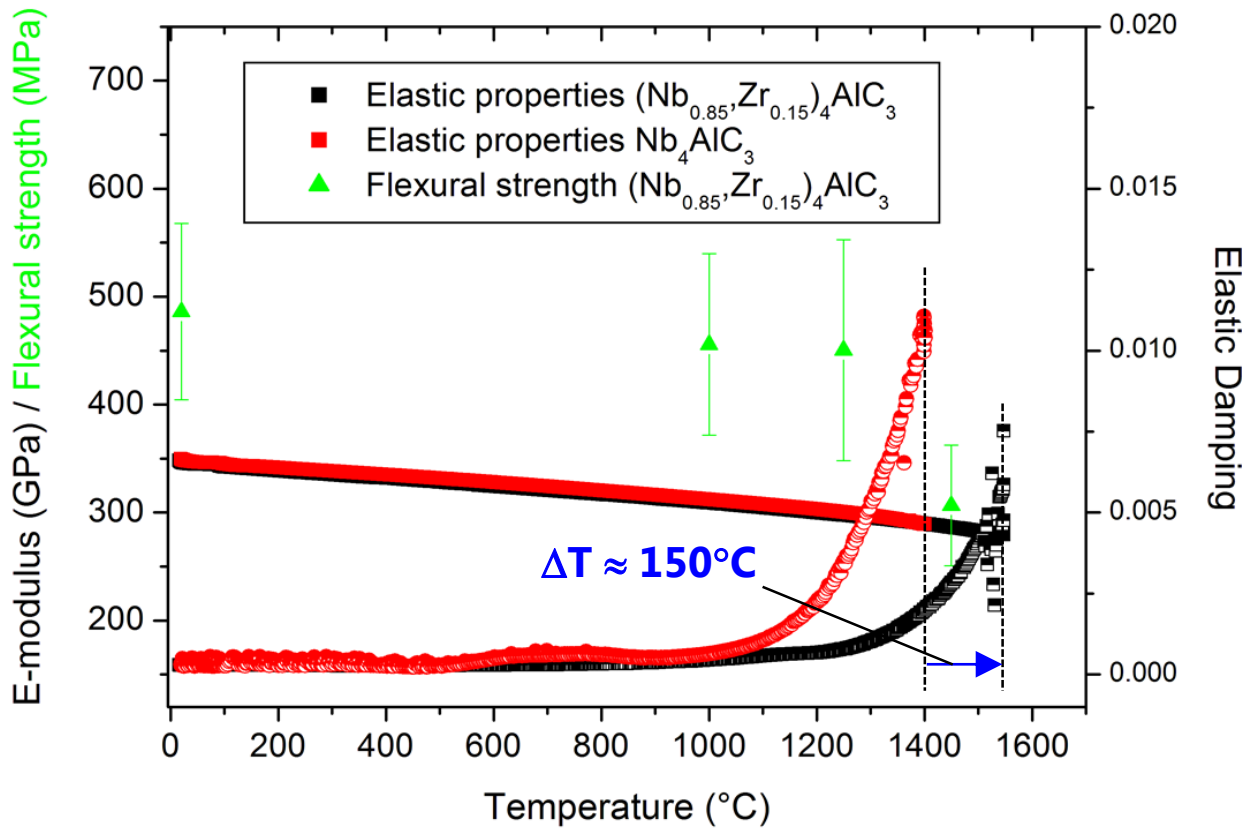
Nb_4AlC_3

ρ (g/cm³)

6.89 ± 0.06 (98% ρ_{th})

Grain size: GS₁/GS₂ (μm)

14 + 5 / 4 + 2

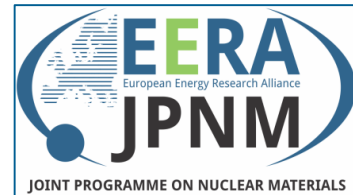
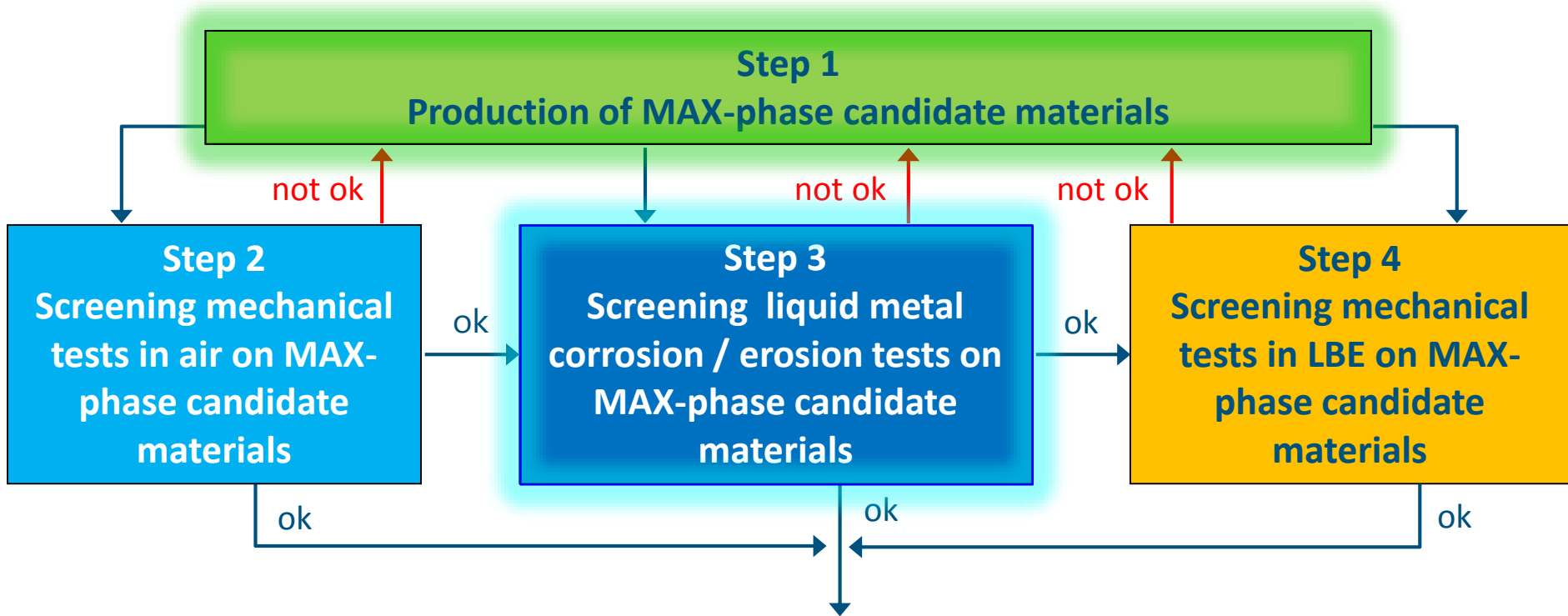


MAXTHAL 312® MAXTHAL 211®

Nb_4AlC_3 $(Nb_{0.85}, Zr_{0.15})_4AlC_3$

MAXTHAL 312® MAX

MAX Phase R&D: Approach, Challenges, Achievements

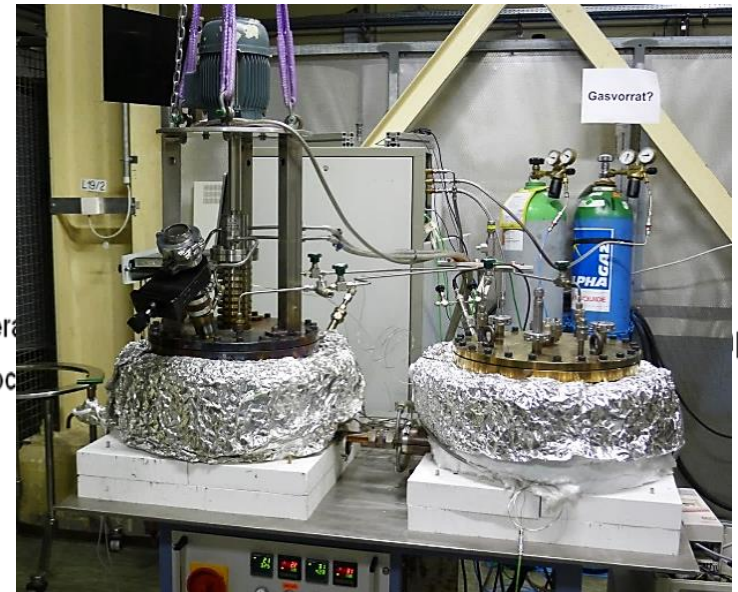


STEP 3

LMC/Erosion: Test Setups



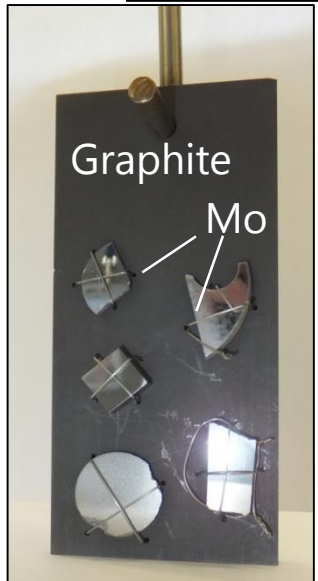
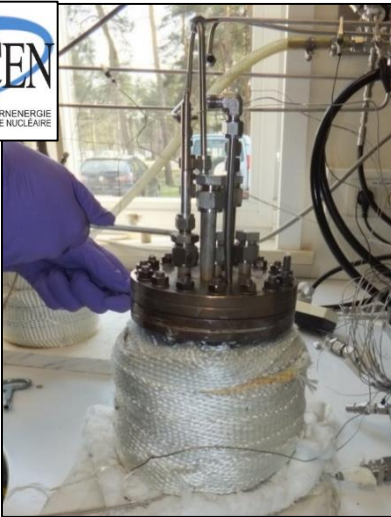
- **Erosion Setup – CORELLA facility:**
 - Fast-flowing Pb/LBE ($v > 10$ m/s)
 - T & [O] (SCK•CEN oxygen sensor)
 - Control [O] by using conditioning gases
- **Tests:** MAX phases & 316L stainless steel (ref); relevant for MYRRHA (300°C) & Gen-IV LFR (500°C) impellers ($v > 8$ m/s)



TCh: test chamber; CCh: conditioning chamber



LMC Setup



- **Tests:** MAX phases vs. 316L; test conditions promoting **dissolution attack** (500°C, [O] < 10⁻⁹ mass%, 1000-3500 h, **static LBE**)

Tempera
Pb veloc

perature

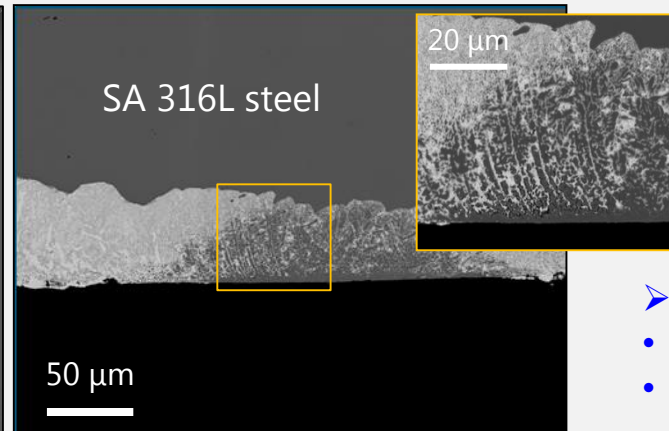
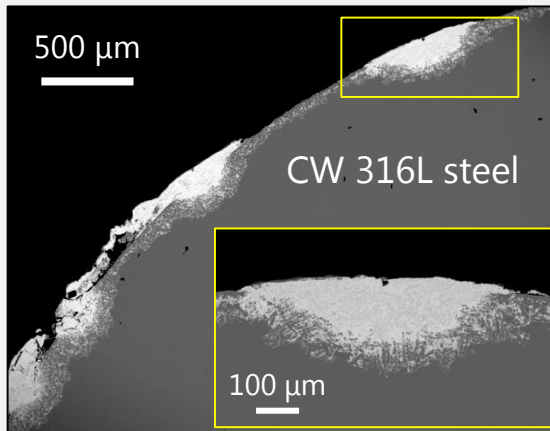
STEP 3

Compatibility with Static LBE (LMC)

- Aim: to assess MAX phase compatibility with **static, oxygen-poor LBE**:
- **500°C**, 3500 h, $[O] < 10^{-9}$ mass%; Maxthal 211[®] & 312[®], Nb₂AlC, Nb₄AlC₃
 - **500°C**, 1000 h, $[O] < 10^{-10}$ mass%; (Nb,Zr)₄AlC₃, (Zr,Ti)₃AlC₂ & (Zr,Ti)₂AlC, Zr₃AlC₂, Zr₂AlC

3282 h

$[O] < 10^{-8}$ mass%



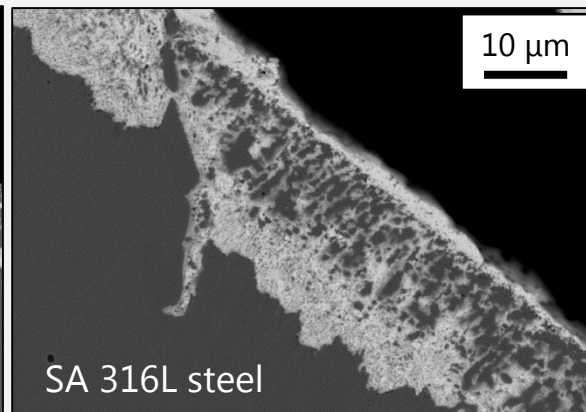
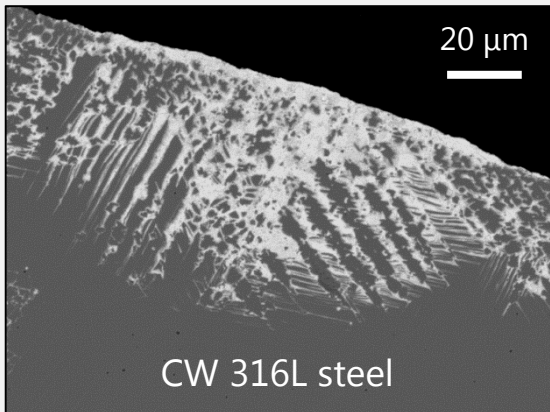
@500°C

CW: cold-worked
SA: solution-annealed

- Depth of dissolution attack:
- 50-265 μm CW steel
 - 9-125 μm SA steel

1000 h

$[O] < 10^{-8}$ mass%



- Depth of dissolution attack:
- 13-128 μm CW steel
 - 14-48 μm SA steel

STEP 3

Compatibility with Static LBE (LMC)



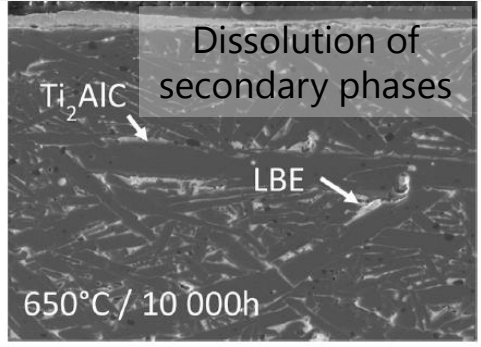
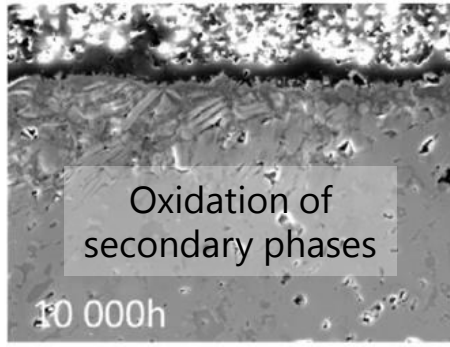
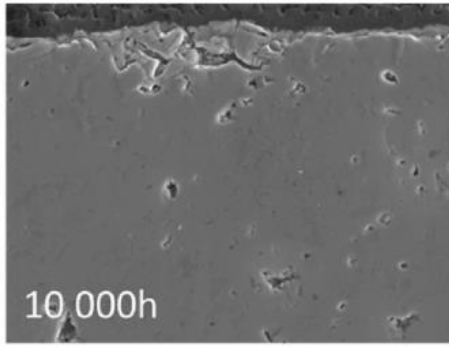
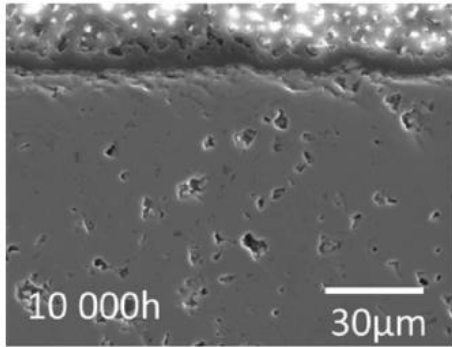
Ti₃SiC₂: 550/650/700°C, static LBE, **10000 h**, [O] ≈ 10⁻⁸ mass%

Ti₂AlC: 650°C, static LBE, **10000 h**, [O] ≈ 10⁻⁸ mass%

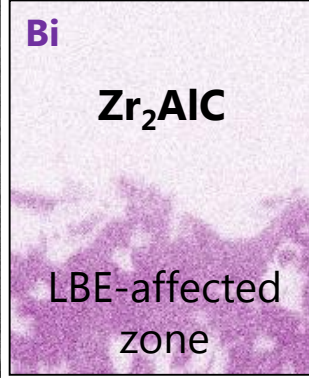
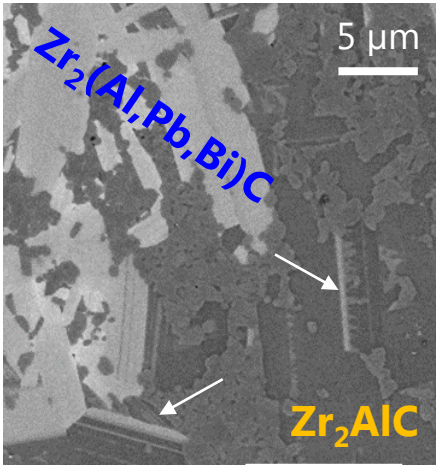
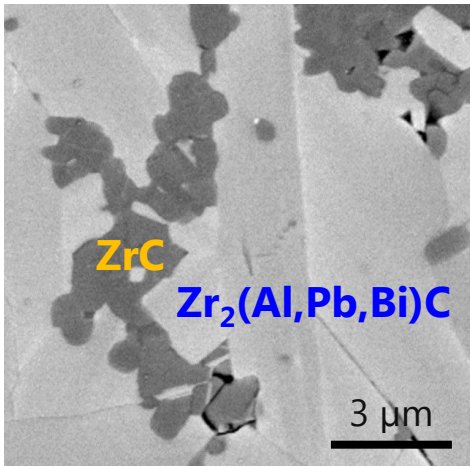
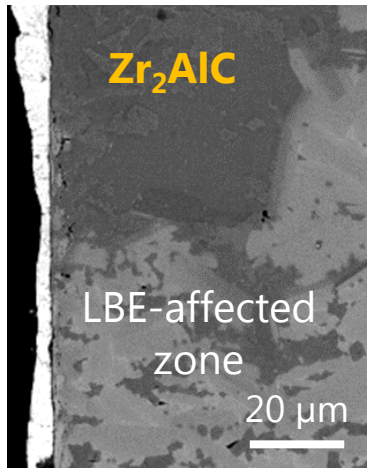
550°C

650°C

700°C



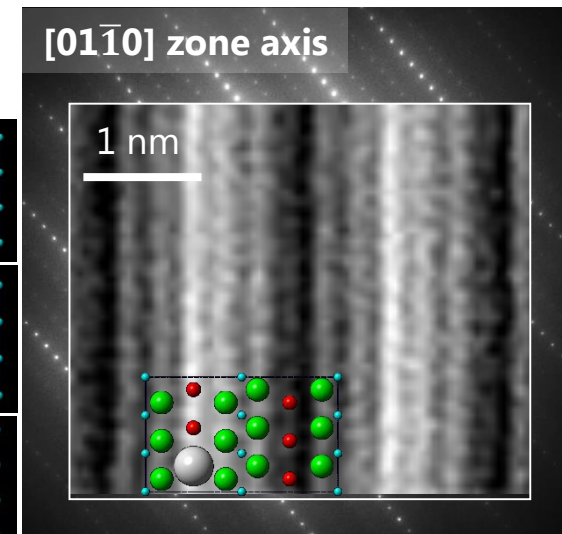
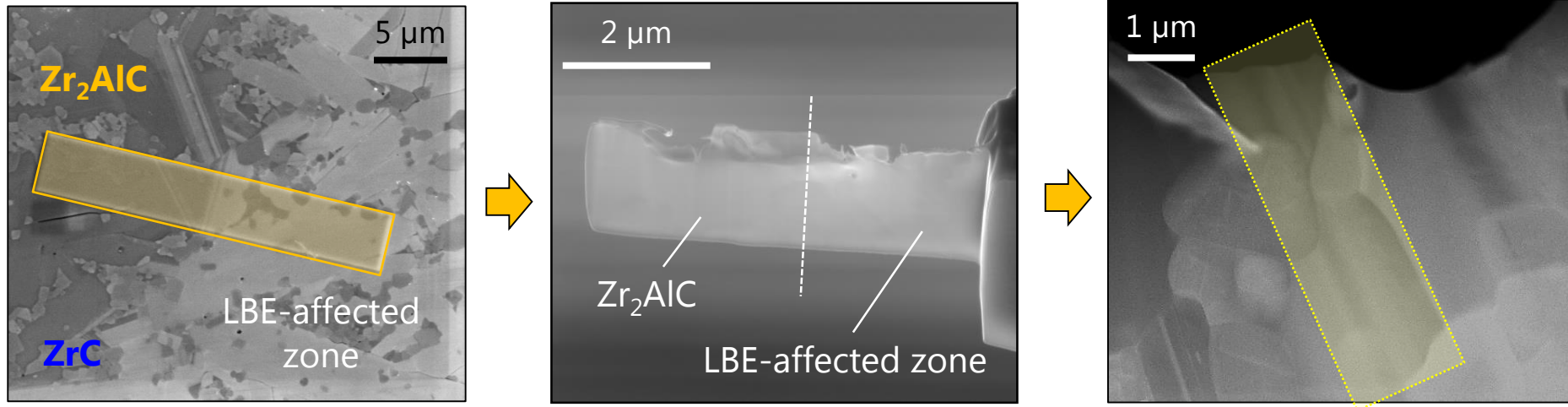
- Specimen maintains its integrity; grain morphology remains unaffected



(*A. Heinzl et al., J. Nucl. Mater. **482** (2016) 114–123)

STEP 3

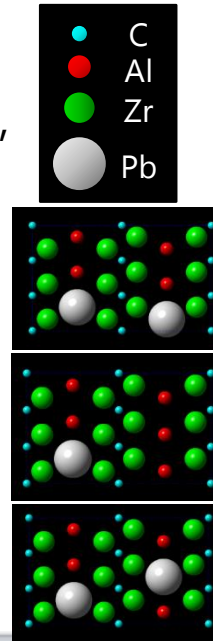
LBE/Zr₂AlC Interaction Mechanism (LMC)



Observations:

- Pb/Bi atoms diffuse along Zr₂AlC basal plane, forming *in situ* Zr₂(Al,Pb)C solid solution
- Superlattice reflections in HRTEM suggest spontaneous Pb/Bi substitution in crystal lattice
- MAX phase maintains their initial shape despite Pb/Bi substitution (SEM & EBSD data)
- MAX phase grains with mixed contrast show a reduced Al content where Pb/Bi increases (TEM EDS data not shown here)

What happens with mechanical properties after *in situ* formation of Zr₂(Al,Pb,Bi)C solid solution?



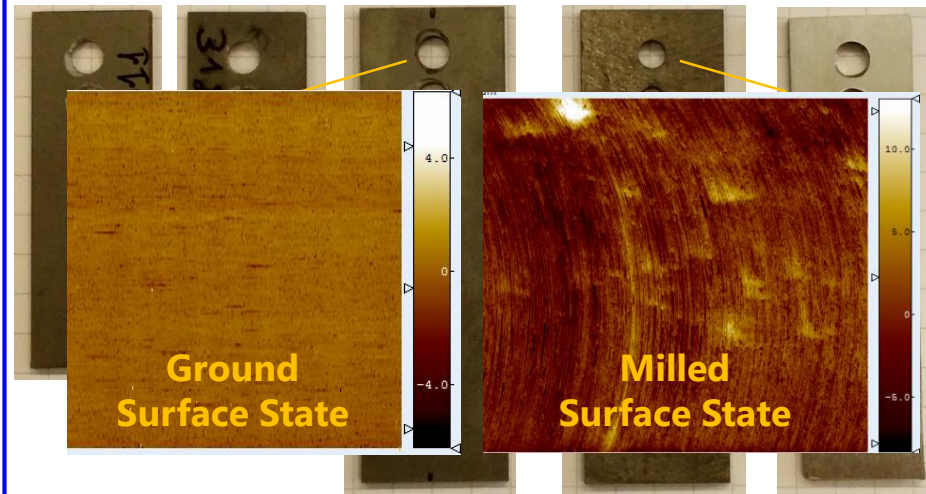
STEP 3

Compatibility with Fast-Flowing LBE (Erosion)

- Test relevant for Gen-IV LFR pump impellers:
 - Materials: Zr_3AlC_2 , Zr_2AlC , $(Nb,Zr)_4AlC_3$ ground & milled, 316L steel ground (ref)
 - Test: 500°C, ~1000 h, LBE with [O] < 10^{-10} mass%, $v \approx 8$ m/s
- Results: Zr_2AlC & Zr_3AlC_2 broke during removal; profilometry & SEM revealed max erosion damages in 316L steel, min damages in $(Nb,Zr)_4AlC_3$

Zr_2AlC (ZrC) Zr_3AlC_2 (ZrC) $(Nb,Zr)_4AlC_3$ Ground $(Nb,Zr)_4AlC_3$ Milled 316L Ground

Zr_2AlC (ZrC) Zr_3AlC_2 (ZrC) $(Nb,Zr)_4AlC_3$ Ground $(Nb,Zr)_4AlC_3$ Milled 316L Ground



Before CORELLA Testing



After CORELLA Testing*

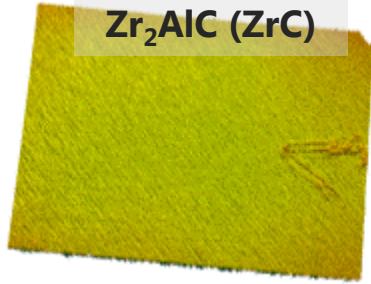
* LBE removal: hot oil & etching by 1:1:1 $H_2O_2/C_2H_5OH/CH_3COOH$

STEP 3

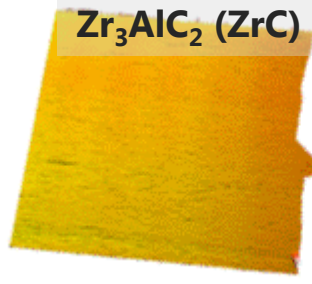
Compatibility with Fast-Flowing LBE (Erosion)

BEFORE

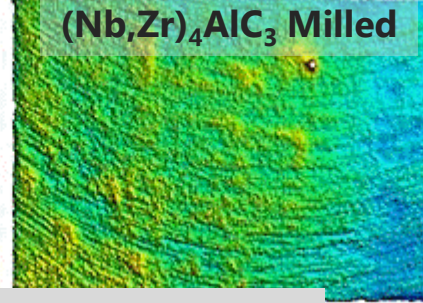
Zr_2AlC (ZrC)



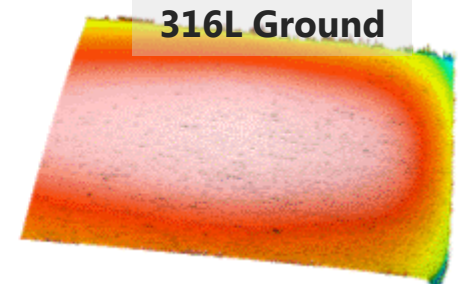
Zr_3AlC_2 (ZrC)



$(Nb,Zr)_4AlC_3$ Milled



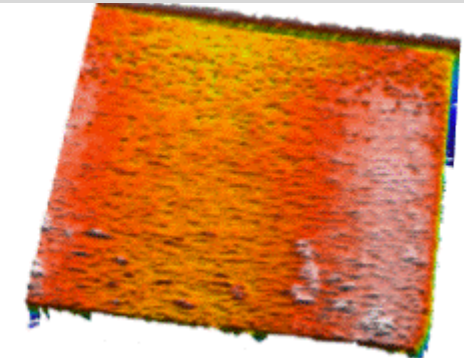
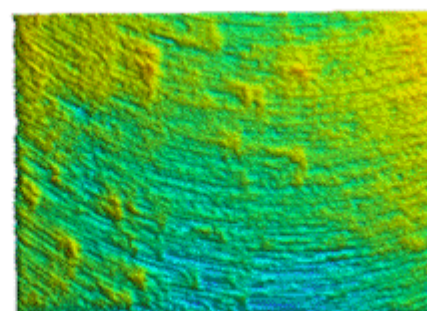
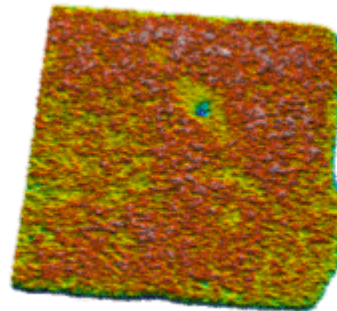
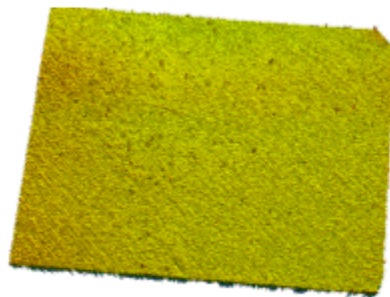
316L Ground



MAX phases: non-measurable erosion damages

316L: erosion damage

AFTER



Zr_2AlC

10 μm

Porous ZrO_2 oxide scale

Zr_3AlC_2

10 μm

$(Nb,Zr)_4AlC_3$

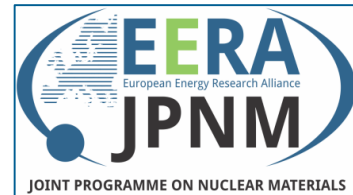
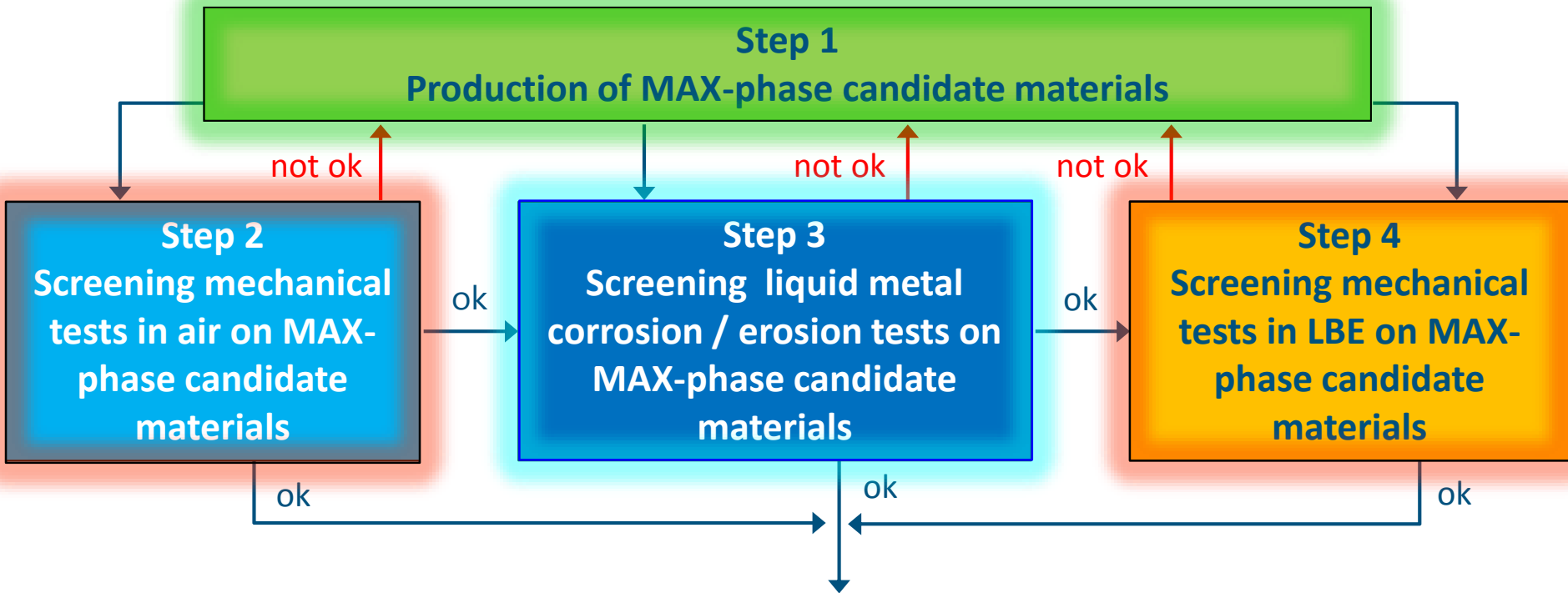
20 μm

LBE

316L steel

20 μm

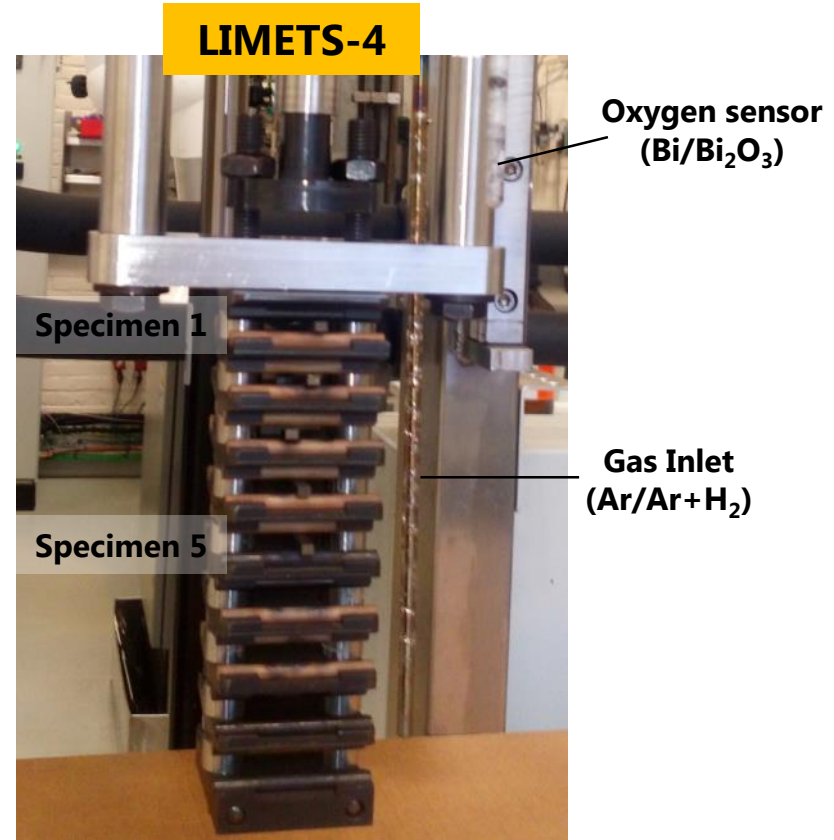
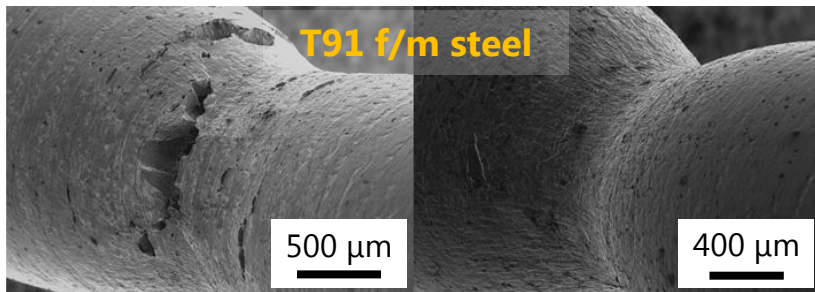
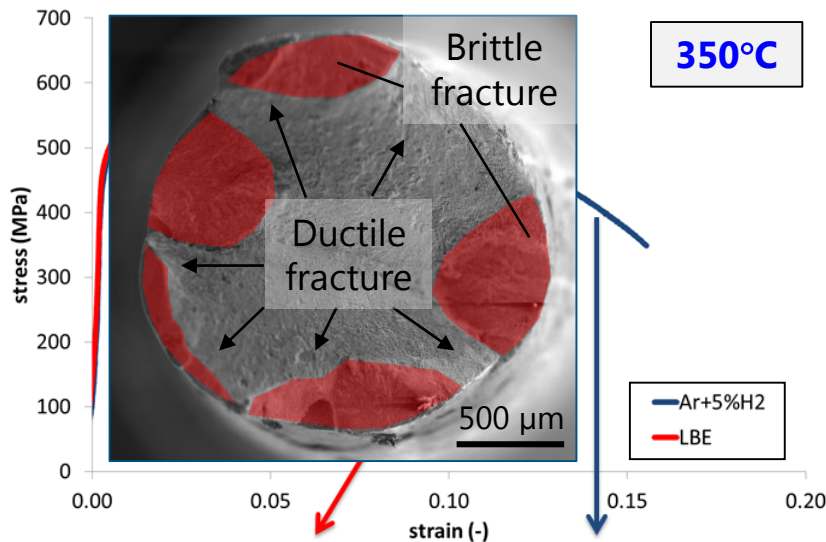
MAX Phase R&D: Approach, Challenges, Achievements



STEP 2**STEP 4**

Mechanical Properties (Air/Ar+H₂ vs. LBE)

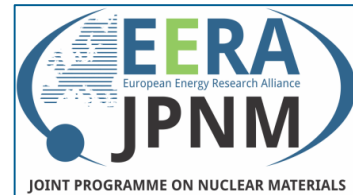
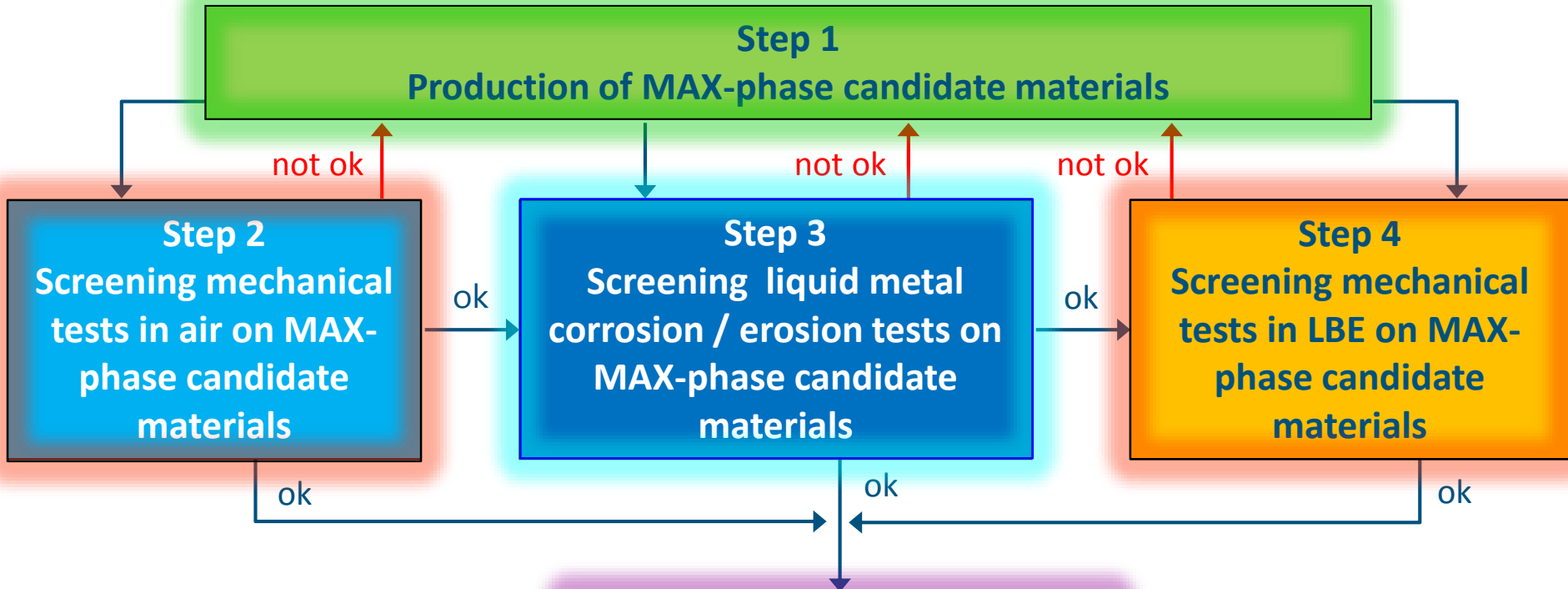
- **Aim:** assess whether the exposure of MAX phases to liquid LBE affects their mechanical properties (flexural strength, fracture toughness)
- Example of **materials degradation** observed in ferritic/martensitic steels in contact with LBE: **liquid metal embrittlement (LME)**



- Evaluation of four point-bending strength (σ_{4PB}) in LIMETS-4
- σ_{4PB} is given as an average of 5 tests per material and condition
 - Materials: Maxthal 211[®] and (Nb_{0.85}Zr_{0.15})₄AlC₃
 - Test Conditions & Methodology:
 - room temperature (RT) in air (T monitored by thermocouple)
 - 350°C in Ar-5 vol% H₂ (T monitored by thermocouple)
 - 350°C* in LBE with [O] < 10⁻¹⁰ mass% (T & [O] monitored – oxygen sensor)
 - Specimen pre-exposure: 48 hours under 20 MPa in test environment
- Results: no environmental degradation of MAX phase flexural strength!

Test Condition	Maxthal 211 [®]	(Nb _{0.85} Zr _{0.15}) ₄ AlC ₃
	σ_{4PB} (MPa)	σ_{4PB} (MPa)
RT in air	204 ± 17	426 ± 30
350°C in Ar-5% H ₂	197 ± 10	418 ± 60
350°C in LBE with [O] < 10 ⁻¹⁰ mass%	214 ± 13	414 ± 56

MAX Phase R&D: Approach, Challenges, Achievements



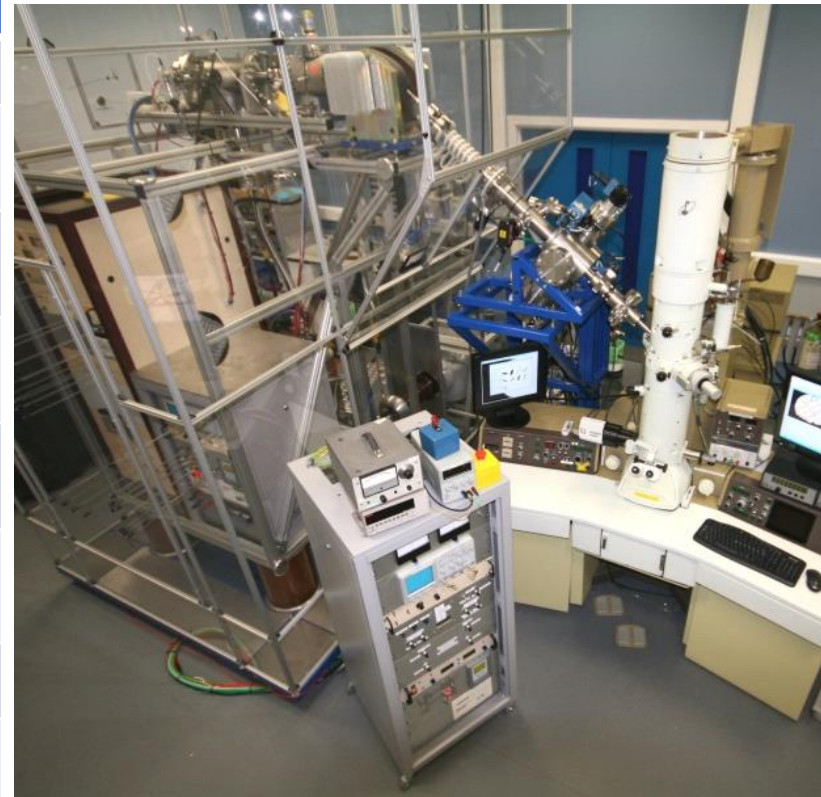
STEP 5

Ion Irradiation of $(\text{Nb}_{0.85}\text{Zr}_{0.15})_4\text{AlC}_3$

Microscope and Ion Accelerator for Materials Investigations (MIAMI-1) Facility

Specifications

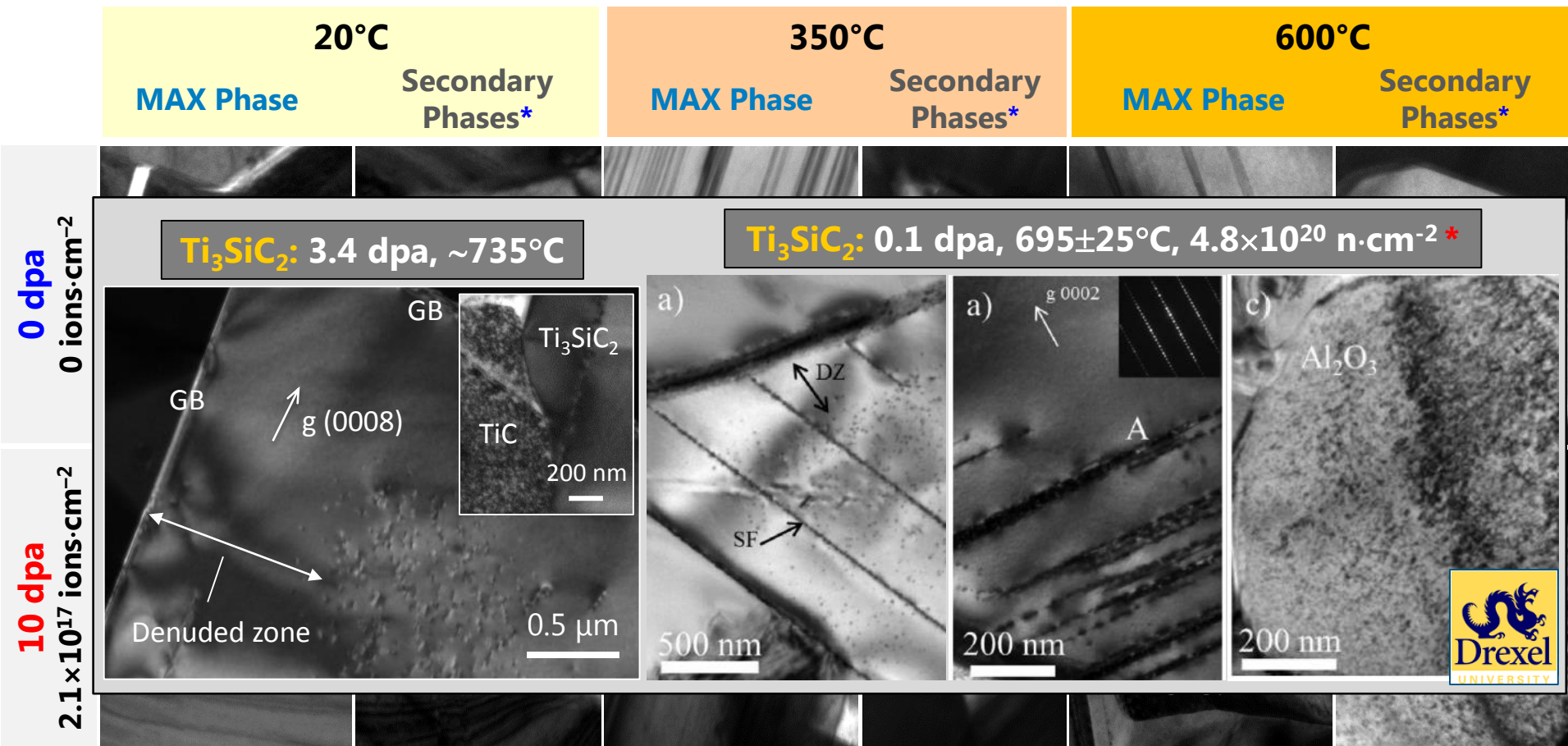
TEM	JEOL JEM-2000FX
Electron acceleration voltage	80 to 200 kV
Ion acceleration voltage	1 to 100 kV
Ion species	Most ions from H^+ to W^+
Electron/ion beam angle	30°
Ion flux	Up to 1.5×10^{14} ions $\text{cm}^{-2} \text{s}^{-1}$ for 6 keV He^+ (for example)
Temperature	(100 to 380 K) or (RT to 1570 K)
Image capture	Gatan ES500W & Gatan Orius SC200 (4 MP)



STEP 5

Ion Irradiation of $(\text{Nb}_{0.85}\text{Zr}_{0.15})_4\text{AlC}_3$

- Irradiation with 6 keV He^+ ; ion flux: 10^{14} ions $\cdot\text{cm}^{-2}\cdot\text{s}^{-1}$
- Electron beam energy: 200 keV; electron beam: off during ion irradiation



500 nm

(*D. Tallman et al., J. Nucl. Mater. **468** (2016) 1–13)

* Al_3Nb (7 wt%) & Al_2O_3 (2-3 wt%)

- Exploring the potential of **MAX phases** for specific applications (*fuel clads, impellers*) in **Gen-IV LFRs & MYRRHA** entails the following challenges:
- i. Strict control of processing to produce **phase-pure materials** with a **tailored microstructure** that meet the targeted property requirements (strength, fracture toughness, fatigue lifetime) of the end application
 - ii. Assess the **compatibility** of produced materials **with the heavy liquid metal coolant** (Pb, LBE) under variable exposure conditions (T, [O], flow velocity) – study liquid metal corrosion/erosion behavior of candidate materials
 - iii. Measure **key mechanical properties** (strength, fracture toughness) of produced materials both in air/inert and heavy liquid metal media to assess possible **susceptibility to environment-assisted material degradation effects** (e.g., LME)
 - iv. Assess the **radiation tolerance** of the optimized materials by designing and executing neutron irradiation campaigns that can validate the materials in an industrially-relevant environment (TRL 5). **Ion/proton irradiation** – when used in the right way – will help to accelerate development of radiation-tolerant MAX phase materials prior to their ultimate validation in neutrons

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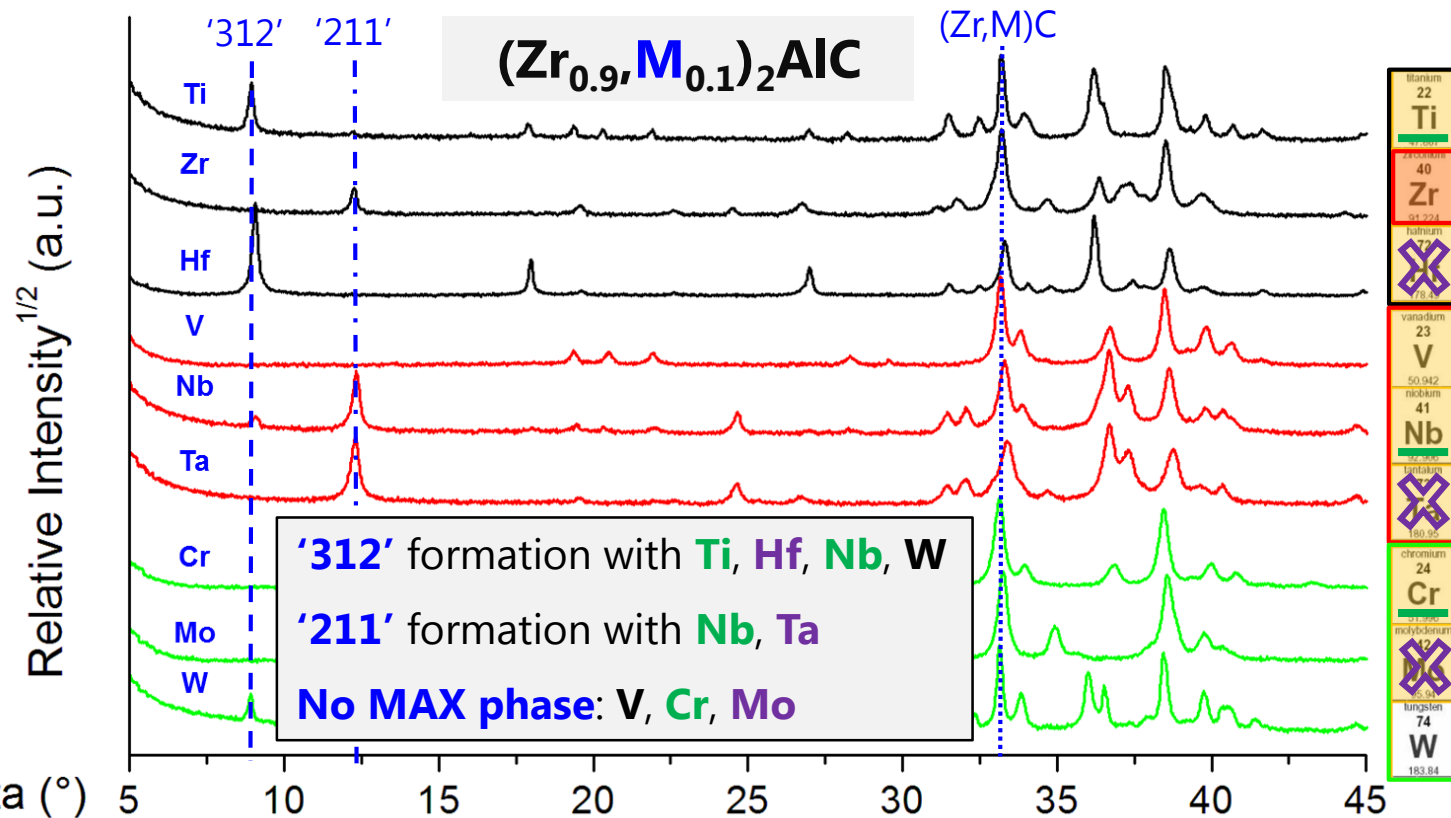
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STUDIECENTRUM VOOR KERNENERGIE
CENTRE D'ETUDE DE L'ENERGIE NUCLEAIRE

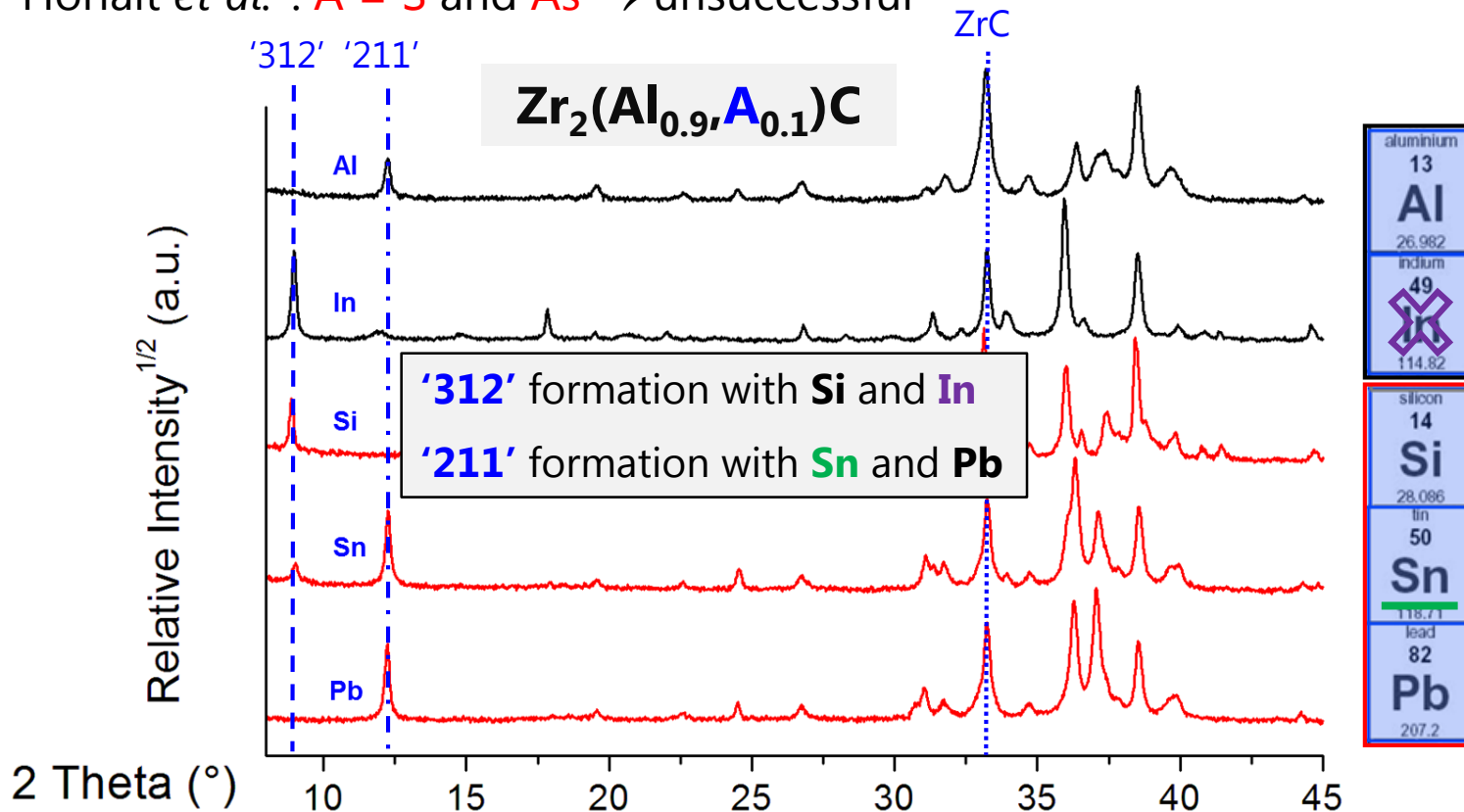
MAX Phase Synthesis in the (Zr,M)-Al-C System

- Aim: synthesize $(Zr_{1-x},M_x)_2AlC$ solid solutions to increase MAX phase content
- Prior attempts reported in literature:
 - Reiffenstein *et al.*¹ & Naguib *et al.*²: **M = Nb** → successful for $x = 0.6$ & 0.8 resp.
 - Horlait *et al.*³: **M = Ti, Cr** and **Mo** → unsuccessful



MAX Phase Synthesis in the Zr-(Al,A)-C System

- Aim: synthesize $Zr_2(Al_{1-x}A_x)C$ solid solutions to increase MAX phase content
- Prior attempts reported in literature:
 - Horlait *et al.*^{1,2}: A = Sn, Pb, Sb & Bi → successful for x = 0.8, 0.65, 0.7 & 0.58 resp.
 - Horlait *et al.*¹: A = S and As → unsuccessful



- Tests relevant for MYRRHA pump impeller:
 - Materials: Maxthal 211[®] & 312[®], 316L stainless steel ground & polished
 - 1st test: 300°C, 500 h, LBE with [O] < 10⁻⁸ mass%, v ≈ 8 m/s
 - 2nd test: 300°C, 500 h, LBE with [O] ≈ 10⁻⁶ – 10⁻⁵ mass%, v ≈ 8 m/s
 - 3rd test: 300°C, 1000 h, LBE with [O] ≈ 10⁻⁷ mass%, v ≈ 8 m/s
- Results: no clear evidence of erosion damage; possible local damages in 316L steel and Maxthal 211[®] – difficult interpretation

SPECIMENS AFTER 2ND TEST

Maxthal 211[®] & 312[®]



316L steel



polished ground

