

Thermo-structural analysis on a UHV gate valve (accidental case LINAC2/4 to PSB)

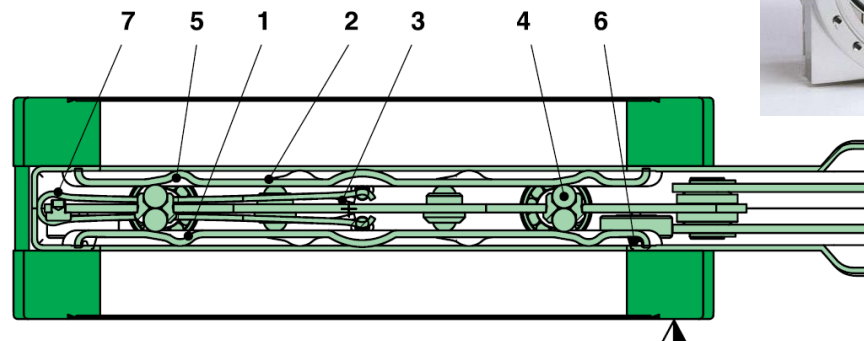
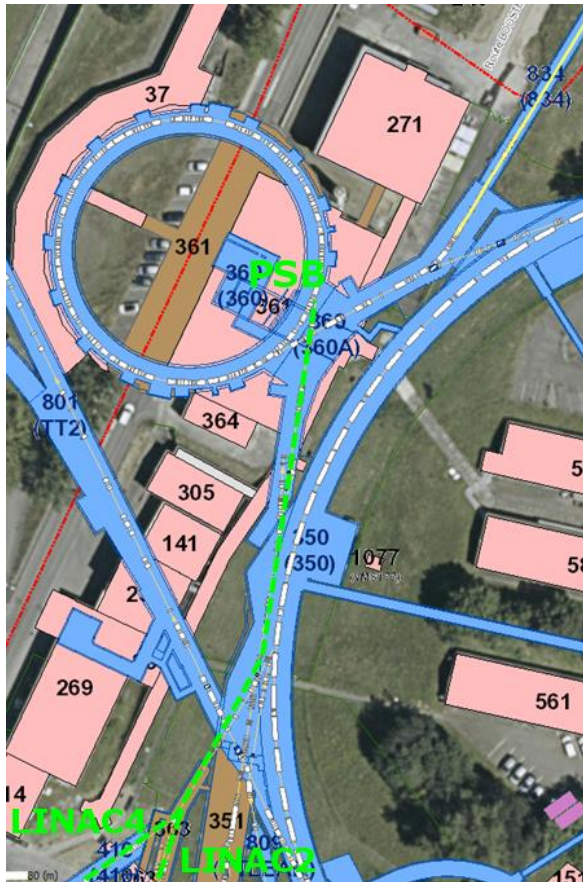
Andre Pilan Zanoni, M. Calviani (EN-STI-TCD)
Jose A. Briz, V. Vlachoudis (EN-STI-FDA)



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0. Valve type / position

- UHV gate valve with pneumatic actuator
- Series 10.8, DN 63 - 200 (2½" - 8"), VAT Vakuumentile
- Housing / mechanism material: AISI 304 (1.4301)



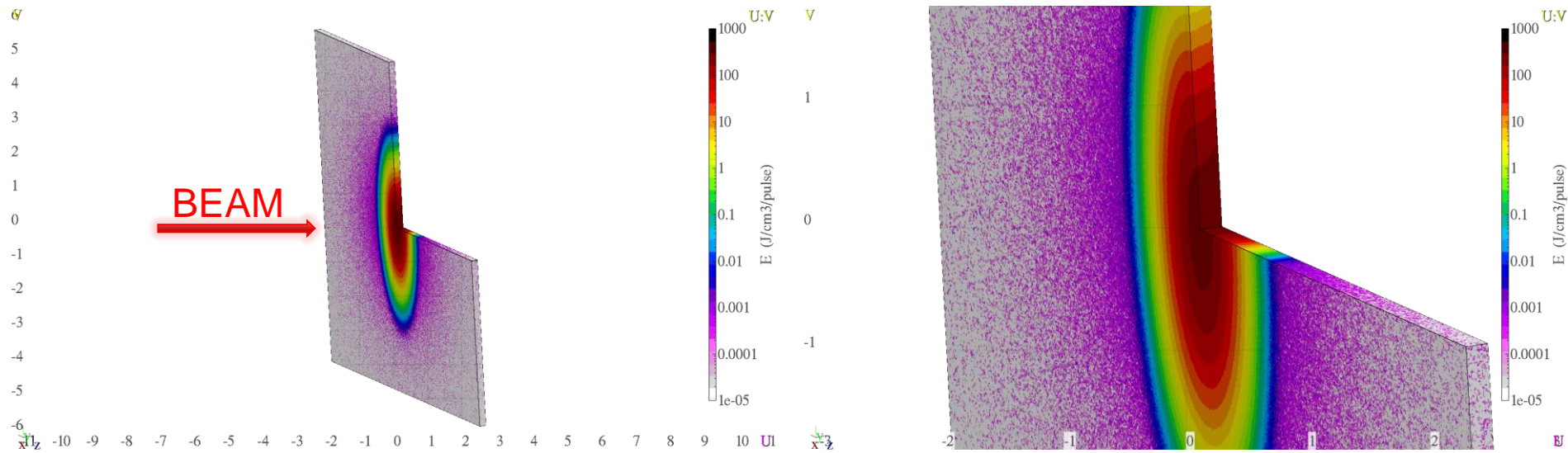
- | | | |
|-----------------|----------------|-------------------|
| 1 Gate | 4 Ball pairs | 7 Spring stop |
| 2 Counter-plate | 5 Ball detents | ▼ Valve seat side |
| 3 Leaf springs | 6 Gate seal | |



1. Simulation conditions

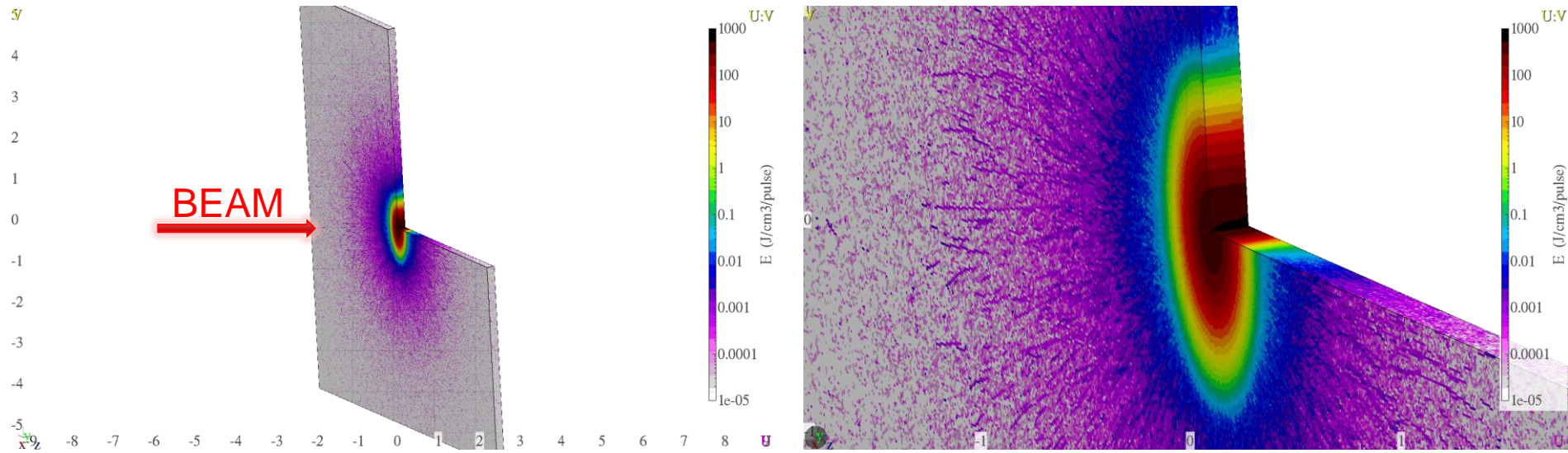
- Proton beam properties:
 - Case 1:
 - Energy: 50 MeV
 - Size: $\sigma_x = 2.9$ mm, $\sigma_y = 6.4$ mm
 - Intensity: 2.3×10^{13} p⁺/pulse
 - Pulse: 21.7 μ s
 - Case 2:
 - Energy: 160 MeV
 - Size: $\sigma_x = 1.2$ mm, $\sigma_y = 1.9$ mm
 - Intensity: 1.6×10^{13} p⁺/pulse
 - Pulse: 100 μ s
- Plate properties:
 - Size: 10 cm x 10 cm x 2 mm
 - Material: SS304L ($\rho = 8.02$ g/cm³)

1.1 50 MeV proton beam



Case 1: 50 MeV, $\sigma_x = 2.9$ mm, $\sigma_y = 6.4$ mm, $I = 2.3 \times 10^{13}$ p⁺/pulse

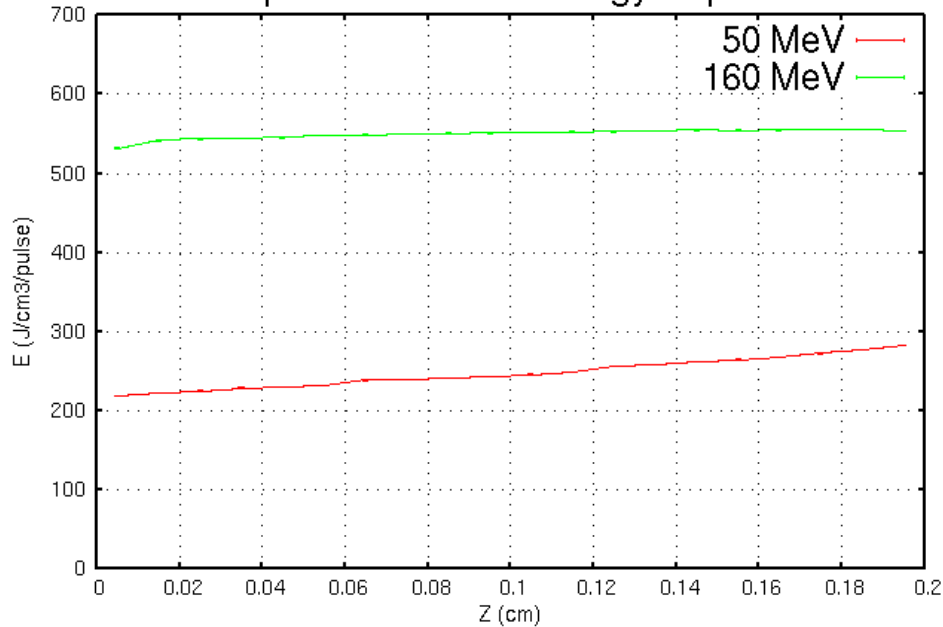
1.2 160 MeV proton beam



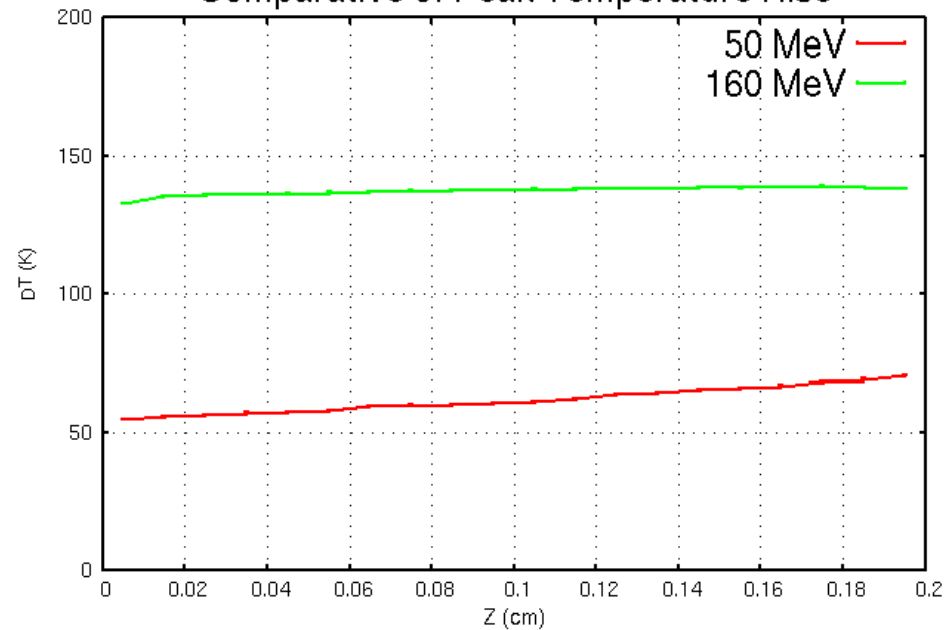
Case 2: 160 MeV, $\sigma_x = 1.2$ mm, $\sigma_y = 1.9$ mm, $I = 1.6 \times 10^{13}$ p⁺/pulse

1.3 Results

Comparative of Peak Energy Deposition



Comparative of Peak Temperature Rise



~560 J/cm³/pulse and ~140 K/pulse are peak values (obtained for 160 MeV)

Adiabatic temperature rise is roughly estimated under the assumption of constant specific heat:

$$\Delta T \left(\frac{\text{K}}{\text{pulse}} \right) = \frac{E \left(\frac{\text{J}}{\text{cm}^3} \right)}{c \left(\frac{\text{J}}{\text{g} \cdot \text{K}} \right) * \rho \left(\frac{\text{g}}{\text{cm}^3} \right)} \text{ with } c_{\text{SS304L}} = 0.5 \text{ J/(g} \times \text{K)} \text{ and } \rho = 8.02 \text{ g/cm}^3$$

1.4 Energy balance

Beam type	Energy deposited (MeV/proton)	Energy deposited (% of incoming energy)	Energy deposited (J/pulse)	Absorbed power (W)
50 MeV	15.7	31.4 %	57.8	48.2
160 MeV	6.2	3.9 %	15.9	13.3

Beam intensities considered:

2.3e13 p/pulse for 50 MeV

1.6e13 p/pulse for 160 MeV

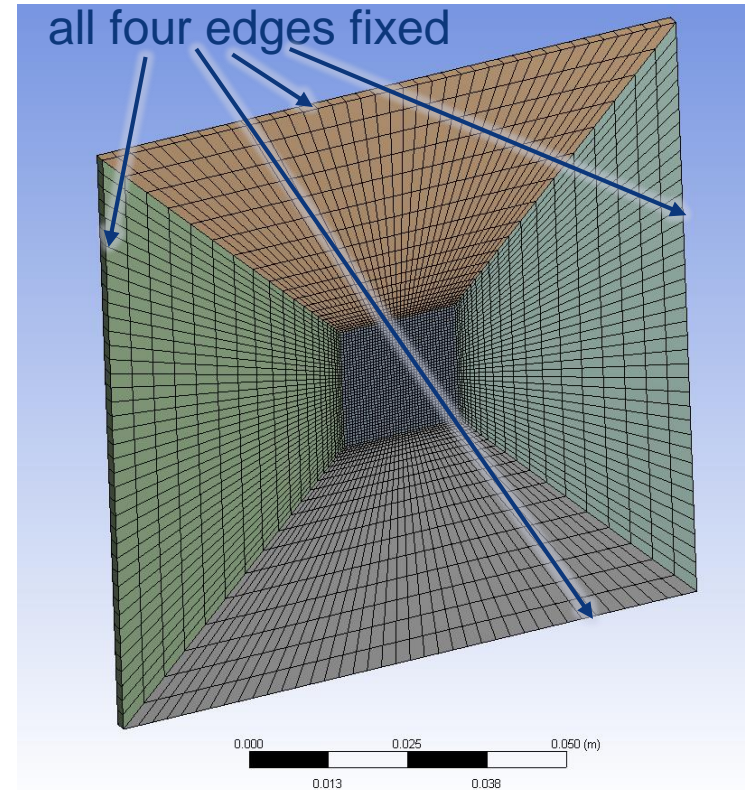
Beam repetition period: 1.2 seconds for both beams

2. Thermal-structural analysis

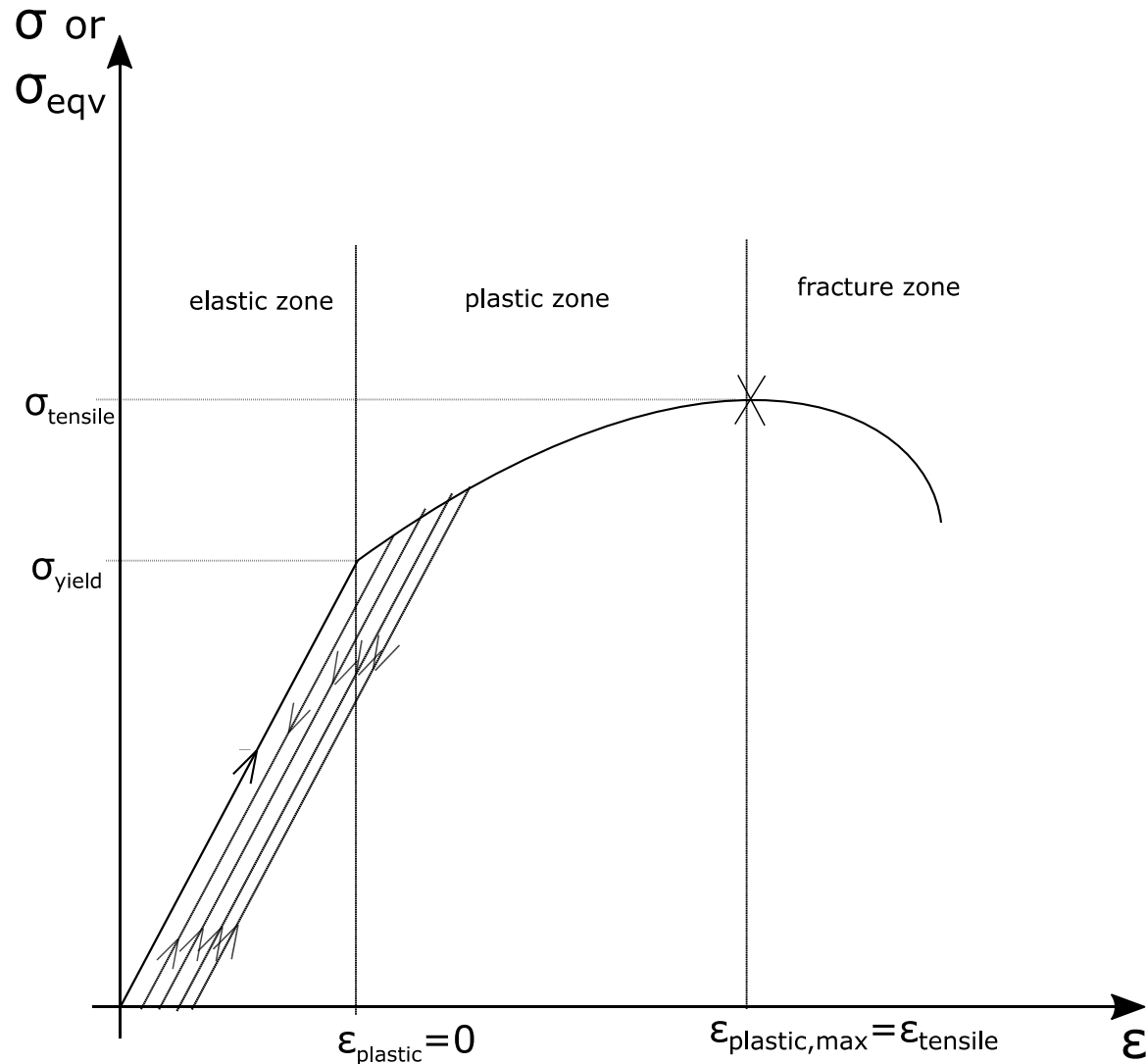
- Repetition rate: 1.2s
- Initial temperature: 22°C

- FEM simulation (Ansys 17.1)
- SHELL131/181 layered elements
 - 20 layers (see EDMS 1610806)
- Boundary conditions:
 - Thermal: conduction through matter (neither convection nor radiation considered)
 - Mechanical: four edges fixed / bilinear isotropic hardening material model*

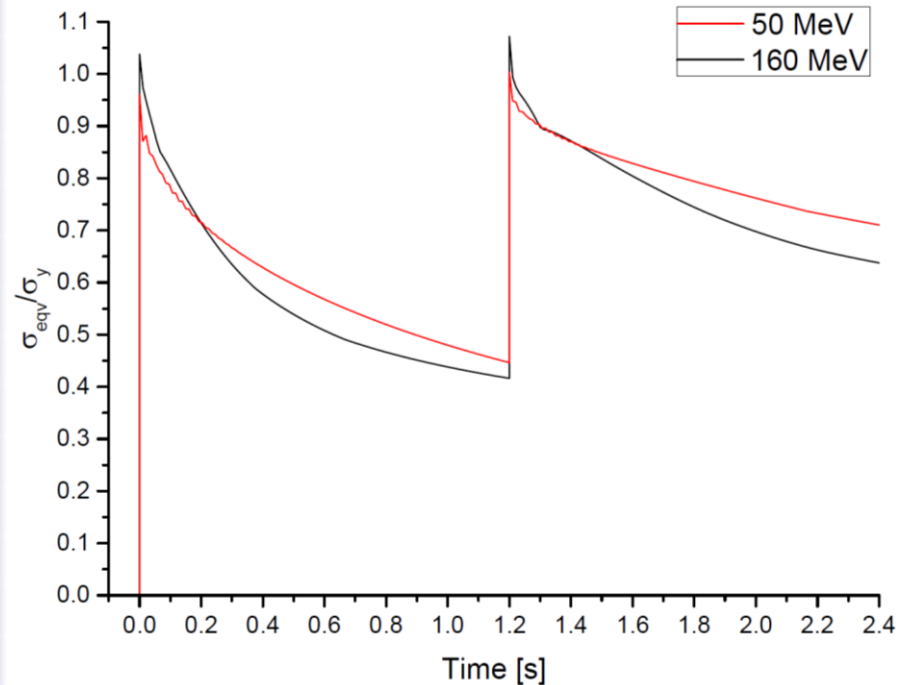
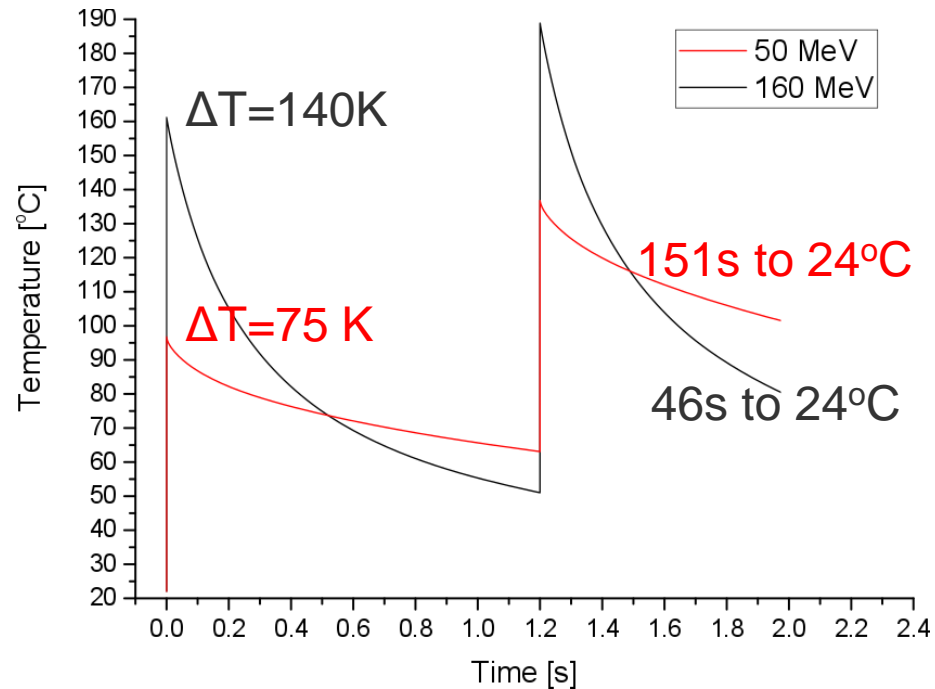
*to account for permanent deformations



Stress strain curve



Results for two repeated pulses

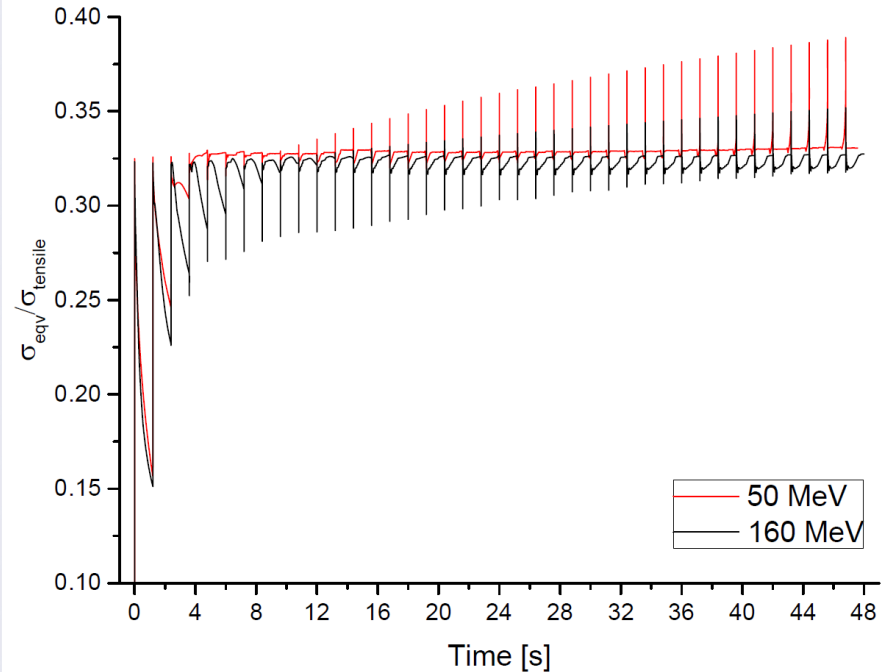
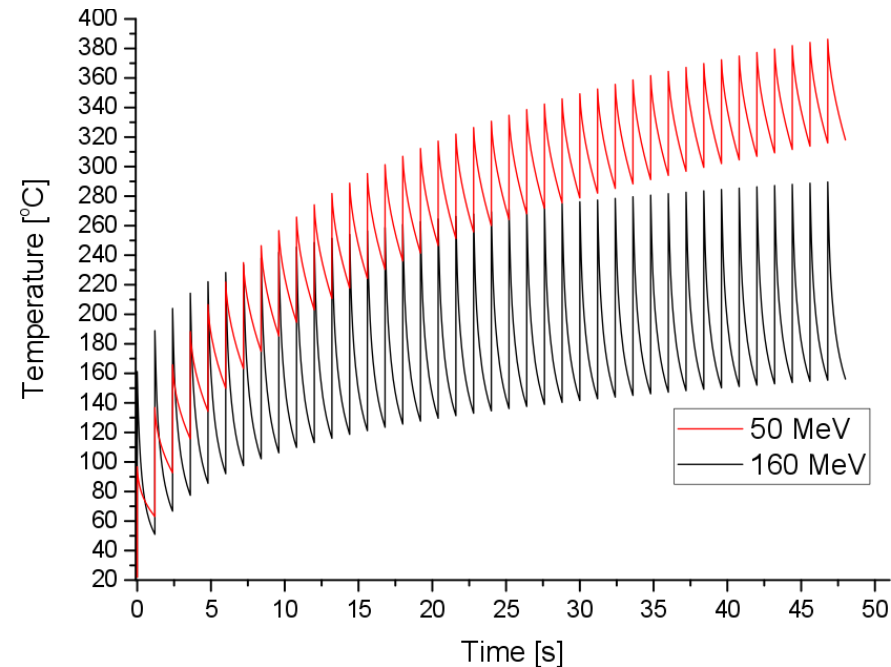


Maximum temperatures reached

$\sigma_{eqv}/\sigma_{yield} > 1$: plastic deformation

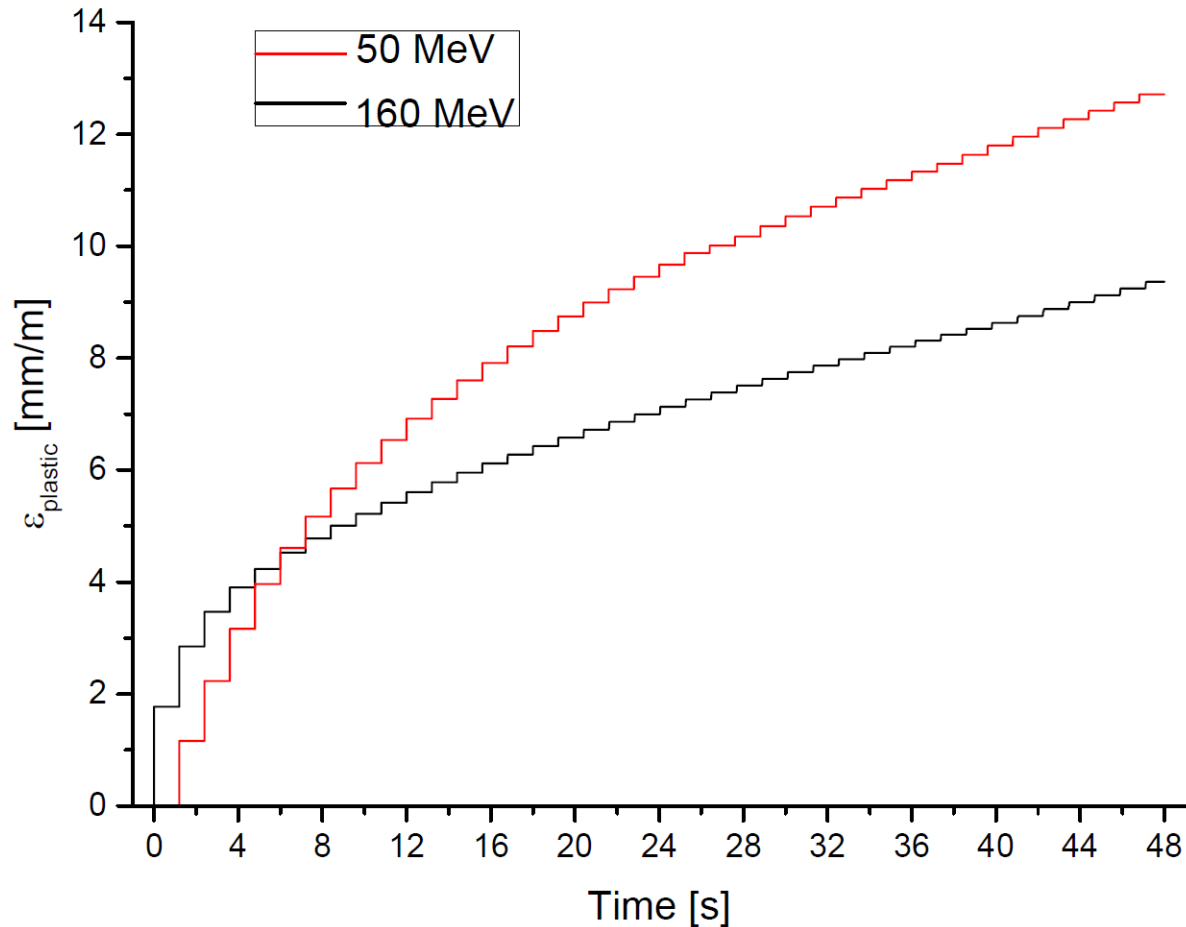
Multiple repeated pulses

- No fracture for 40 repeated pulses ($\sigma_{\text{eqv}} < \sigma_{\text{tensile}}$)



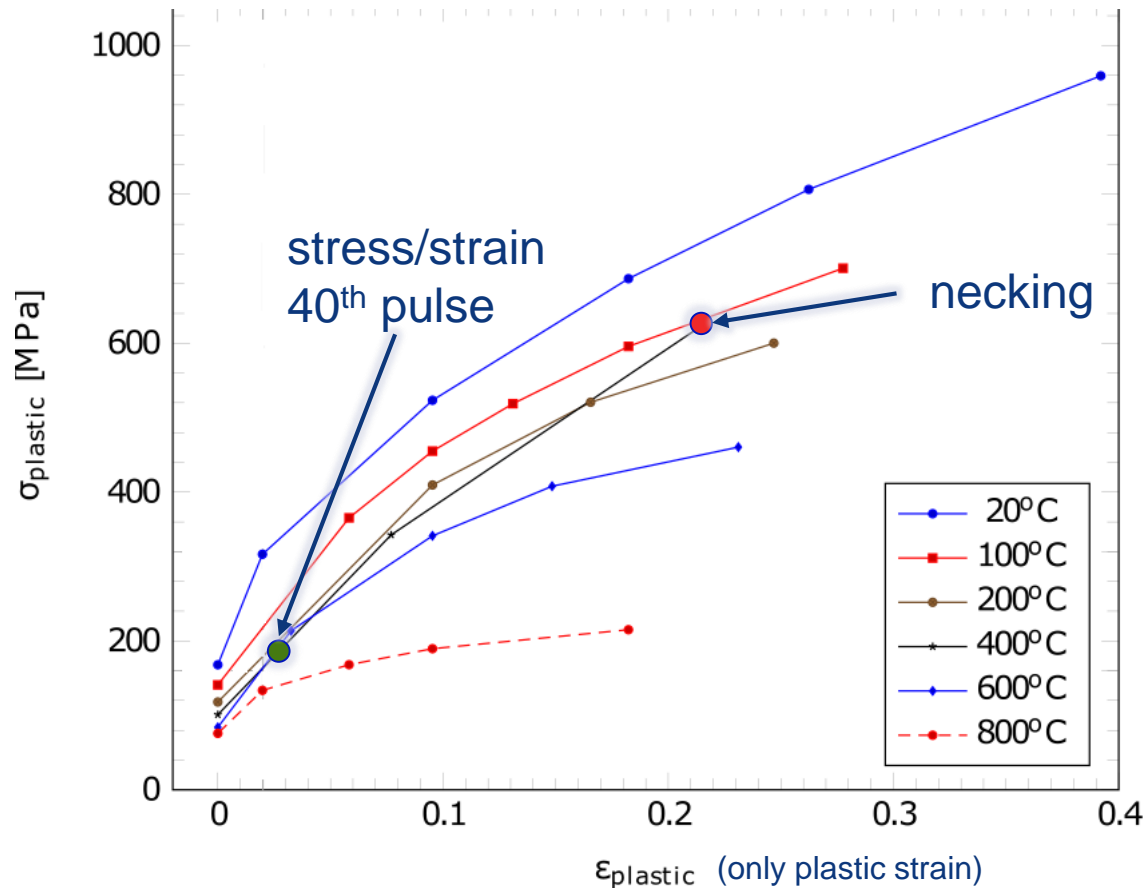
- Tensile strength is not reached after 40 repeated pulses ($\sigma_{\text{eqv}} < \sigma_{\text{tensile}}$)

Plastic deformation



- $\epsilon_{\text{plastic,max}} \sim 200 \text{ mm/m}$
- Rough prediction: between 900* and 1300** pulses until fracture starts
 - * thermo-mechanical fatigue (model needs to be better studied) / ** linear extrapolation from results

Stress-strain curve (true stress)

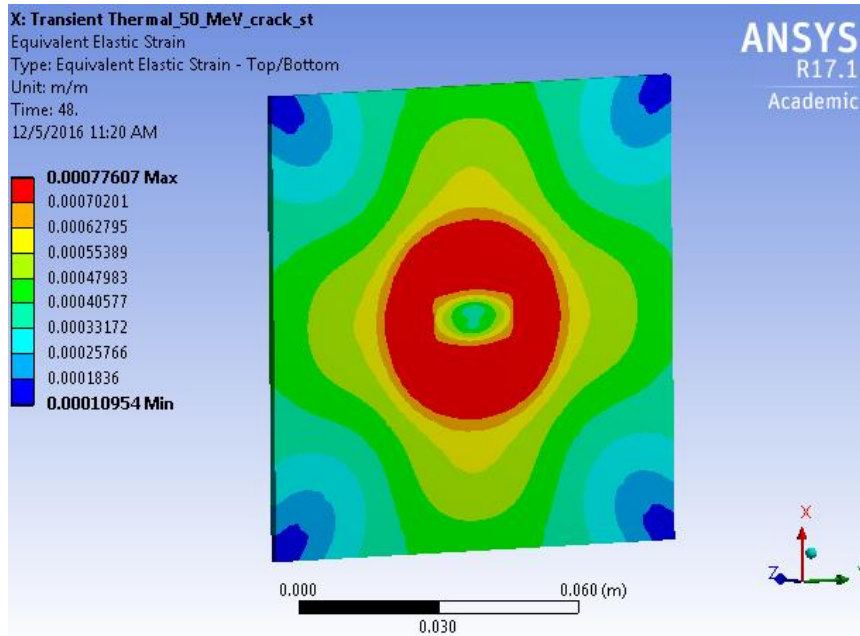


Multilinear model

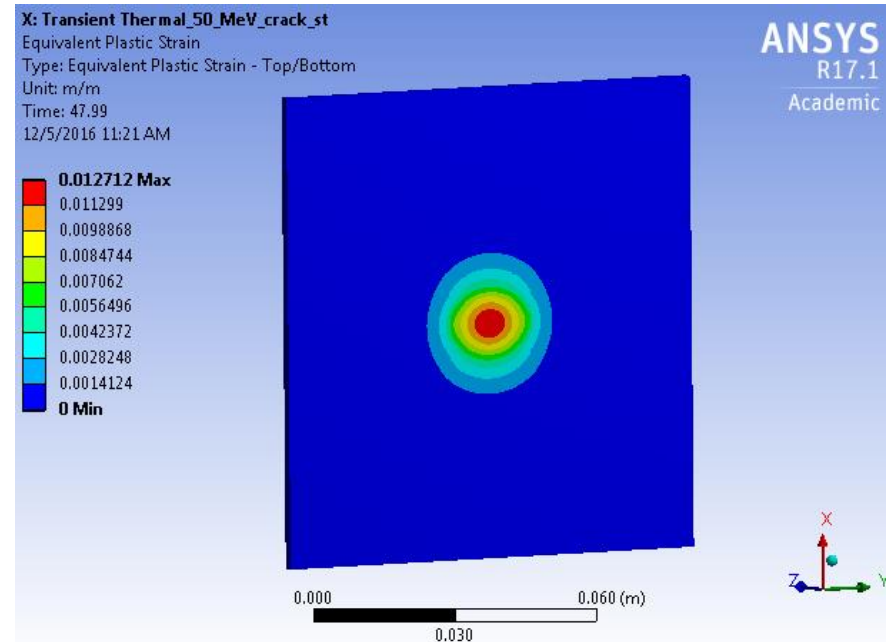
Curves from: Dempsey, J. Franklin, et al. "Temperature dependent ductile material failure constitutive modeling with validation experiments." Challenges in Mechanics of Time-Dependent Materials and Processes in Conventional and Multifunctional Materials, Volume 2. Springer New York, 2013. 7-15.

Border deformation

Elastic strain after 40 pulses

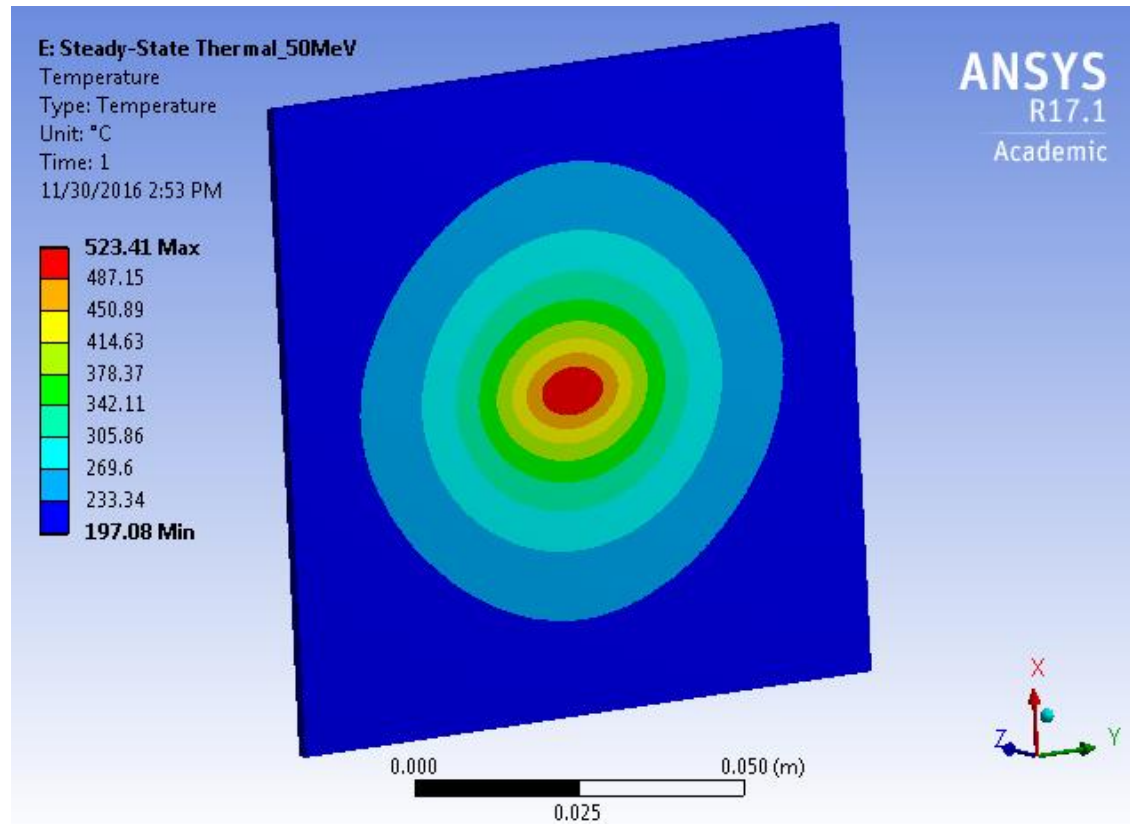


Plastic strain after 40 pulses



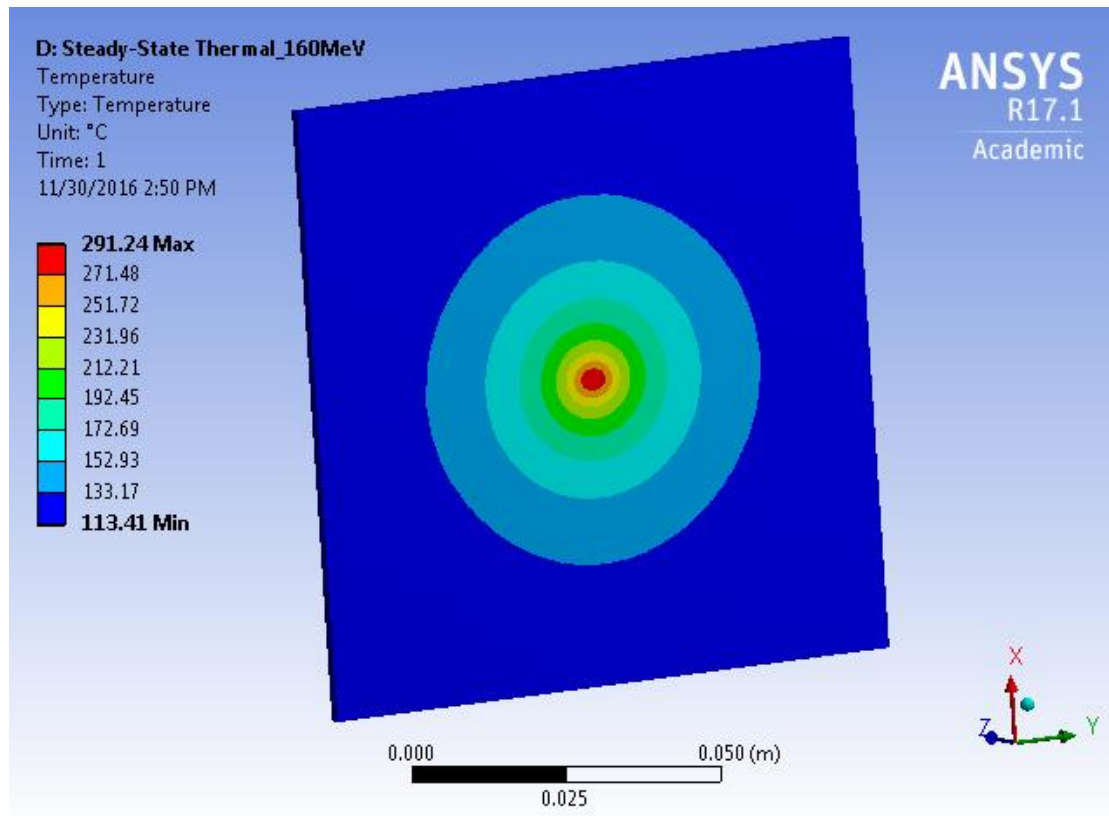
- No plastic deformation on the border for 40 pulses
- Plastic strain in the plate center: 13 mm/m \rightarrow 30 μ m thru-thickness deformation
- However steady-state temperature must be considered for irradiation over longer time

Steady-state results (50 MeV)



- Heat sink: radiation from the plate ($\epsilon=0.6$ to the environment) only
 - No convection
 - Conduction to the plate supports implemented
- Maximum temperature: **523°C** (operational limit at $T_{\text{creep}}=550^\circ\text{C}$)

Steady-state results (160 MeV)



- Heat sink: radiation from the plate ($\epsilon=0.6$ to the environment) only
 - No convection
 - Conduction to the plate supports implemented
- Maximum temperature: **291°C** (operational limit at $T_{\text{creep}}=550^\circ\text{C}$)

3. Conclusion

- 2 repeated pulses:
 - $\Delta T_{50\text{MeV,max}}=75^{\circ}\text{C}$ $\Delta T_{160\text{MeV,max}}=140^{\circ}\text{C}$
- Plastic deformation after 1 pulse
 - However no permanent deformation on plate borders for 40 pulses
- Structural limits for the plate:
 - $T_{\text{max},50\text{ MeV}}=523^{\circ}\text{C}$ (steady-state)
 - $T_{\text{max},160\text{ MeV}}=291^{\circ}\text{C}$ (steady-state)
- Unclear how the material will behave over hundreds of pulses:
 - Further studies would be needed
- For more information: EDMS 1758139



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