

INVERSE KINEMATICS STUDY

A. Di Crescenzo, M.C. Montesi,
A. Lauria, A. Pastore

FOOT Collaboration Meeting
Napoli, 25th May 2017

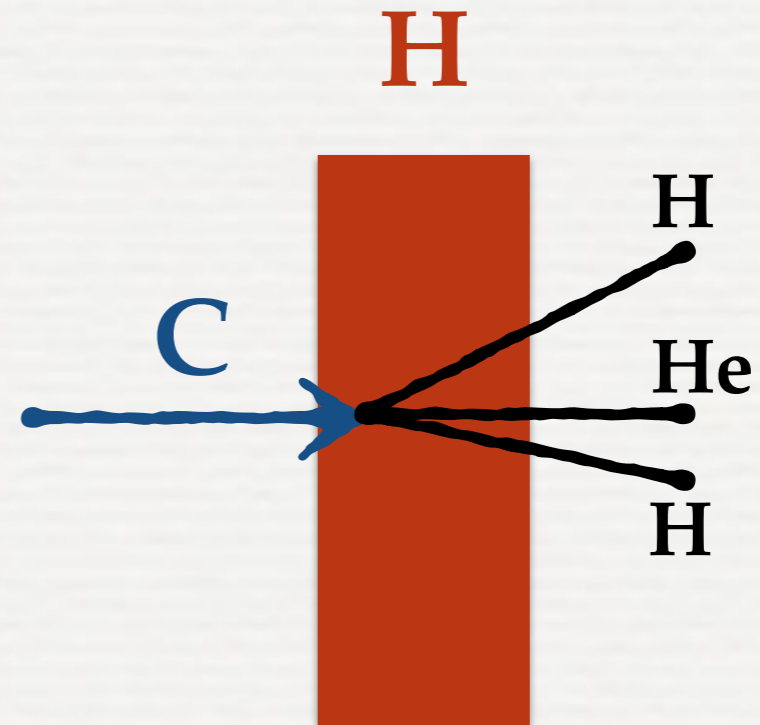
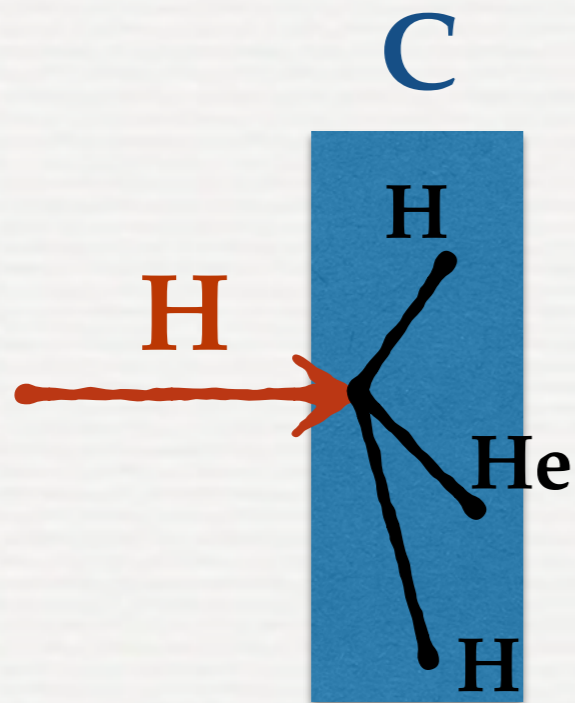
OUTLINE

- **Aim:** estimation of $H \rightarrow C$ differential cross-section in inverse kinematics
- **Framework:** official FOOT simulation software on Tier3
- Estimation of fragments kinematical variables in direct and inverse kinematics
- Estimation of energy resolution in direct and inverse kinematics
- Estimation of differential cross sections in inverse kinematics for different fragments
- Estimation of $H \rightarrow C$ cross-section

INVERSE KINEMATICS

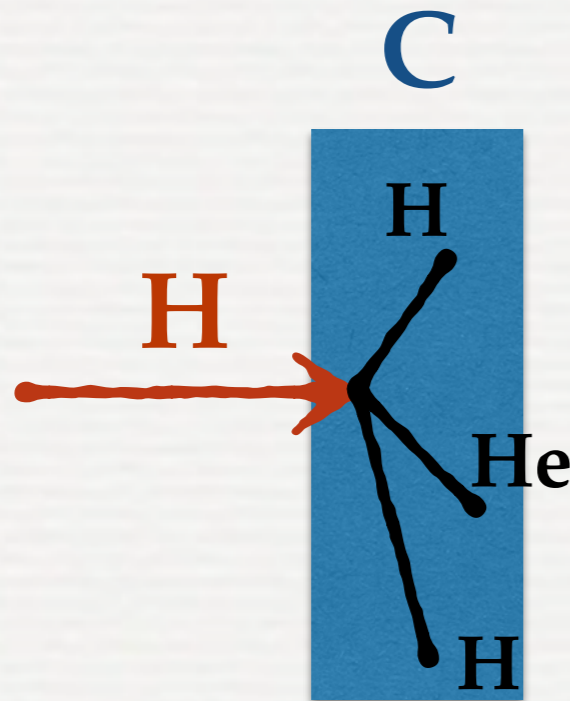
proton on patient

patient on proton



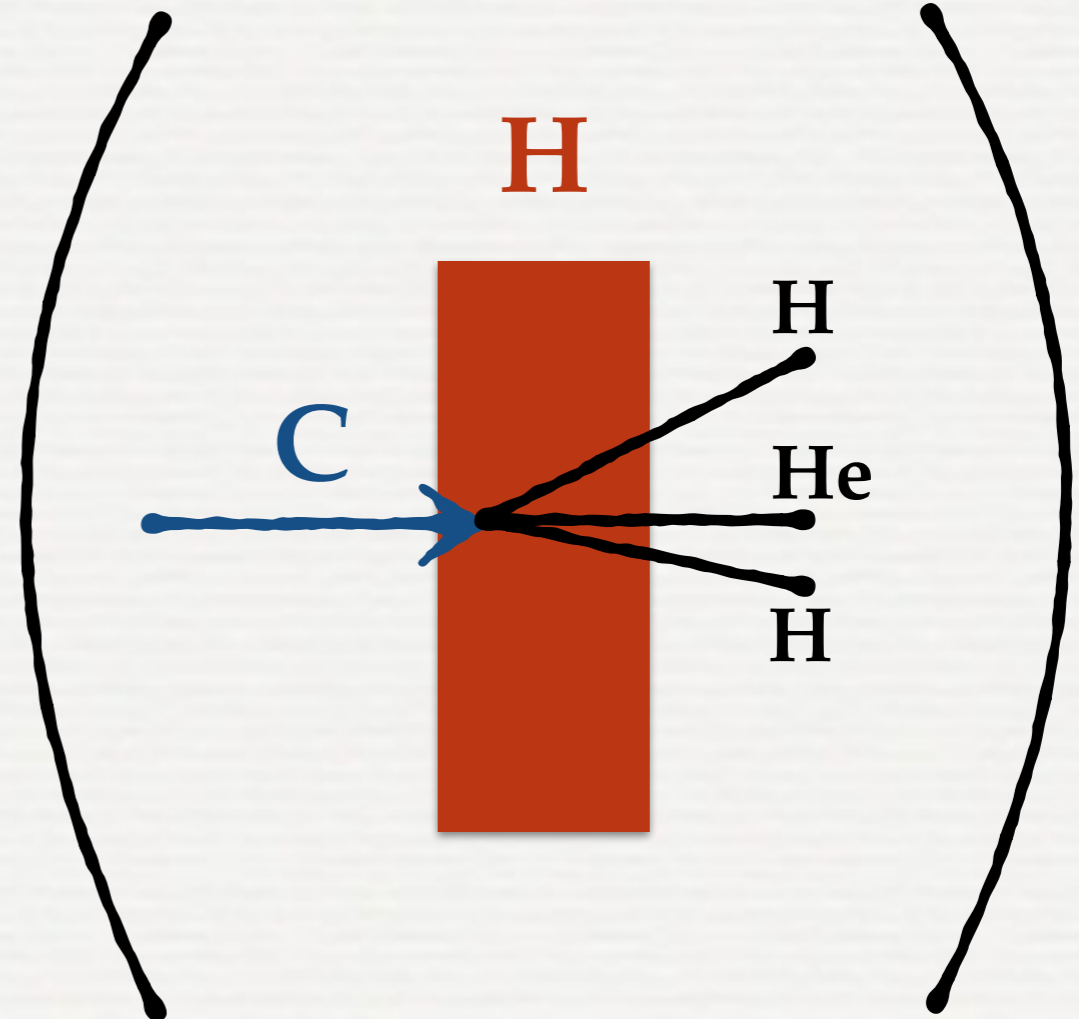
INVERSE KINEMATICS

proton on patient



== Lorentz Boost

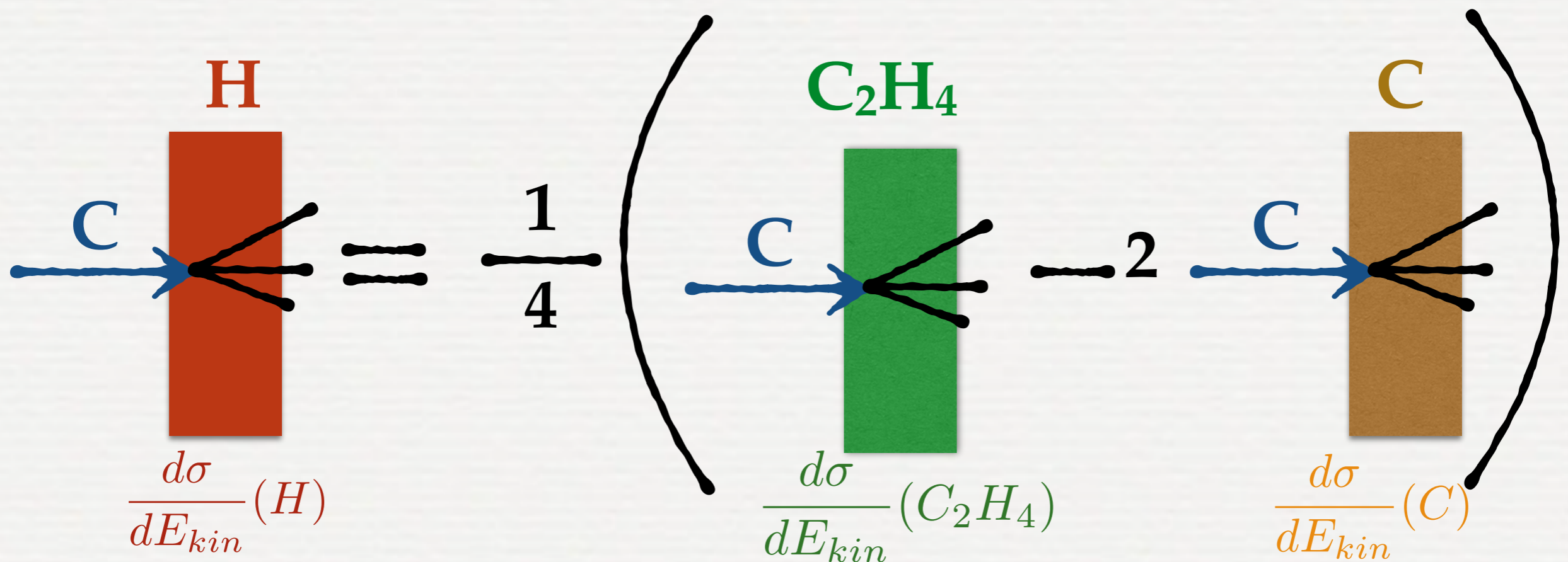
patient on proton



CROSS-SECTION COMBINATION

- Measurements performed with C_2H_4 and C targets
- $C \rightarrow H$ cross-section estimated as a combination of $C \rightarrow C_2H_4$ and $C \rightarrow C$ cross-sections

$$\Delta\sigma(C_2H_4, C) = \frac{d\sigma}{dE_{kin}}(H) = \frac{1}{4} \left(\frac{d\sigma}{dE_{kin}}(C_2H_4) - 2 \frac{d\sigma}{dE_{kin}}(C) \right)$$



ESTIMATION OF $H \rightarrow C$ CROSS-SECTION

- Procedure

- 1) Evaluate $C \rightarrow C_2H_4$ cross section for different fragments
- 2) Evaluate $C \rightarrow C$ cross section for different fragments
- 3) Apply Lorentz boost to retrieve $C_2H_4 \rightarrow C$ and $C \rightarrow C$ cross-sections (inverse kinematics)
- 4) Evaluate $H \rightarrow C$ cross section as the difference between $C_2H_4 \rightarrow C$ and $C \rightarrow C$ cross-sections
- 5) Compare with $C \rightarrow H$ Monte Carlo production

- Monte Carlo data files

Beam: ^{12}C , 200 MeV/n
Target: C_2H_4 , C
Thickness: 1 mm
Tot statistics: 10^7

[/gpfs_data/local/foot/Simulation/NewGeo/MagOff_HT/1mm_ok/*.root](#)

Beam: ^{12}C , 200 MeV/n
Target: C_2H_4 , C
Thickness: 2 mm
Tot statistics: 10^7

[/gpfs_data/local/foot/Simulation/NewGeo/MagOff_HT/*.root](#)
[/gpfs_data/local/foot/Simulation/NewGeo/MagOff_HT/C_H/*.root](#)
[/gpfs_data/local/foot/Simulation/NewGeo/MagOff_HT/H_C/*.root](#)

Beam: ^{12}C , 200 MeV/n
Target: C_2H_4 , C
Thickness: 4 mm
Tot statistics: 10^7

[/gpfs_data/local/foot/Simulation/NewGeo/MagOff_HT/4mm_ok/*.root](#)

GEOMETRICAL ACCEPTANCE

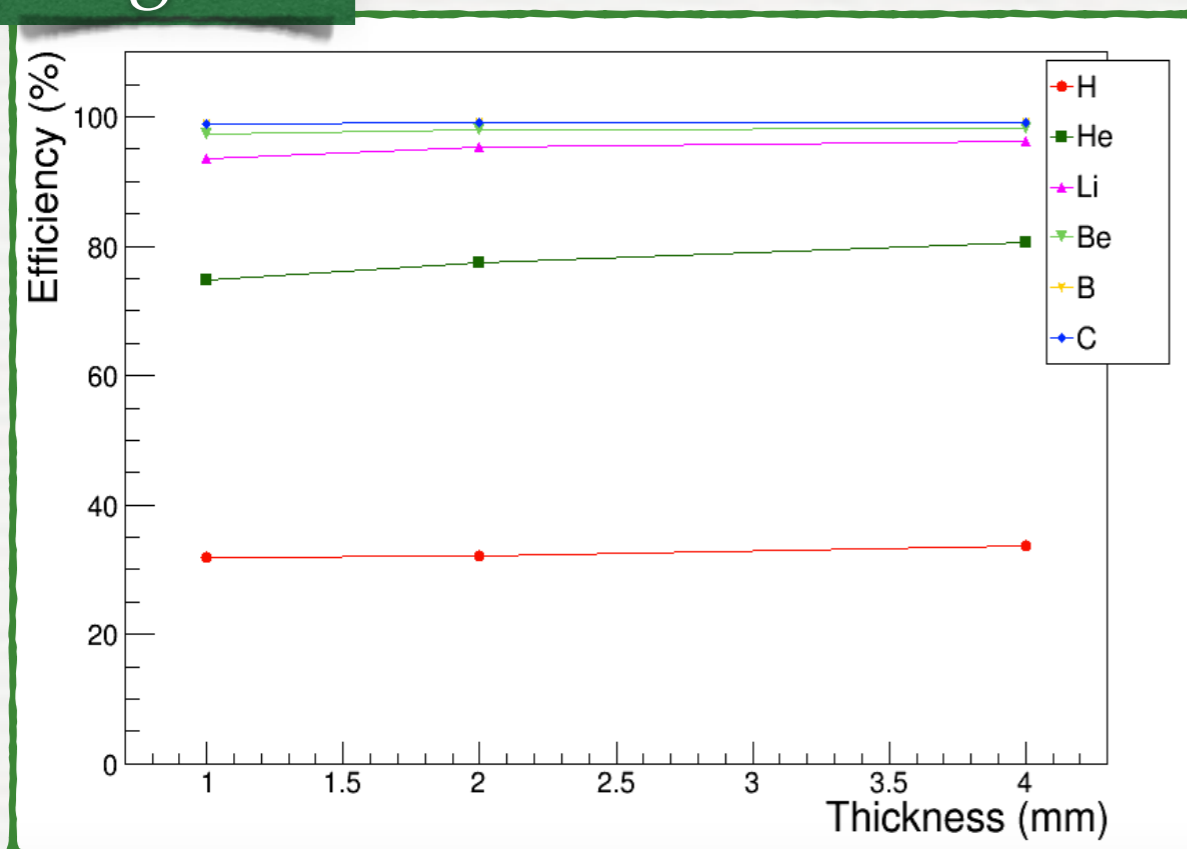
- Geometrical efficiency $\epsilon_{\text{geo}} = N_{\text{cal}} / N_{\text{target}}$

N_{cal} = Number of fragments reaching the calorimeter

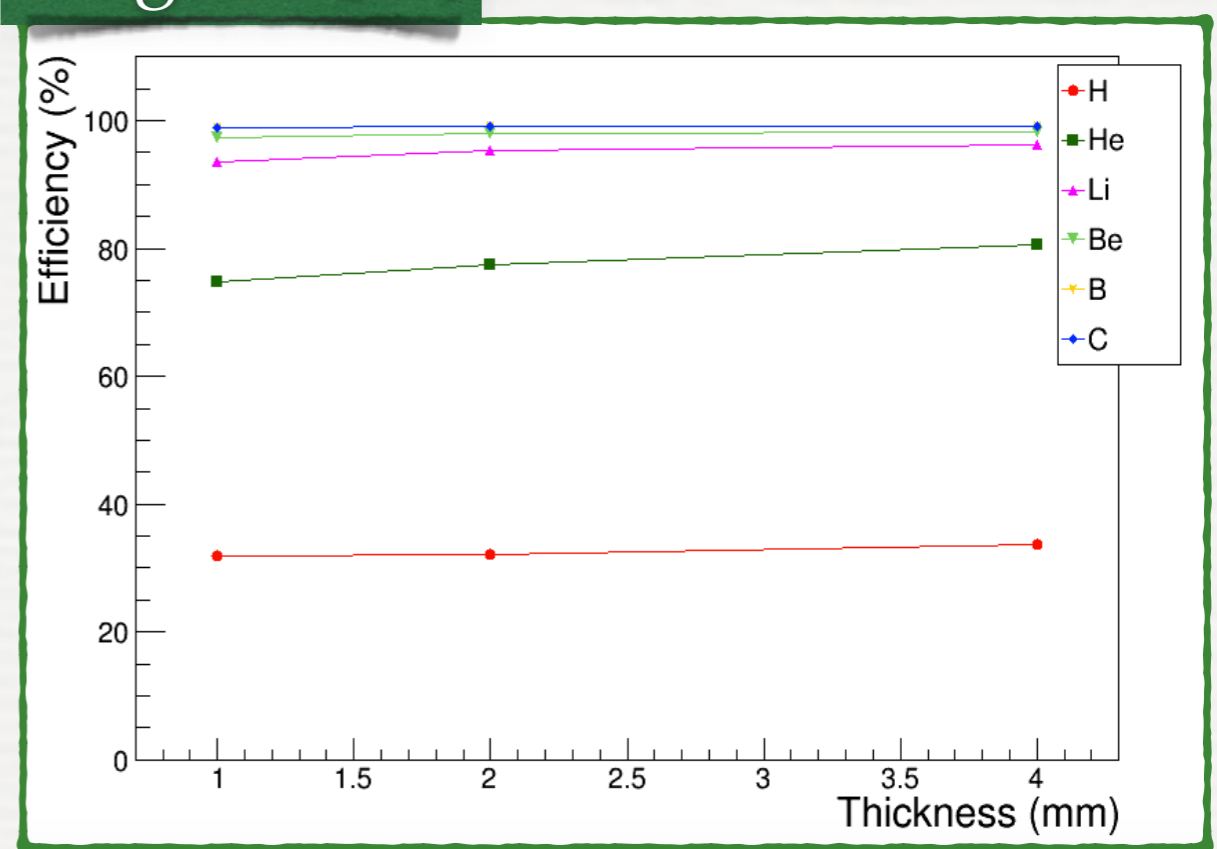
N_{sec} = Number of fragments exiting the target

Selection criteria: fragments produced by C beam fragmentation

Target: C



Target: C₂H₄



ENERGY DISTRIBUTION - DIRECT KIN

- Kinetic energy / nucleon for fragments produced in C beam fragmentation in the target
- Selection criteria: fragments reaching the calorimeter
- Target material: C
- Target thickness: 2 mm

$$\{\sigma_{\theta}^{\text{beam}} = 3 \text{ mrad}\}$$

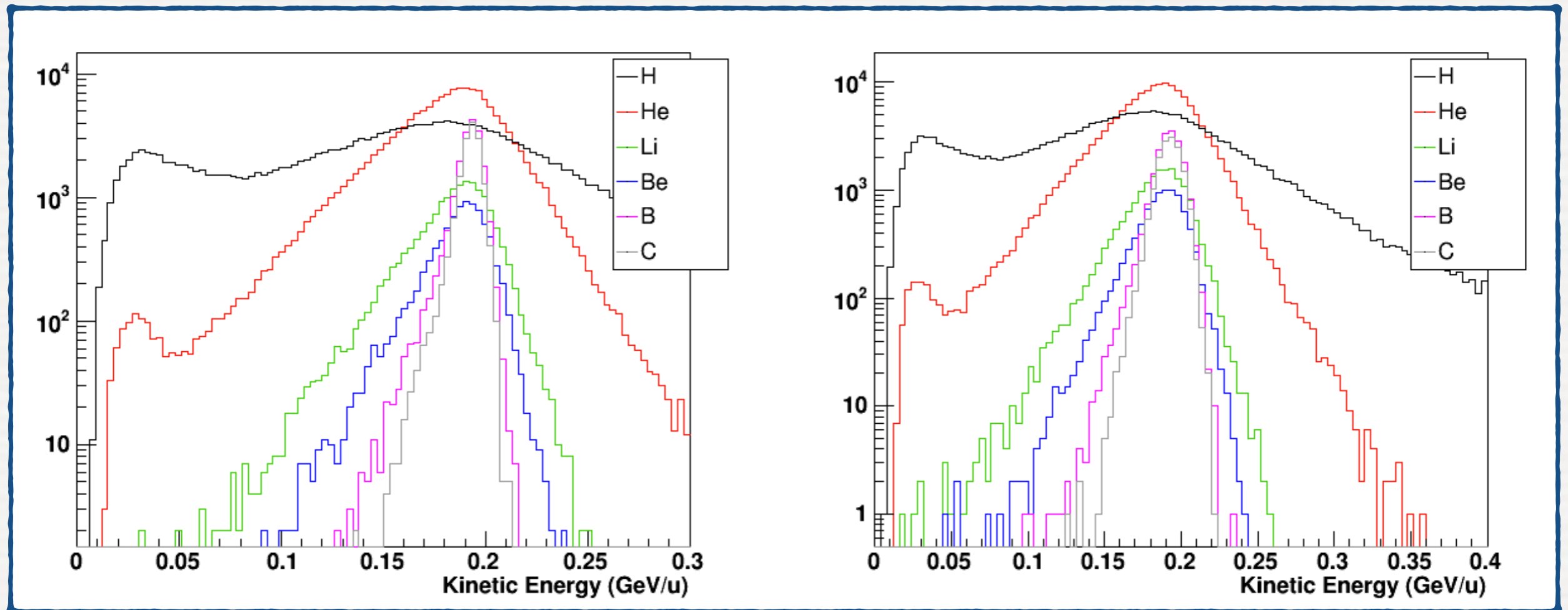
$$\{\sigma_{\theta}^{\text{frag}} = 3 \text{ mrad}\}$$

$$\{\sigma_E/E = 3\%\}$$

$$\{\sigma_P/P = 4\%\}$$

MC TRUE

SMEARING



ENERGY DISTRIBUTION - INVERSE KIN

- Kinetic energy / nucleon for fragments produced in C beam fragmentation in the target
- Selection criteria: fragments reaching the calorimeter
- Target material: C
- Target thickness: 2 mm

$$\{\sigma_{\theta}^{\text{beam}} = 3 \text{ mrad}\}$$

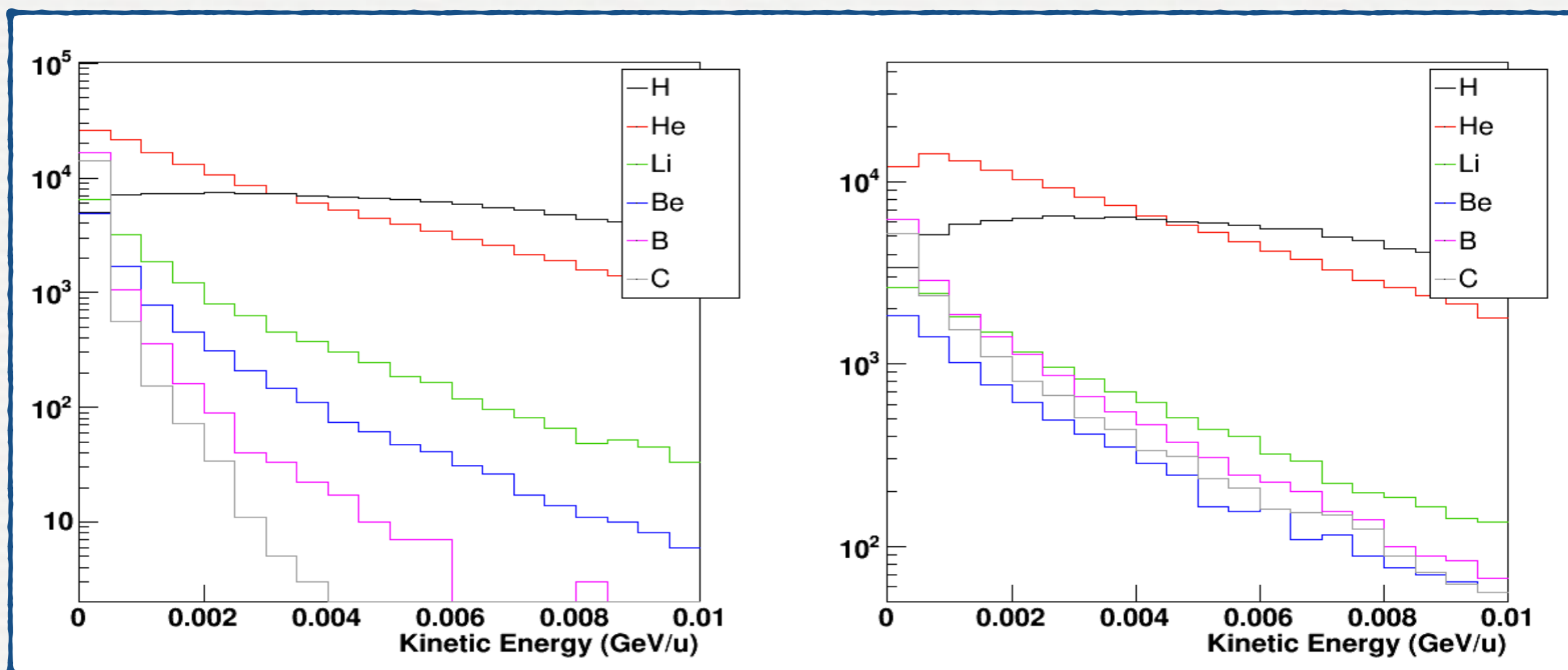
$$\{\sigma_{\theta}^{\text{frag}} = 3 \text{ mrad}\}$$

$$\{\sigma_E/E = 3\%\}$$

$$\{\sigma_P/P = 4\%\}$$

MC TRUE

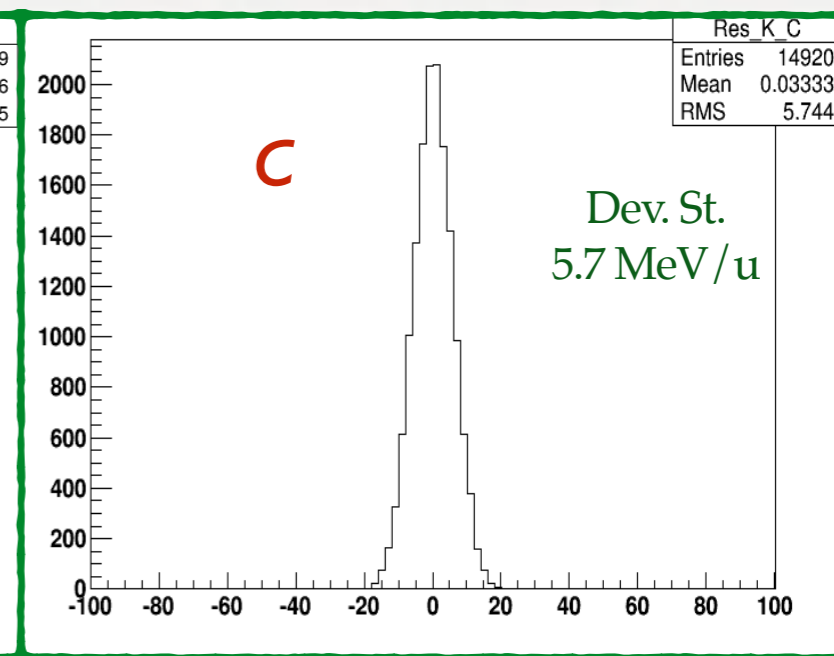
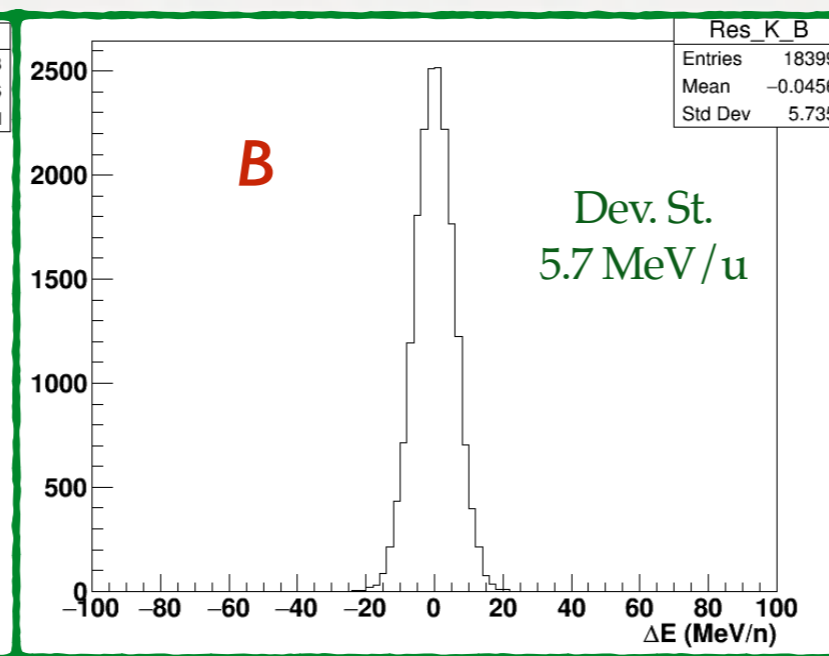
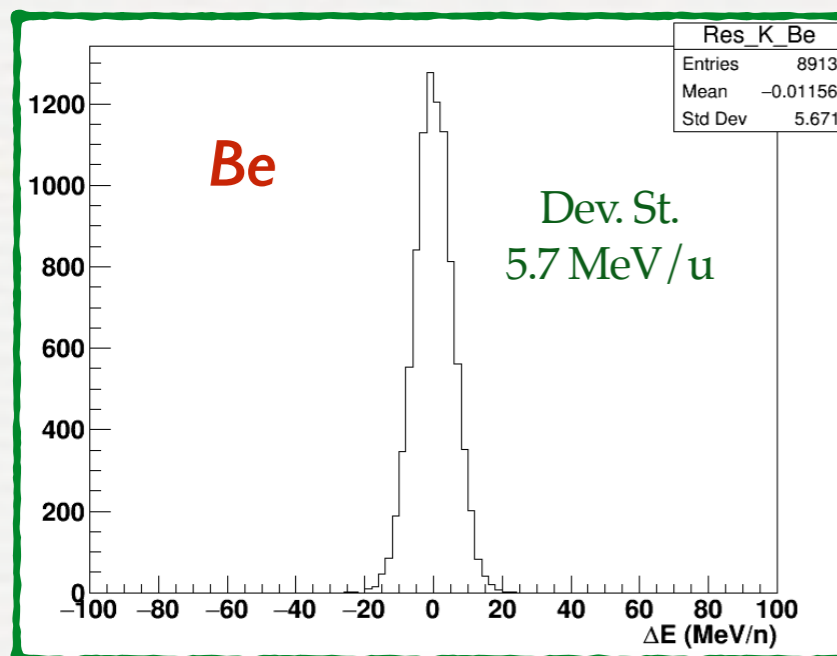
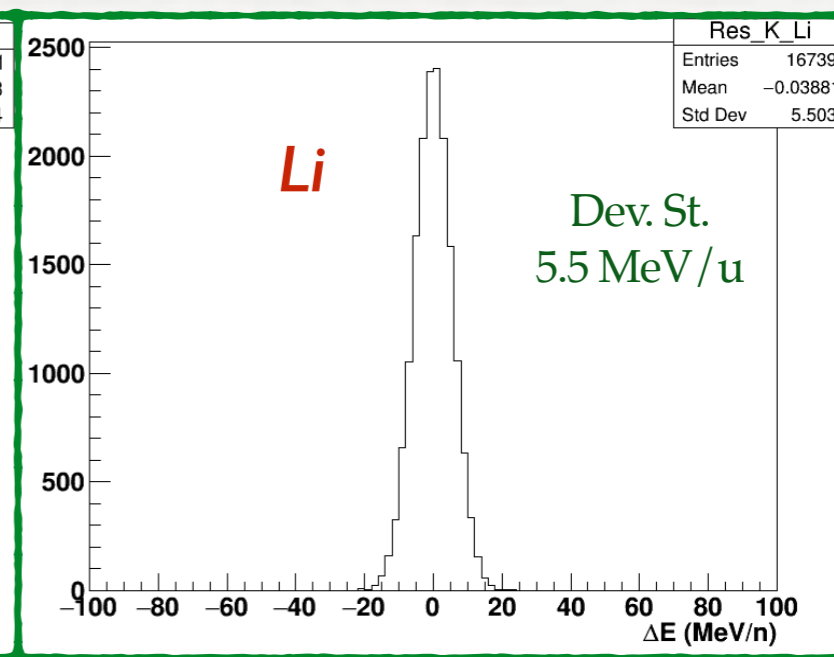
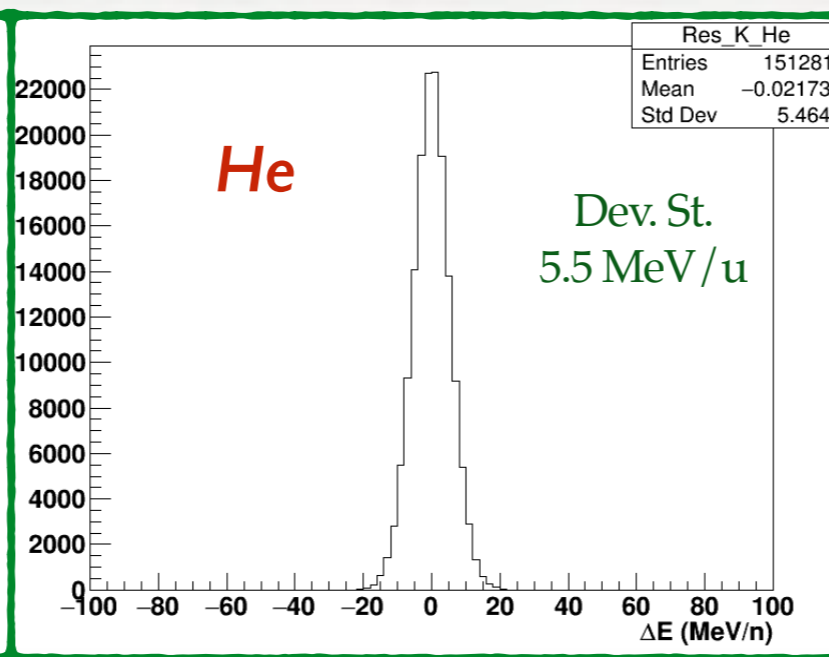
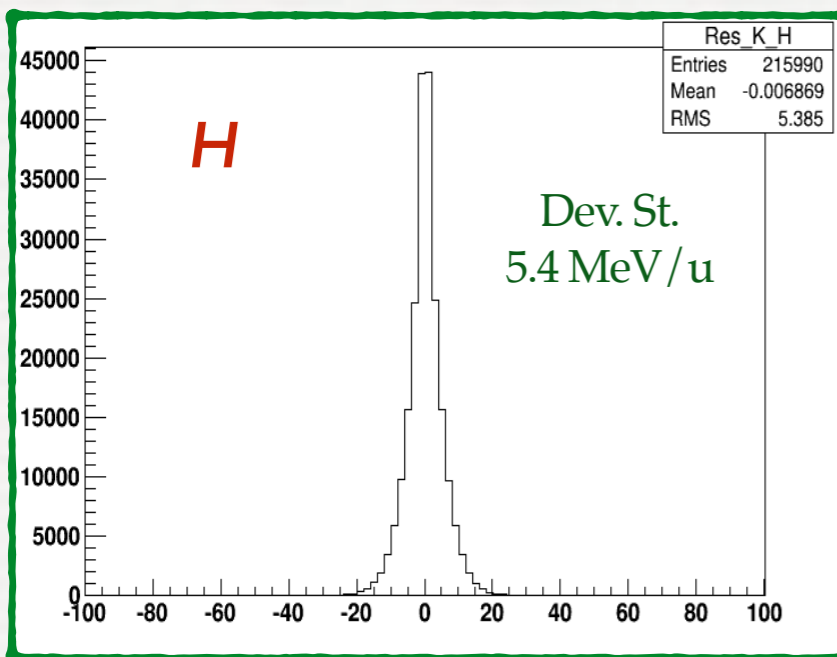
SMEARING



ENERGY RESOLUTION - DIRECT KINEMATICS

- Target material: C
- Target thickness: 2 mm

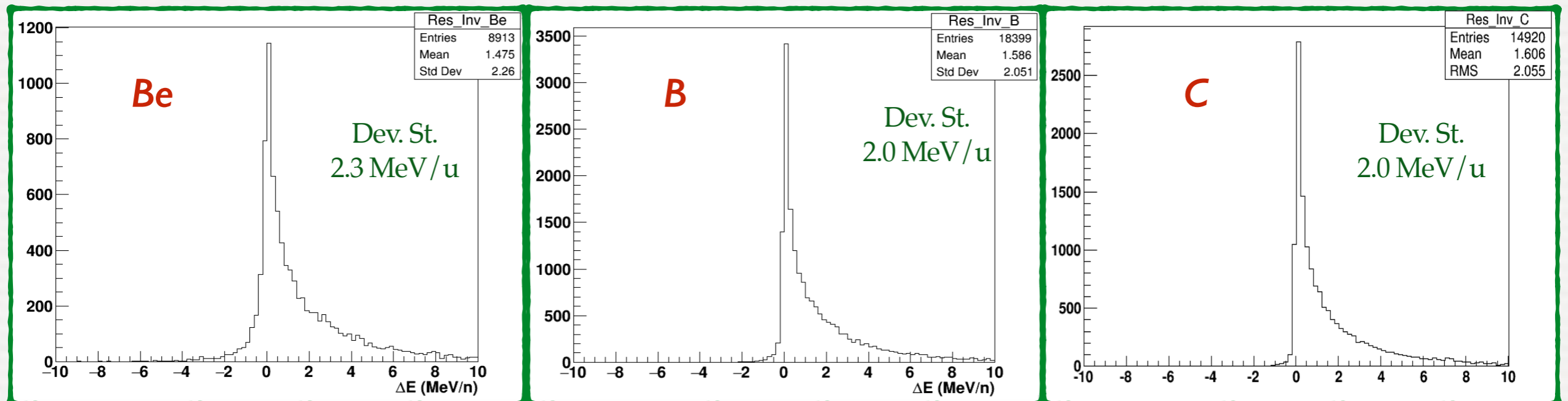
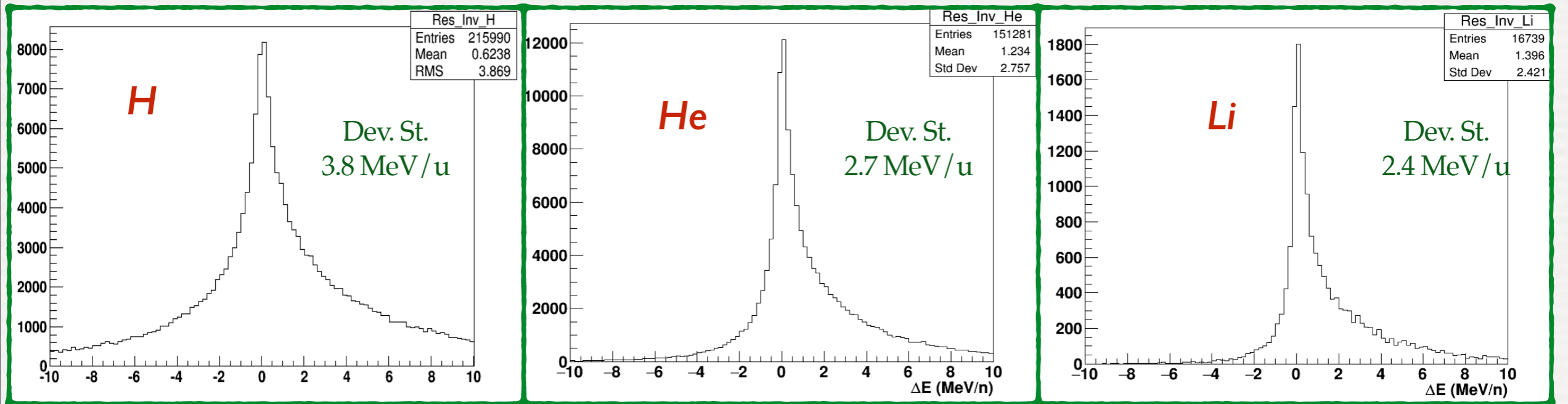
$$\text{Residuals} = E_{\text{kin,smear}} - E_{\text{kin,true}}$$



ENERGY RESOLUTION - INVERSE KINEMATICS

- Target material: C
- Target thickness: 2 mm

$$\text{Residuals} = E_{\text{kin,smear}} - E_{\text{kin,true}}$$



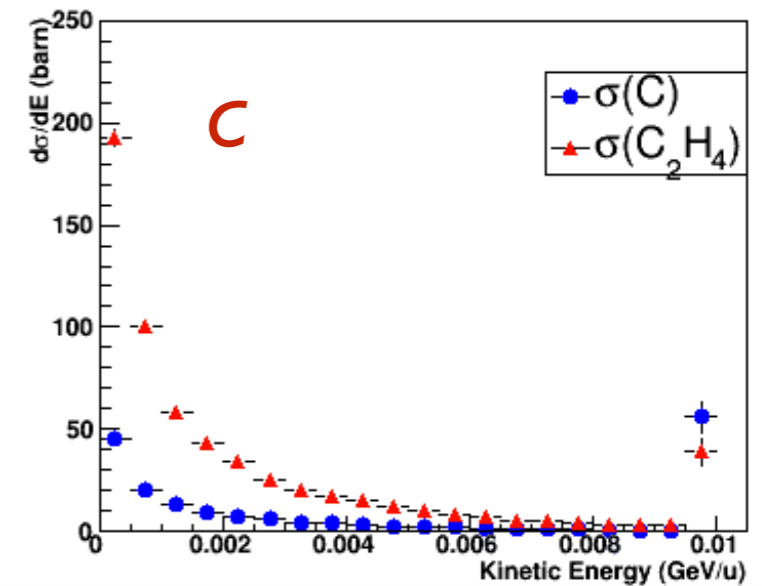
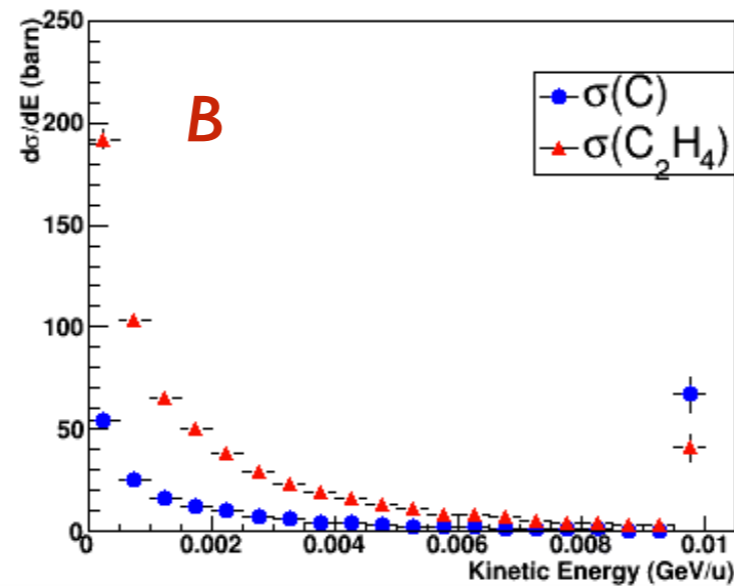
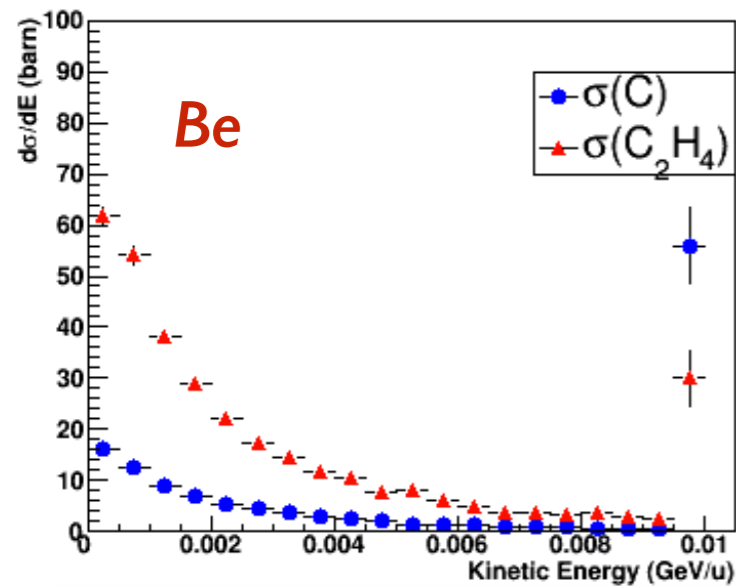
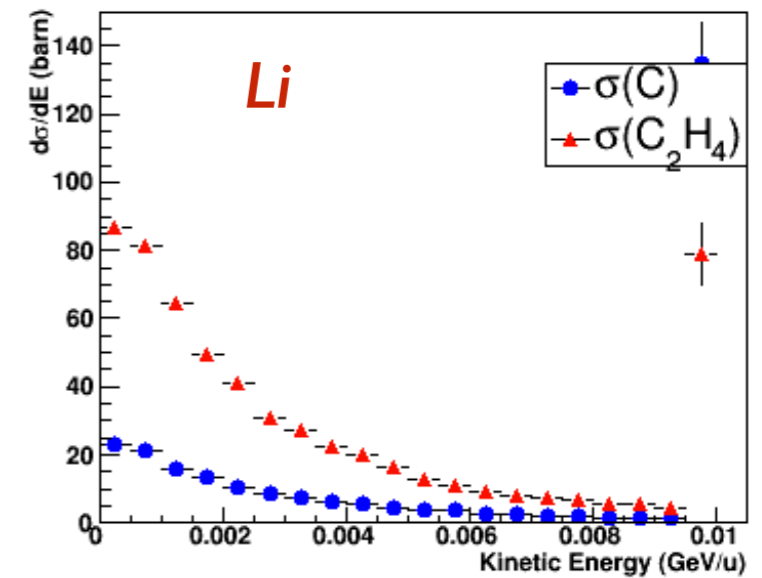
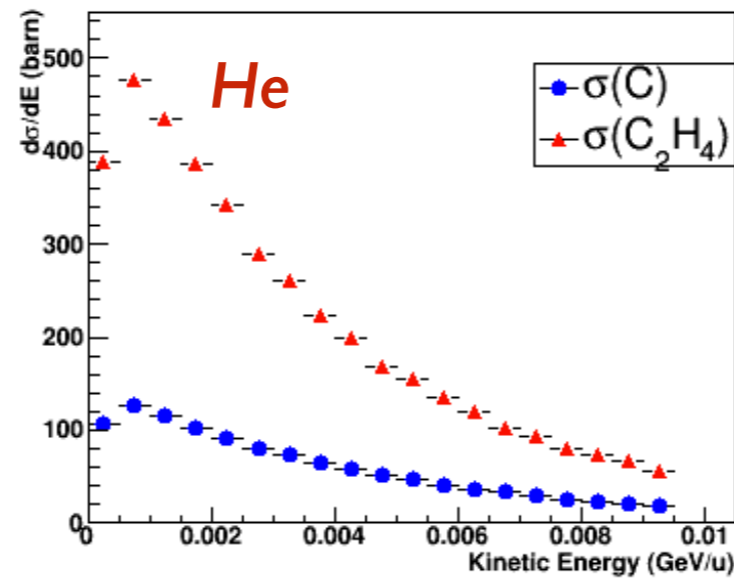
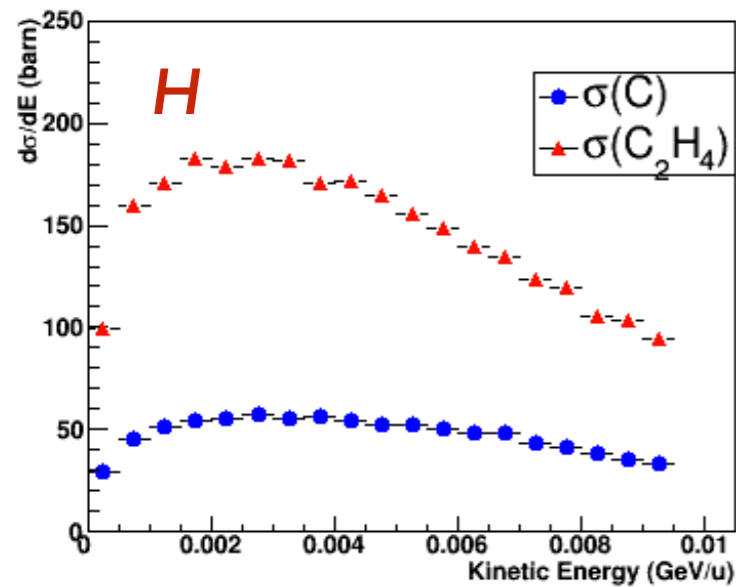
DIFFERENTIAL CROSS SECTION

Inverse kinematics

2 mm

$$\sigma(C_2H_4) = \frac{d\sigma}{dE_{kin}}(C_2H_4)$$

$$\sigma(C) = \frac{d\sigma}{dE_{kin}}(C)$$

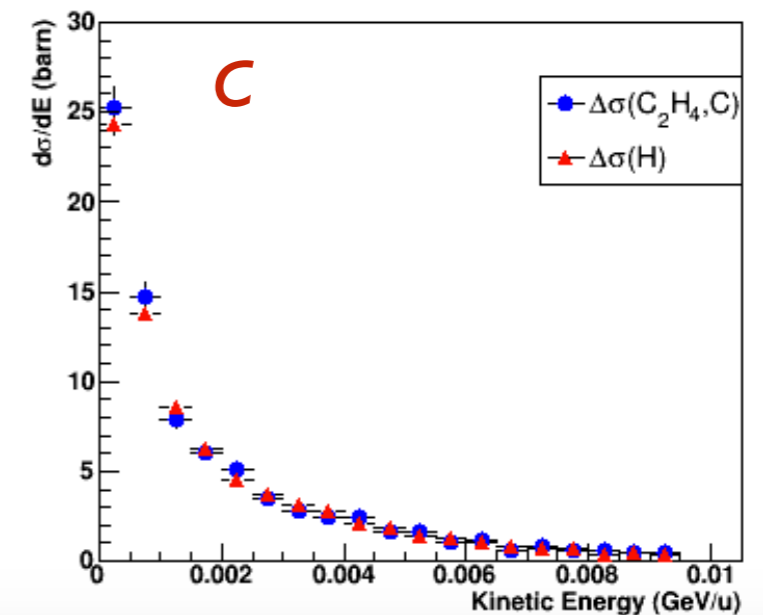
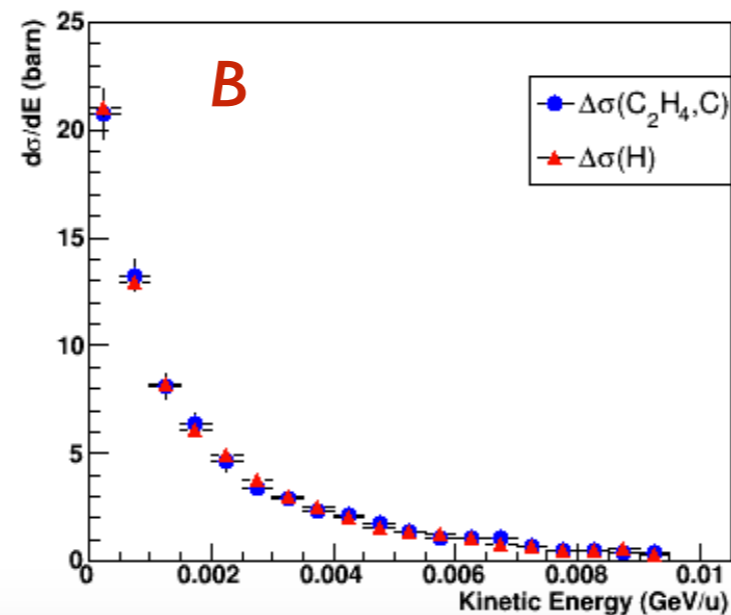
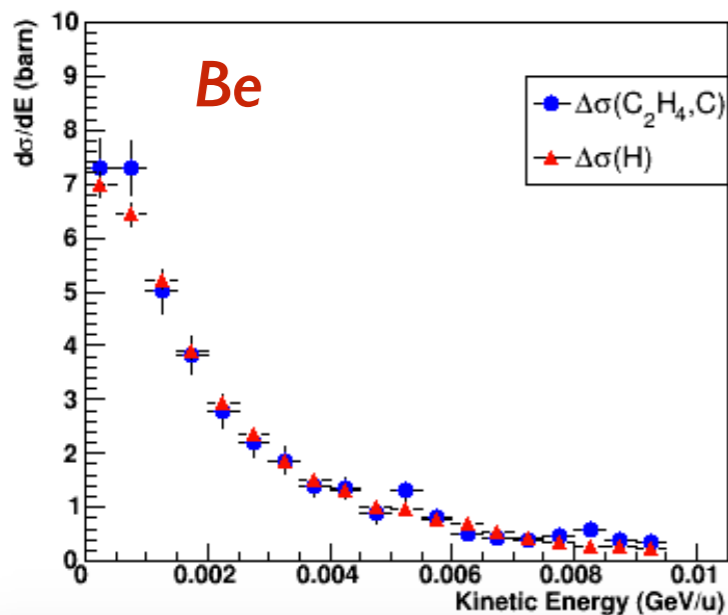
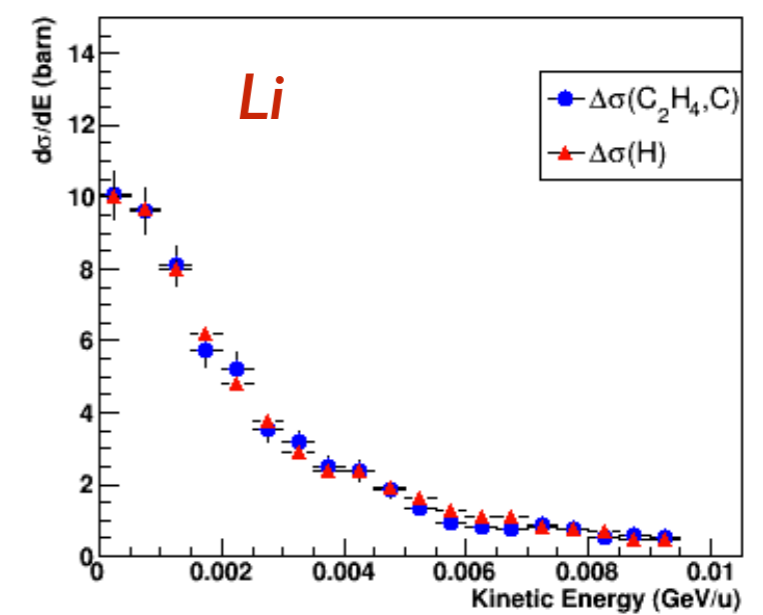
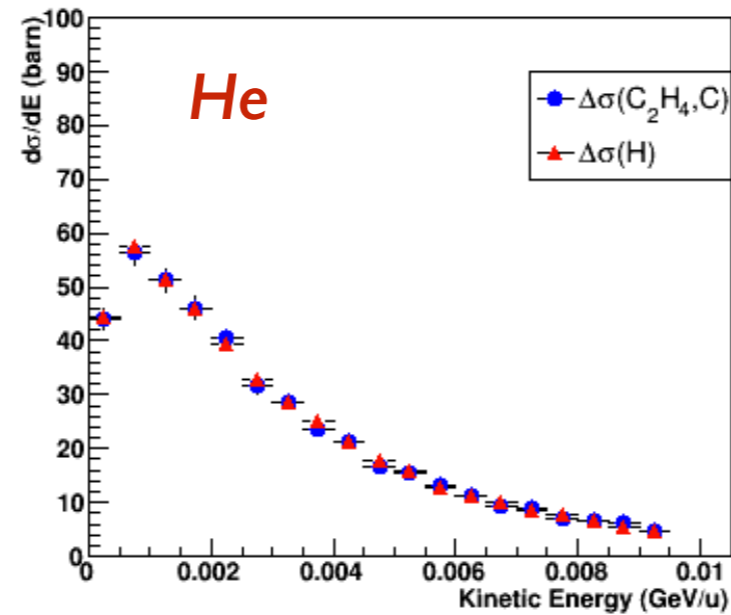
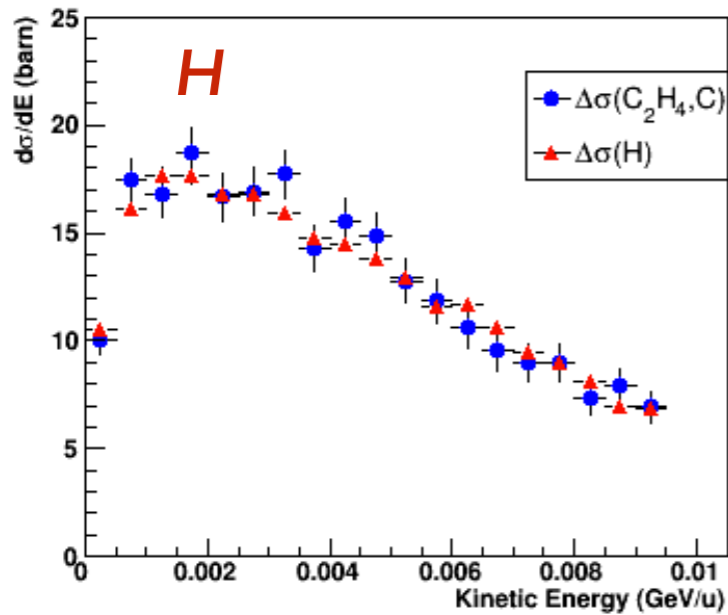


H→C DIFFERENTIAL CROSS SECTION

Inverse kinematics

2 mm

$$\Delta\sigma(C_2H_4, C) = \frac{1}{4} \left(\frac{d\sigma}{dE_{kin}}(C_2H_4) - 2 \frac{d\sigma}{dE_{kin}}(C) \right) \quad \sigma(H) = \frac{d\sigma}{dE_{kin}}(H)$$



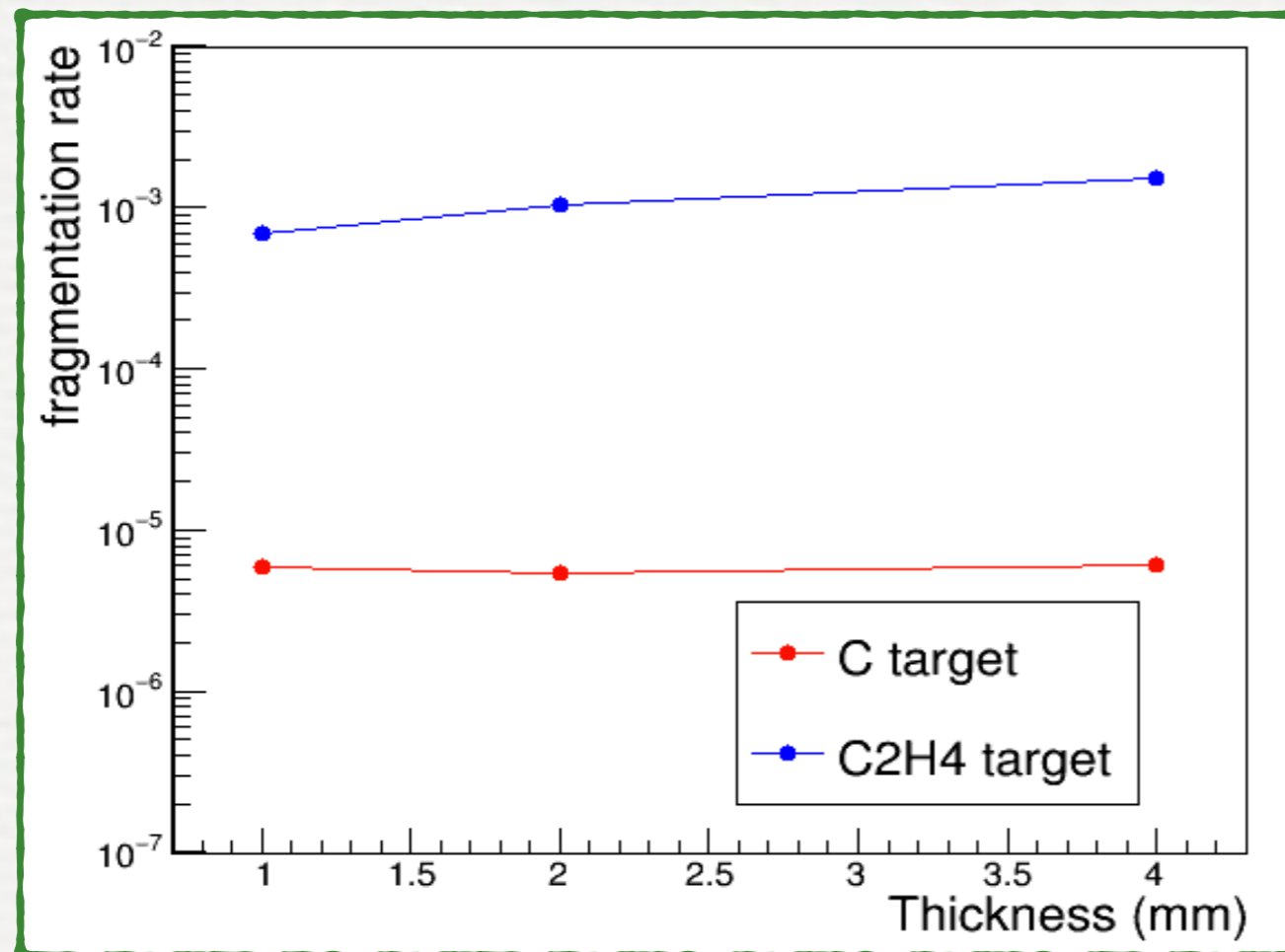
RE-FRAGMENTATION IN THE TARGET

- Re-fragmentation rate $R = N_{\text{sec}} / (N_{\text{sec}} + N_{\text{pri}})$

N_{pri} = Number of fragments produced by C beam fragmentation

N_{sec} = Number of fragments produced by re-fragmentation

Selection criteria: fragments exiting the target



CONCLUSIONS

- Good agreement in H->C cross section evaluated as difference between C₂H₄ and C targets
- No significant loss in efficiency when different target thickness is used

NEXT STEPS (After CDR)

- Use detector response instead of smeared MC true information
- Use different incident beam particles (¹⁶O) and energies

BACKUP SLIDES

RE-FRAGMENTATION IN THE TARGET

Selection criteria: fragments exiting the target

target: C	N _{pri}	N _{sec}	N _{sec} /(N _{pri} +N _{sec})
1mm	507070	3	0,0000059
2mm	928951	5	0,0000054
4mm	1675389	10	0,0000060

target: C ₂ H ₄	N _{pri}	N _{sec}	N _{sec} /(N _{pri} +N _{sec})
1mm	255321	174	0,00068
2mm	484506	510	0,00105
4mm	921482	1387	0,00150

	C	C ₂ H ₄
N _{pri} 2mm/ N _{pri} 1mm/	1,83	1,90
N _{pri} 4mm/ N _{pri} 2mm/	1,80	1,90
N _{pri} 4mm/ N _{pri} 1mm/	3,30	3,61

	C	C ₂ H ₄
N _{sec} 2mm/ N _{sec} 1mm/	1,7	2,9
N _{sec} 4mm/ N _{sec} 2mm/	2,0	2,7
N _{sec} 4mm/ N _{sec} 1mm/	3,3	8,0

RE-FRAGMENTATION IN THE TARGET

Selection criteria: reaching the calorimeter

target: C	N_{pri}	N_{sec}	$N_{sec}/(N_{pri}+N_{sec})$
1mm	227339	0	0,0000000
2mm	426242	0	0,0000000
4mm	809483	0	0,0000000

target: C ₂ H ₄	N_{pri}	N_{sec}	$N_{sec}/(N_{pri}+N_{sec})$
1mm	128242	17	0,00013
2mm	246858	68	0,00028
4mm	487588	171	0,00035

	C	C ₂ H ₄
$N_{pri2mm}/N_{pri1mm}/$	1,87	1,92
$N_{pri4mm}/N_{pri2mm}/$	1,90	1,98
$N_{pri4mm}/N_{pri1mm}/$	3,56	3,80

	C	C ₂ H ₄
$N_{sec2mm}/N_{sec1mm}/$	-	4,0
$N_{sec4mm}/N_{sec2mm}/$	-	2,5
$N_{sec4mm}/N_{sec1mm}/$	-	10,1