



Microchannel cooling techniques for the LHCb VELO Upgrade

Oscar Augusto on behalf of
LHCb VELO Upgrade and CERN PH-DT groups

CERN

26th International Workshop on Vertex Detectors

Las Caldas, Asturias, Spain

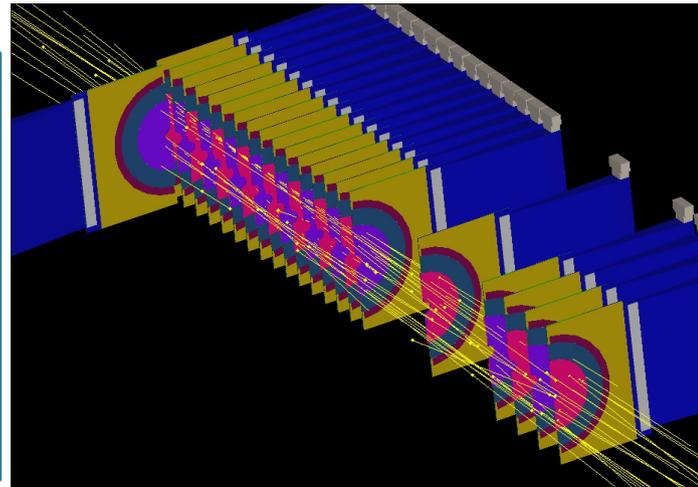
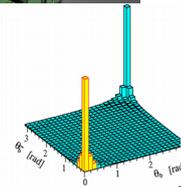
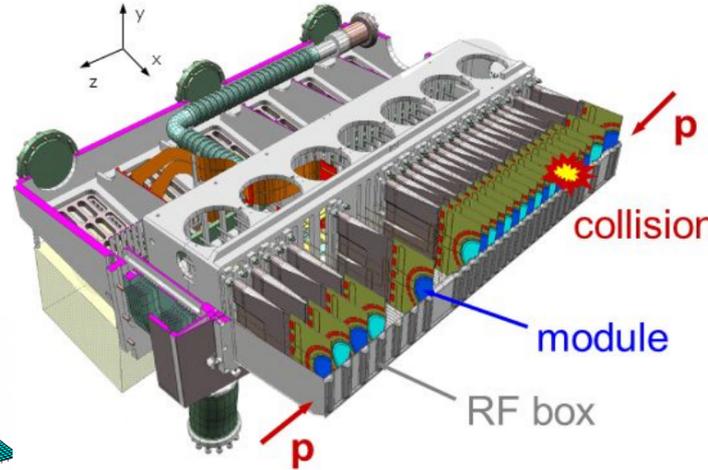
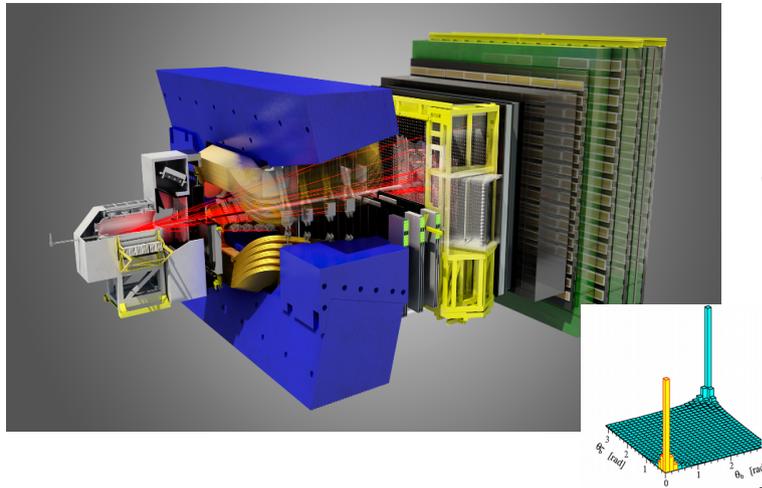
12/09/17

Summary

- Introduction
- Microchannels
 - Design
 - Cooling performance
 - Attachment of the fluidic connector
 - Reliability tests of the attachment
 - Fluidic characterization
- Back-up alternatives
 - Tubes embedded in ceramics
 - Titanium 3D printing
- Conclusion

LHCb experiment

[Performance of the LHCb Vertex Locator - arXiv:1405.7808](https://arxiv.org/abs/1405.7808)



Current VELO

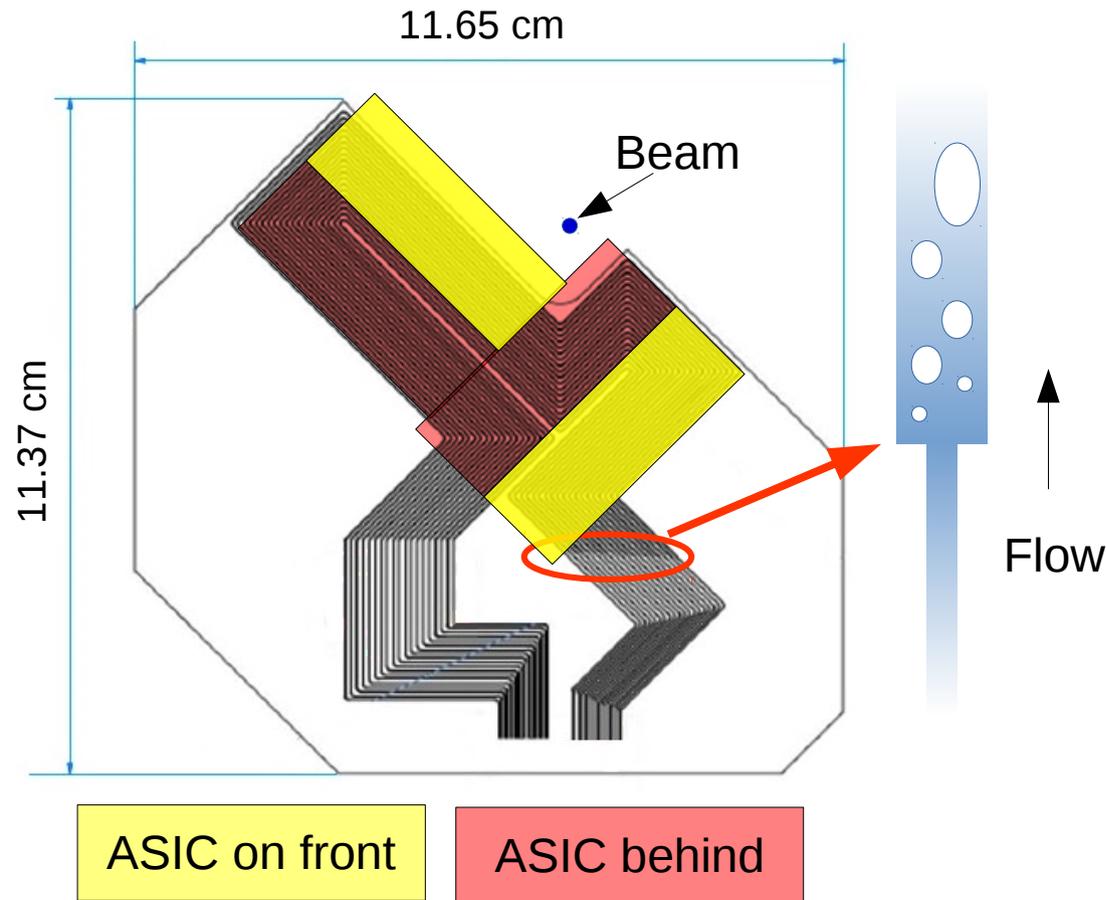
- Subdetector located around the p-p collisions
- Responsible for vertex and track reconstruction
- 88 Si-strip sensors surrounding the interaction point
- Modules are moved away during the beam injection
- Excellent impact parameter resolution (down to $11.6 \mu\text{m}$)
- Excellent single hit resolution $\sim 4 \mu\text{m}$
- Total power dissipated is $\sim 16.5\text{W/module}$

LHCb experiment:

- One of the 4 major experiments at LHC
- Forward spectrometer designed to measure CP violation, study rare decays of c and b hadrons and search for new physics.

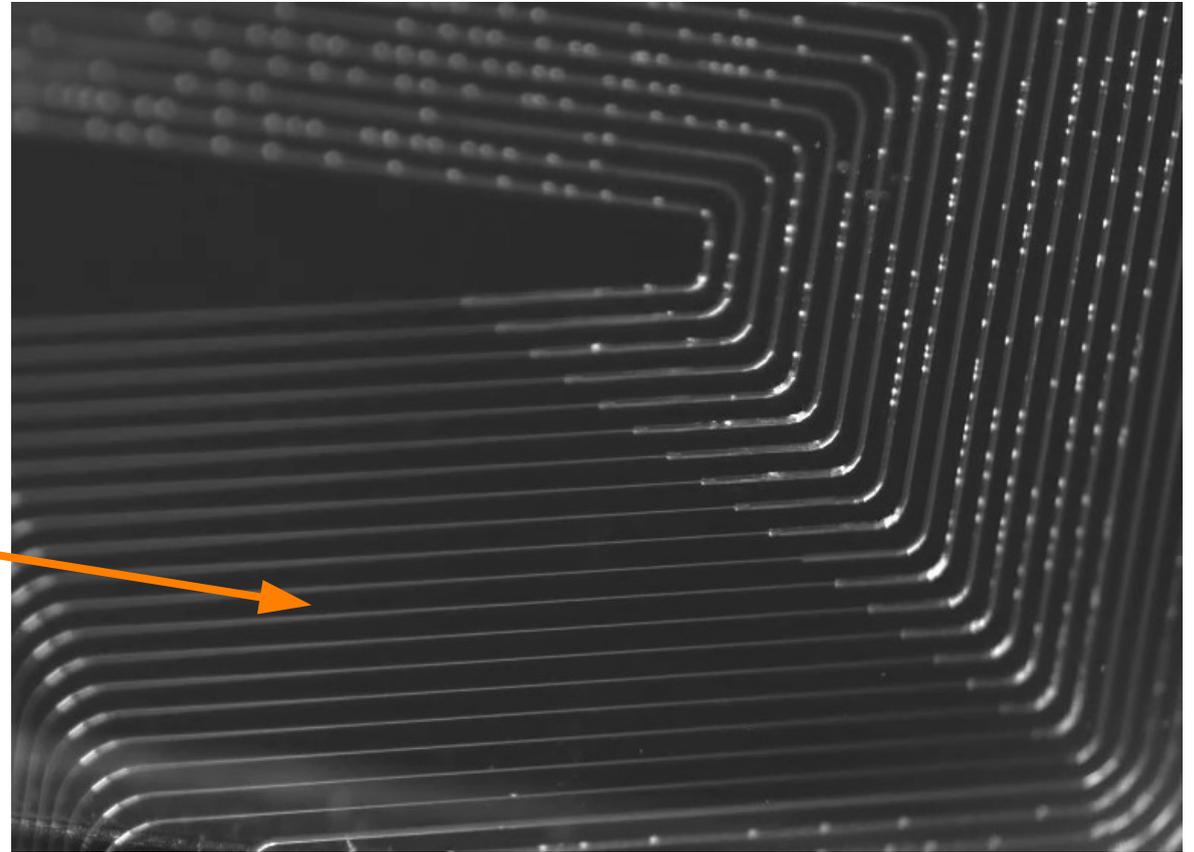
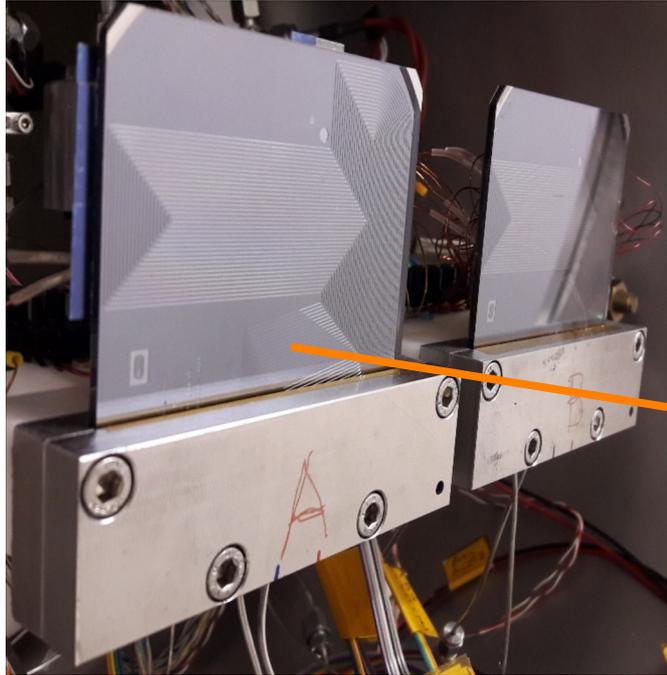
More details at Emma's and Edgar's talks

Microchannels etched in silicon



- Narrow restrictions at the entrance
 - $60\ \mu\text{m} \times 60\ \mu\text{m}$ (40 mm long)
 - Dominant pressure drop
 - Prevents instabilities among the channels
- Main channels
 - $120\ \mu\text{m} \times 200\ \mu\text{m}$ (~260 mm in average)
 - Heat provided by electronics is absorbed by the CO_2 changing the ratio of gas/liquid
- The sudden increase in cross section between the restriction and the main channels triggers the boiling

CO₂ boiling inside micro-channels



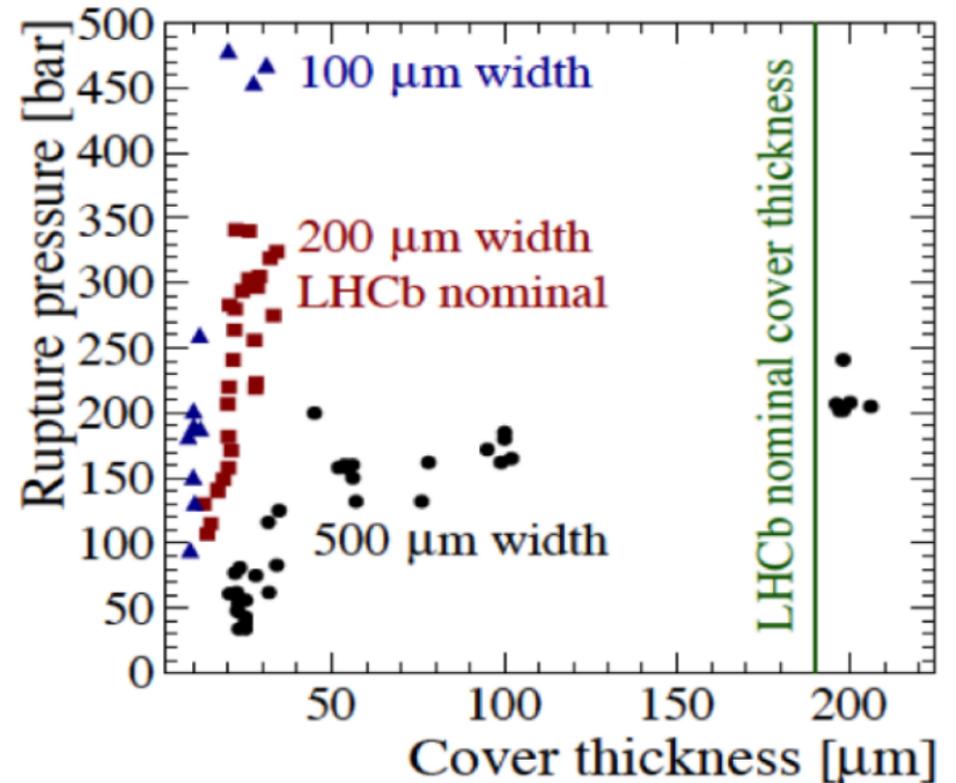
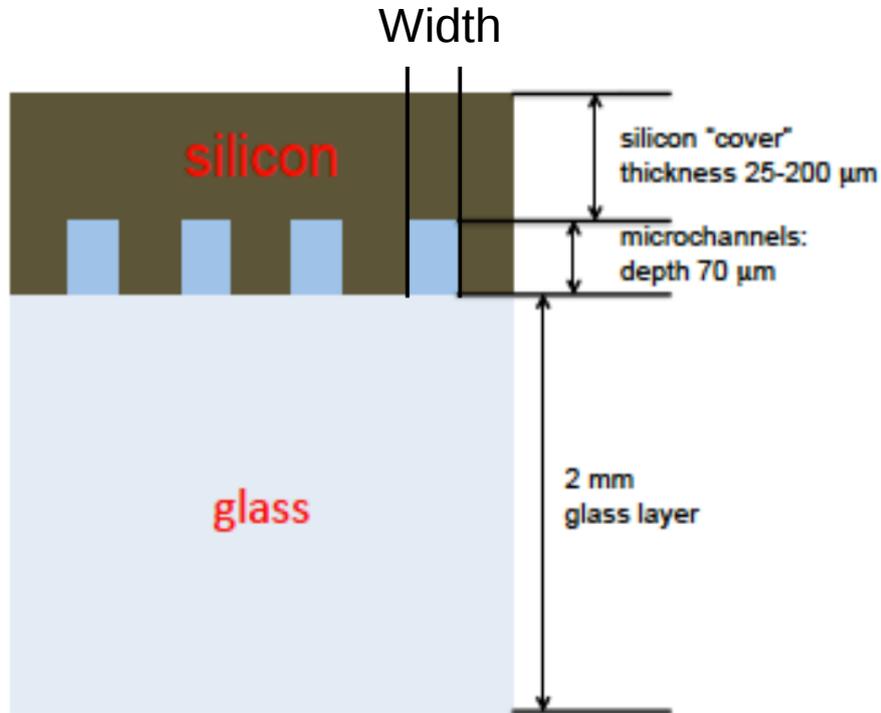
Nice video in the following [link!](#)



Oscar Augusto

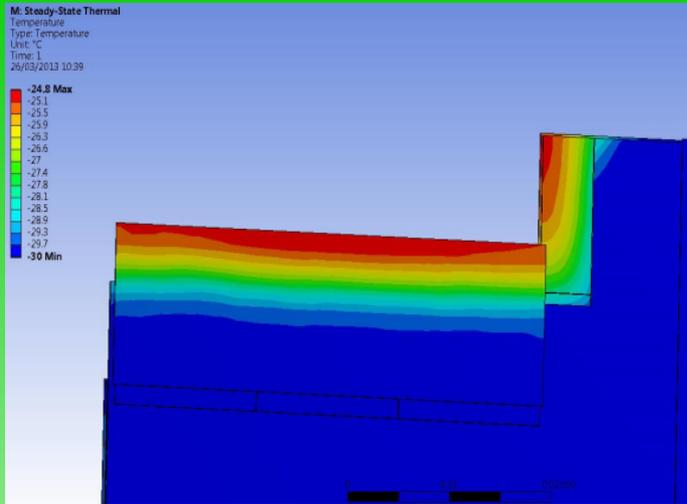
Resistance to high pressure

At room temperature, the saturation pressure of the CO₂ is around 65 bar. For safety reasons, the system is validated to 186 bar.



Cooling performance

Simulation

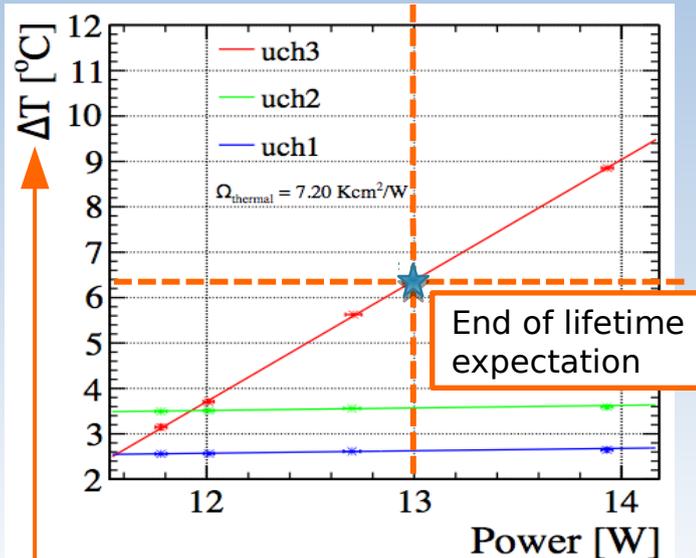
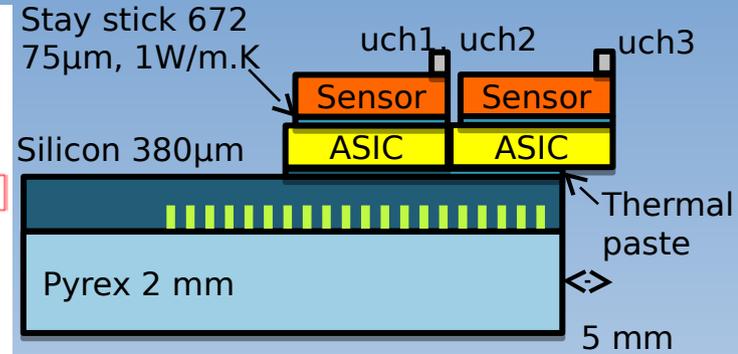
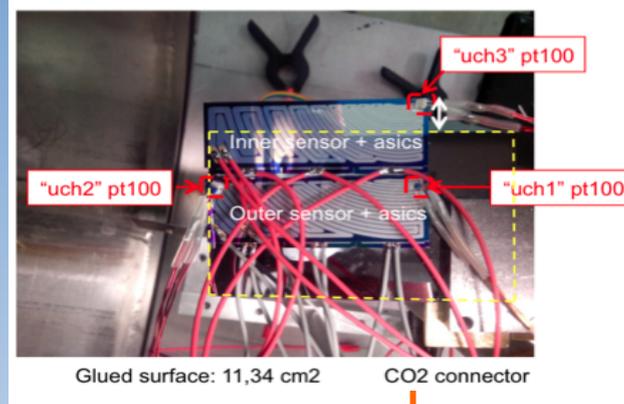


ANSYS simulation:

- ◆ 3W/ASIC (36W/module)
- ◆ No power consumption on the sensors
- ◆ CO₂ at -30 °C
- ◆ 100 μm stycast® 8550 FT + catalyst 9 (1.25W/mK)
- ◆ $\Delta T \sim 5^\circ\text{C}$ (Due to the 5 mm overhang)

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Experimental Test

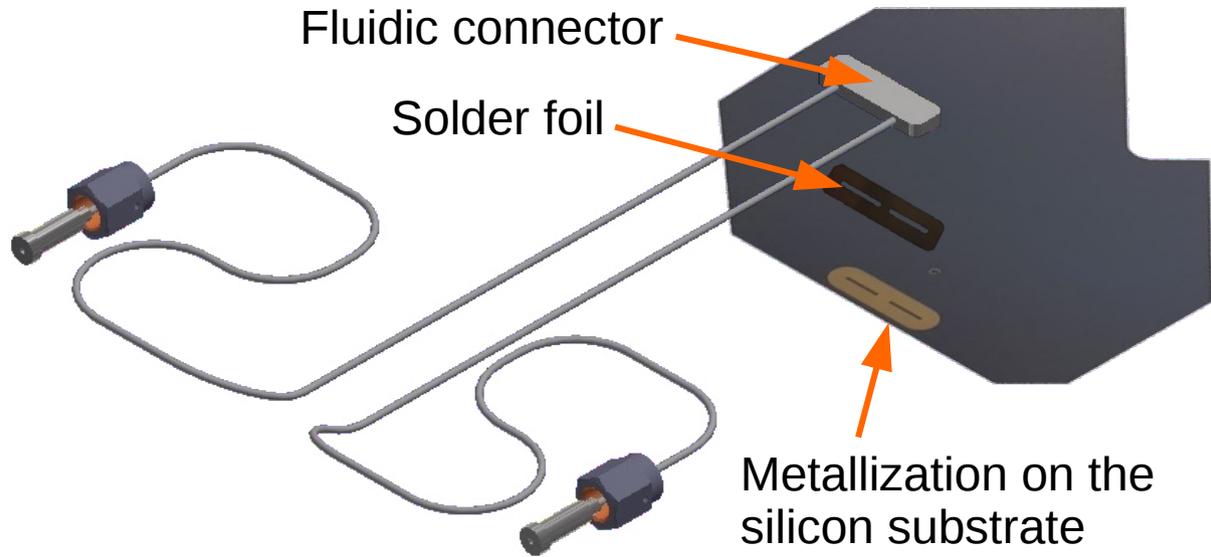


ΔT with respect to the output CO₂ temperature

The power dissipation of half of a module was simulated:
 → ~ 11.5 W on the 6 ASIC mockups
 → 1.5 W on the innermost sensor mockup

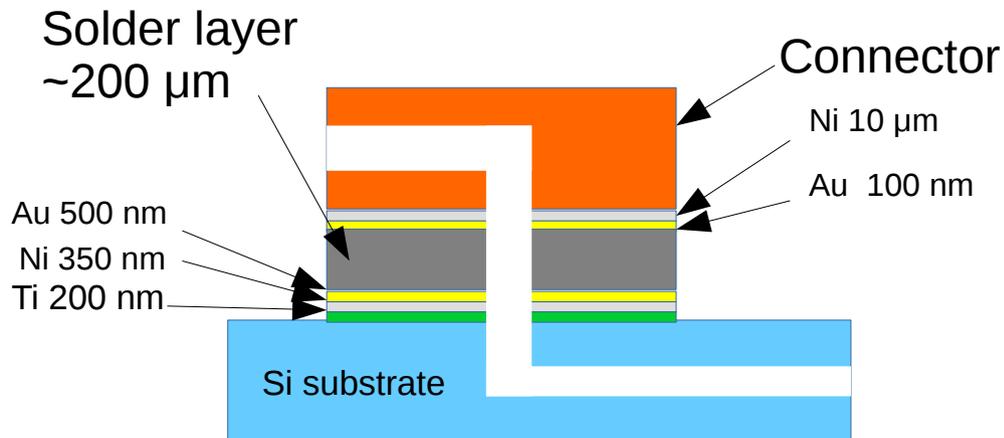
Max $\Delta T \sim 6.5^\circ\text{C}$ for the end of lifetime expectation

Attachment of the fluidic connector



Challenges involved:

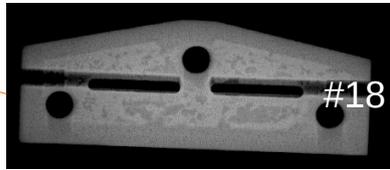
- Leak tight (modules are in the secondary vacuum)
- Planarity
- Voids on the solder layer
- No flux
- High pressure (up to 186 bar)



Attachment of the fluidic connector

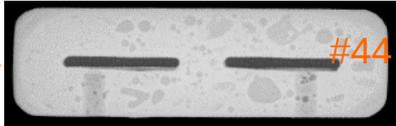
March 2017

#1

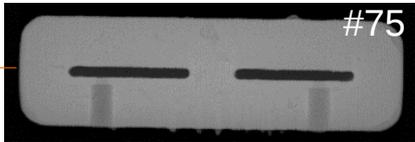


#18

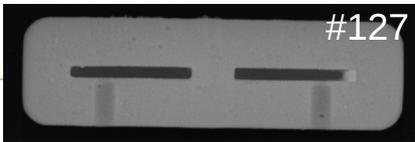
Small samples



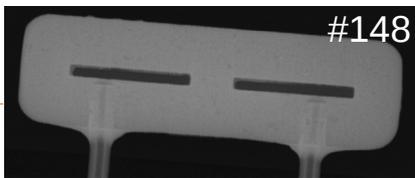
#44



#75



#127



#148

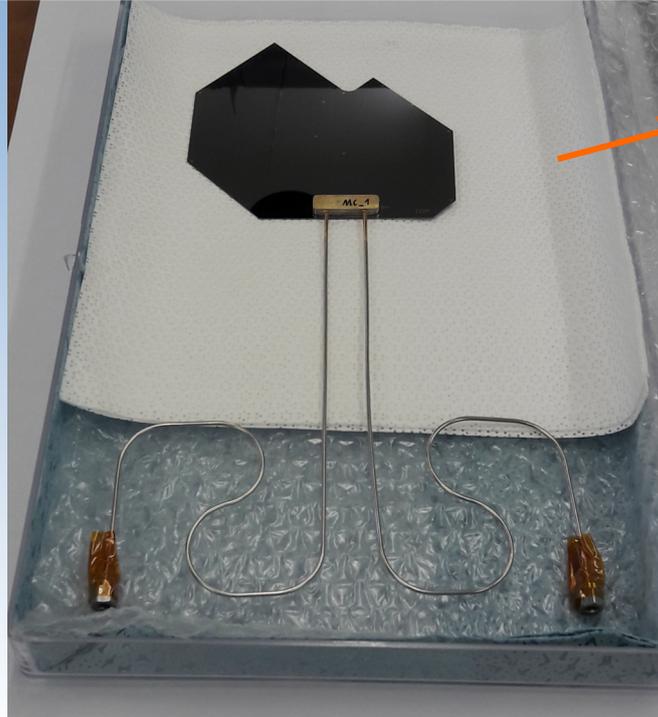
Large samples

#160

MC1

Sep 2017

First microchannels soldered on September 1st 2017

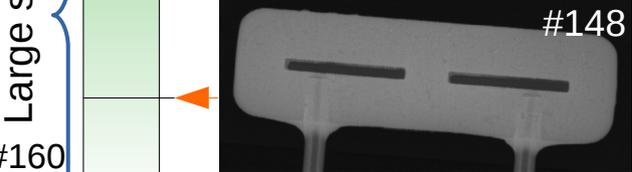
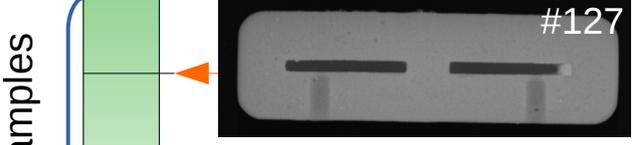
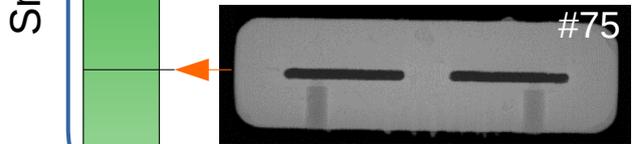
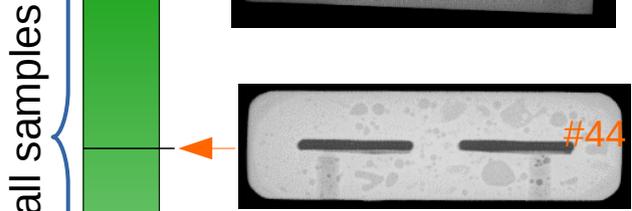
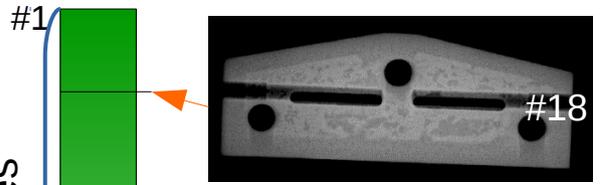


X-ray of the solder joint

LHCb - VELO Micro Channel Cooling - Kovar/Si - MC1

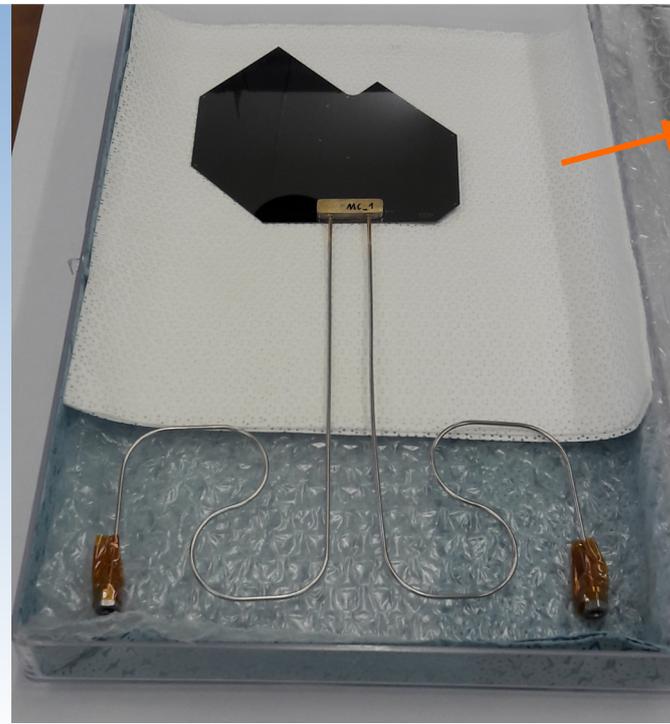
Attachment of the fluidic connector

March 2017



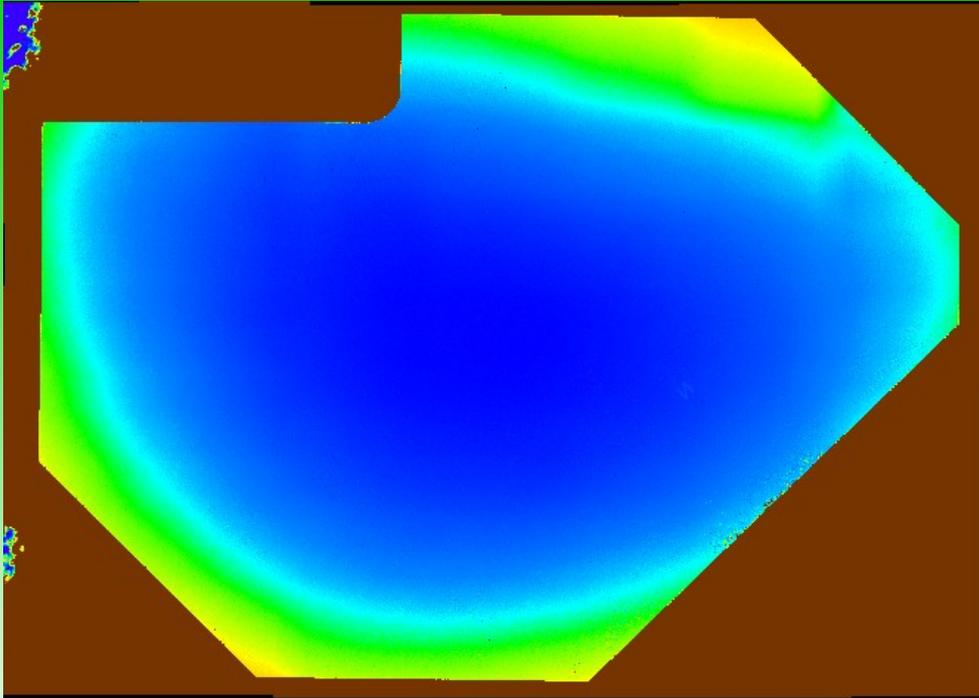
Sep 2017

First microchannels soldered on September 1st 2017



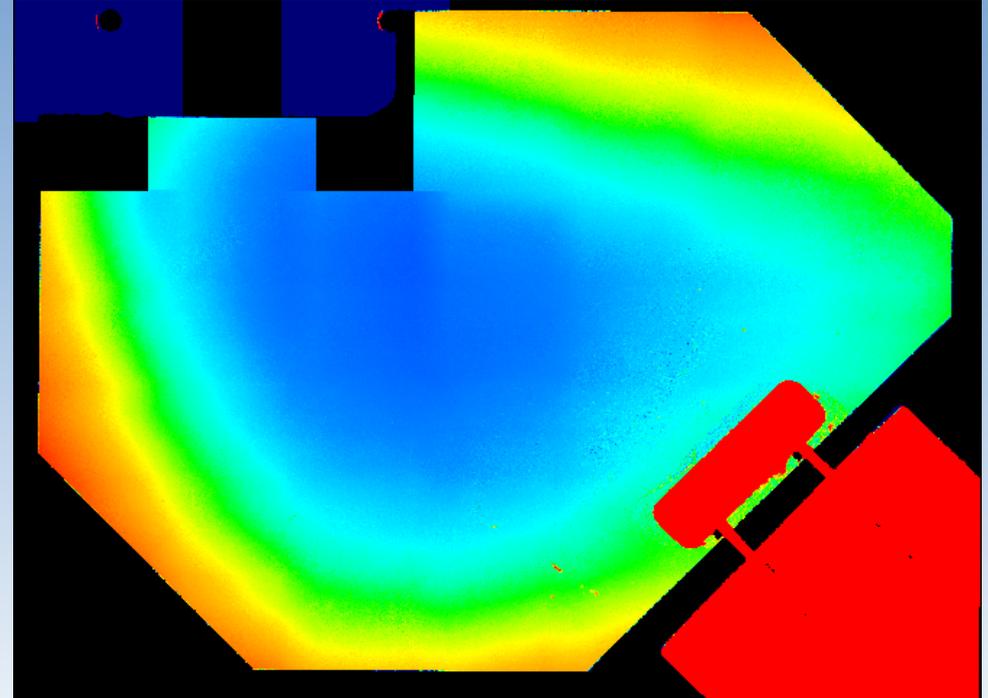
Planarity before soldering

Before soldering



Max deviation: +26 μm
Min deviation: -60 μm
Total variation: 86 μm

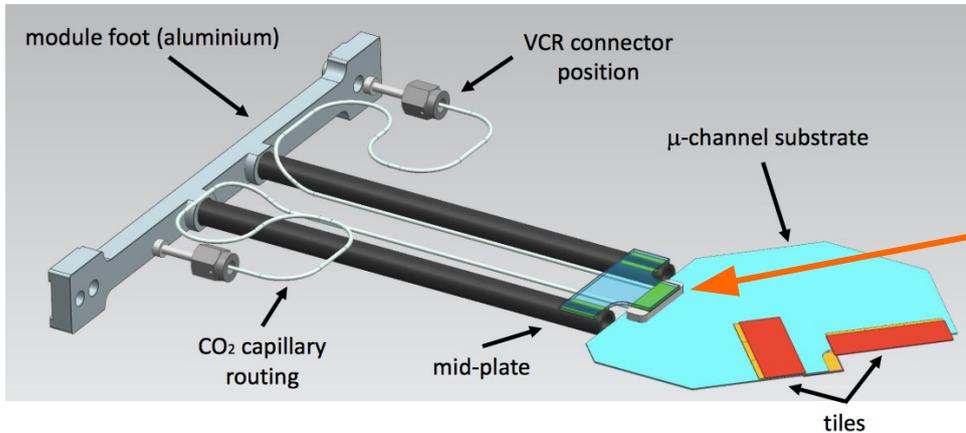
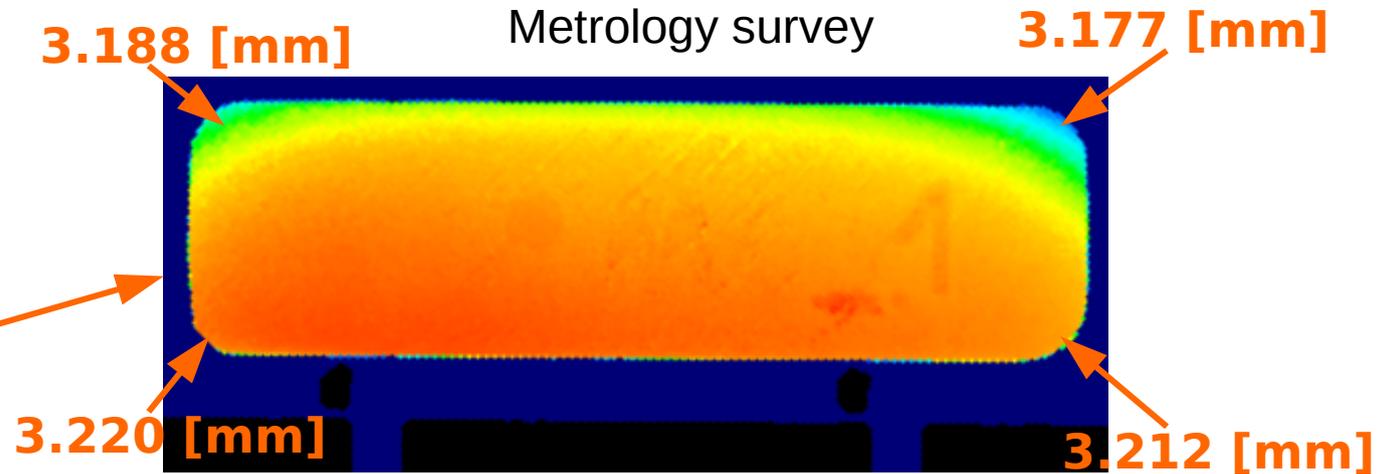
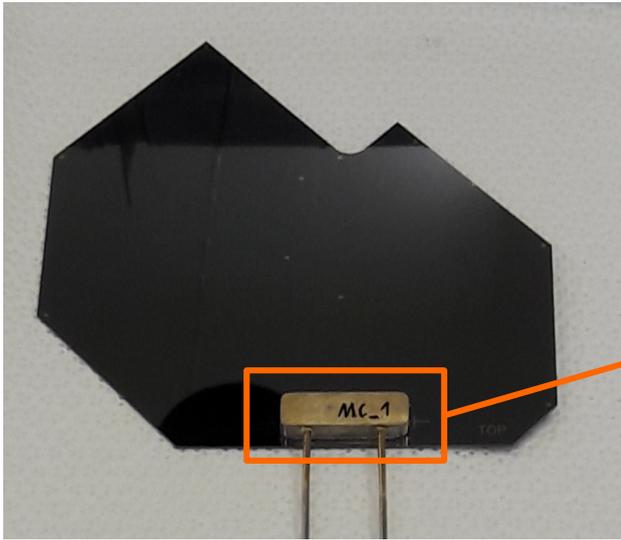
After soldering



Max deviation: +25 μm
Min deviation: -50 μm
Total variation: 75 μm

No significant change on the planarity of the silicon plate.
Therefore, no significant stress generated by the soldering procedure.

Connector/Silicon planarity

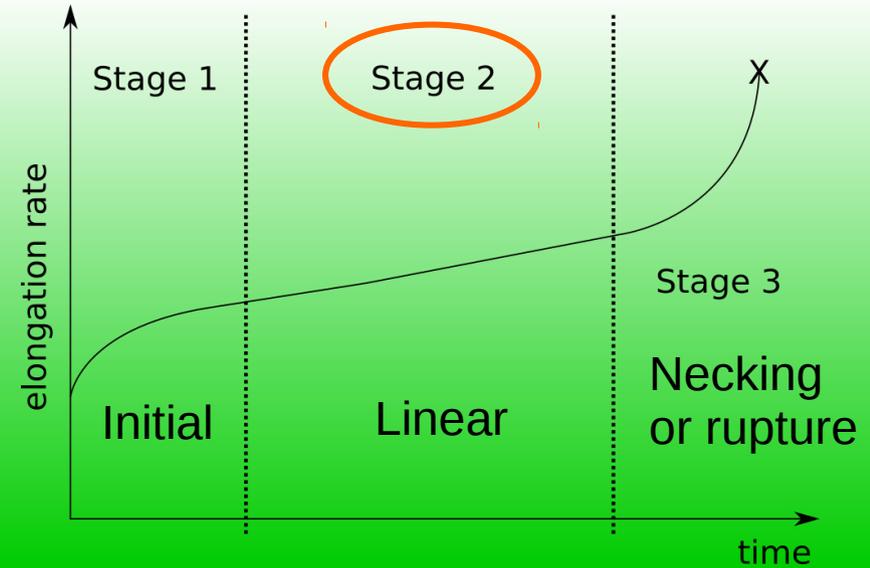


The variation of 43 μm can be easily absorbed by the glue layer between the connector and the midplate

Reliability tests of the solder joint

1 - “Creep is the plastic deformation of a material at very low mechanical stress levels”

- **Very temperature and load dependent**
- **Relevant when the temperature > 50 % of melting temperature of the material**
- **Typically, it is a very slow phenomena (might take years or more)**



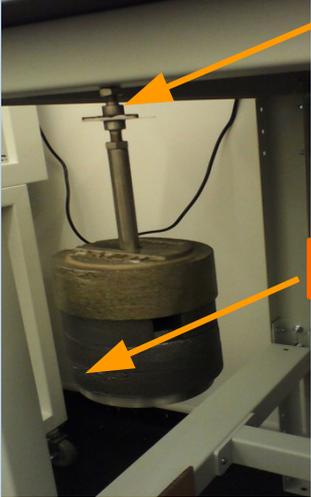
2 - “Fatigue is the weakening of the material due to repeatedly applied load.”

The cracks found in the asphalt after temperature and pressure cycles are a good example



Creep testing of the solder joint

Simple creep test is done with weight at room temperature



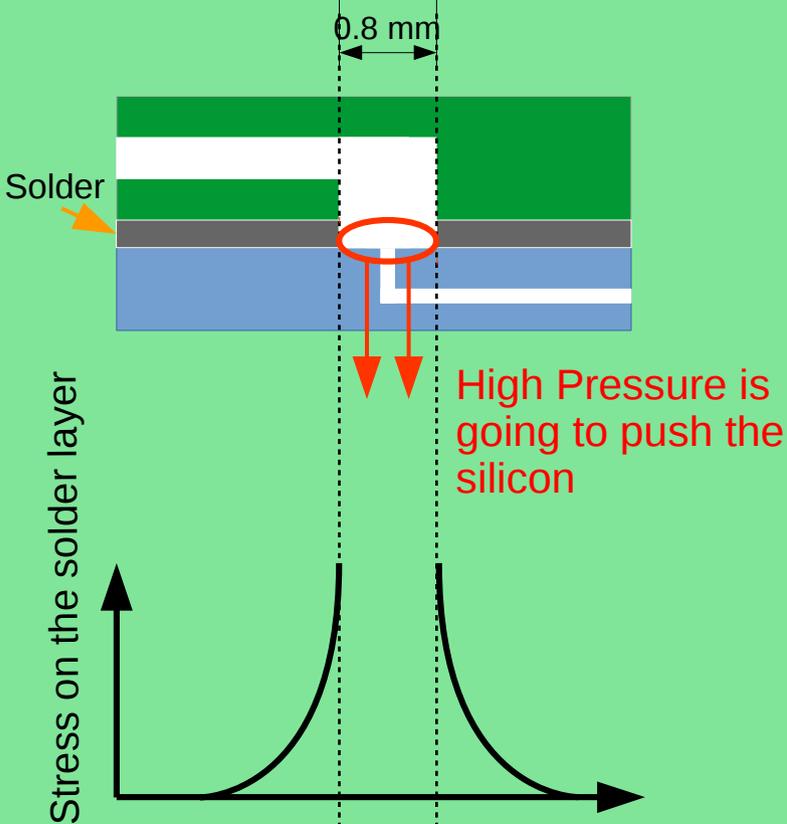
Sample

~2.5 years

8 kg

At nominal conditions, the pressure of the CO2 will be around 20 bar. This corresponds to a force of ~ 28 N pushing the silicon away.

Realistic case

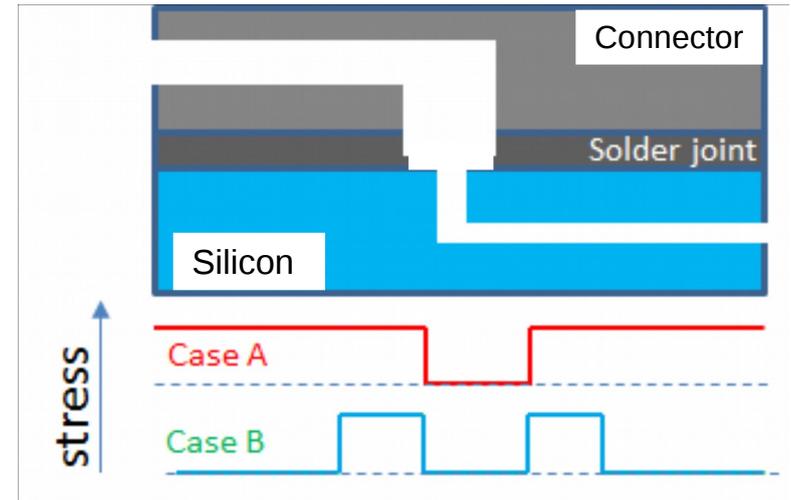
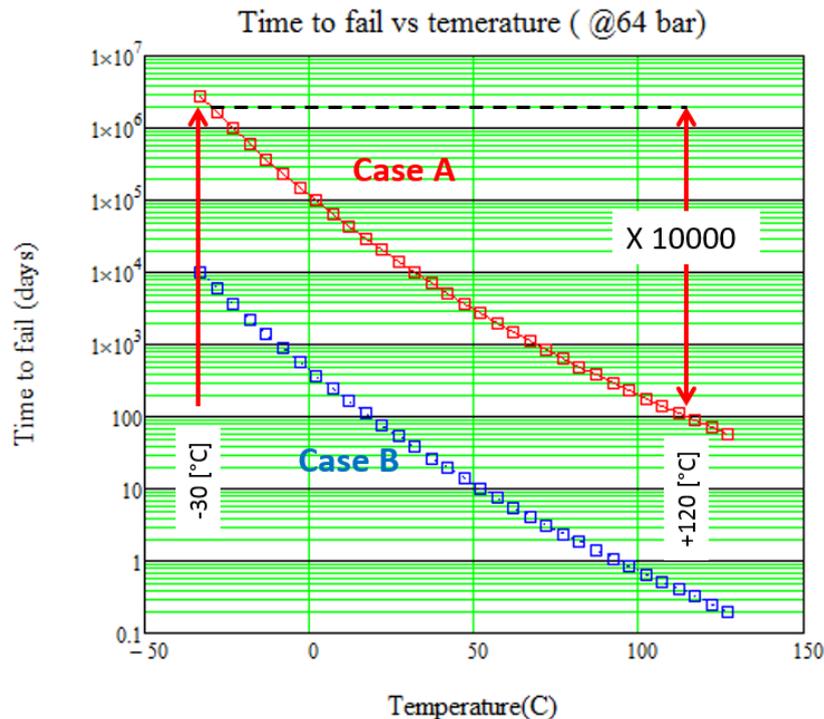


Accelerated creep modelling

The model based on [1] can only predict the behaviour at the linear stage.

Based on this model, we want to estimate the acceleration factor using higher temperatures and loads.

The failure is defined as 1% (arbitrary) of elongation



Two load cases:

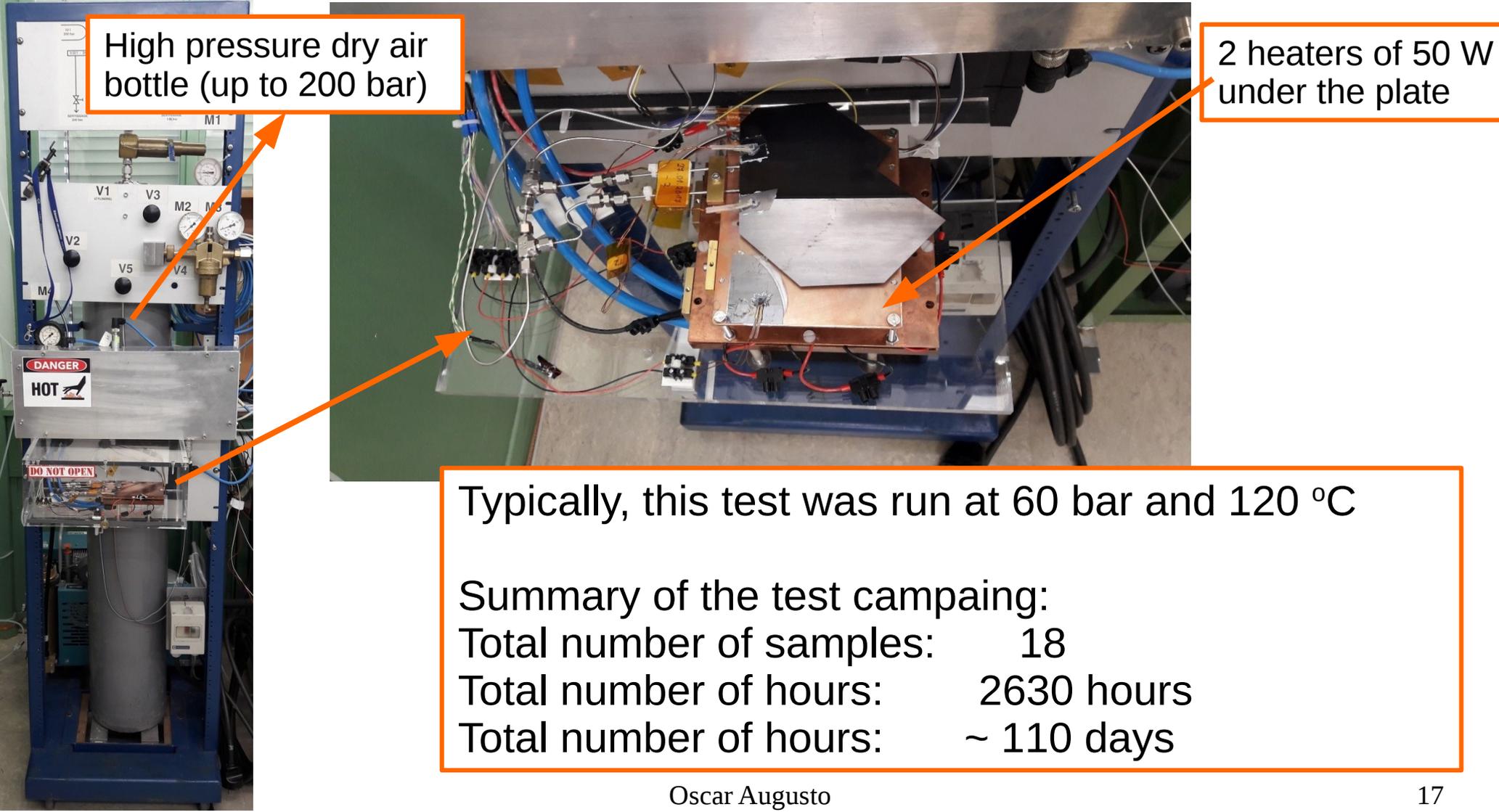
case A – The stress is uniformly distributed over the solder layer

case B – The stress is concentrated in the region close to the input/output

Changing the temperature from nominal (-30°C) to +120°C, the time to fail decreases by a factor 10000 (1h → ~ 1 year)

[1] - "A new creep constitutive model for eutectic solder alloy". Shi, Wang, Zhou, Pang, Yang. Transactions of the ASME page 84, Vol124, June 2002.

Creep test



High pressure dry air bottle (up to 200 bar)

2 heaters of 50 W under the plate

Typically, this test was run at 60 bar and 120 °C

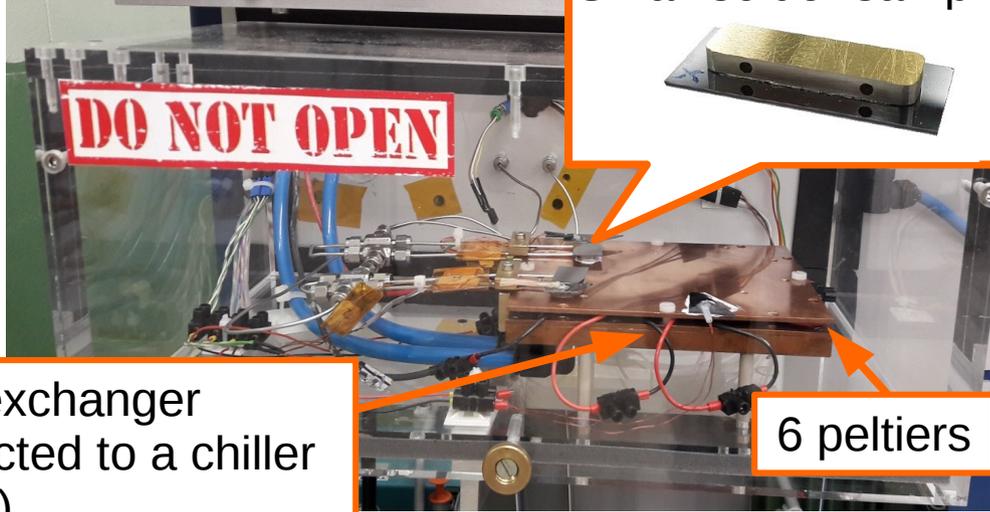
Summary of the test campaigning:

Total number of samples: 18

Total number of hours: 2630 hours

Total number of hours: ~ 110 days

Fatigue test of the solder joint



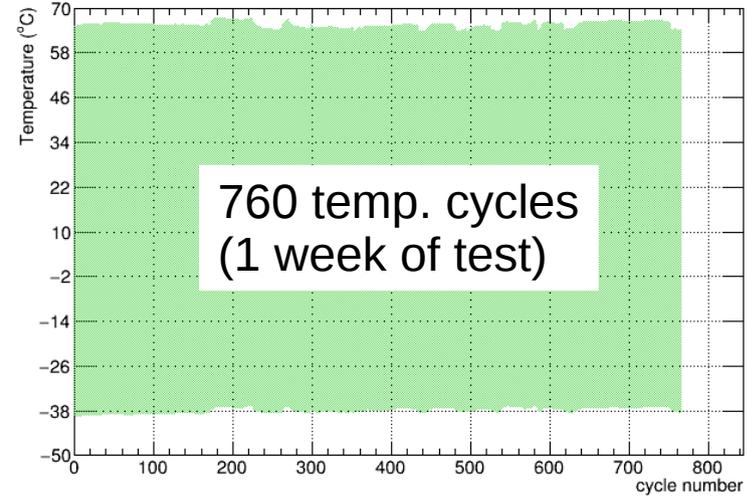
Small solder samples



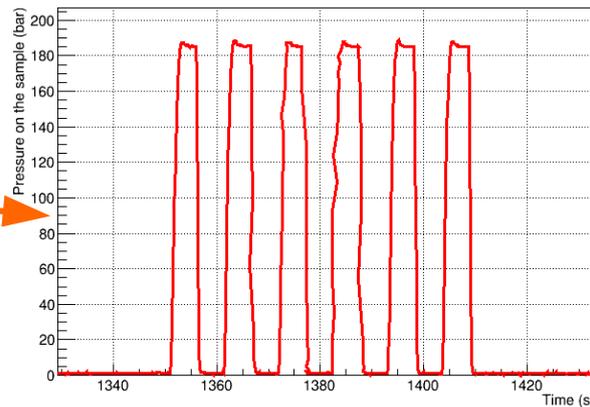
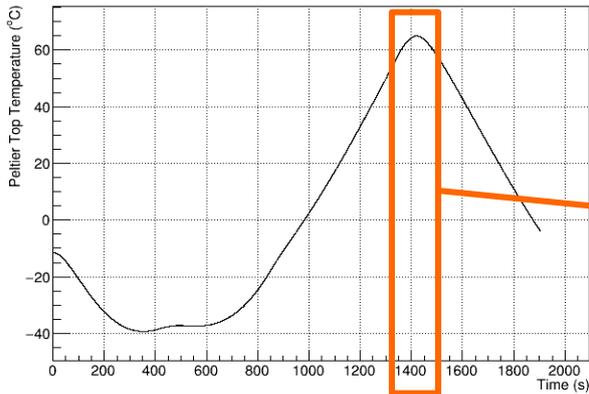
Heat exchanger connected to a chiller (-17°C)

6 peltiers

Max and Min Temperature on the Sample_S74_S75

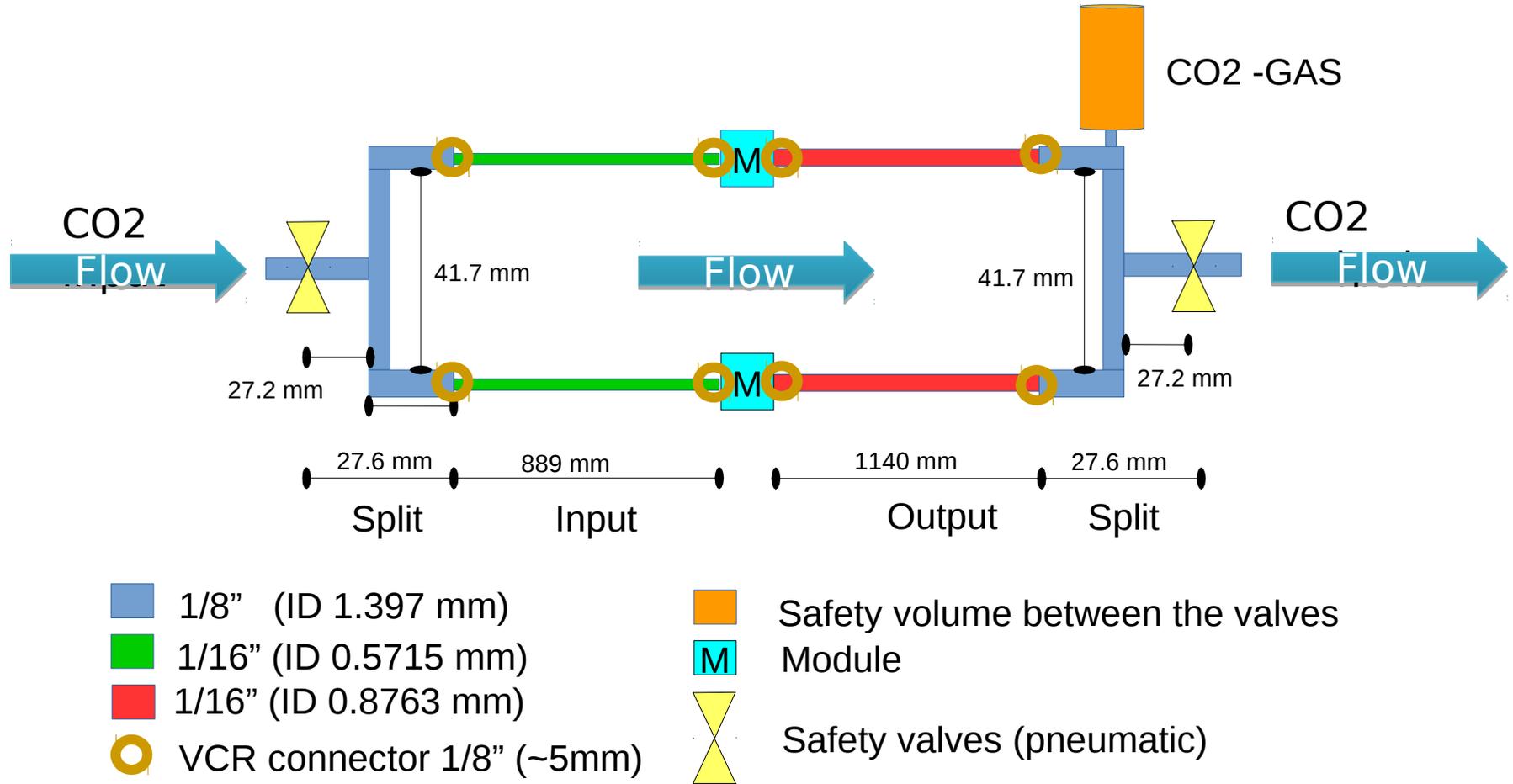


Simultaneous temperature cycles and pressure cycles

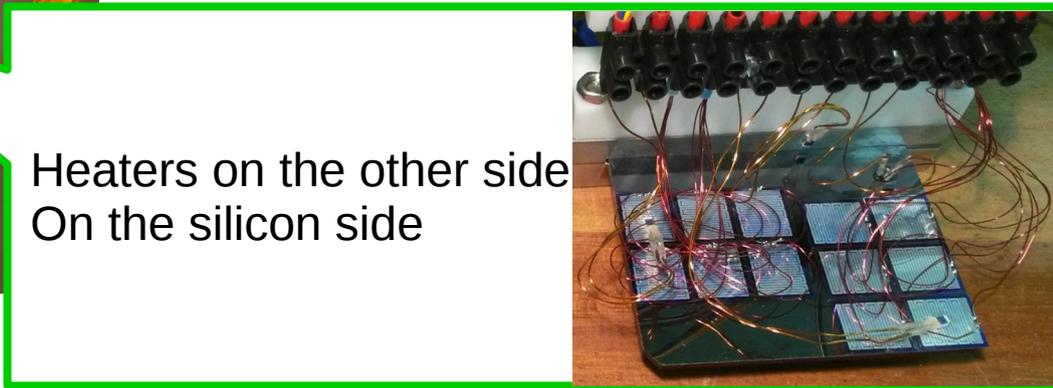
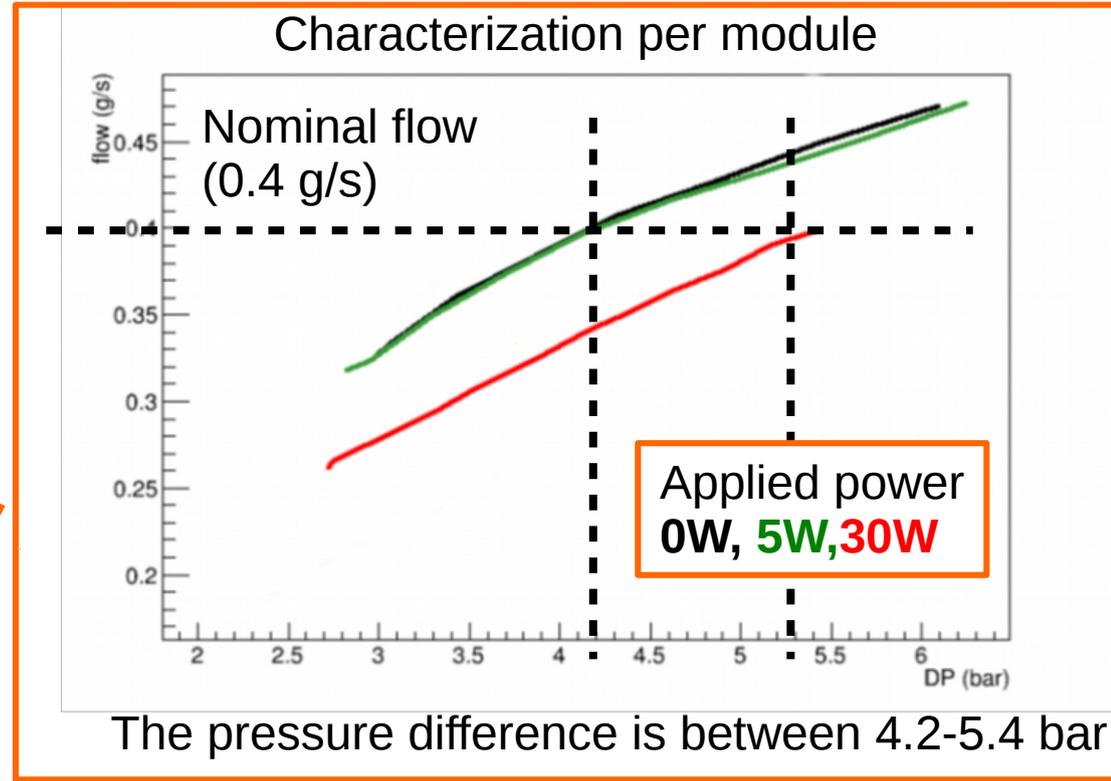
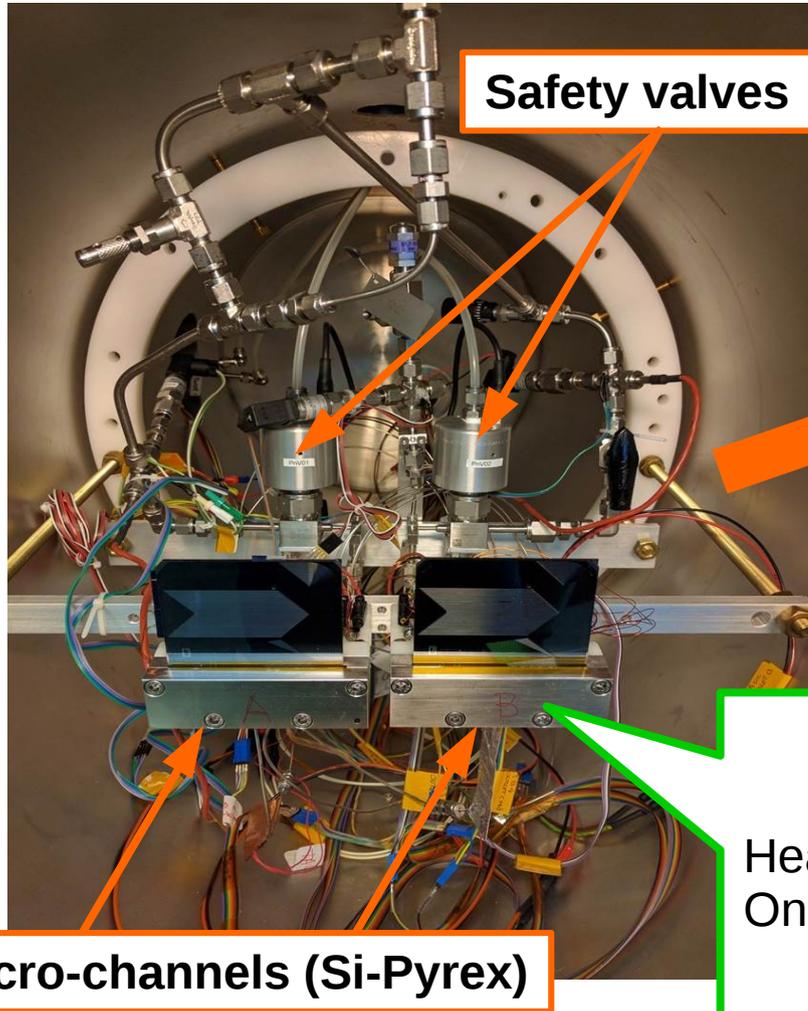


Summary of tests:
Samples: 9
Total number of temp. cycles: 5232

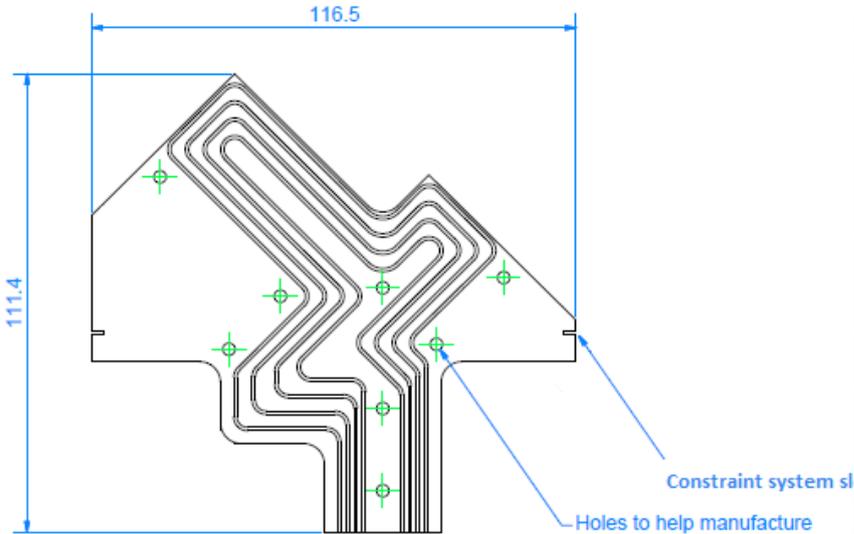
Plan-A: Fluidic characterization at -25C



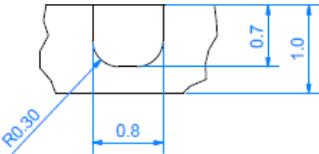
Plan-A: Fluidic characterization at -25C



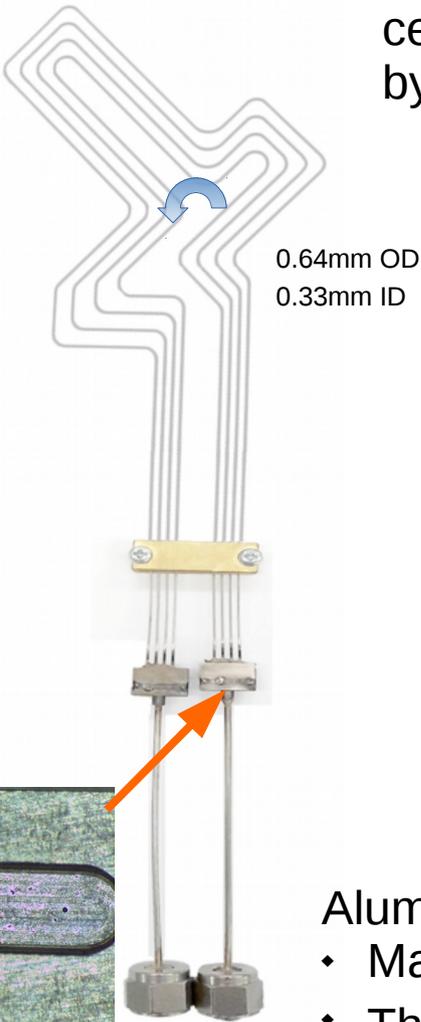
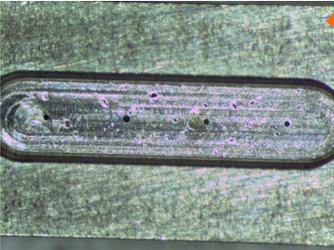
Tubes embedded in ceramics



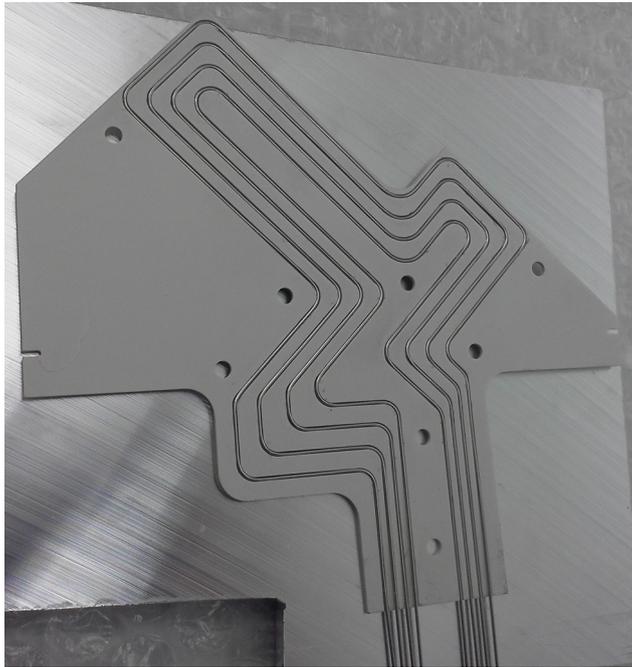
Detail of sheet thickness and channels



Orifices (125 +/- 5 μm) in the input trigger the boiling of the CO₂ and prevent instabilities among the channels



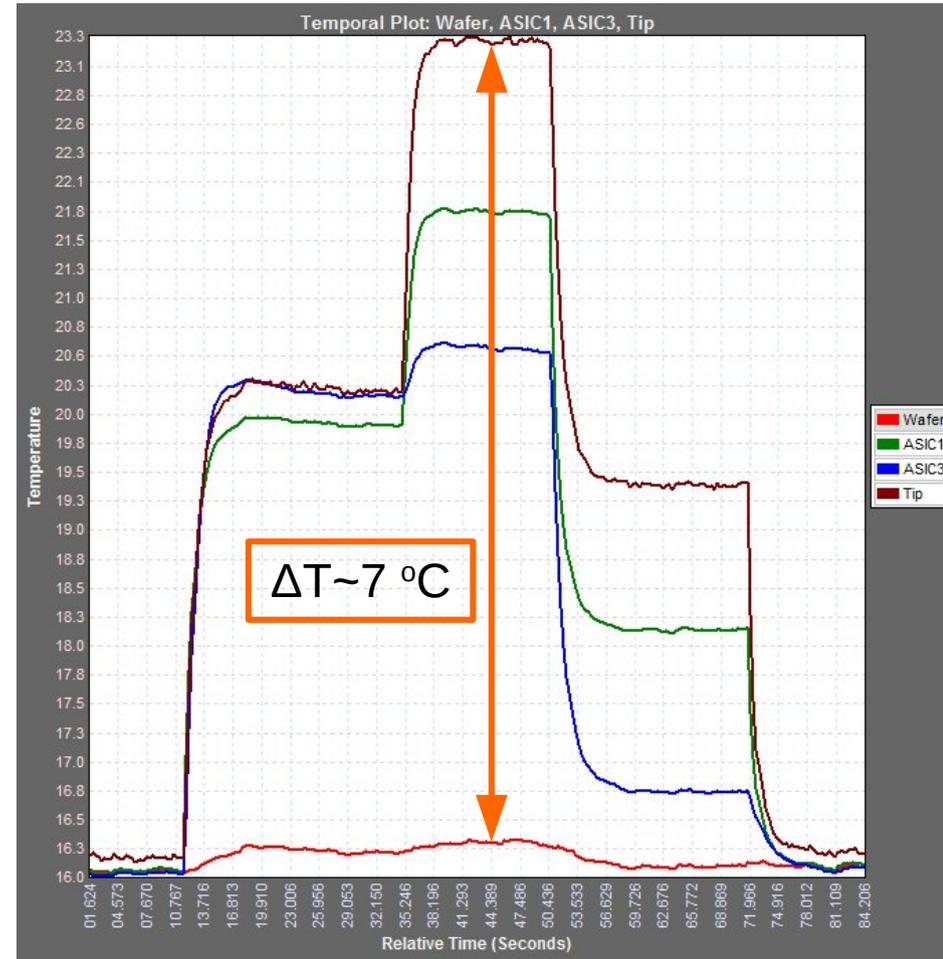
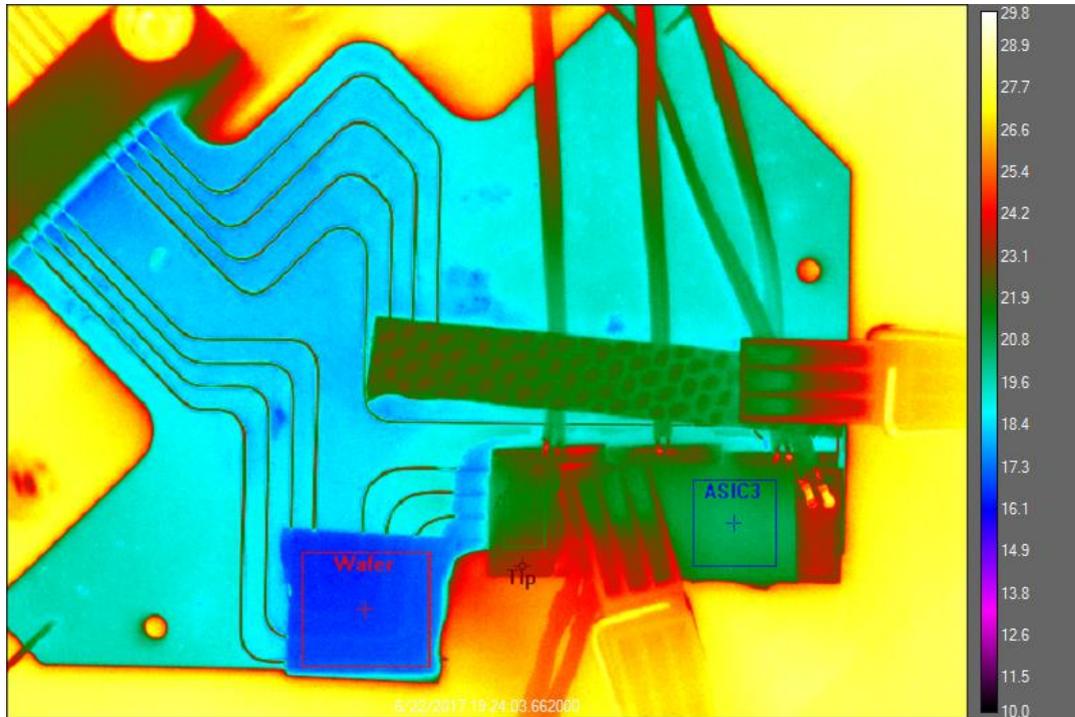
Tubes are fixed in the trenches on the ceramic with glue previously applied by robot (122-39 (SD) – 3.5 W/mK)



- Aluminum Nitride (Shapal):
- Machinable ceramic
 - Thermal expansion coefficient: 4.8×10^{-6}
 - Thermal conductivity: 92 W/m°C

Cooling performance

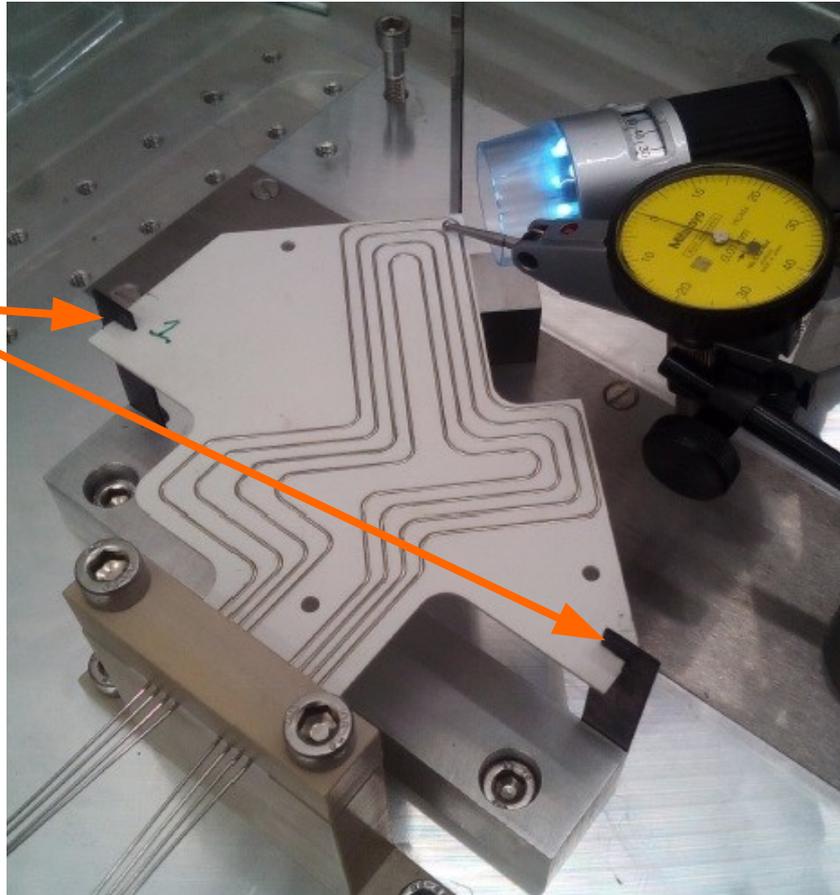
Cooling performance was evaluated with $\frac{1}{4}$ of the system glued with Stycast: 3 ASICs mockups + 1 sensor mockup (3 x 2W + 1W)



The temperature of the output CO₂ was 15 °C. Therefore, the max DT is around $\sim 8^\circ\text{C}$.

Deflection measurement

Carbon fiber
constraint system

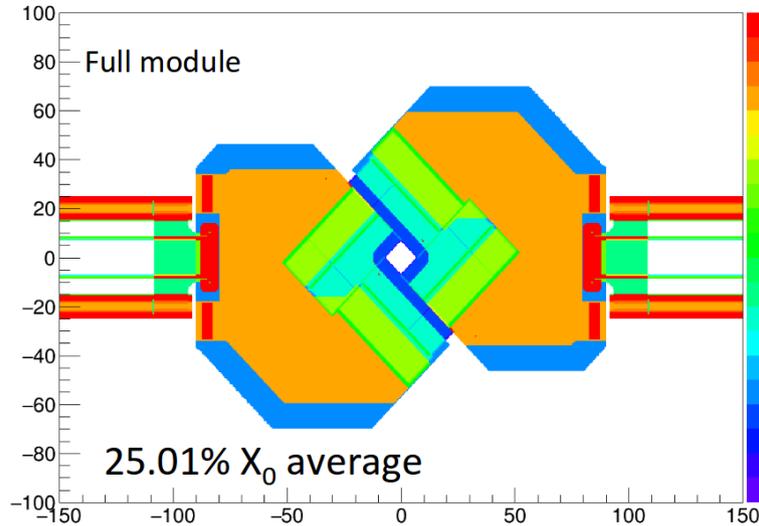


Thermal expansion coefficients
Shapal - $4.8 \times 10^{-6} / \text{K}$
Stainless steel - $16 \times 10^{-6} / \text{K}$

Deflections are $< 100 \mu\text{m}$ due
to the variations of temperature

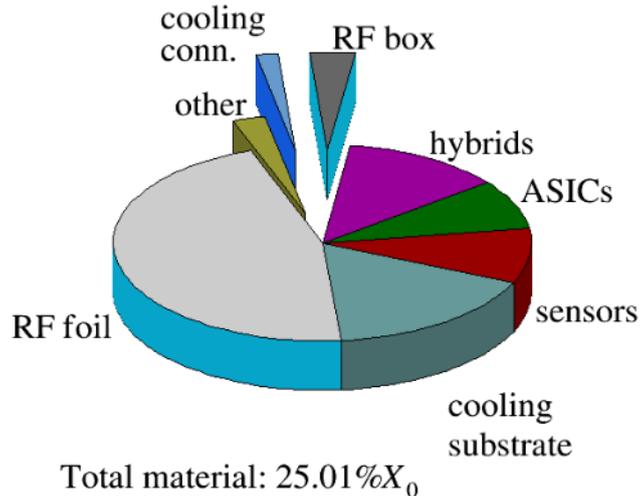
Comparison of the material budget

Microchannels

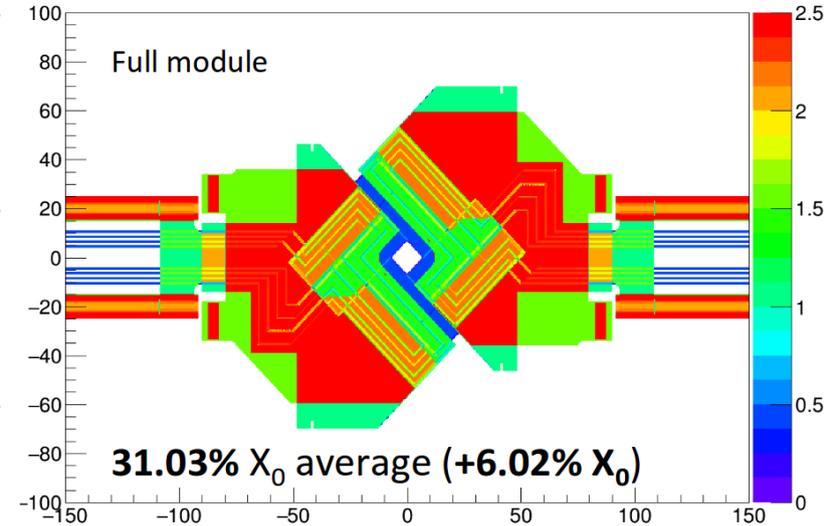


Plan-A

LHCb simulation

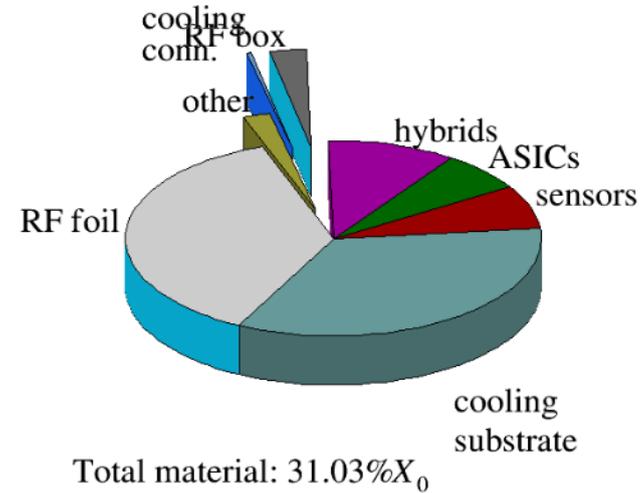


Tubes embedded in Ceramics



Plan-B

LHCb simulation



Ti 3D printing

Key features:

Material: grade 2 Ti

Easier to handle (compared to Si)

Easy to weld

Cheap (~250 EUR excluding welding)

Fast turnaround for design changes (few weeks)

Fast production: 25/batch, 1 batch/ few days

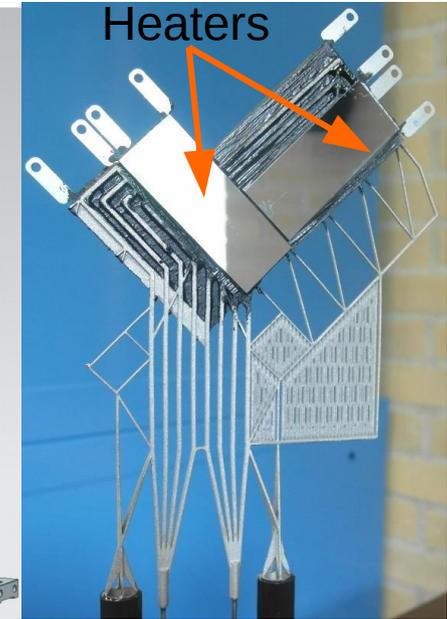
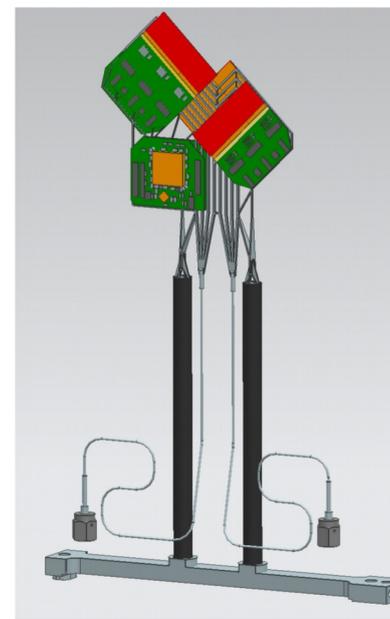
Restrictions can be integrated in the inlet

(0.35 mm x 0.35 mm x 40 mm)

Disadvantages:

Low thermal conductivity (16 W/m K)

CTE mismatch (6 ppm/K)



- ✓ High pressure test (up to 250 bar)
- ✓ Leak tight (at least 250 μm wall)
- ✓ Deflection due to temperature variations ($< 100 \mu\text{m}$)

Work on going:

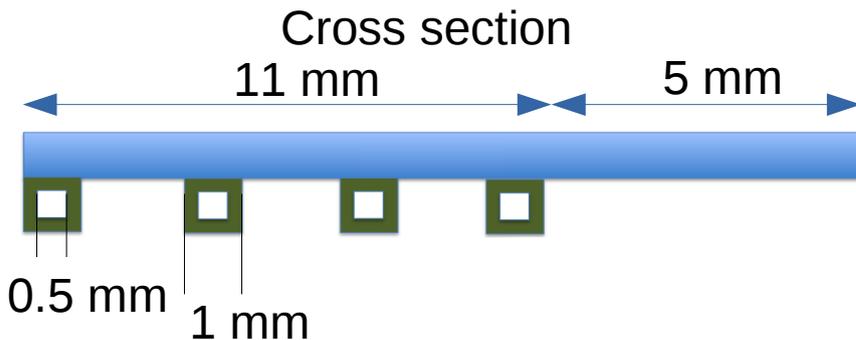
Glue layer

Thermal simulation

Cooling performance

Flatness

Reproducibility



Conclusion

1) Micro-channels

- ◆ Better physics performance due to less material
- ◆ No CTE mismatch between the substrate and electronics
- ◆ No fatigue or accumulated stress effects were observed by doing cyclic tests
- ◆ First micro-channel successfully soldered

2) Back-ups are designed to match the micro-channels fluidic characteristics and easier to handle

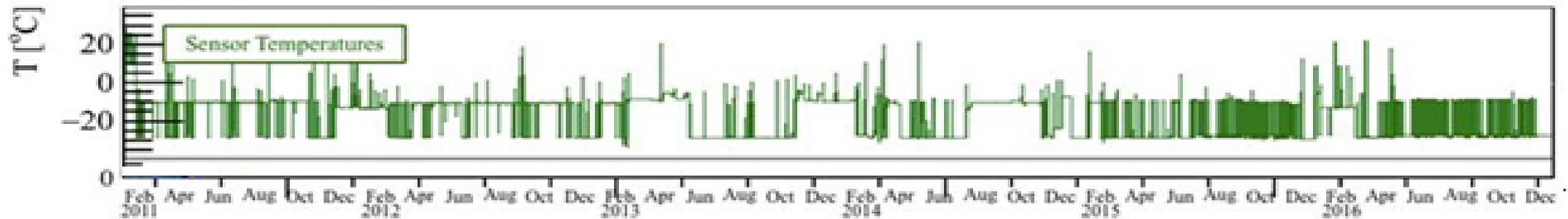
- ◆ Tubes embedded in ceramics:
 - ◆ Good cooling performance
- ◆ Ti 3D printing
 - ◆ Fast prototyping and cheaper

These technologies will be reviewed on September 28th and the decision will be taken shortly after

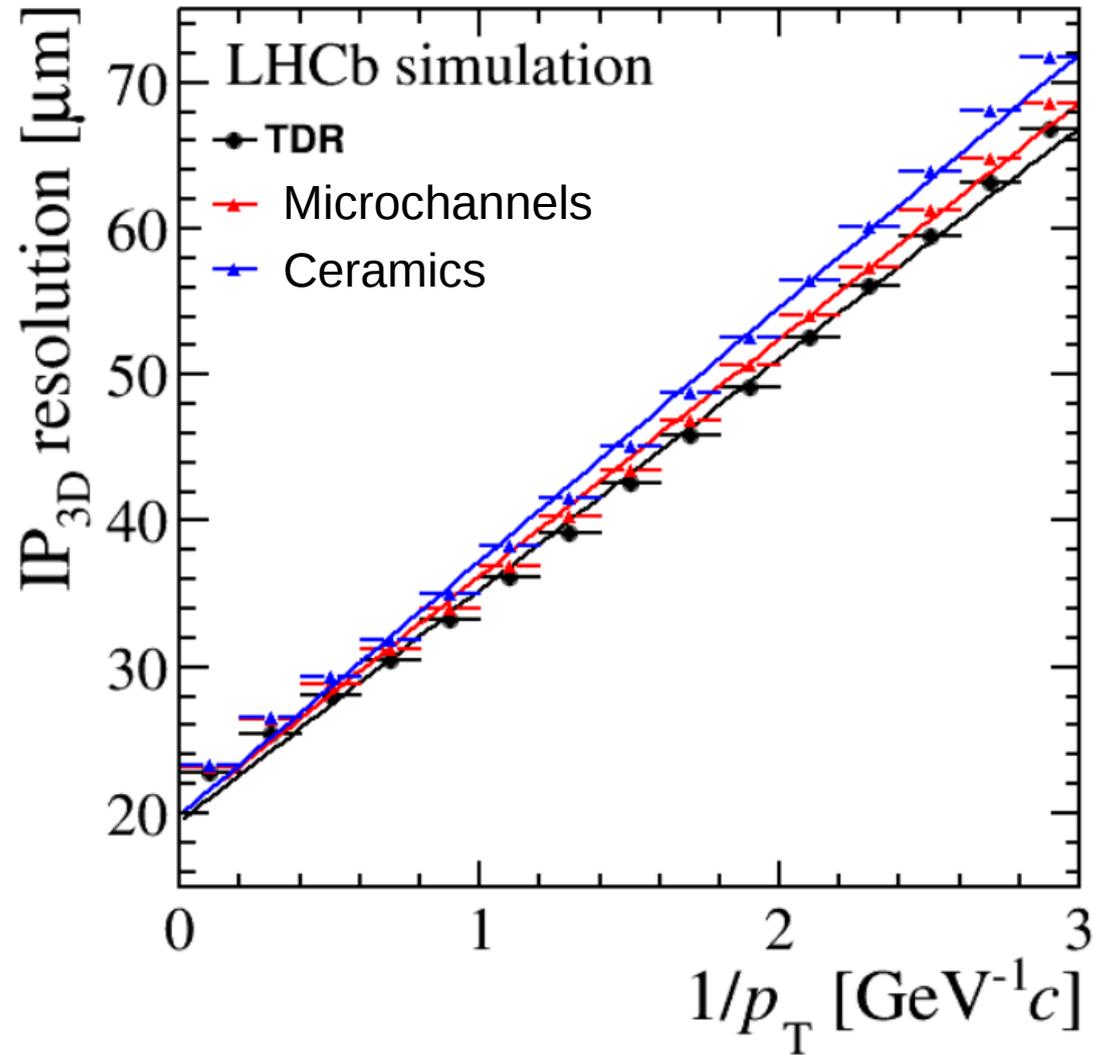
Backup slides

Fatigue of the solder joint

the current VELO endured 200-300 temperature and pressure cycles between 2011 until the end of 2016



Comparison of the impact parameter resolution



Microchannels manufacturing



DRIE etching of channels



Si - Si direct bonding



Thinning



Plasma etching of fluidic inlets



Metalization for soldering connectors