



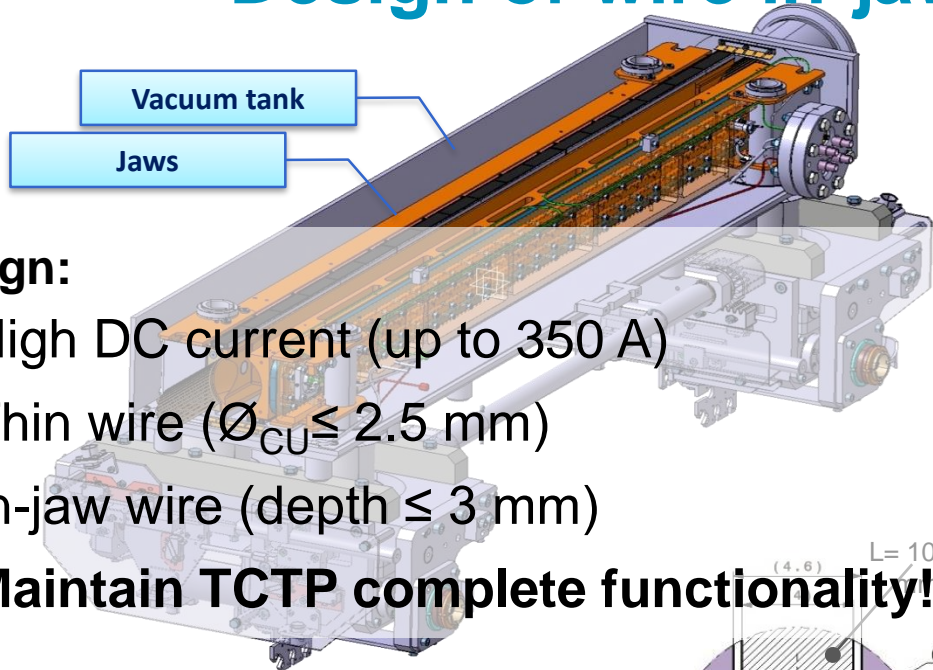
## Wire: logic of interlock

A. Rossi on behalf of (alphabetical):

*BE-ABP, BE-BI, BE-OP, EN-MME, EN-ACE, EN-STI, TE-EPC, TE-VSC*

*144<sup>th</sup> MPP meeting, 07 April 2017*

# Design of wire in-jaw collimator

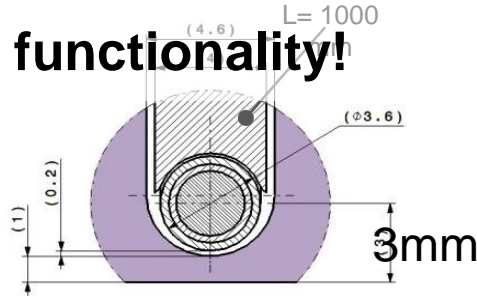
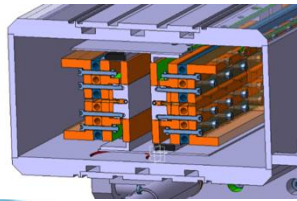


Vacuum tank

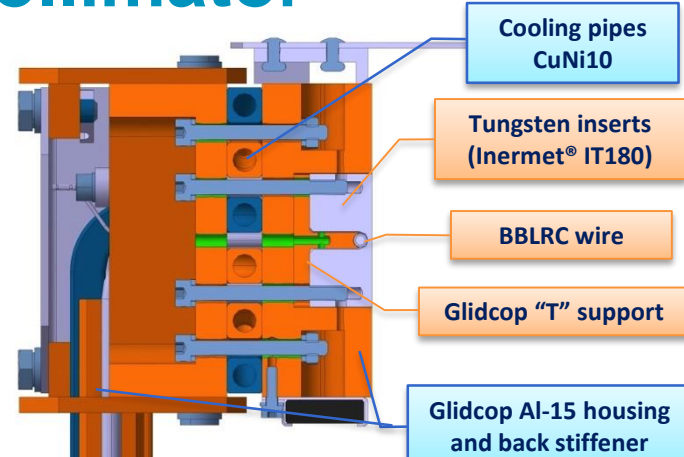
Jaws

## Design:

- High DC current (up to 350 A)
- Thin wire ( $\varnothing_{\text{Cu}} \leq 2.5 \text{ mm}$ )
- In-jaw wire (depth  $\leq 3 \text{ mm}$ )
- Maintain TCTP complete functionality!**



L. Gentini (EN-MME) & O. Aberle (EN-STI)



Cooling pipes  
CuNi10

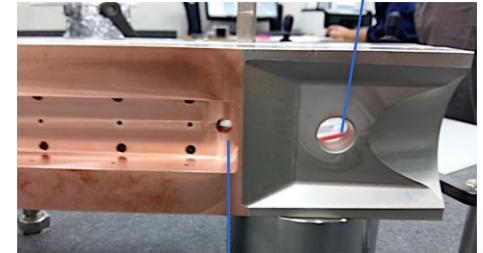
Tungsten inserts  
(Inermet® IT180)

BBLRC wire

Glidcop "T" support

Glidcop Al-15 housing  
and back stiffener

BPM button housing



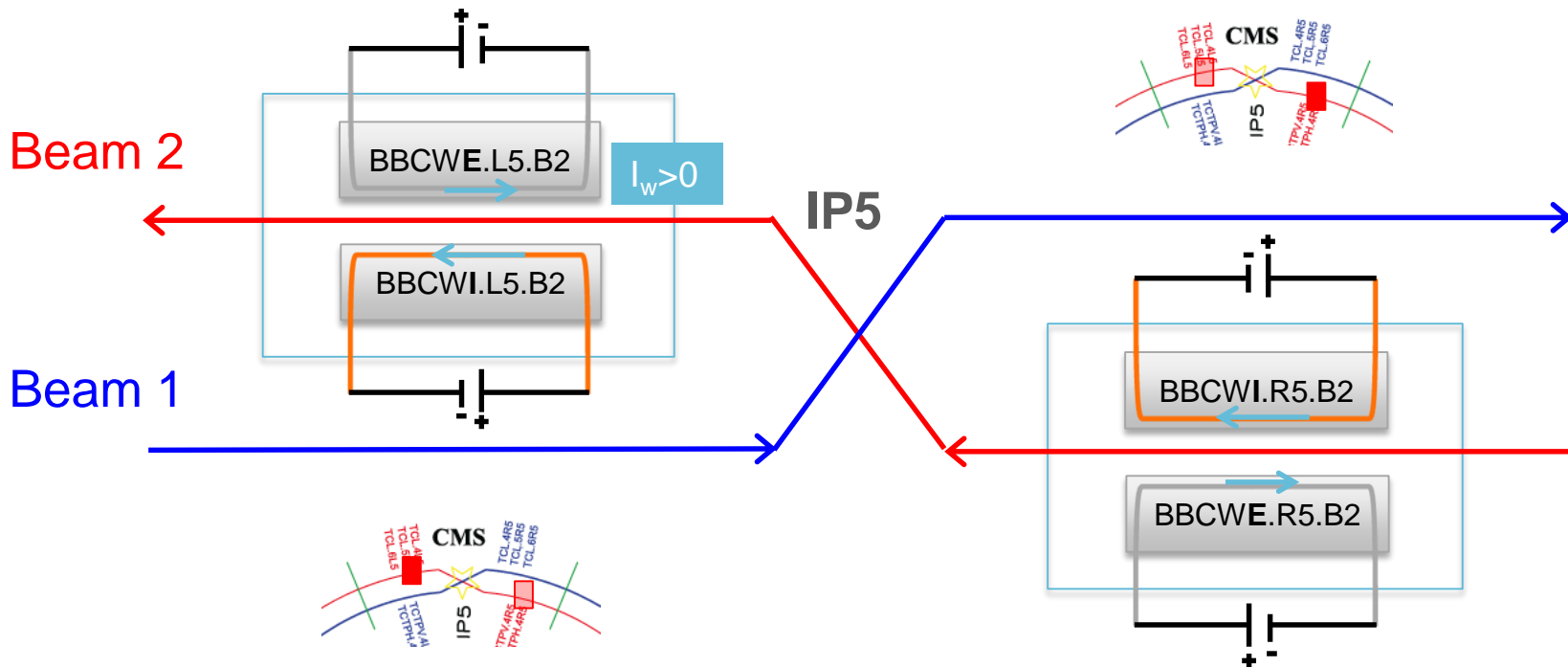
Holes for wire

# In-jaw wire collimators installed during EYETS

2016-17

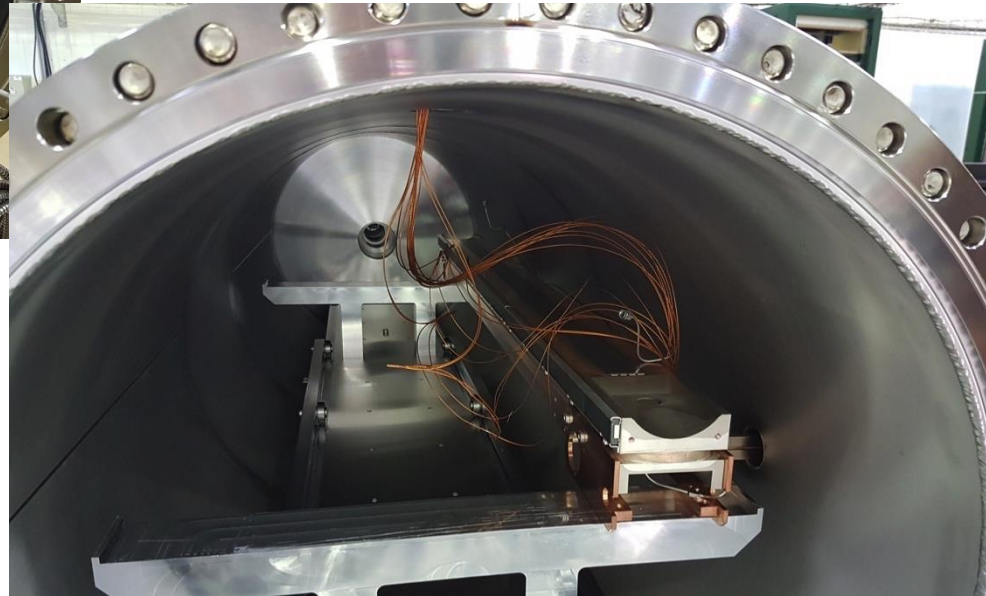
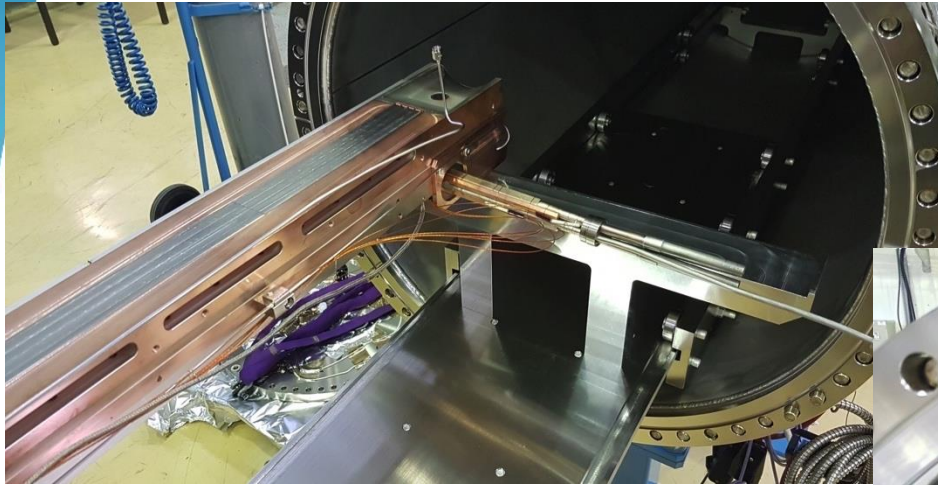
TCL.4L5.B2

TCTPH.4R5.B2



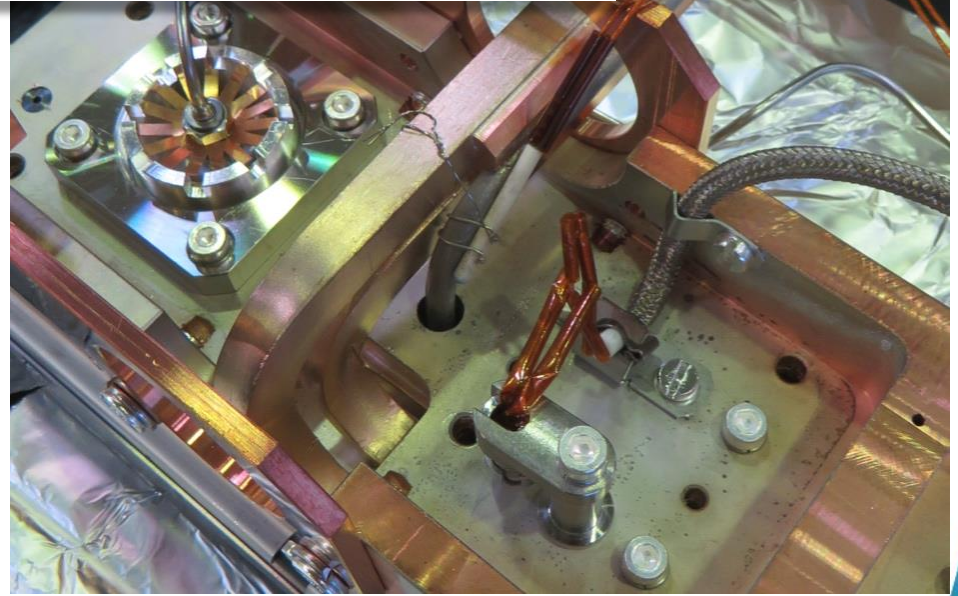
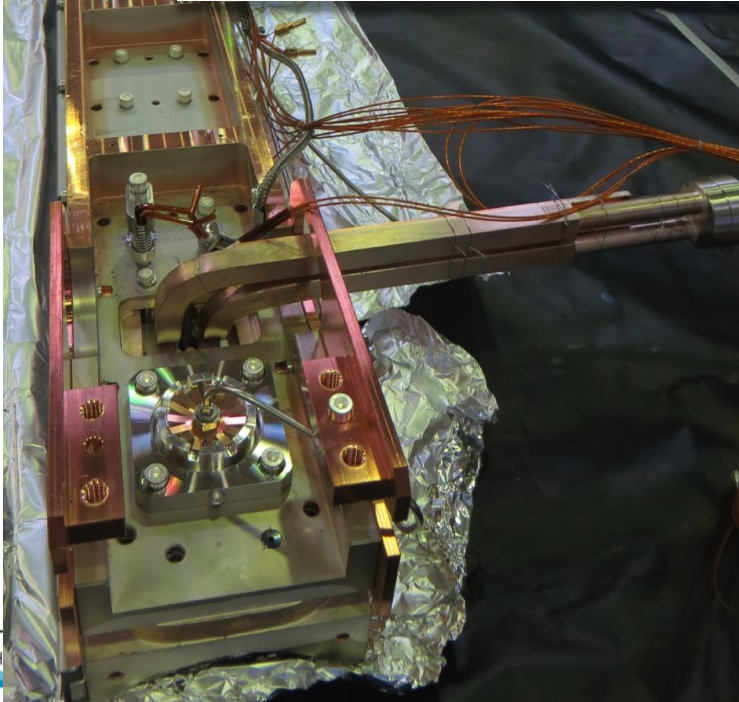
Polarity set for LRBB compensation

# Prototype jaw for lab tests



- $U_w = R_w(T_w) \times I$
- Lab: measure  $U_w$  and  $T_w$  as  $f(I)$
- Tunnel: Measure  $U_w$  to infer  $T_w$

- ✧ T1 et T5 : standard TCTP sensors on back-stiffener
- ✧ T2 et T6 : wire elbows just outside jaw
- ✧ T3 et T7 : wire on cooling tube
- ✧ T4 et T8 : next to flange brazing



# Wire current and tension with cooling

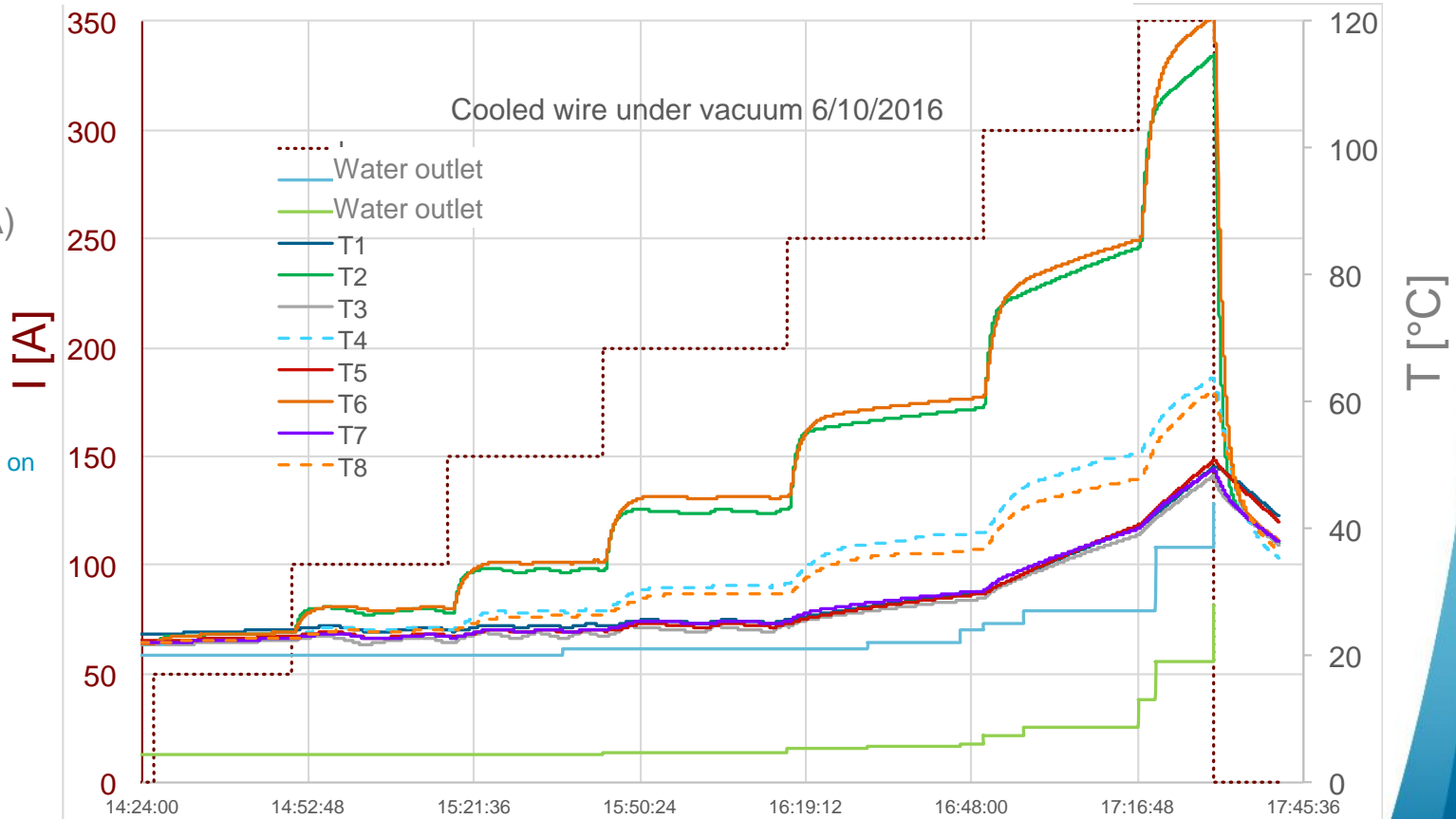
Measurements confirmed by simulations (~180°C @ 350A)

-T1 et -T5 : standard TCTP sensors on back-stiffener

-T2 et -T6 : wire elbows just outside jaw

-T3 et -T7 : wire on cooling tube

--T4 et --T8 : next to flange brazing



# All temperature at 100A – no cooling

## hottest part wire under vacuum, not in contact with jaw

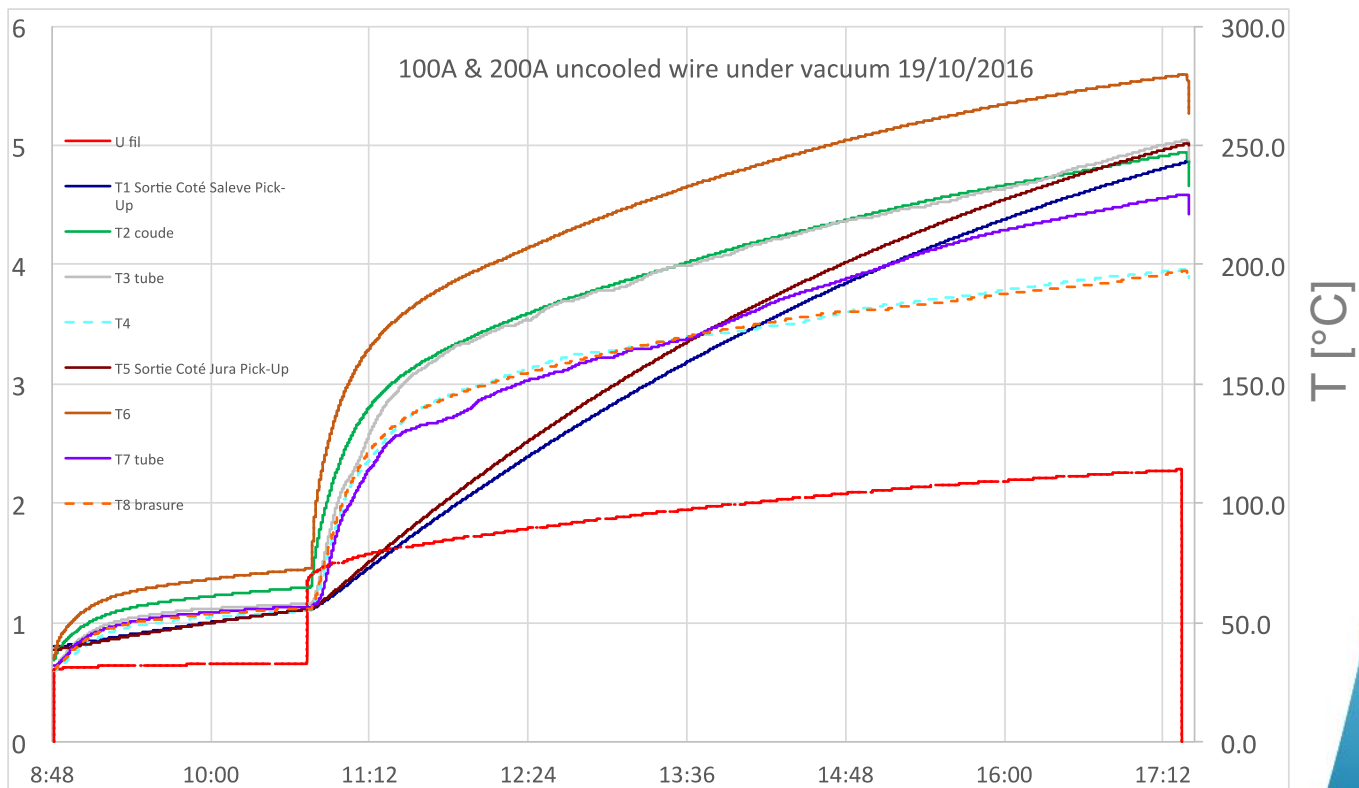
-T1 et -T5 :  
standard TCTP sensors  
on back-stiffener

-T2 et -T6 :  
wire elbows just outside  
jaw

-T3 et -T7 :  
wire on cooling tube

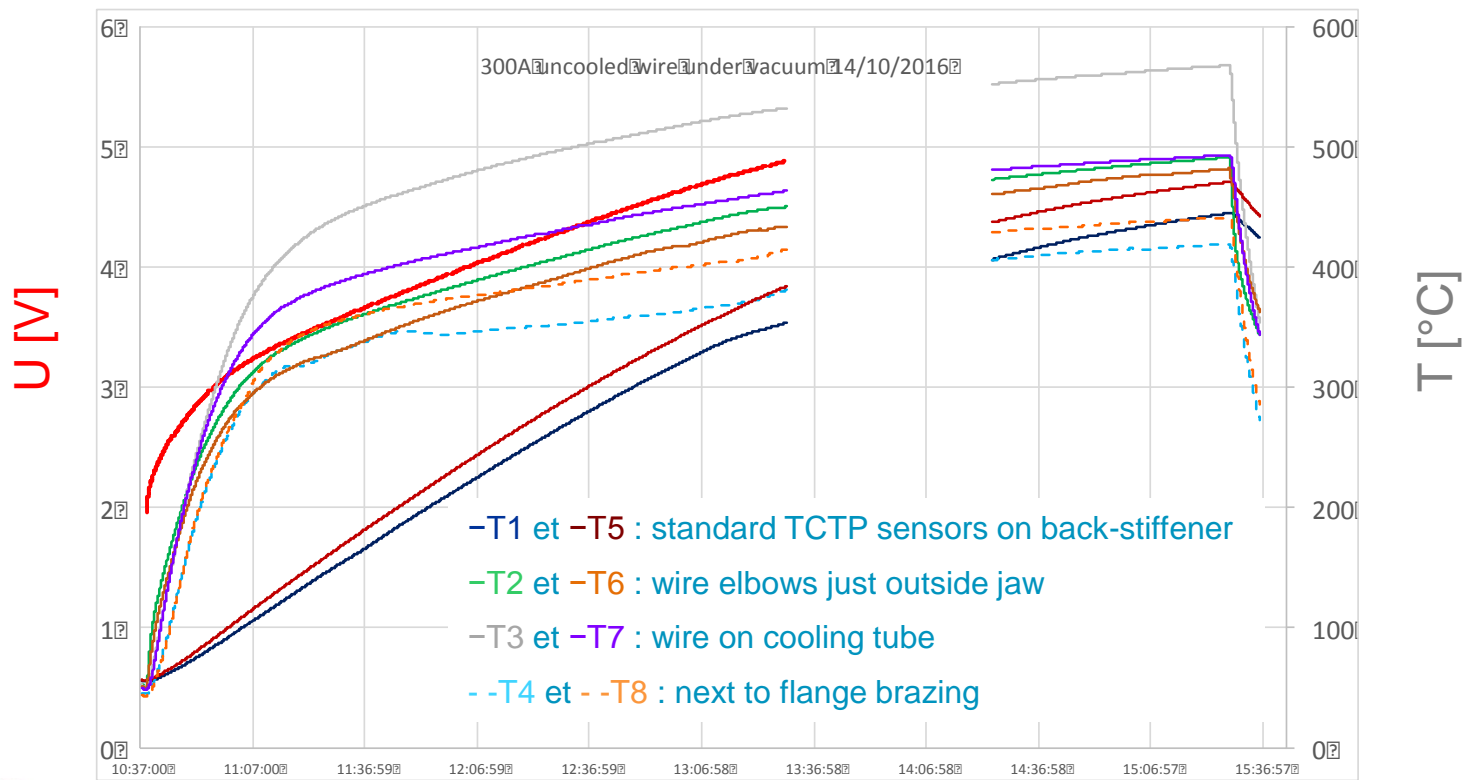
--T4 et --T8 :  
next to flange brazing

U [μm]



T [°C]

# All temperature at 300A – no cooling hottest part wire under vacuum, not in contact with jaw





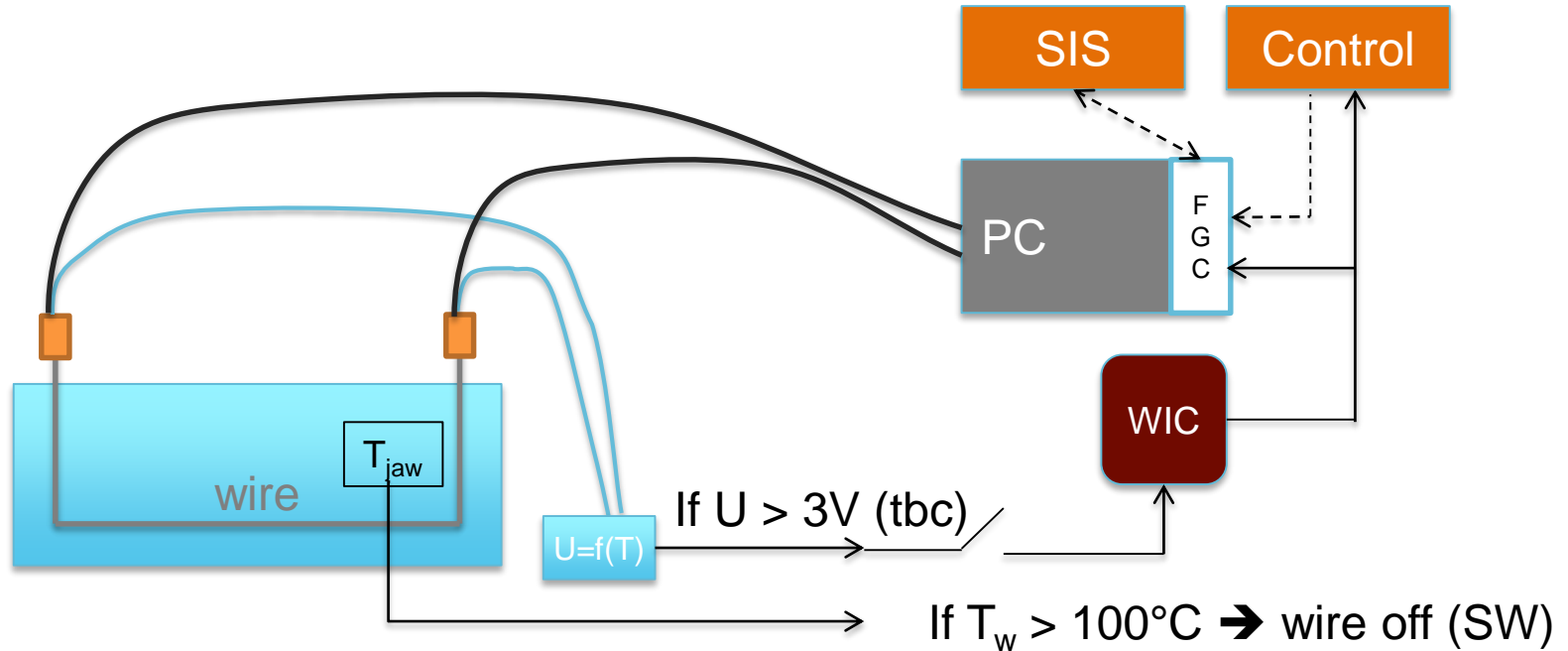
# If wire on accidentally during standard LHC operations

- The maximum kick  $<$  beam-beam effect, which so far has not caused any machine protection issues
- SIS interlock on the status of the PC

$\Delta r' = -\frac{B_w L_w}{(B\rho)}$ $B_w = \frac{\mu_0 I_w}{2\pi r}$	TCT.4R5.B2		TCL.4L5.B2	
	Injection energy	Collision energy	Injection energy	Collision energy
$\beta$ at collimator (m)	159	2148	79	772
$\sigma$ (mm)	1.08	1.04	0.76	0.62
collimator setting ( $\sigma$ )	13	9	25	15
r (mm)	17.00	12.38	21.98	12.37
B (T)	3.53E-03	4.85E-03	2.73E-03	4.85E-03
$\Delta r'$ ( $\mu$ rad) @ 300A	2.61	0.25	2.02	0.25
$\sigma'$ ( $\mu$ rad)	6.77	0.48	9.61	0.81
ratio $\Delta r'/\sigma'$	0.39	0.51	0.21	0.31

- [LHC RunII pp physics – injection, optics 2016](#)
- [LHC Run II pp physics – Collision \(0.4m\), optics 2016](#)

# Wire protection and interlocks

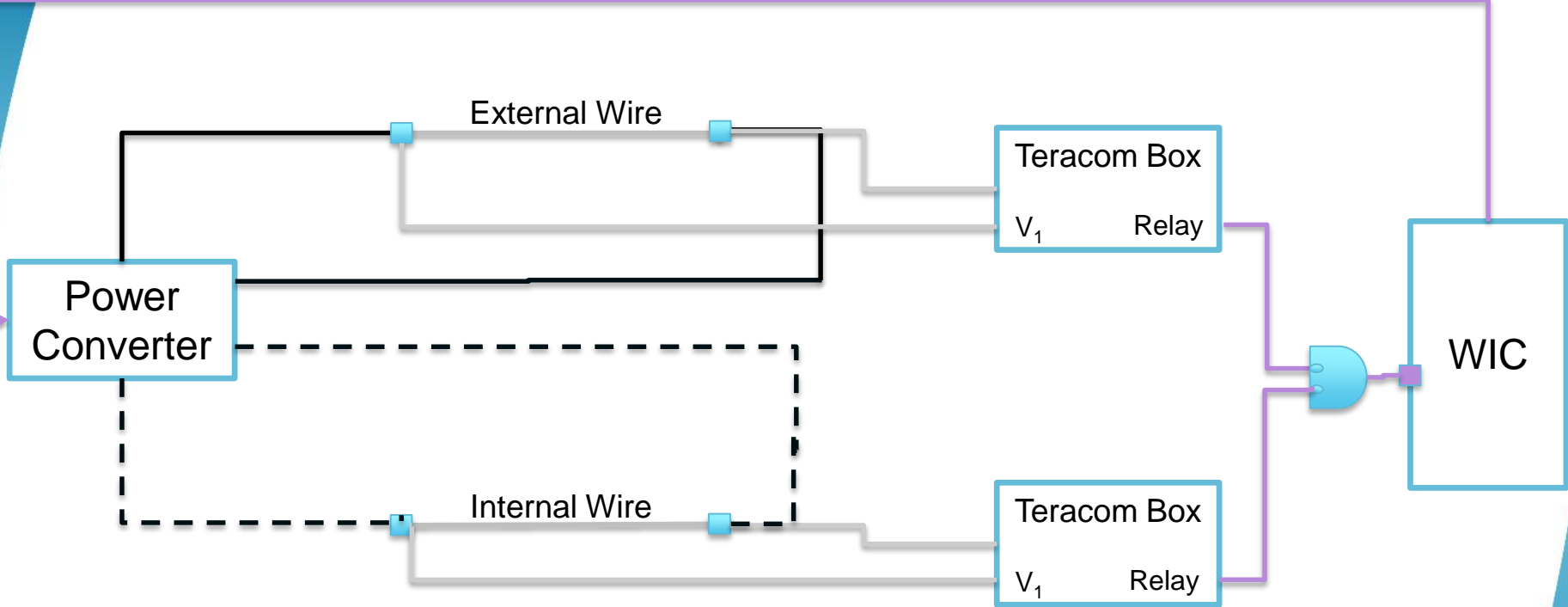


# Long-range beam-beam wire compensators - Low Level Interlocks

# Introduction

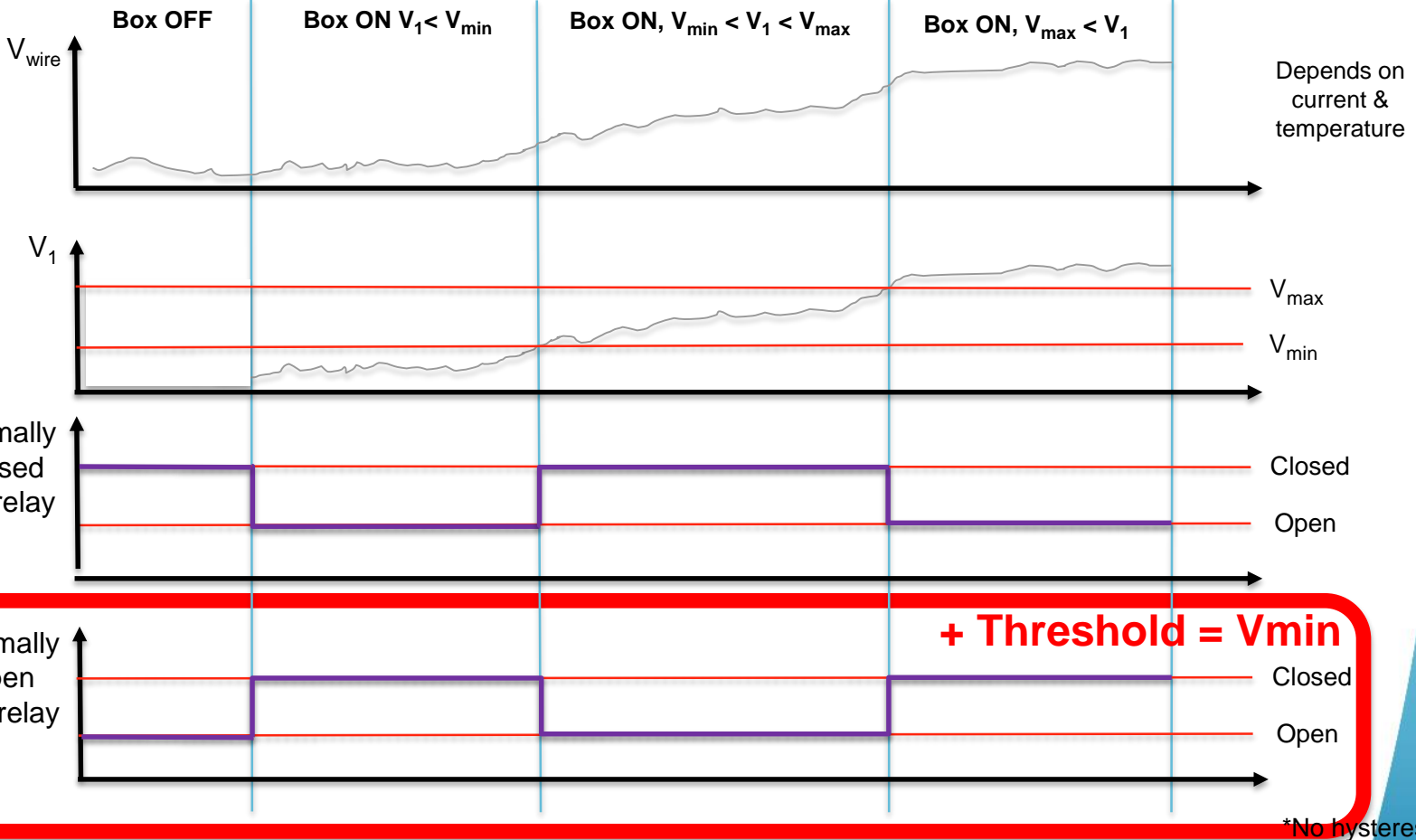
- Wires in collimator jaws used to compensate beam effects
- High currents needed
  - Temperature increase
  - Cooling system should compensate up to some point
- Need an interlock for protection
  - $V$  on wire proportional to temperature
  - Set the interlock when  $V >$  threshold
  - Failsafe

Interlock signal



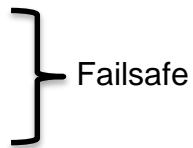
- \*Diagram represents one of the sides in P5 (L or R)
- \*The PC can only power one wire at a time (manual switch)

Teracom  
Box



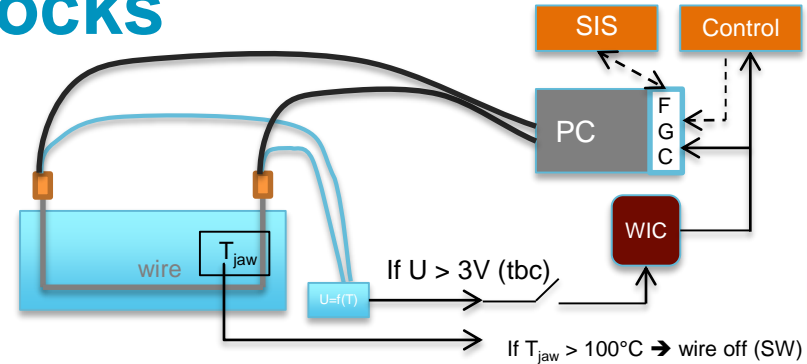
# Status

- Proposal
  - Use NO contacts
  - Vmin as threshold
  - Vmax to a non-reachable value (max 60V)
- Tests @ P5
  - Re-cabled L5 connections to use NO contacts [J. Albertone]
  - Tested successfully on 4<sup>th</sup> April
    - Wire (BBCWE.L5.B2) + PC (RPMC.USC55.RBBCW.L5B2)
    - PC permit only when  $U_w < V_{min}$
    - Box disconnection triggered PC switch off
- Potential Issues?
  - Need to have 2 Teracom boxes active even if only one wire can be used at a time
  - 4 Teracom boxes in the same enclosure (2 left side + 2 right side)
- New requirements
  - Bipolar currents
  - ...



# Wire protection and interlocks

- $U=f(T)$  unipolar + always ON
- PC polarity set by FGC (SW)
- HW interlocks works for high current
  - SIS interlock to limit  $-10 < I_w < 10A$  with beam through REMOVE\_PERMIT to PC – to be masked during MD
  - Could add a SIS interlock to restrict to unipolar range throughout the full year (e.g.  $-10A \dots 300A$ ) through REMOVE\_PERMIT to PC
  - Optimal: The SIS could read the  $T_{\text{jaw}}$  and REMOVE\_PERMIT to PC if  $T_{\text{jaw}} > 100^\circ\text{C}$
- Wire current with RBAC role to expert only
- MD procedure :
  - Check polarity of PC
  - Check sanity of box ( $V_{\text{min}} = 0$ )
  - Display all relevant signals in the CCC throughout the MD (PC current, temperatures, box reading....)





# For a mid/long-term solution (from Markus)

- We need a bipolar measuring unit, which is isolated from the measurement on the wire. Introducing a ground through the measurement device not only limits bipolar use, but bears a considerable risk if you have shorts and the power converter ground fuse blows, in which case your device will get the full current from the converter.... Is it too late to add a simple isolation amplifier before the box?
- A PLC based solution or even using a (differently) programmed quench detector (which are built for exactly such purpose) might be something worth looking into?  
**Seems to me too much**

# Hardware readiness

- Wire tests on the surface
  - Collimator under pumping (after bake-out) and with cooling on:
    - LVDTs reading when wire @ 350A : no sensitivity observed
    - Pressure when wire @ 350A :  $\sim 10^{-8}$  mbar
    - Jaw temperature  $< 50^{\circ}\text{C}$
    - Wire temperature outside collimator tank  $\sim 300^{\circ}\text{C}$  after thermal bridge adjusted
  - Both collimators installed + bake-out + standard commissioning completed
  - Wire HW tests + HW interlock completed
    - LVDTs reading when wire @ 350A : no sensitivity observed
    - Pressure when wire @ 350A + cooling  $< \text{few } 10^{-10}$  mbar
    - Jaws moved with wire @ 350A
    - Temperature increase of the jaw  $< \text{few degrees}$
    - Temperature of wire outside jaw  $\sim 150\text{-}170^{\circ}\text{C}$
    - WIC ok
    - NO interlock on WIC ok
  - Detailed presentation at CWG on 8<sup>th</sup> of May.
- Control system to be completed and commissioned



***Thank you for your attention  
and thank you to all contributors***

Possibly not all :

BE-ABP: S.Redaeli, Y.Papaphilippou, S.Fartoukh, G.Sterbini . . .

BE-BI: H.Schmickler, J.Albertone, C.Boccard, M.Gonzalez Berges, R.Jones . . .

BE-OP: M.Pojer . . .

EN-MME: A. Bertarelli, A. Dallochio, M. Garlasche, L.Gentini, F.Carra . . .

EN-STI: O.Aberle; I.Lamas Garcia; J.Lendaro; M.Di Castro . . .

EN-ACE: D.Tortrat, JF.Fuchs . . .

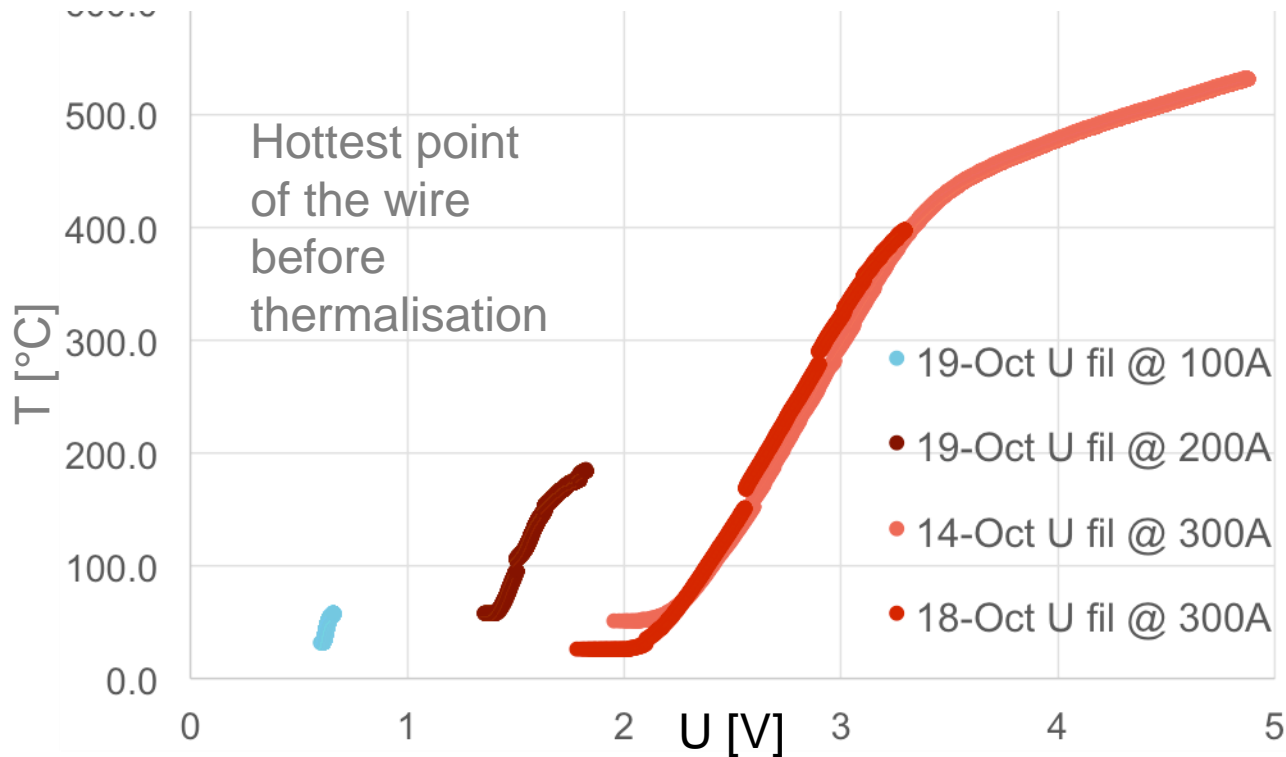
TE-EPC V.Montabonnet, C.Coupat, L.Ceccone, M.Magrans de Abril, Q.King . . .

TE-MPE: R.Mompo, D.Wollmann, M.Zerlauth, J.Uythoven

TE-VSC: G.Cattaneoz, G.Bregliozzi . . .

# Wire temperature and tension without cooling

U	=	R @ 50°C	x	I
0.63	=	6.30E-03	x	100
1.26	=	6.30E-03	x	200
1.89	=	6.30E-03	x	300
U	=	R @ 200°C	x	I
0.98	=	9.80E-03	x	100
1.96	=	9.80E-03	x	200
2.70	=	9.00E-03	x	300



By limiting the wire tension we avoid overheating in case of loss of cooling