



WIR SCHAFFEN WISSEN – HEUTE FÜR MORGEN

G. Montenero<sup>1</sup> , B. Auchmann<sup>1,2</sup> , and G. Rolando<sup>2</sup>

1) Paul Scherrer Institut

2) CERN

# 2D Sensitivity Study and Critical Tolerances of CD1 Magnet

26 June 2017

- **2D Mechanical modelling of CD1 dipole with ANSYS**
- **Design's objectives**
- **Baseline Design (+ excursus on CD2)**
- **Nominal Design vs. Material Properties**
- **Mechanical tolerances**
- **Parametric Study**
- **Conclusions**

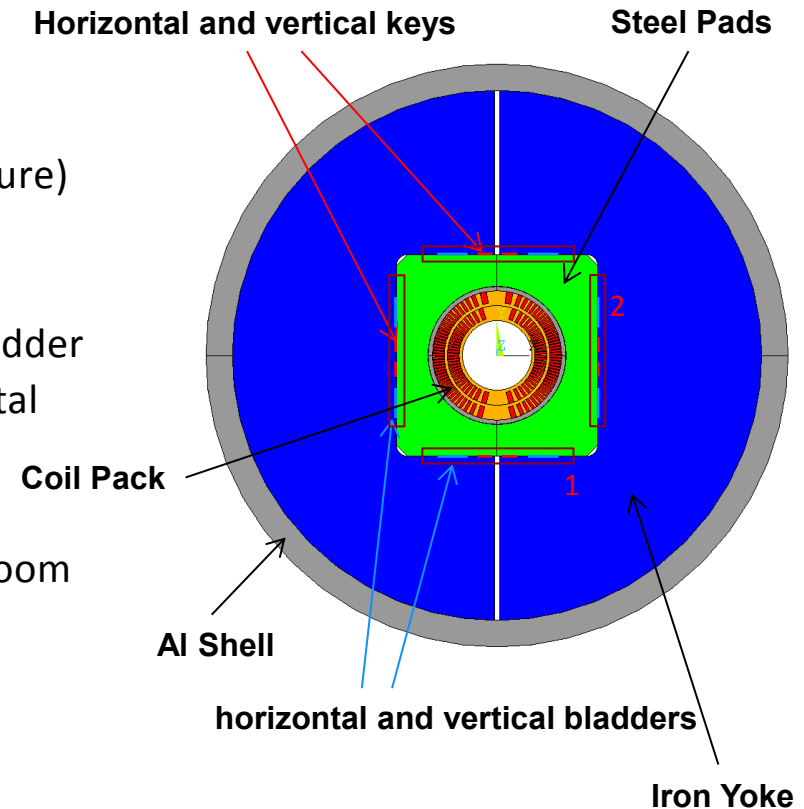
- **2D Mechanical modelling of CD1 dipole with ANSYS**
- Design's objectives
- Baseline Design (+ excursus on CD2)
- Nominal Design vs. Material Properties
- Mechanical tolerances
- Parametric Study
- Conclusions

# 2D Mechanical modelling

## Setup of the numerical simulations (ANSYS)

**The simulation is divided in 5 load steps:**

1. Vertical bladders inflation (max 40 MPa pressure) and vertical keys insertion
2. Vertical bladders deflation and horizontal bladder inflation (max 40 MPa pressure) with horizontal keys insertion
3. Horizontal bladders deflation-> assembly at room temperature
4. Cool down of the assembly to 1.9 K
5. Operation->Lorenz forces acting on the conductor according to short sample limit (1.9 K, 12 T)



- 2D Mechanical modelling of CD1 dipole with ANSYS
- **Design's objectives**
  - Baseline Design (+ excursus on CD2)
  - Nominal Design vs. Material Properties
  - Mechanical tolerances
  - Parametric Study
  - Conclusions

# Design's Objectives

## ▪ What we care the most

- Limit the maximum stress on the conductor
- Keep the maximum stress of the mandrel below 0.2% yield stress

Material	Stress limit (MPa)	
	293 K	4.2 K
<i>Coil</i>	130	130
<i>Al-Bronze</i>	250	400

- Guarantee:
  - pad/pad contact interface
  - Extra margins for steel pads configuration (using in the simulations Lorenz force maps associated to ultimate load (12 T,  $I_{ss}=20$  kA at 1.9 K))

## ▪ For the other materials of the assembly

- Aluminum for external and coil assembly shells (Al 7075)
- Ferromagnetic Iron yoke
- Steel for the pads (316LN)

Material	Stress limit (MPa)	
	293 K	4.2 K
<i>Al 7075</i>	480	690
<i>Ferromagnetic Iron</i>	180	720
<i>Austenitic steel 316LN</i>	350	1050

- 2D Mechanical modelling of CD1 dipole with ANSYS
- Design's objectives
- **Baseline Design** (+ excursus on CD2)
- The Design vs. Material Properties
- Mechanical tolerances
- Parametric Study
- Conclusions

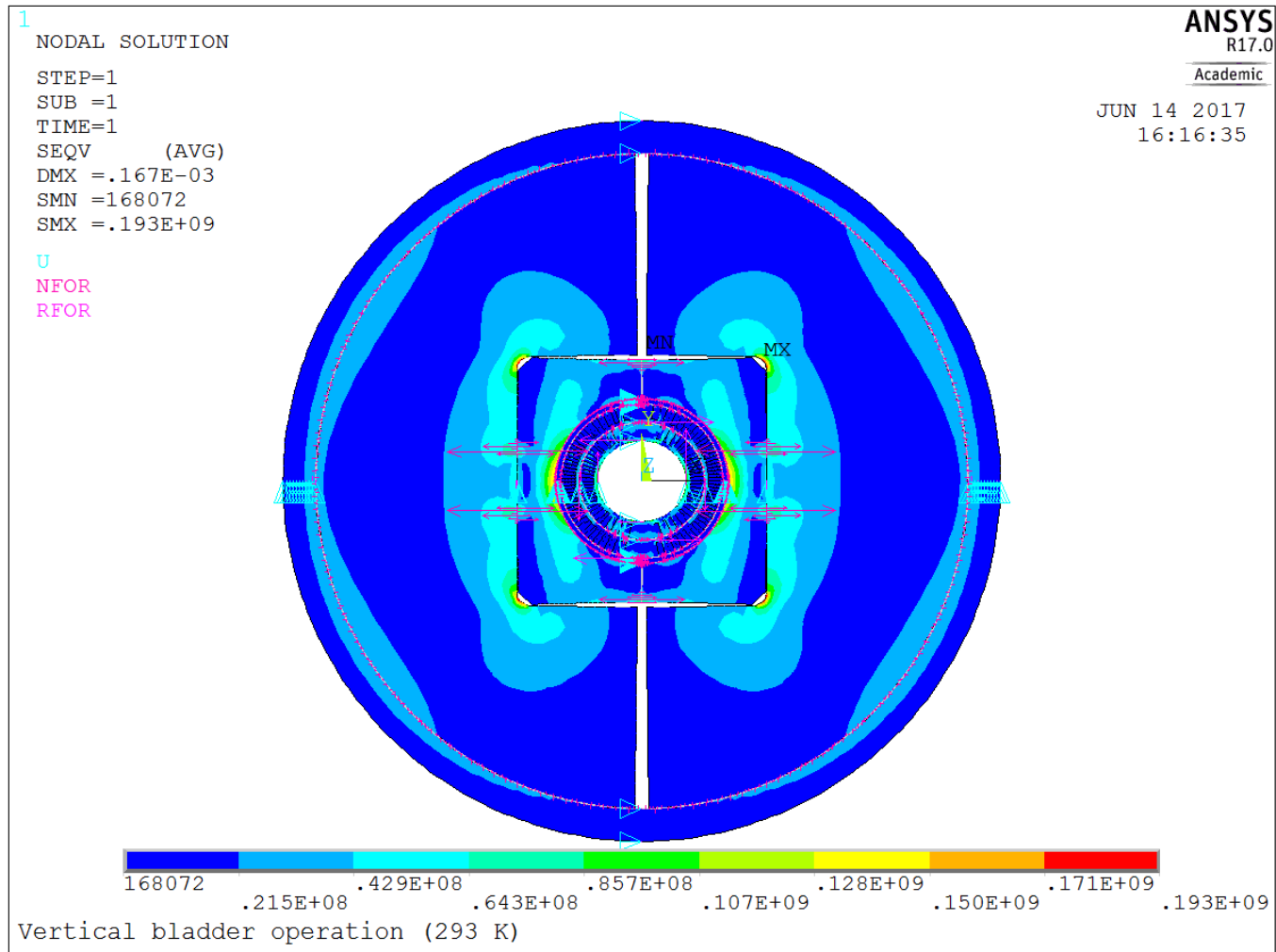
# The Magnet



# The Magnet

## Vert. bladder operation

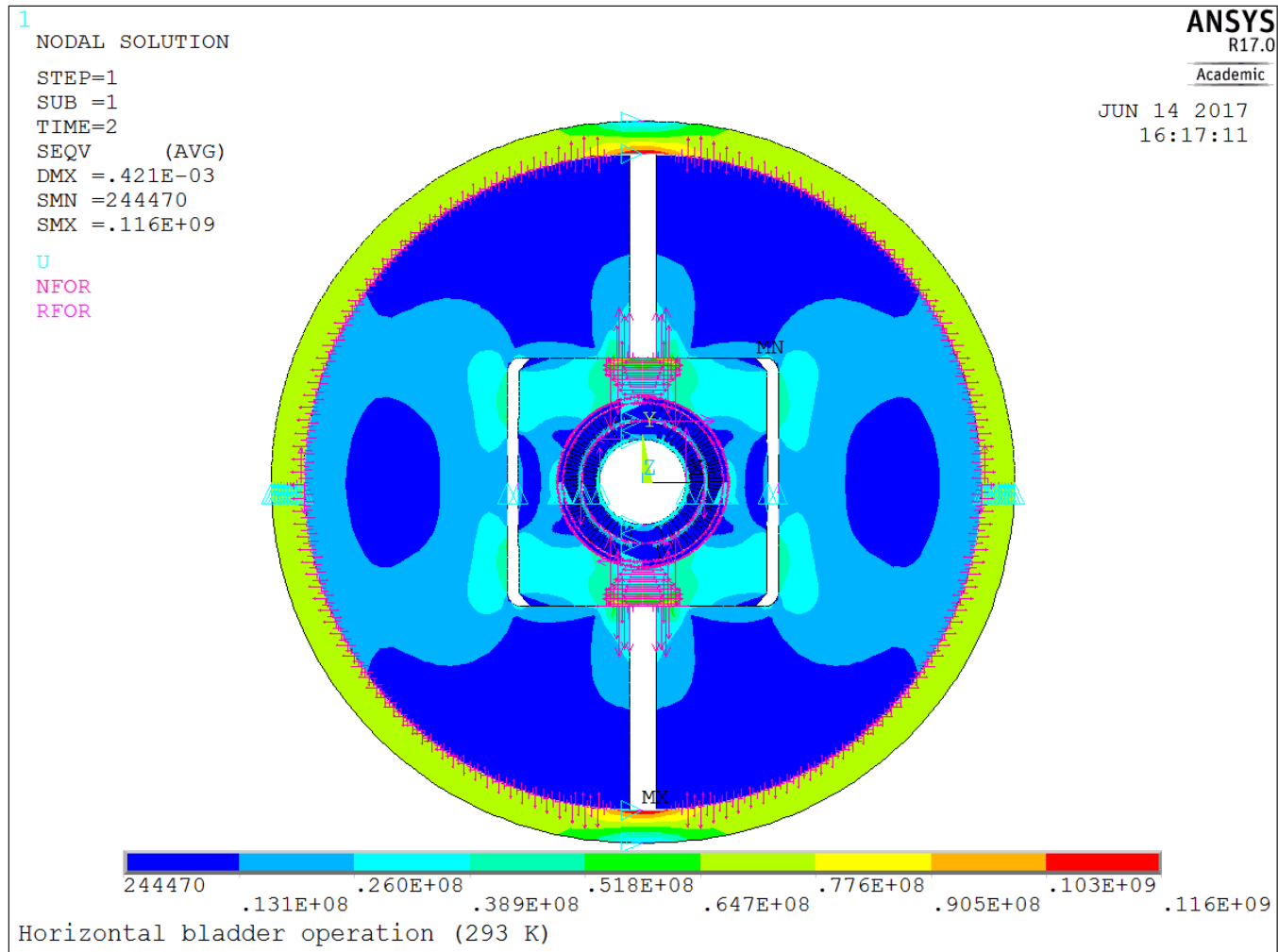
Room temp. steps



# The Magnet

## Hor. bladder operation

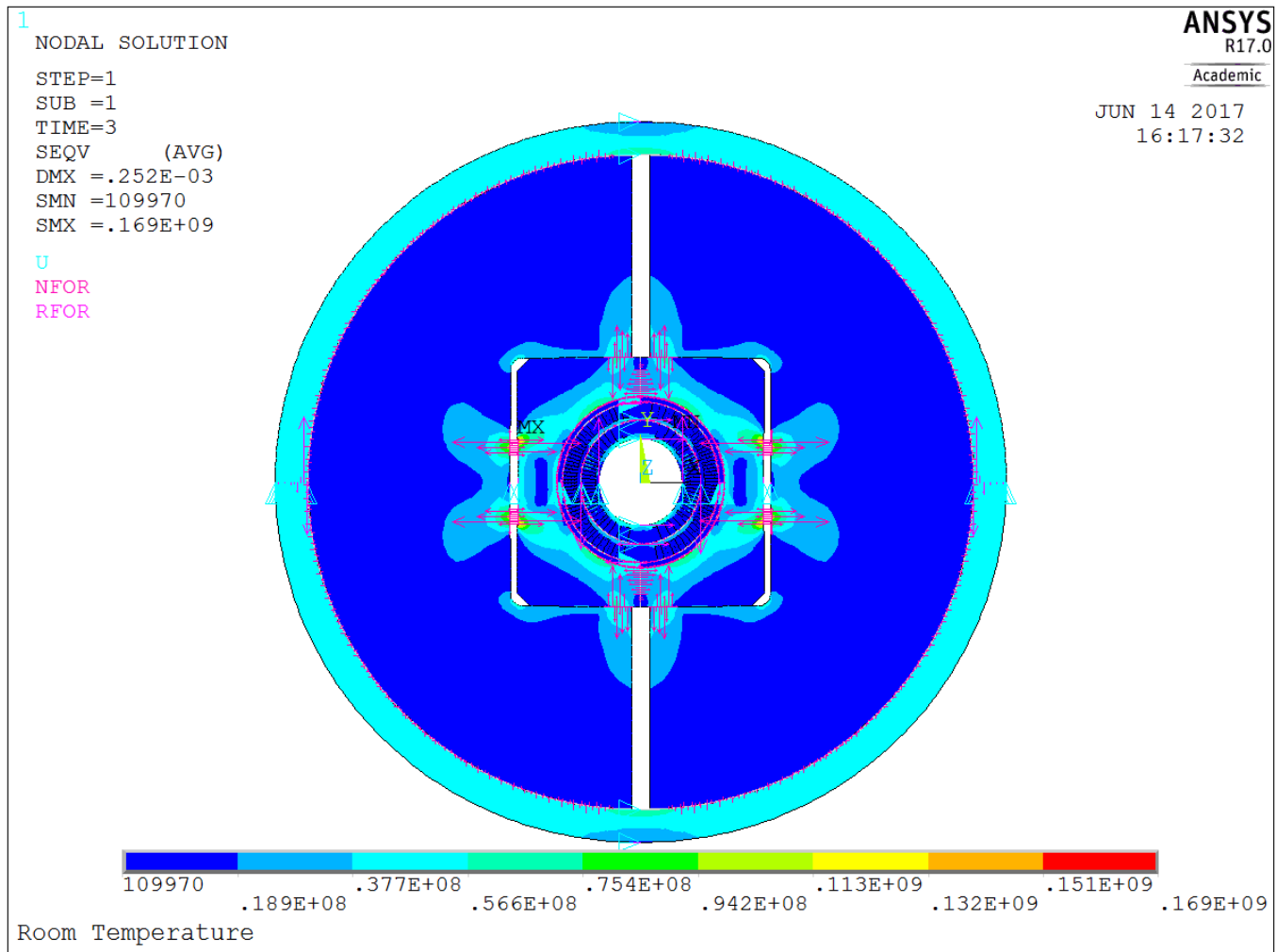
Room temp. steps



# The Magnet

## Assembly - room temp.

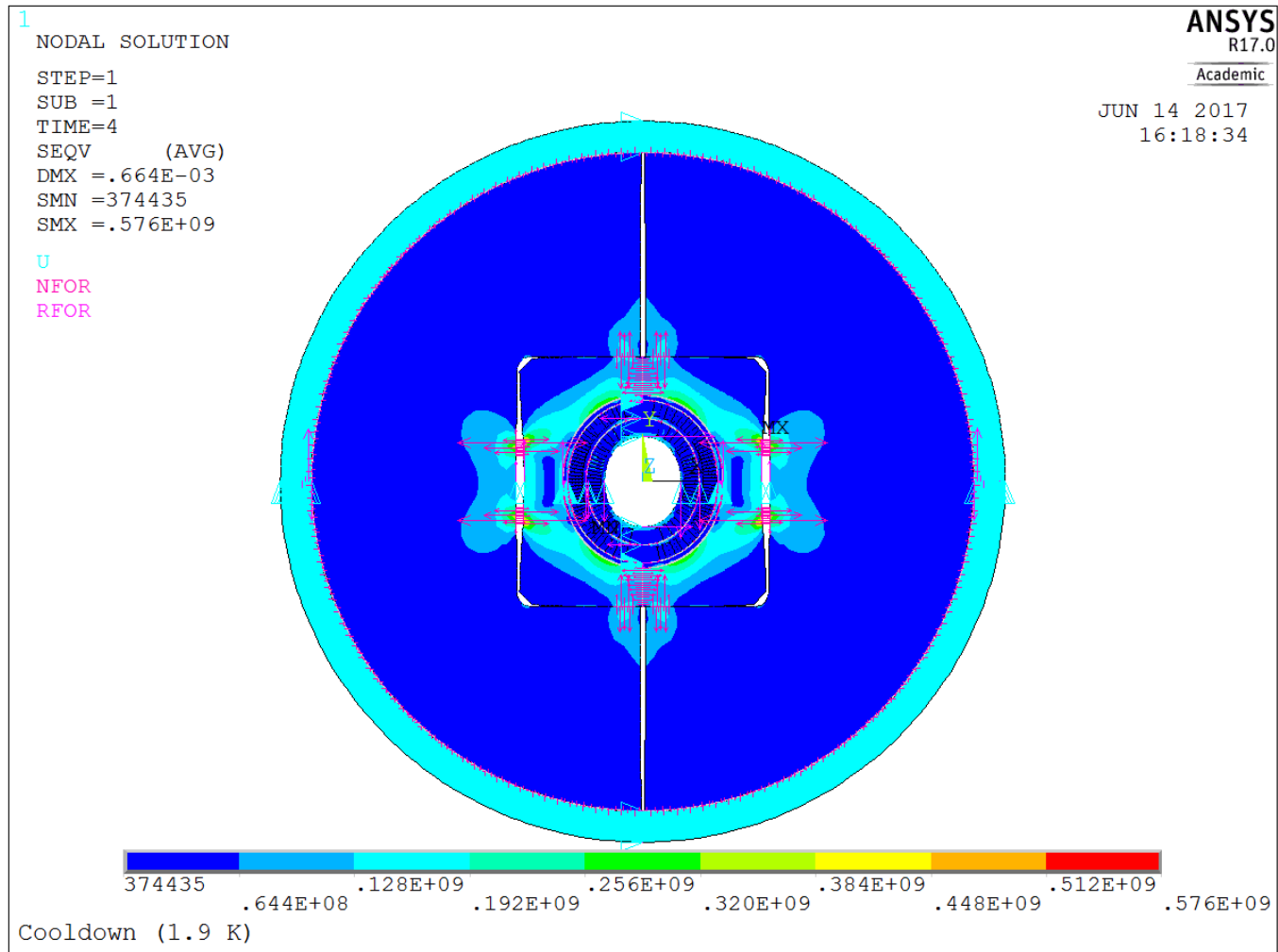
Room temp. steps



# The Magnet

## Cool down 1.9 K

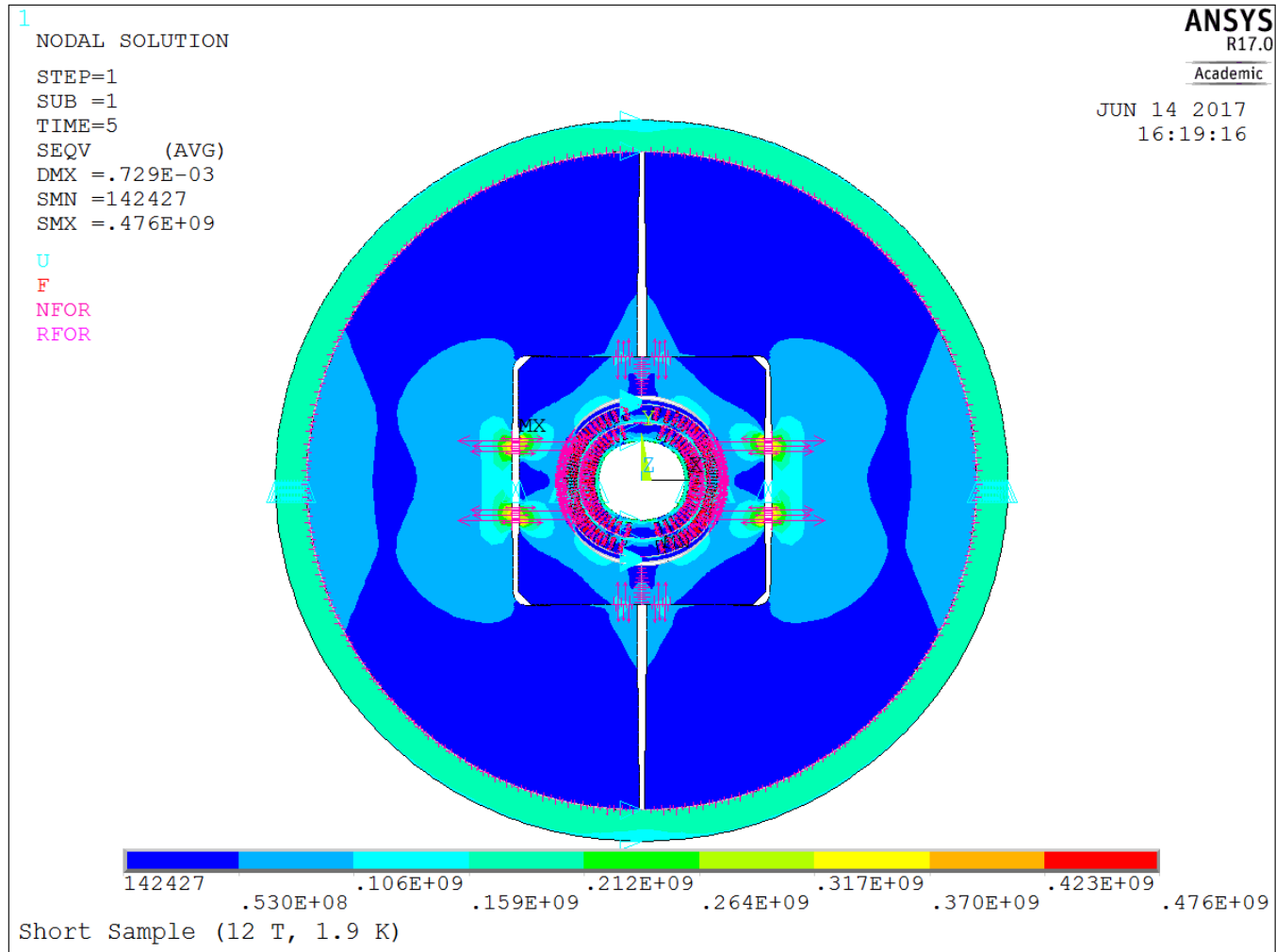
1.9 K steps



# The Magnet

## Operation at short sample limit (1.9 K, 12 T)

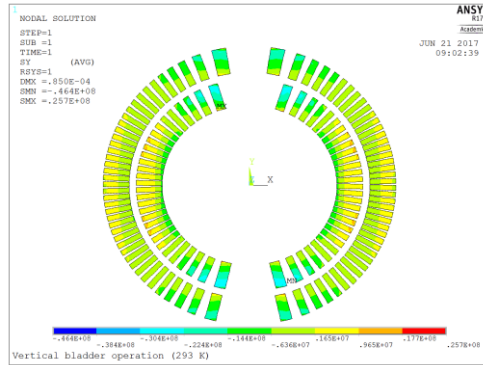
1.9 K steps



# The Coil

Room temp. steps  
( $\sigma_\theta$  - Azimuthal)

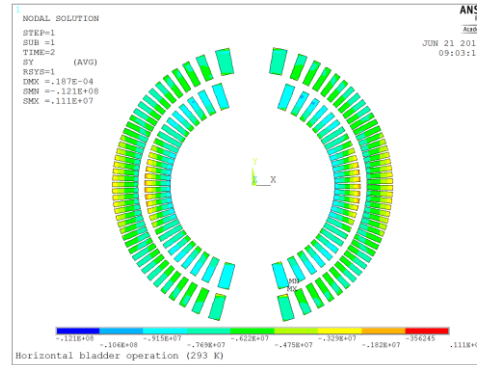
## Vert. bladder operation



Cable  $\sigma_\theta = [-46.4, 25.7]$  MPa

Cable  $\sigma_v^{\max} = 45.6$  MPa

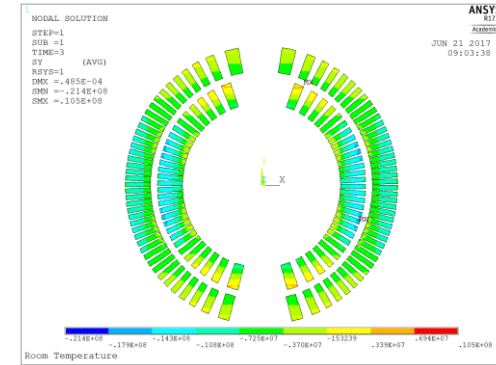
## Hor. bladder operation



Cable  $\sigma_\theta = [-12.1, 1.1]$  MPa

Cable  $\sigma_v^{\max} = 11.6$  MPa

## Assembly - room temp.



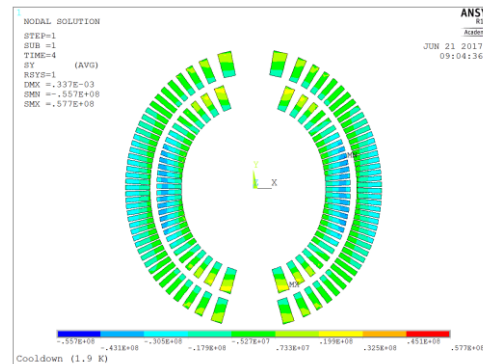
Cable  $\sigma_\theta = [-21.5, 10.5]$  MPa

Cable  $\sigma_v^{\max} = 19.8$  MPa

Operation at short sample limit  
(1.9 K, 12 T)

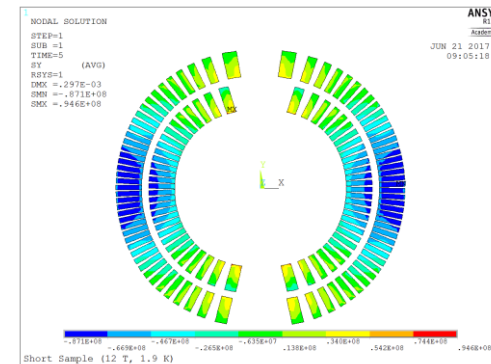
## Cool down 1.9 K

Cool down  
and  
operation steps  
( $\sigma_\theta$  - Azimuthal)



Cable  $\sigma_\theta = [-55.7, 57.7]$  MPa

Cable  $\sigma_v^{\max} = 66.45$  MPa



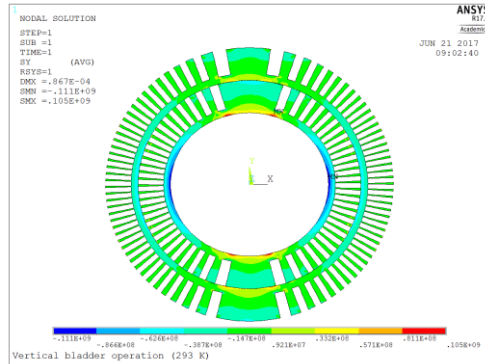
Cable  $\sigma_\theta = [-87.1, 94.6]$  MPa

Cable  $\sigma_v^{\max} = 101$  MPa

# The Former

Room temp. steps  
( $\sigma_\theta$  - Azimuthal)

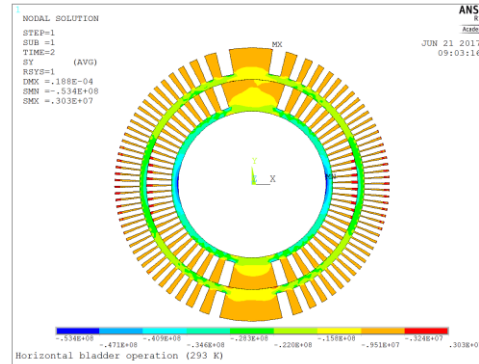
### Vert. bladder operation



Former  $\sigma_\theta = [-110.6, 105.0]$  MPa

Former  $\sigma_v^{\max} = 110.6$  MPa

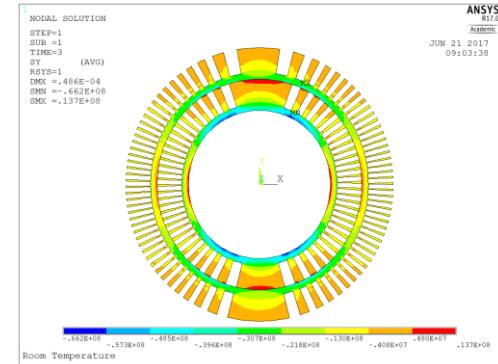
### Hor. bladder operation



Former  $\sigma_\theta = [-53.4, 3.0]$  MPa

Former  $\sigma_v^{\max} = 53.4$  MPa

### Assembly - room temp.



Former  $\sigma_\theta = [-66.2, 13.7]$  MPa

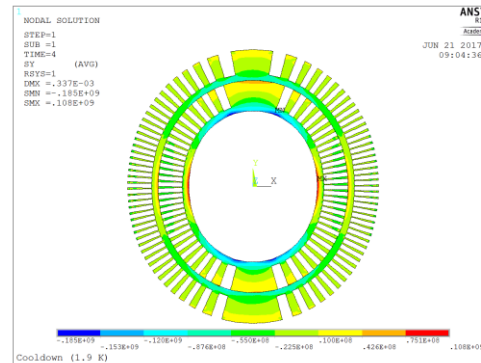
Former  $\sigma_v^{\max} = 65.9$  MPa

Operation at short sample limit

(1.9 K, 12 T)

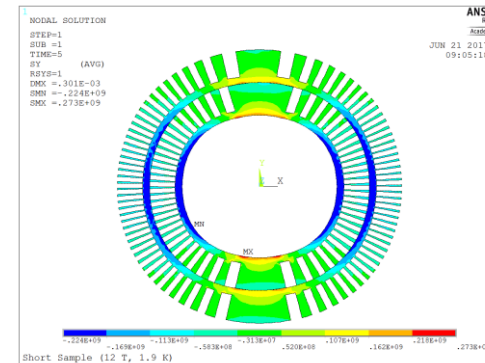
Cool down 1.9 K

Cool down  
and  
operation steps  
( $\sigma_\theta$  - Azimuthal)



Former  $\sigma_\theta = [-185.2, 108]$  MPa

Former  $\sigma_v^{\max} = 184.8$  MPa



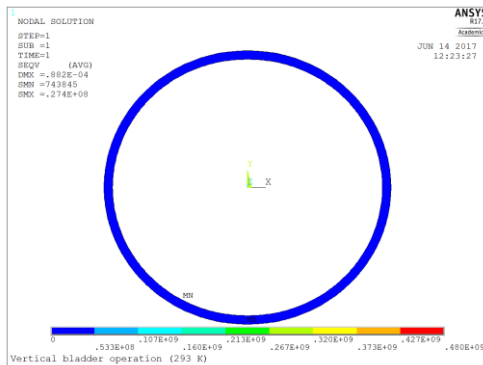
Former  $\sigma_\theta = [-224.0, 273.0]$  MPa

Former  $\sigma_v^{\max} = 271.6$  MPa

# The Protective Coil Pack Shell

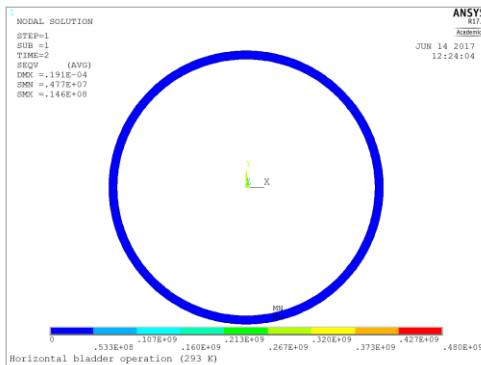
Room temp. steps

## Vert. bladder operation



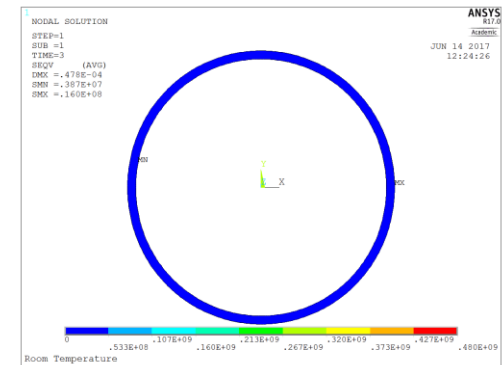
Prot. Shell  $\sigma_v^{\max} = 27.4$  MPa

## Hor. bladder operation



Prot. Shell  $\sigma_v^{\max} = 14.6$  MPa

## Assembly - room temp.

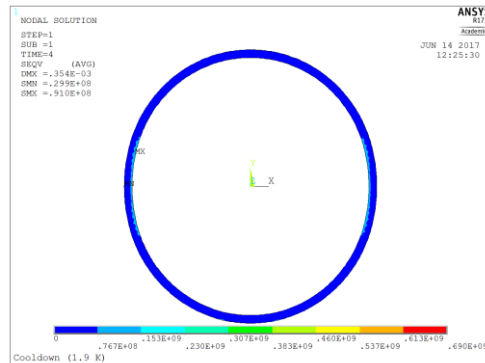


Prot. Shell  $\sigma_v^{\max} = 16.0$  MPa

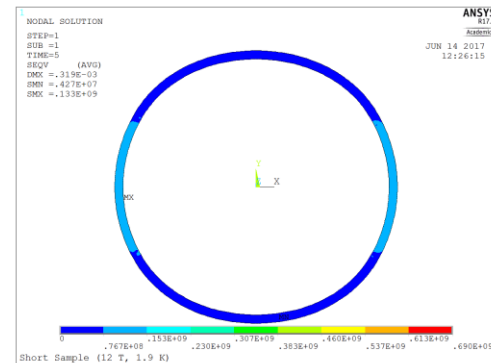
Operation at short sample limit  
(1.9 K, 12 T)

Cool down 1.9 K

Cool down  
and  
operation steps



Prot. Shell  $\sigma_v^{\max} = 91.0$  MPa



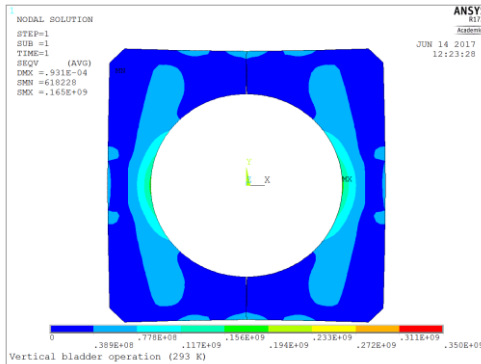
Prot. Shell  $\sigma_v^{\max} = 133.5$  MPa



# The Steel Pads

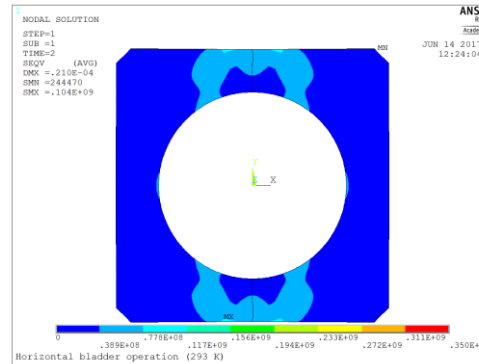
Room temp. steps

## Vert. bladder operation



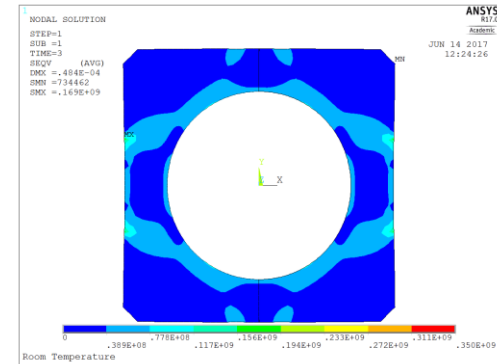
Pads IR  $\sigma_v^{\max} = 165.5 \text{ MPa}$

## Hor. bladder operation



Pads IR  $\sigma_v^{\max} = 48.0 \text{ MPa}$

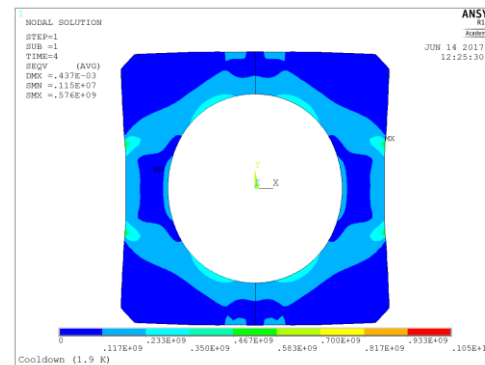
## Assembly - room temp.



Pads IR  $\sigma_v^{\max} = 80.6 \text{ MPa}$

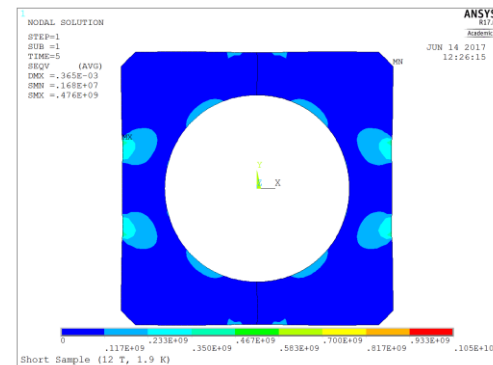
## Operation at short sample limit (1.9 K, 12 T)

### Cool down 1.9 K



Pads IR  $\sigma_v^{\max} = 316.3 \text{ MPa}$

Cool down  
and  
operation steps

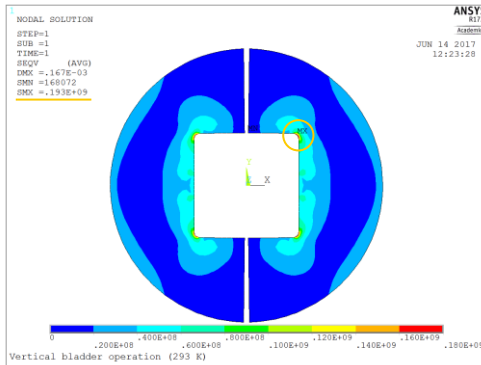


Pads IR  $\sigma_v^{\max} = 161.0 \text{ MPa}$

# The Iron Yoke

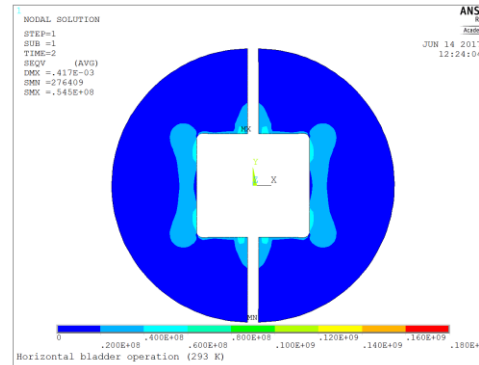
Room temp. steps

Vert. bladder operation



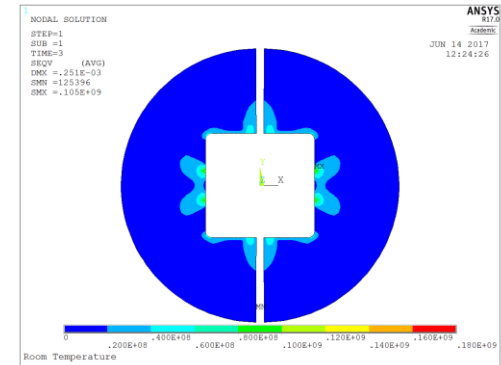
Yoke  $\sigma_v^{\max} > 180$  MPa

Hor. bladder operation



Yoke  $\sigma_v^{\max} = 54.5$  MPa

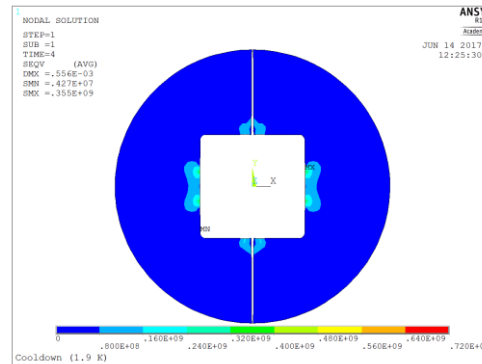
Assembly - room temp.



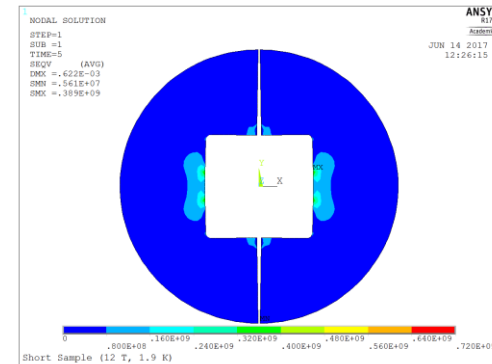
Yoke  $\sigma_v^{\max} = 105.0$  MPa

Operation at short sample limit  
(1.9 K, 12 T)

Cool down 1.9 K



Yoke  $\sigma_v^{\max} = 355.0$  MPa



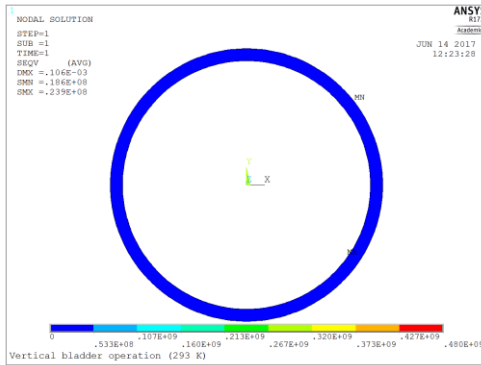
Yoke  $\sigma_v^{\max} = 389.0$  MPa

Cool down  
and  
operation steps

# The Support Shell

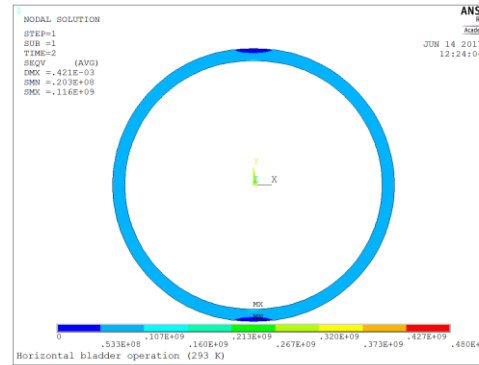
Room temp. steps

## Vert. bladder operation



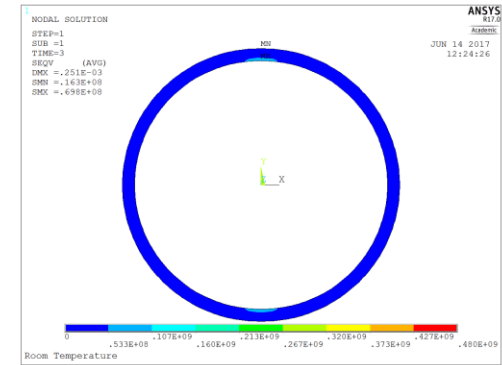
Shell  $\sigma_v^{\max} = 23.9 \text{ MPa}$

## Hor. bladder operation



Shell  $\sigma_v^{\max} = 116.3 \text{ MPa}$

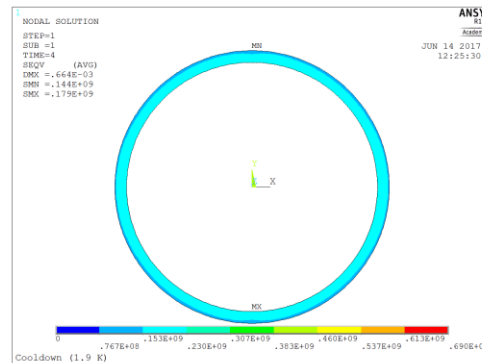
## Assembly - room temp.



Shell  $\sigma_v^{\max} = 69.8 \text{ MPa}$

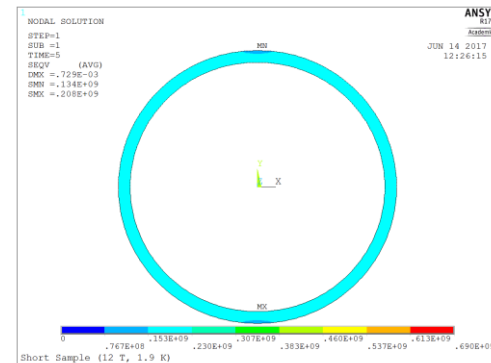
## Operation at short sample limit (1.9 K, 12 T)

### Cool down 1.9 K



Shell  $\sigma_v^{\max} = 179.0 \text{ MPa}$

### Short Sample (12 T, 1.9 K)

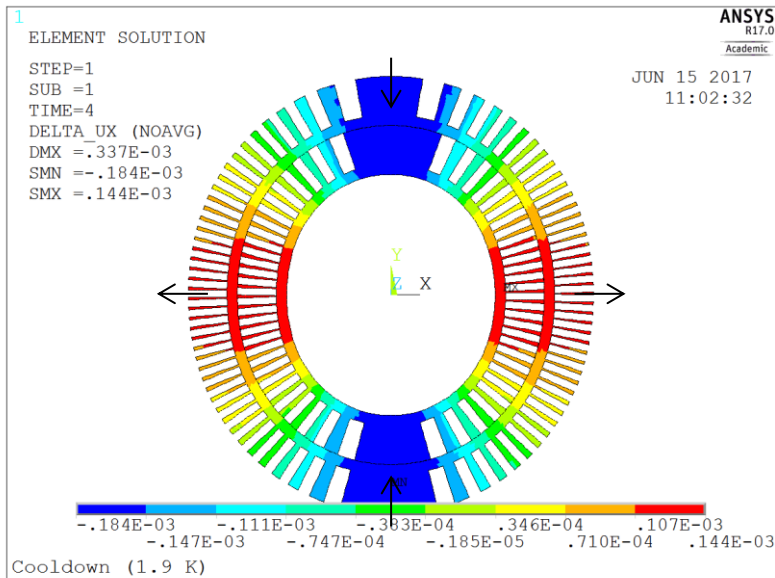


Shell  $\sigma_v^{\max} = 208.0 \text{ MPa}$

Cool down  
and  
operation steps

# Former Displacement

**Radial displacement difference of the former between cool down and short sample load steps**



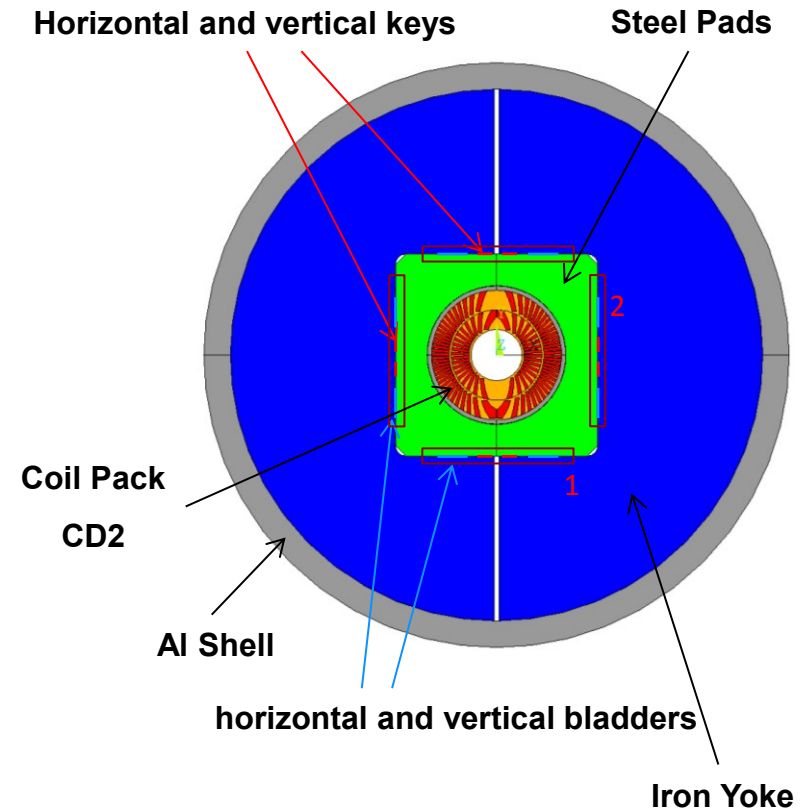
- The arrow indicates the radial movement direction from cool down to operation on X and Y axes
- Along Y axes the coil pack squeeze of roughly of  $180\ \mu\text{m}$
- Along X axes the coil pack expand of roughly of  $\sim 140\ \mu\text{m}$

- 2D Mechanical modelling of CD1 dipole with ANSYS
- Design's objectives
- **Baseline Design (+Excursus on CD2)**
- The Design vs. Material Properties
- Mechanical tolerances
- Parametric Study
- Conclusions

# CD2 mechanical structure

## The CD2 design:

1. Same Layer-2 OD =122 mm of CD1
2. Inclined cable channels
3. Same Bladder and Key structure of CD1
4. 2D Simulations -> 5 steps (as for CD1) and same B&K config.
  - Operation->Lorenz forces acting on the conductor according to test condition (4.2 K, 10.5 T) , limited by the test station  $I_{\max}=22$  kA

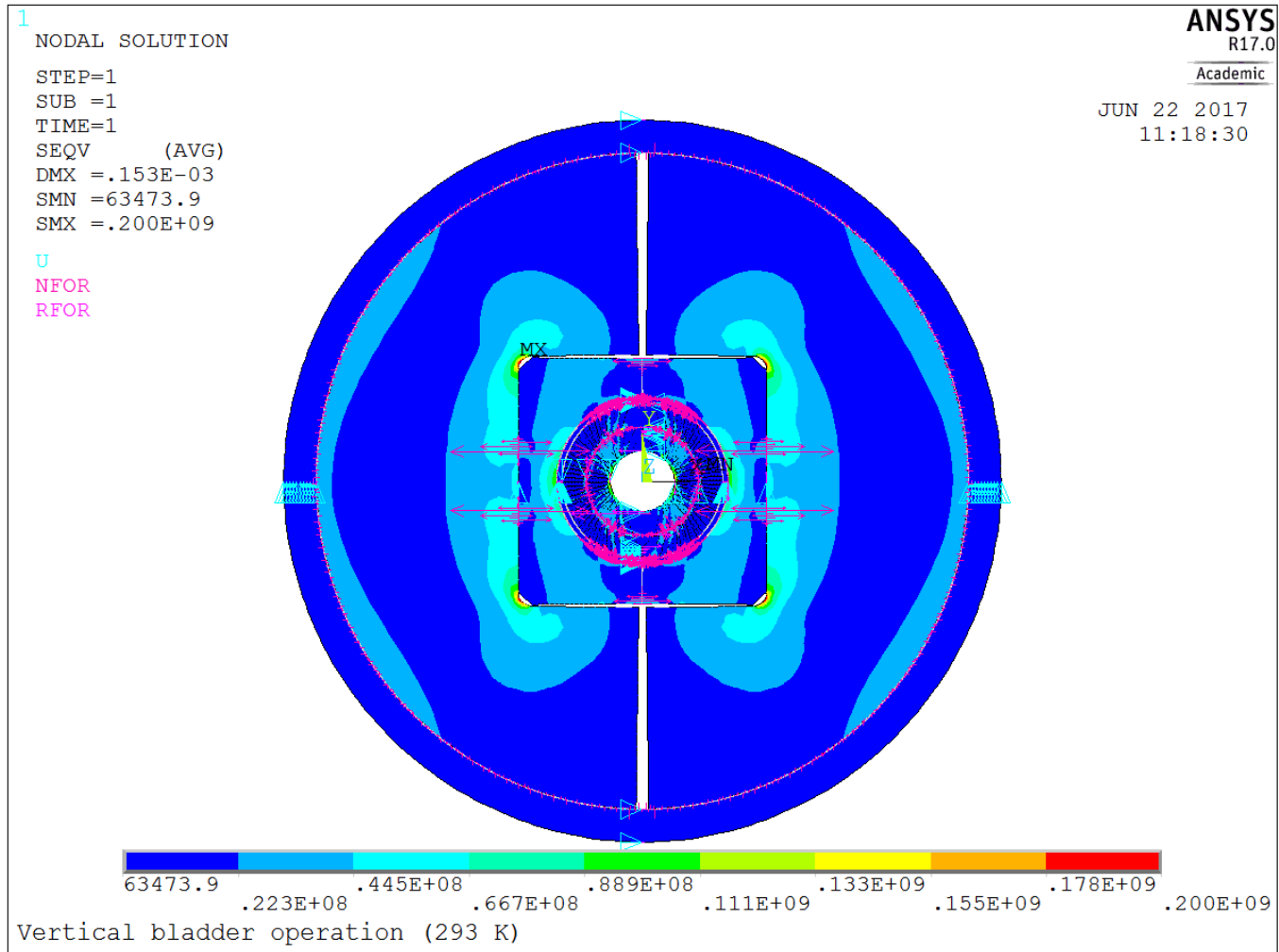


# CD2 Magnet

## CD2 Magnet

## Vert. bladder operation

Room temp. steps

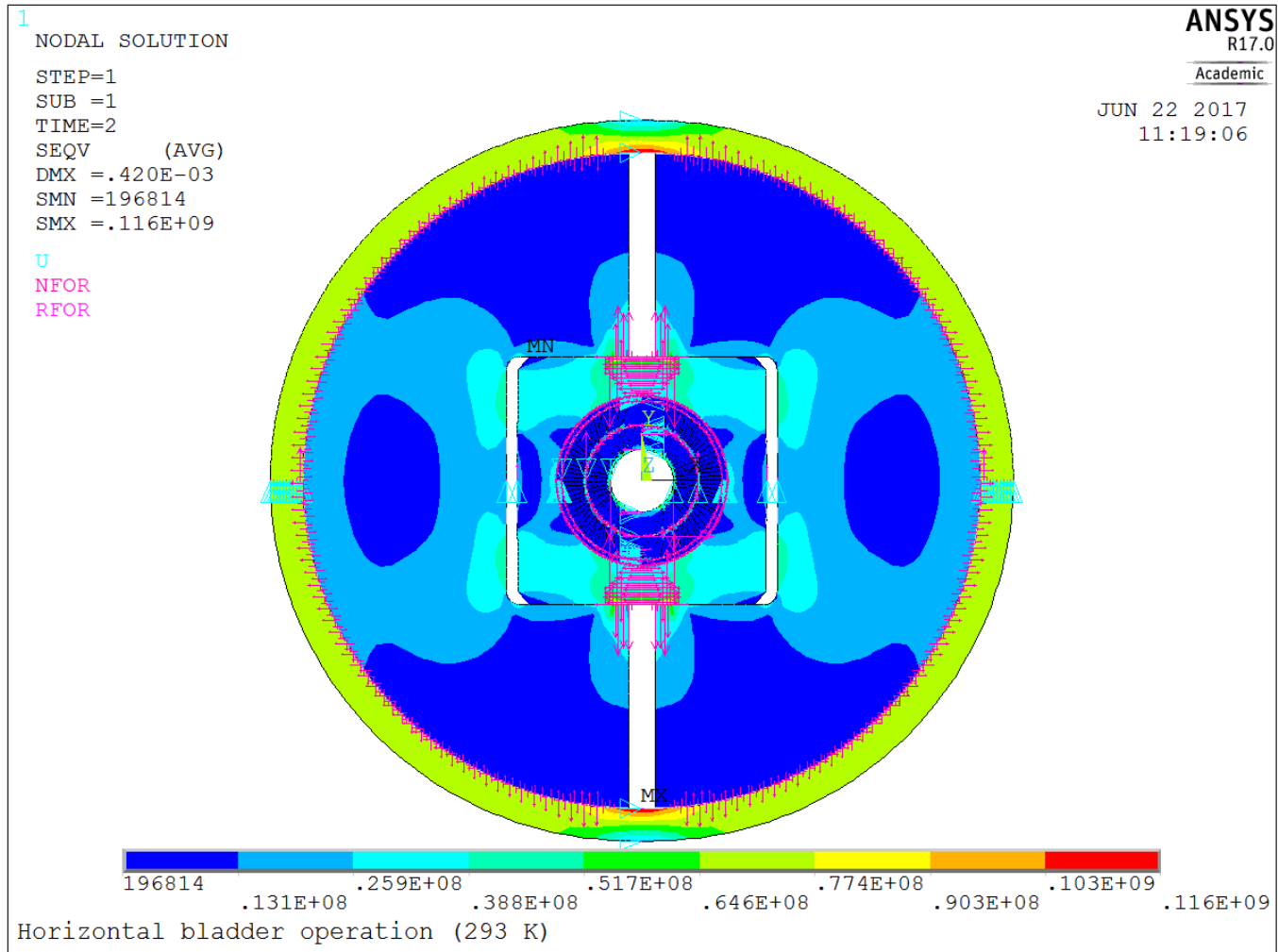




## CD2 Magnet

## Hor. bladder operation

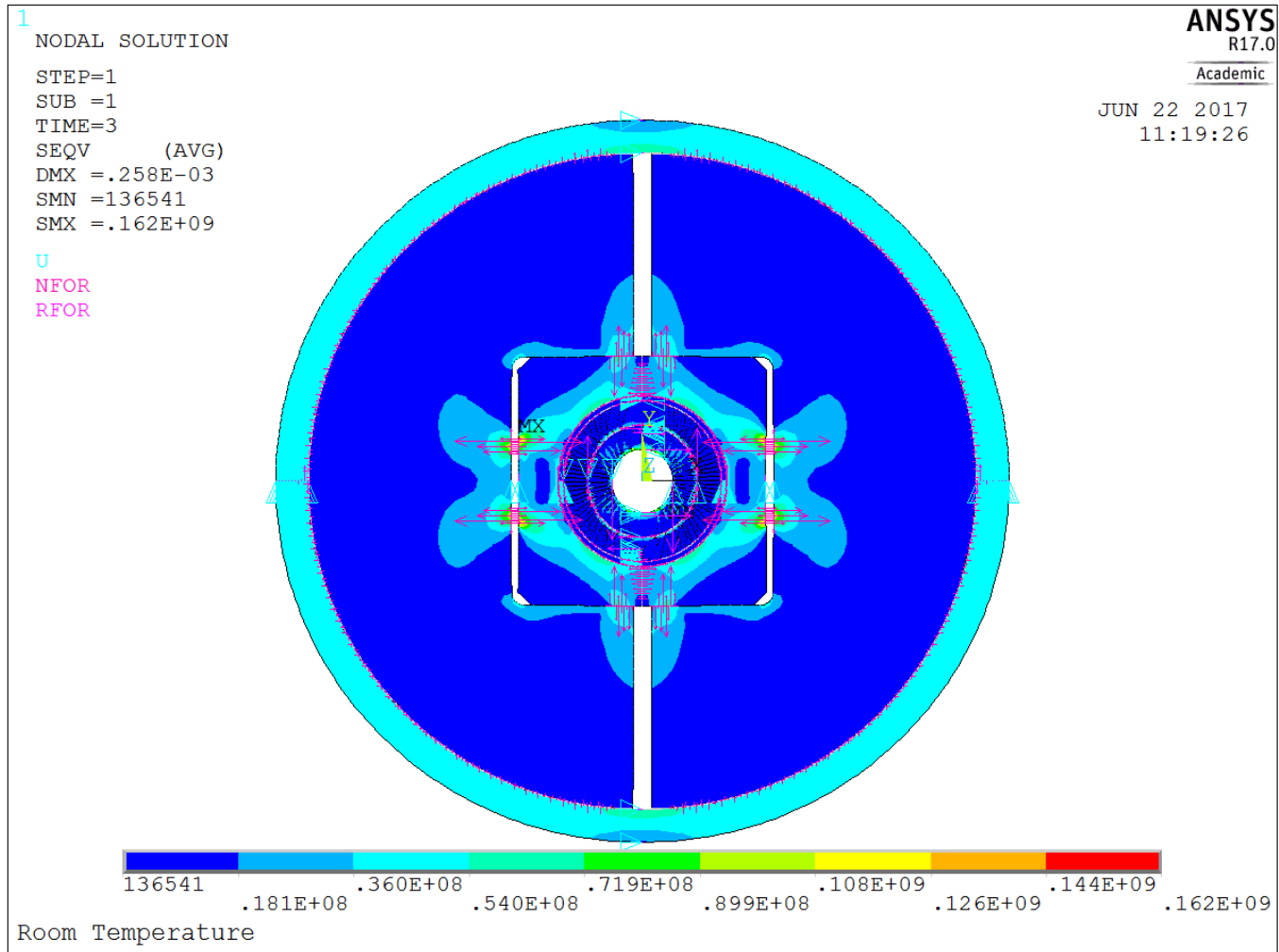
Room temp. steps



## CD2 Magnet

## Assembly - room temp.

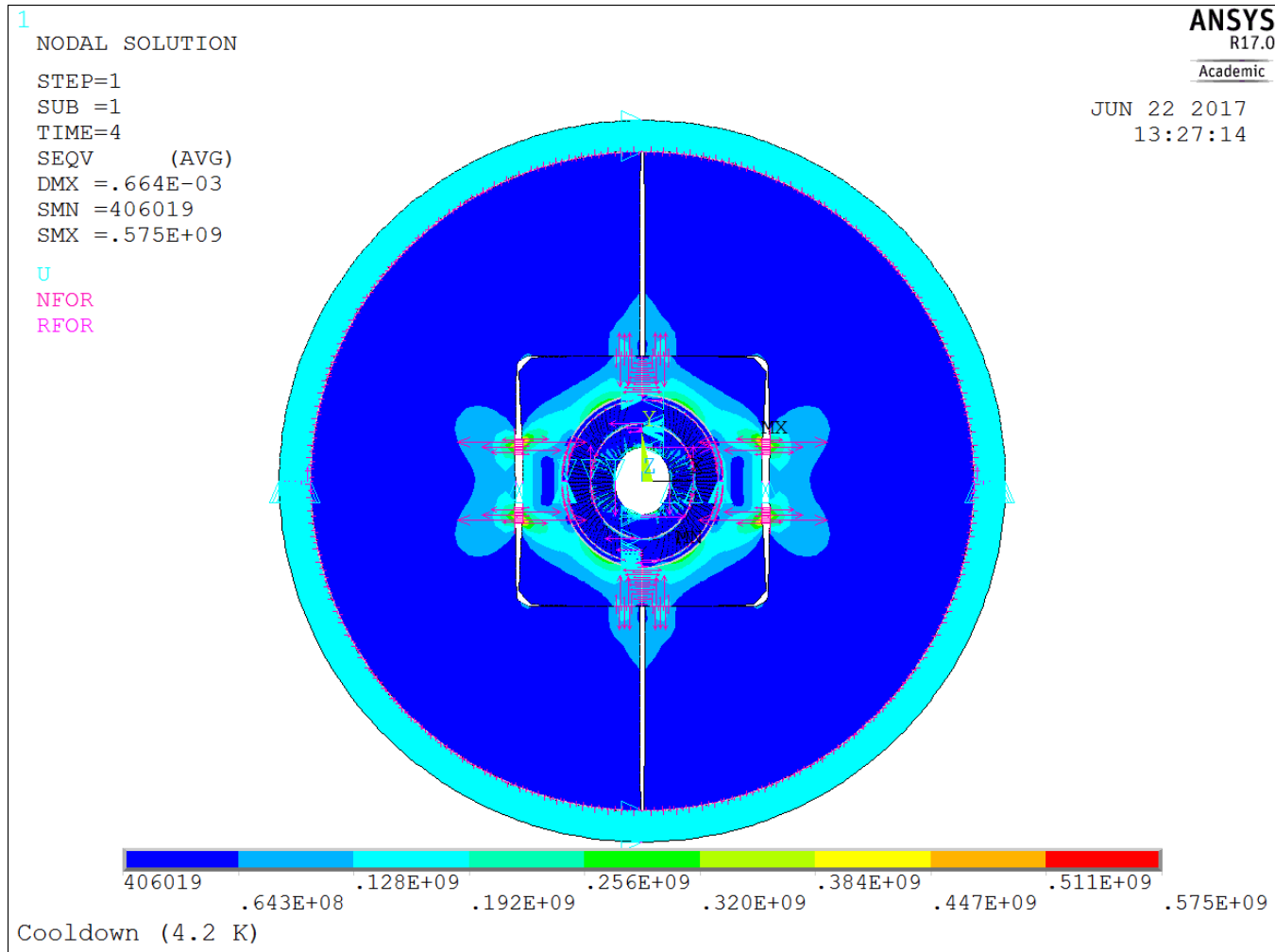
Room temp. steps



## CD2 Magnet

## Cool down 4.2 K

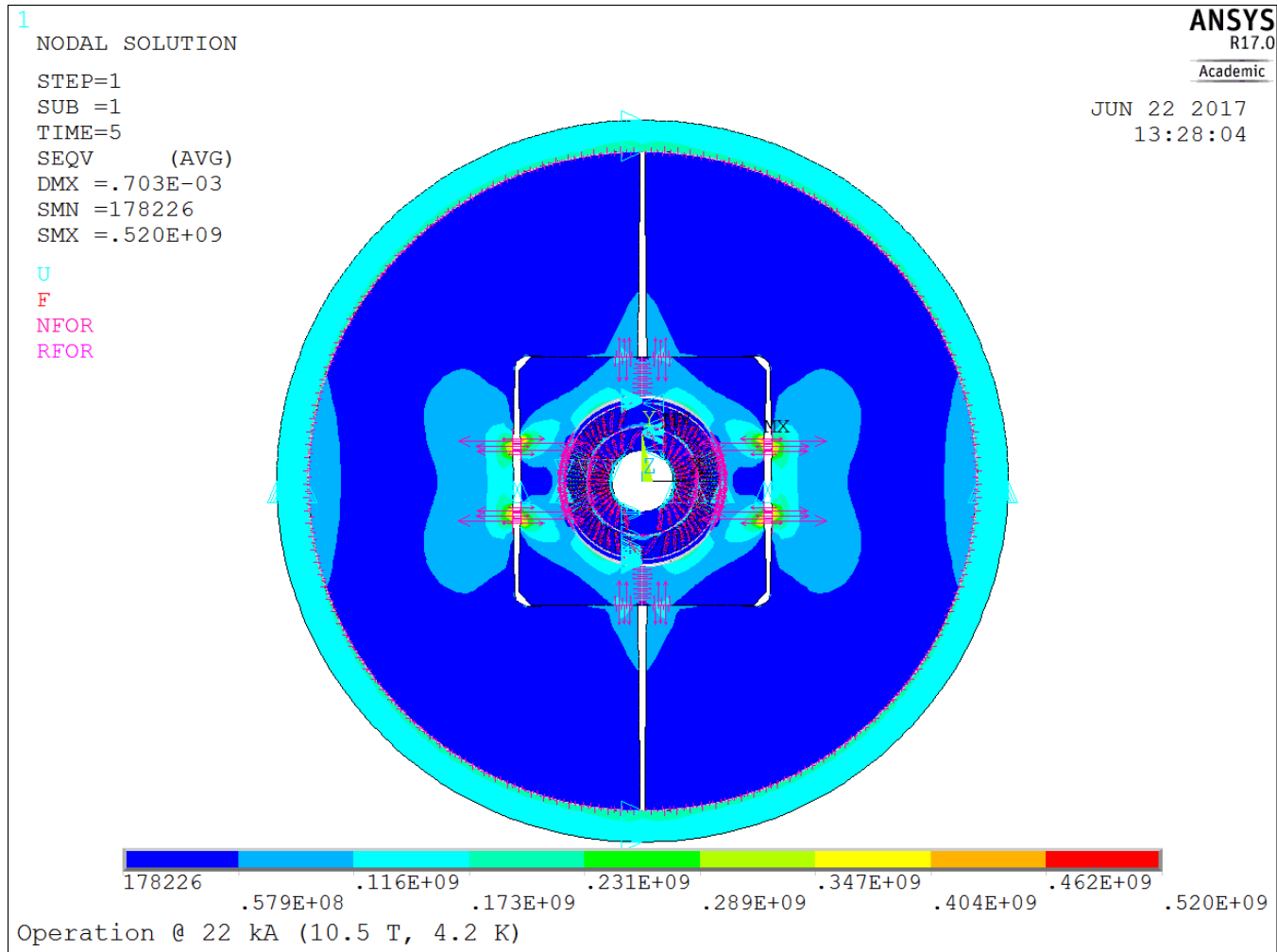
4.2 K steps



## CD2 Magnet

## Operation (4.2 K, 10.5 T)

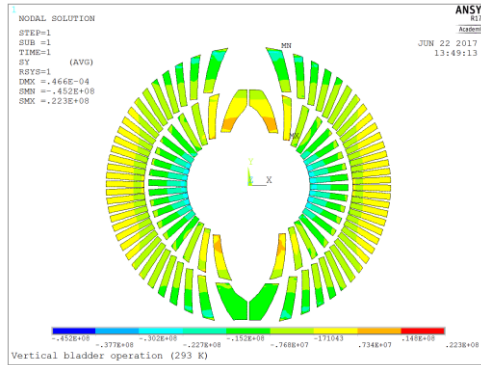
4.2 K steps



## CD2- The Coil

Room temp. steps  
( $\sigma_\theta$  - Azimuthal)

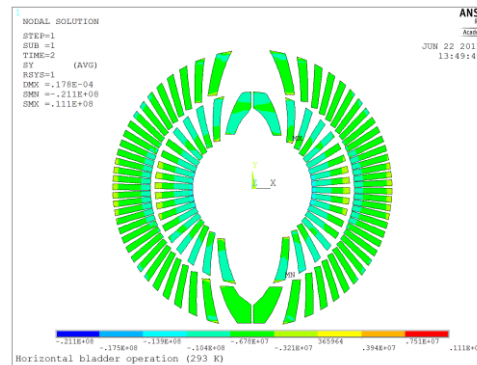
Vert. bladder operation



Cable  $\sigma_\theta$  = [- 45.2, 22.3] MPa

Cable  $\sigma_v^{\max}$  = 46.2 MPa

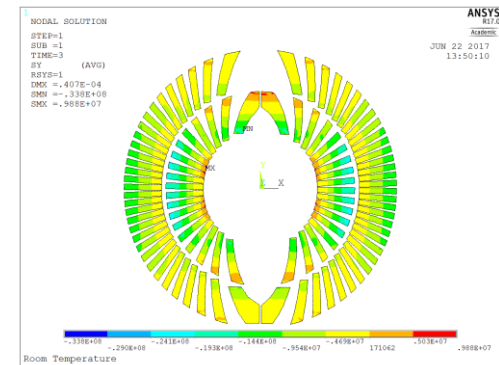
Hor. bladder operation



Cable  $\sigma_\theta$  = [-21.1, 11.1] MPa

Cable  $\sigma_v^{\max}$  = 20.8 MPa

Assembly - room temp.

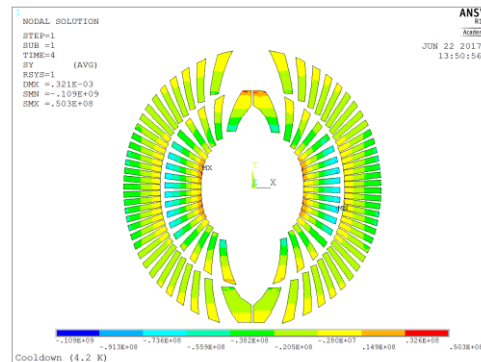


Cable  $\sigma_\theta$  = [-33.8, 9.8] MPa

Cable  $\sigma_v^{\max}$  = 33.0 MPa

Operation at short sample limit  
(1.9 K, 12 T)

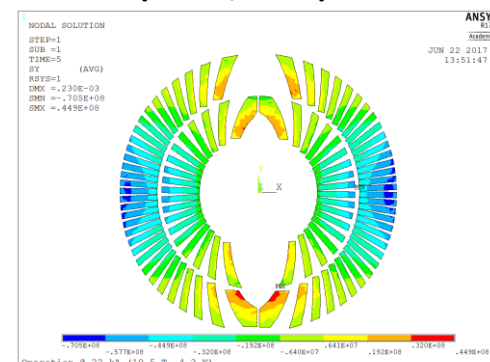
Cool down 1.9 K



Cable  $\sigma_\theta$  = [-109.0, 50.3] MPa

Cable  $\sigma_v^{\max}$  = 102.0 MPa

Cool down  
and  
operation steps  
( $\sigma_\theta$  - Azimuthal)



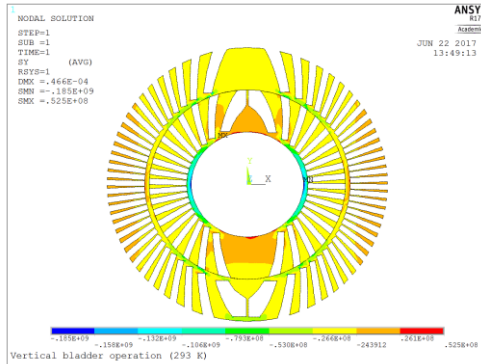
Cable  $\sigma_\theta$  = [-70.5, 44.9] MPa

Cable  $\sigma_v^{\max}$  = 72.4 MPa

## CD2-The Former

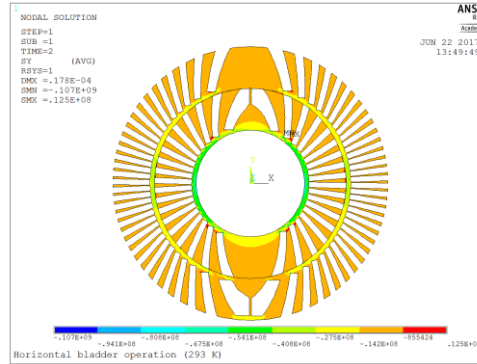
Room temp. steps  
( $\sigma_\theta$  - Azimuthal)

Vert. bladder operation



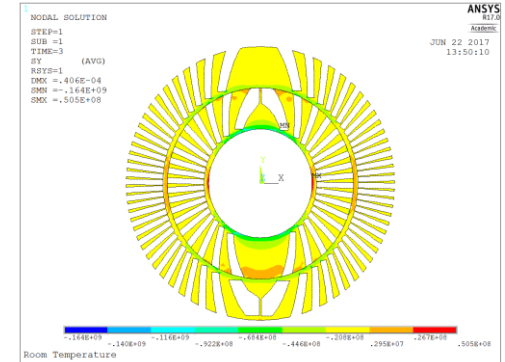
Former  $\sigma_\theta = [-185.0, 52.5]$  MPa  
Former  $\sigma_v^{\max} = 185$  MPa

Hor. bladder operation



Former  $\sigma_\theta = [-107.0, 12.5]$  MPa  
Former  $\sigma_v^{\max} = 100$  MPa

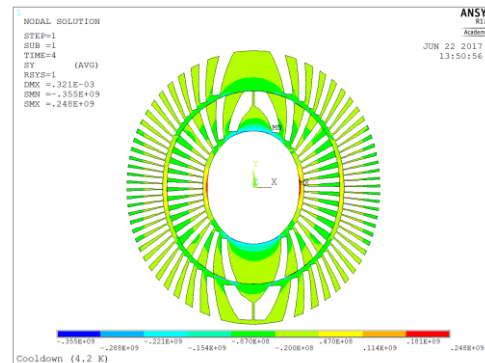
Assembly - room temp.



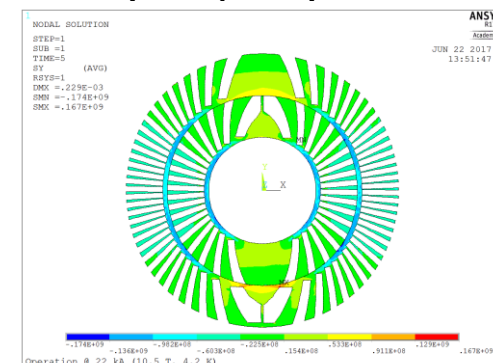
Former  $\sigma_\theta = [-164.0, 50.5]$  MPa  
Former  $\sigma_v^{\max} = 158$  MPa

Operation at short sample limit  
(1.9 K, 12 T)

Cool down 1.9 K



Former  $\sigma_\theta = [-355.0, 248.0]$  MPa  
Former  $\sigma_v^{\max} = 340$  MPa



Former  $\sigma_\theta = [-174.0, 167.0]$  MPa  
Former  $\sigma_v^{\max} = 175.0$  MPa

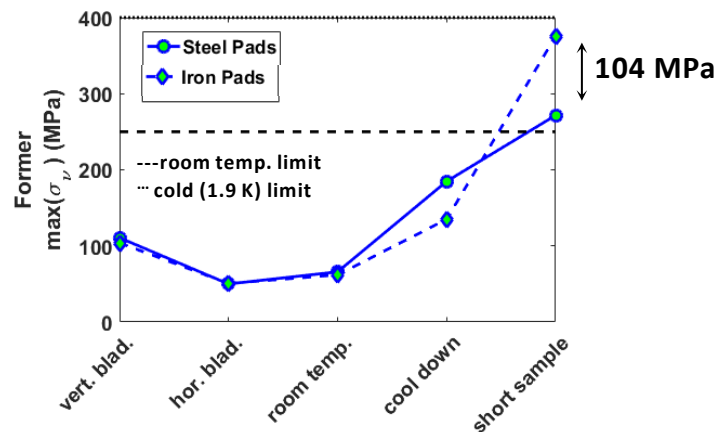
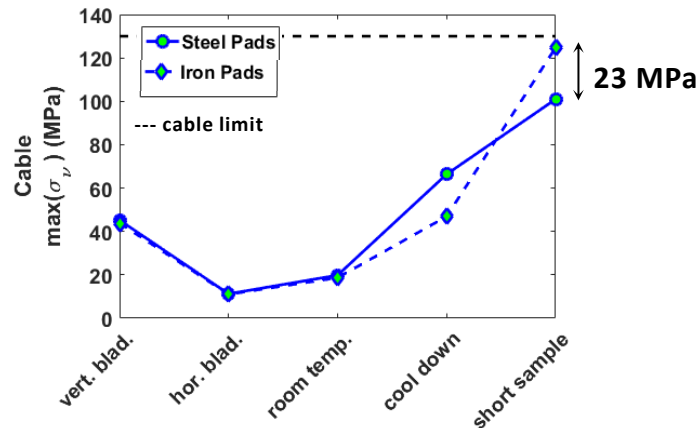
Cool down  
and  
operation steps  
( $\sigma_\theta$  - Azimuthal)

- 2D Mechanical modelling of CD1 dipole with ANSYS
- Design's objectives
- Baseline Design
- **Nominal Design vs. Material Properties**
- Mechanical tolerances
- Parametric Study
- Conclusions

# Pads: Steel vs. Iron

Von Mises ( $\sigma_v$ ) maximum stresses

cable and former for the 5 load steps



## Why steel instead of iron

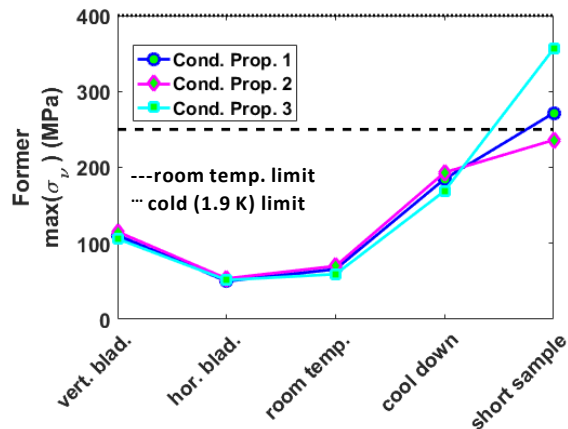
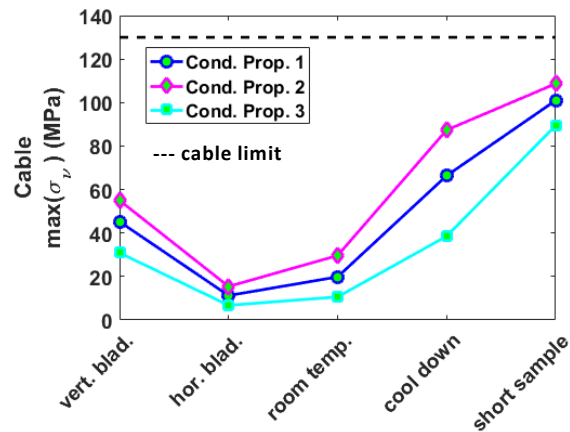
- Thermal contraction of steel higher than iron
- Thermal contraction of steel much closer to the one for the coil pack
- For the iron pads, after cool down the differential thermal contraction gives a smaller value of pre-stress leading to higher maximum stress at operating conditions



# Conductor's Mechanical Properties

Von Mises ( $\sigma_v$ ) maximum stresses

cable and former for the 5 load steps



Mechanical Properties for comparison

Used for simulations

Cond. Prop. 1		Cond. Prop. 2		Cond. Prop. 3	
E (GPa)		E (GPa)		E (GPa)	
293 K	4.2 K	293 K	4.2 K	293 K	4.2 K
EX=33	EX=30	EX=54	EX=54	EX=14	EX=14
EY=27.5	EY=25	EY=44	EY=44	EY=7.74	EY=7.74
GXY=21	GXY=21	GXY=21	GXY=21	GXY=21	GXY=21

The only remarkable differences are

- 7.7 MPa higher peak stress for Cond. Prop.2 on the cable at short sample operating condition
- 85 MPa higher peak stress for Cond. Prop.3 on the former at short sample operating condition

- 2D Mechanical modelling of CD1 dipole with ANSYS
- Design's objectives
- Baseline Design
- The Design vs. Material Properties
- **Mechanical tolerances**
- Parametric Study
- Conclusions

# Mechanical Tolerances

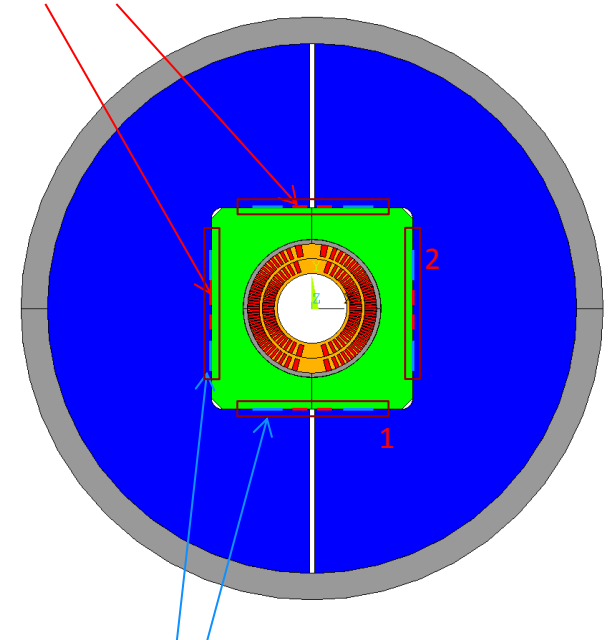
## Tolerances of interest:

- Mismatch between radii of coil and pads assemblies ( $OR1-IR2 \neq 0$ ) (**coil/pad radial**)
- Horizontal key tolerance (**hor. key**)
- Vertical key tolerance (**vert. key**)
- Pad/pad interface contact (**pad/pad cont.**)

## Use ANSYS contact technology

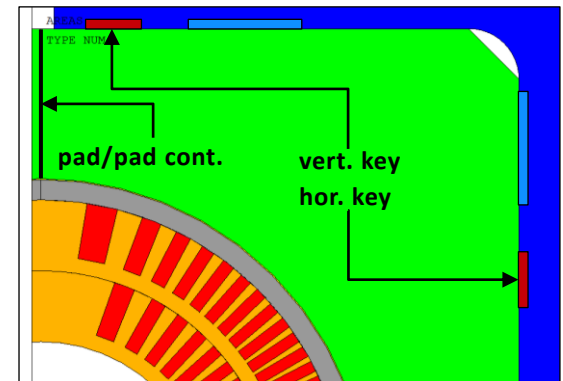
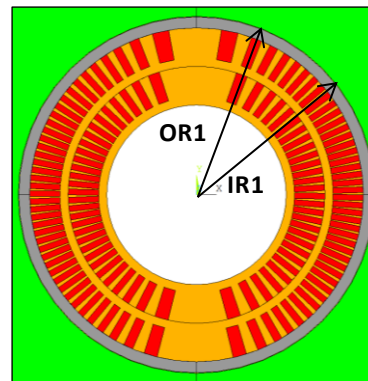
- (**coil/pad radial**)  $< 0 \rightarrow$  gap
- (**coil/pad radial**)  $> 0 \rightarrow$  compression
- (**hor. or vert. key**)  $< 0 \rightarrow$  undersize key
- (**hor. or vert. key**)  $> 0 \rightarrow$  oversize key
- (**pad/pad cont.**)  $< 0 \rightarrow$  undersize pads
- (**pad/pad cont.**)  $> 0 \rightarrow$  oversize pads

Horizontal and vertical keys



horizontal and vertical bladders

Coil pack



- 2D Mechanical modelling of CD1 dipole with ANSYS
- Design's objectives
- Baseline Design
- The Design vs. Material Properties
- Mechanical tolerances
- **Parametric Study**
- Conclusions

# Parametric study and design's objective

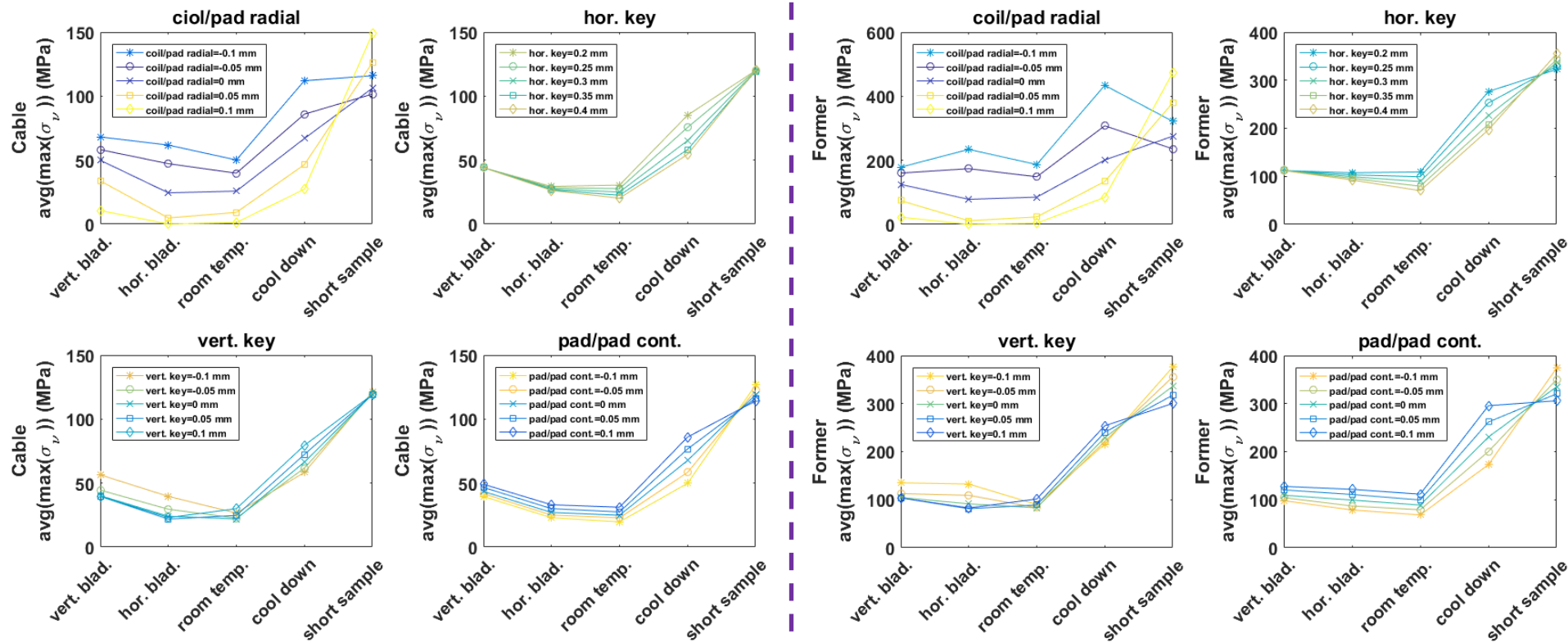
- **Use a  $\pm 100$   $\mu\text{m}$  tolerance on the parameters of interest with a 50  $\mu\text{m}$  step (five values for each parameter, reasonable computation time)**
- **Nominal values of the parameters**
  - coil/pad radial gap equals to 0.0 mm
  - hor. key interference of 0.3 mm
  - vert. key interference of 0.0 mm
  - pad/pad contact gap equal to 0.0 mm
- **For any combination of the parameters tolerances:**
  - **Maximum stress on the conductor below 130 MPa**
  - **Maximum stress on the former below 250 MPa at room temp and 400 MPa. at 1.9 K**
  - **The pad/pad interface has to be in contact during all the operating conditions.**
- **If any of the maximum allowed stresses on the conductor and on the former are exceeded, the parameters combination is considered to be harmful for the magnet operation**
- **A pad/pad interface not in contact during all the steps**

# Sensitivity to Parameters

## One-factor-at-the-time

### One-factor-at-the-time (quick check of important parameters)

- Average the stress values over all the simulations runs for a given param. value and load step
- Display the average as a function of the load step and param. value
- Color map identify the spread on the results



- Coil/pad radial mismatch has the larger influence on maximum stresses
- Horizontal and vertical keys tolerances have a minor influence
- Pad/pad contact tolerance can play a role

We can restrict ourselves to the interactions between two parameters

# Sensitivity to Parameters

## Two Parameters Analysis

Varying two parameters while keeping the others at their nominal value:

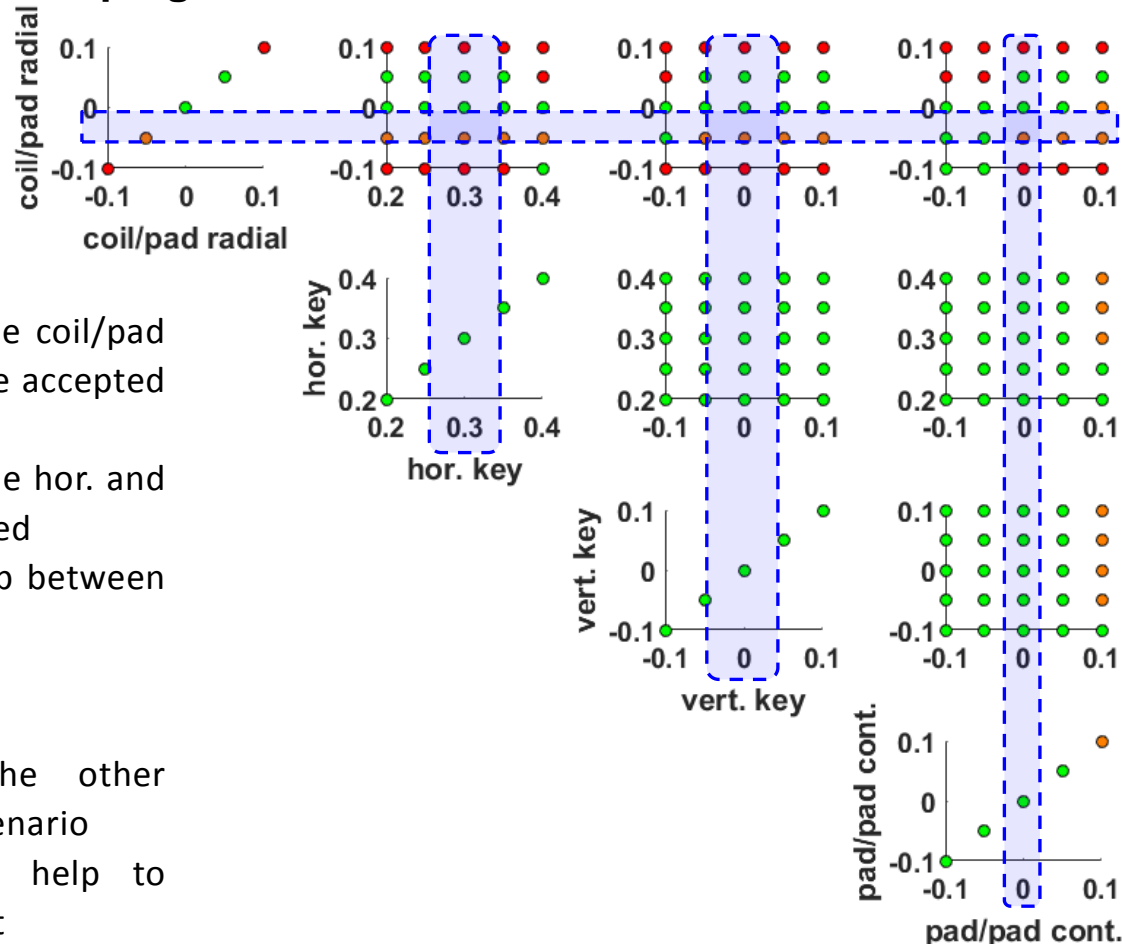
- All good
- Pad/pad interface
- Stresses values exceeded

### FIRST ROW

1.  $\pm 100 \mu\text{m}$  tolerance on the coil/pad radial mismatch can not be accepted (required below  $50 \mu\text{m}$ );
2. A  $\pm 50 \mu\text{m}$  tolerance on the hor. and vert. key must be considered
3. Better to leave a small gap between coil and pad ( $\leq 50 \mu\text{m}$ )

### 2<sup>nd</sup>, 3<sup>rd</sup> and 4<sup>th</sup> ROWS

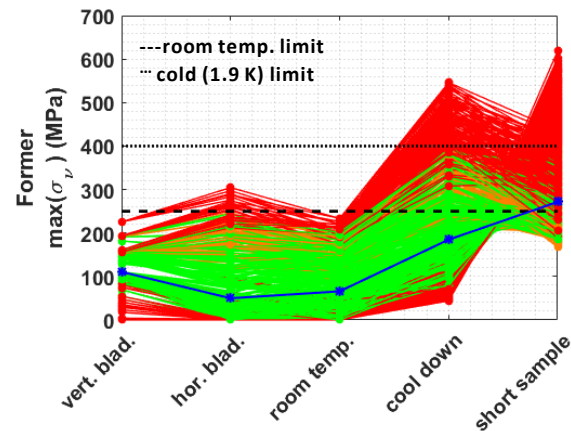
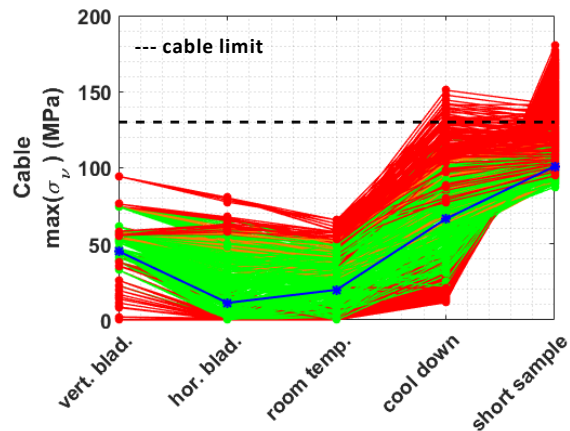
1. Any combination of the other parameters gives a safe scenario
2. Using tighter tolerances help to guarantee pad/pad contact



# A Glance to the Overall Results

## Results from full parametric study

- Within the requested limits
- Pad/pad interface contact not guaranteed (at room temp.)
- Stresses values exceeded the design limits
- Nominal design



**Need to verify that tolerances from two parameters analysis allow to stay within the stress limits!**



# Defining Tolerances

**Target tolerances (according to the procurement of mechanical parts)**

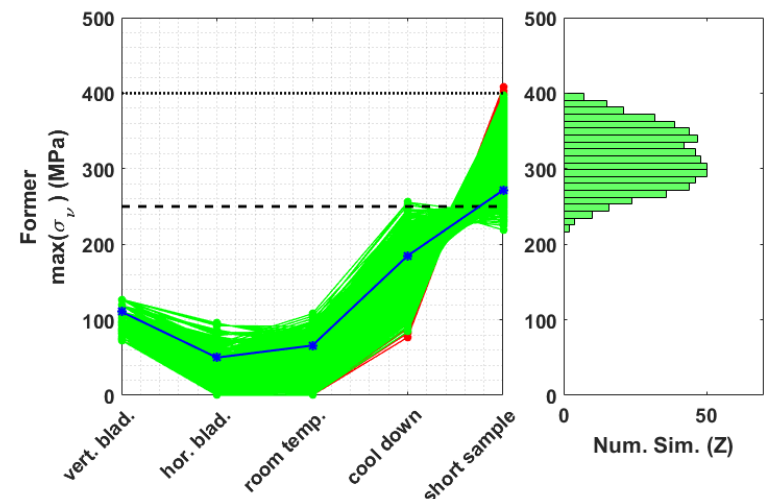
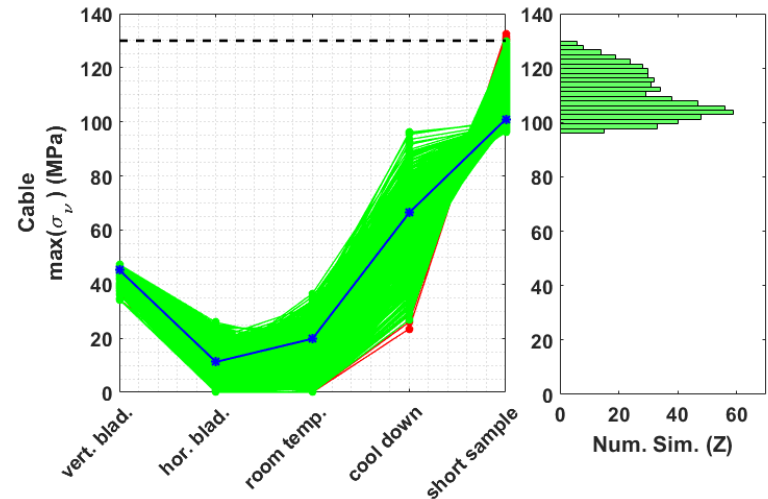
- coil/pad radial  $\rightarrow [-40, 0] \mu\text{m}$
- hor. key  $\rightarrow \pm 50 \mu\text{m}$
- vert. key  $\rightarrow \pm 50 \mu\text{m}$
- pad/pad contact  $\rightarrow \pm 25 \mu\text{m}$

**4 simulations runs above limit -by a small amount- out of 625 simulations (5 values per tolerance):**

coil/pad radial ( $\mu\text{m}$ )	hor. Key ( $\mu\text{m}$ )	vert.key ( $\mu\text{m}$ )	pad/pad contact( $\mu\text{m}$ )	Cable (Mpa)	Former (Mpa)
-40	25	25	25	130.46	
-40	25	50	13	130.115	
-40	27.5	50	13	132.6	407.85
-40	27.5	50	25	131.23	402.36

**THIS IS NOT GOING TO BE A PROBLEM: WE HAVE EXTRA MARGINS!**

**Results from parametric study with target tolerances**



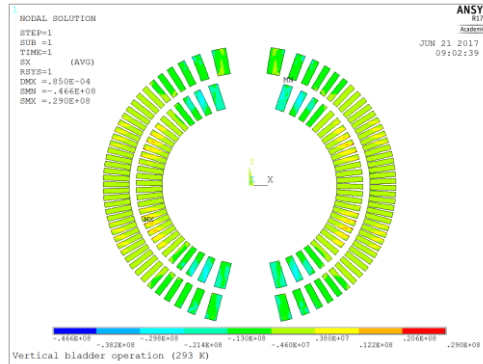
- 2D Mechanical modelling of CD1 dipole with ANSYS
- Design's objectives
- Baseline Design
- The Design vs. Material Properties
- Mechanical tolerances
- Parametric Study
- **Conclusions**

- **A parametric study on the 2D model of CD1 magnet is carried out**
- **Critical tolerances a parameter sensitivity is investigated**
- **Tolerances for technical design are defined**
- **Numerical Results from 2D simulations show the feasibility of the CD1 design**

# CD1 - The Coil Radial Stress

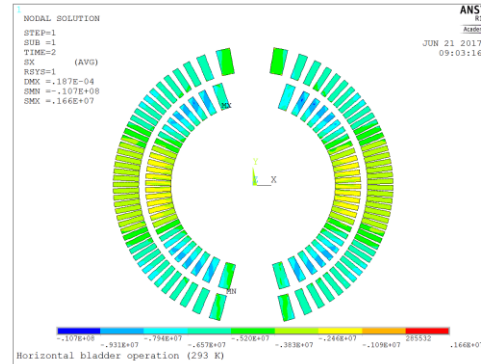
Room temp. steps  
( $\sigma_r$  - Radial)

Vert. bladder operation



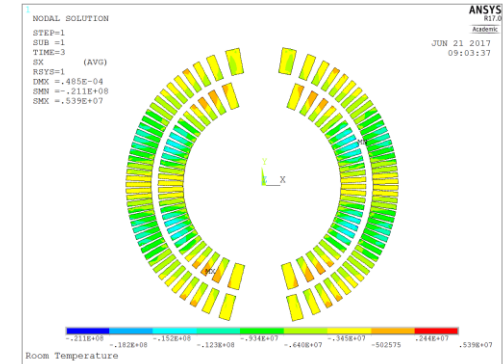
Cable  $\sigma_r$  = [- 46.6, 29.0] MPa

Hor. bladder operation



Cable  $\sigma_r$  = [-10.7, 16.6] MPa

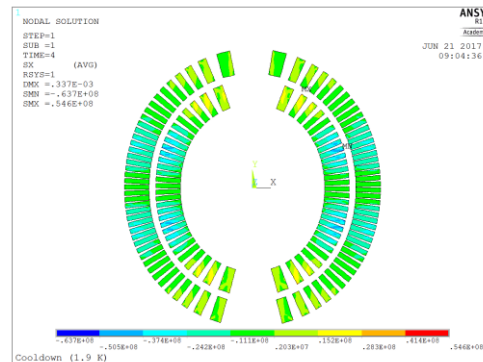
Assembly - room temp.



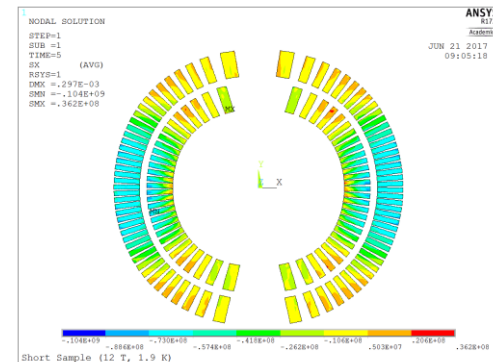
Cable  $\sigma_r$  = [-21.1, 5.3] MPa

Operation at short sample limit  
(1.9 K, 12 T)

Cool down 1.9 K



Cable  $\sigma_r$  = [-63.7, 54.6] MPa



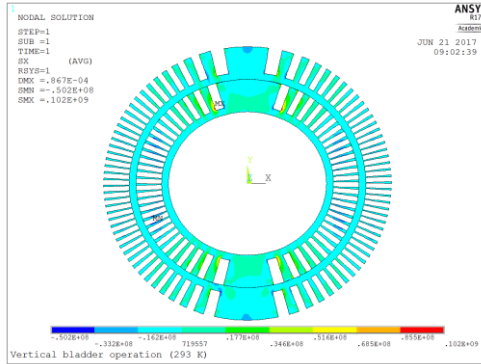
Cable  $\sigma_r$  = [-104.0, 36.2] MPa

Cool down  
and  
operation steps  
( $\sigma_r$  - Radial)

# CD1 - The Former Radial Stress

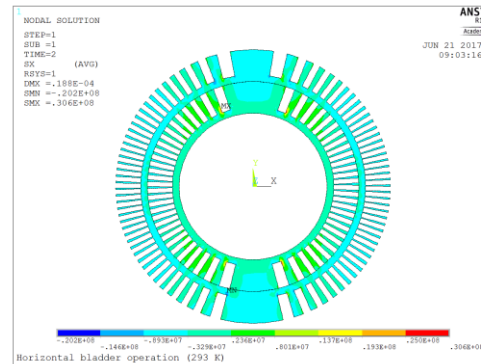
Room temp. steps  
( $\sigma_r$  - Radial)

## Vert. bladder operation



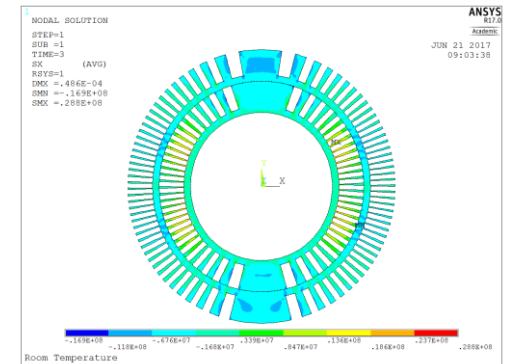
Former  $\sigma_r$  = [-50.2, 102.0] MPa

## Hor. bladder operation



Former  $\sigma_r$  = [- 20.2, 30.6] MPa

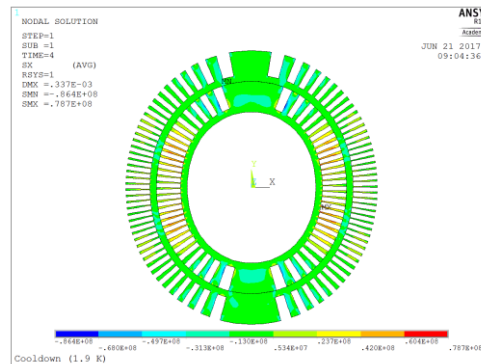
## Assembly - room temp.



Former  $\sigma_r$  = [-16.9, 28.8] MPa

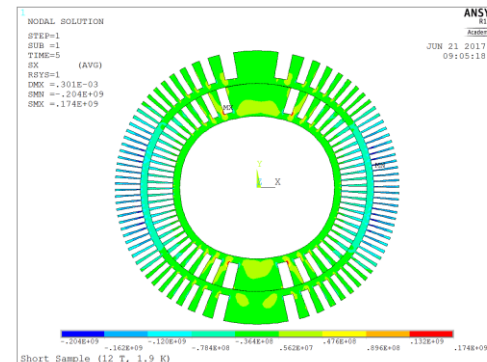
## Operation at short sample limit (1.9 K, 12 T)

### Cool down 1.9 K



Former  $\sigma_r$  = [-86.4, 78.7]MPa

Cool down  
and  
operation steps  
( $\sigma_r$  - Radial)

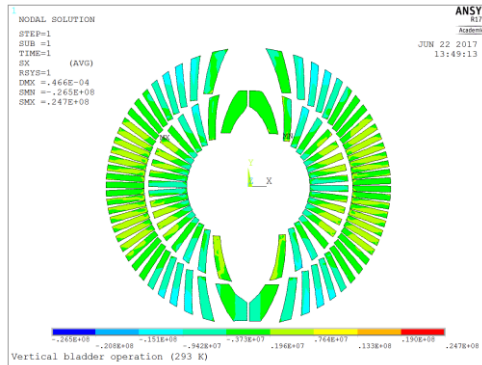


Former  $\sigma_r$  = [-204.0, 174.0]MPa

# CD2 - The Coil Radial Stress

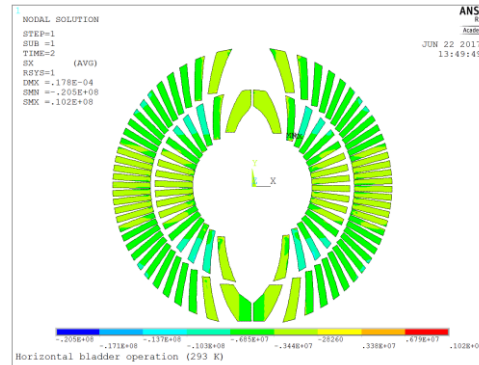
Room temp. steps  
( $\sigma_r$  - Radial)

## Vert. bladder operation



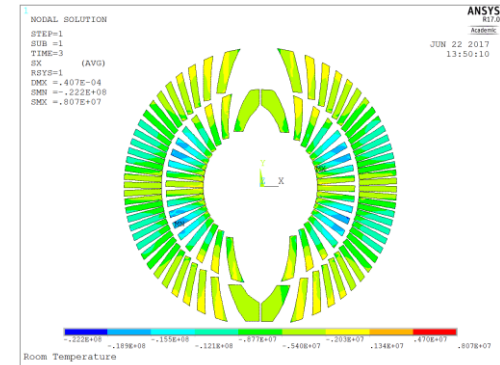
Cable  $\sigma_r$  = [-26.5, 24.7] MPa

## Hor. bladder operation



Cable  $\sigma_r$  = [- 20.5, 10.2] MPa

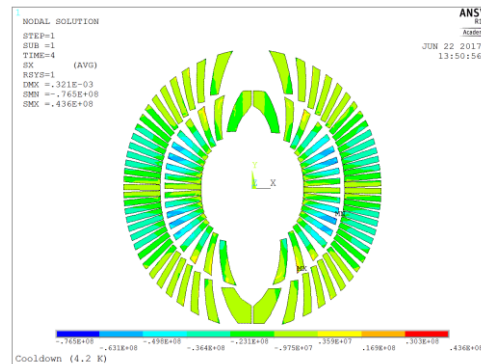
## Assembly - room temp.



Cable  $\sigma_r$  = [-22.2, 8.7] MPa

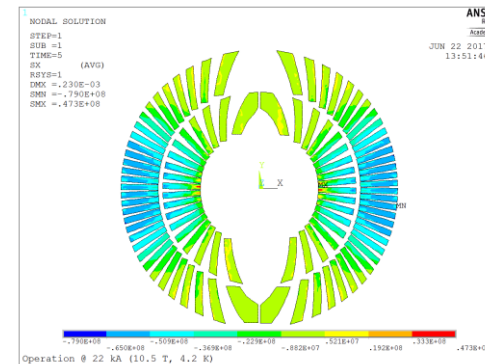
## Operation at short sample limit (4.2 K, 10.5 T)

### Cool down 4.2 K



Cable  $\sigma_r$  = [-76.5, 43.6] MPa

Cool down  
and  
operation steps  
( $\sigma_r$  - Radial)

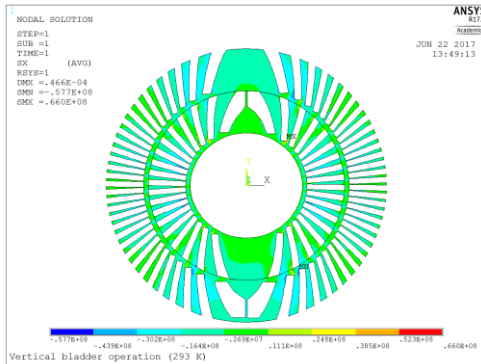


Cable  $\sigma_r$  = [-79.0, 47.3] MPa

# CD2 - The Former Radial Stress

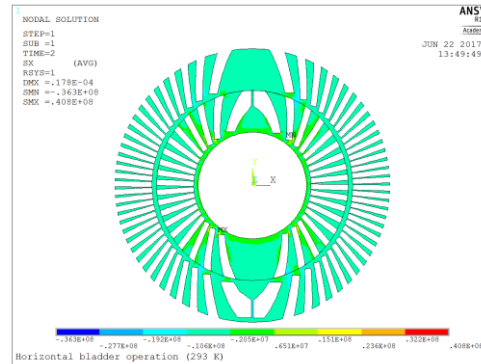
Room temp. steps  
( $\sigma_r$  - Radial)

Vert. bladder operation



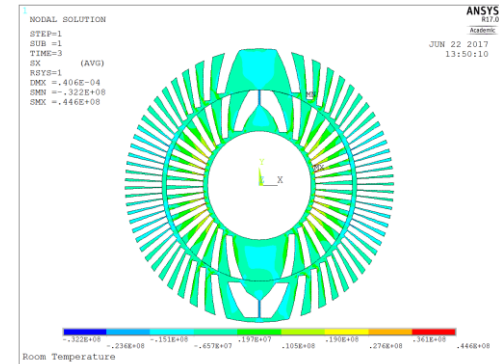
Cable  $\sigma_r$  = [-57.7, 66.0] MPa

Hor. bladder operation



Cable  $\sigma_r$  = [- 36.3, 40.8] MPa

Assembly - room temp.

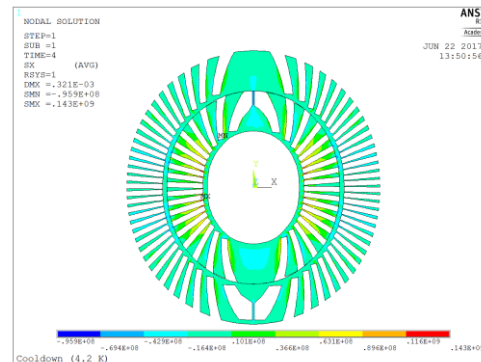


Cable  $\sigma_r$  = [-32.2, 44.6] MPa

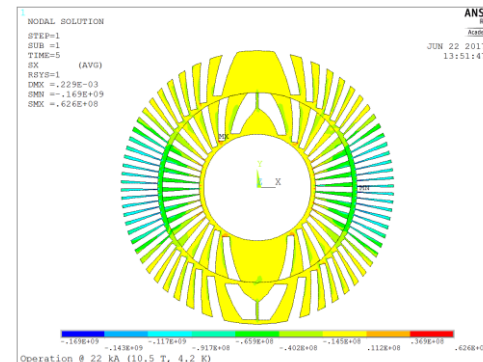
Operation at short sample limit  
(4.2 K, 10.5 T)

Cool down 4.2 K

Cool down  
and  
operation steps  
( $\sigma_r$  - Radial)



Cable  $\sigma_r$  = [-95.9, 143.0] MPa



Cable  $\sigma_r$  = [-169.0, 62.6] MPa