704 MHz Cavities

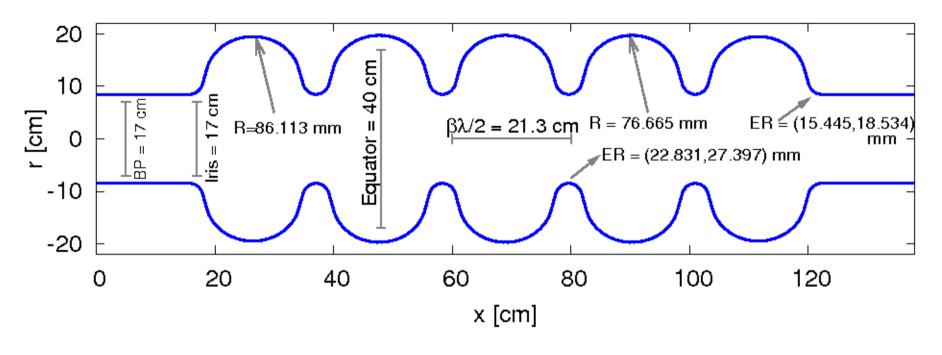
R. Calaga, BNL, Nov 12, 2009

Cavity design (High Q, Less W/m)

Transition section & HOM damping concepts

Future work

Baseline Cavity Design



Eacc = 18 - 25 MV - 5 cells

 $Epk/Eacc \sim 41.4 - 57.5 (x2.3)$

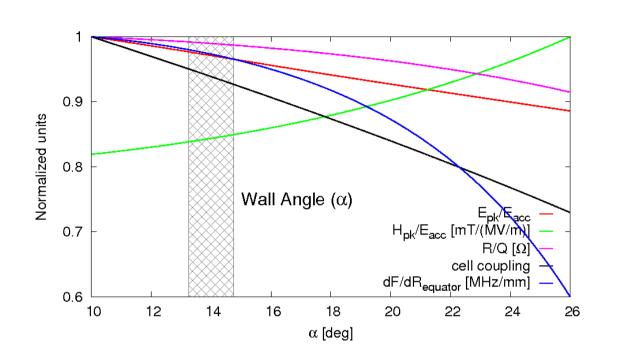
Bpk/Eacc $\sim 80.1 - 111.5 \text{ mT} (4.5 \text{ mT/MV/m})$

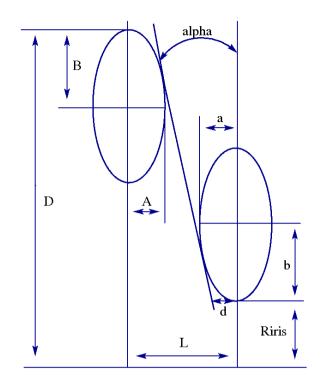
 $R/Q \sim 490 \Omega$

Stiffness (thickness: 3mm)

(Tuner Comp \sim 2.5 mm, Tuner load \sim 2334 lb, dF \sim 0.335 MHz)

SINGLE CELL OPTIMIZATION, FUNDAMENTAL





Parametric scans of the geometrical parameters with RF observables Best compromise for surface fields, cell-to-cell coupling & R/Q

FIELD FLATNESS

Adjust end-cells for frequency & field flatness

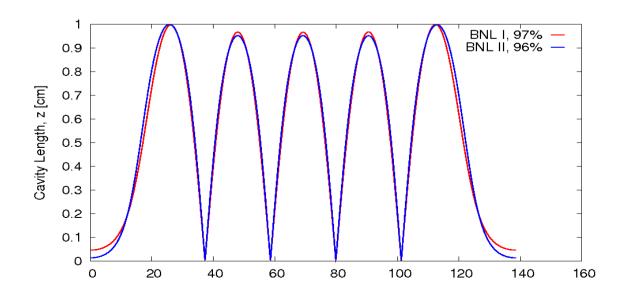
$$\eta = N^2/\beta k_{cc}$$

Fundamental Mode:

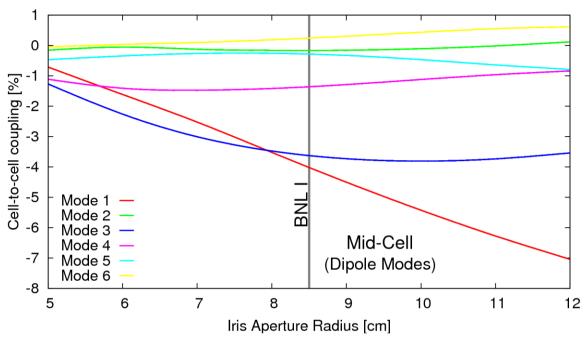
Field flatness between 95-99 %

End-cells become significantly different (99%) \rightarrow HOM Trapping

Fundamental power coupler \rightarrow symmetrizing stub



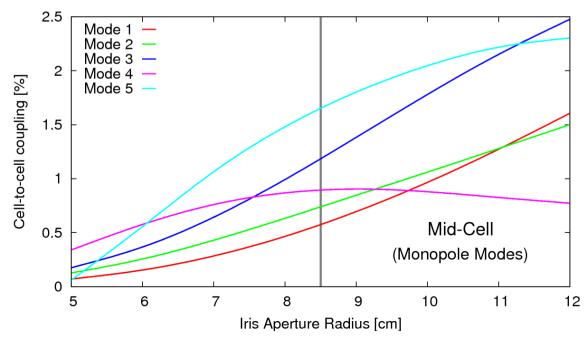
SINGLE CELL OPTIMIZATION, HOMS



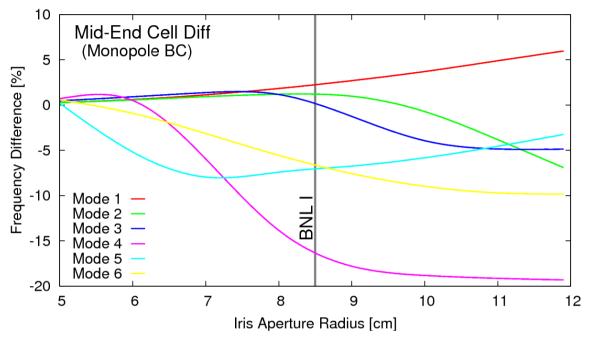
Monopole modes: > 7cm rad

Dipole modes: >7 cm rad

Condition important but no good threshold Fundamental mode $\sim 4.5\%$



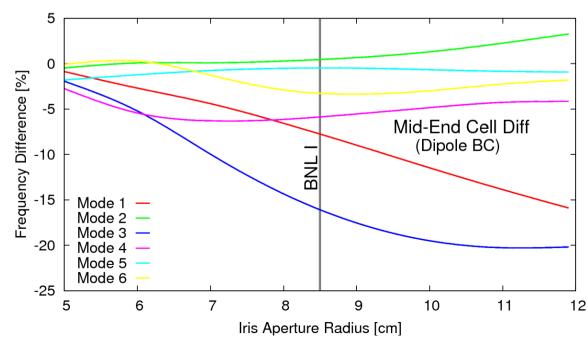
Frequency Difference, HOMs



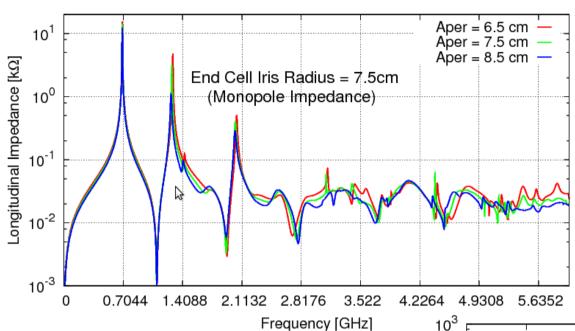
Monopole modes: <8cm rad

Dipole modes: <8 cm rad

But this condition is less strict 1% @1GHz \sim 10 MHz



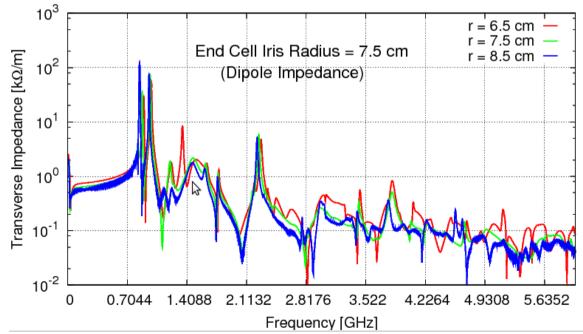
Overlap on Harmonics, HOMs



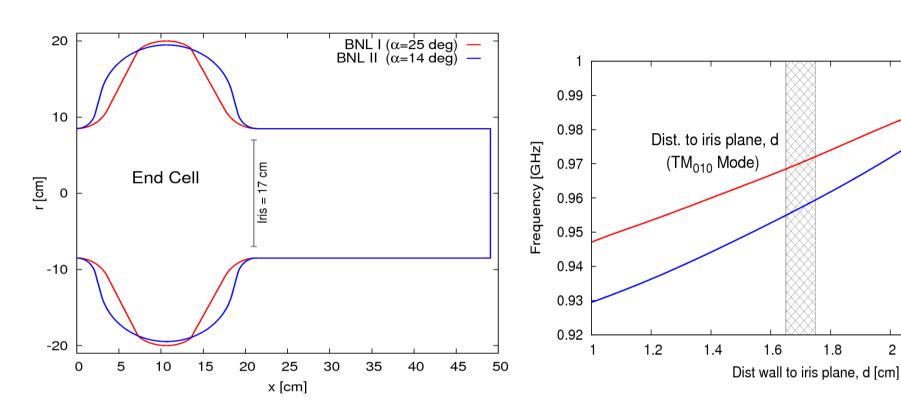
Monopole modes: <8cm rad

Dipole modes: <8 cm rad

But this condition is less strict 1% @1GHz \sim 10 MHz



END-CELL OPTIMIZATION

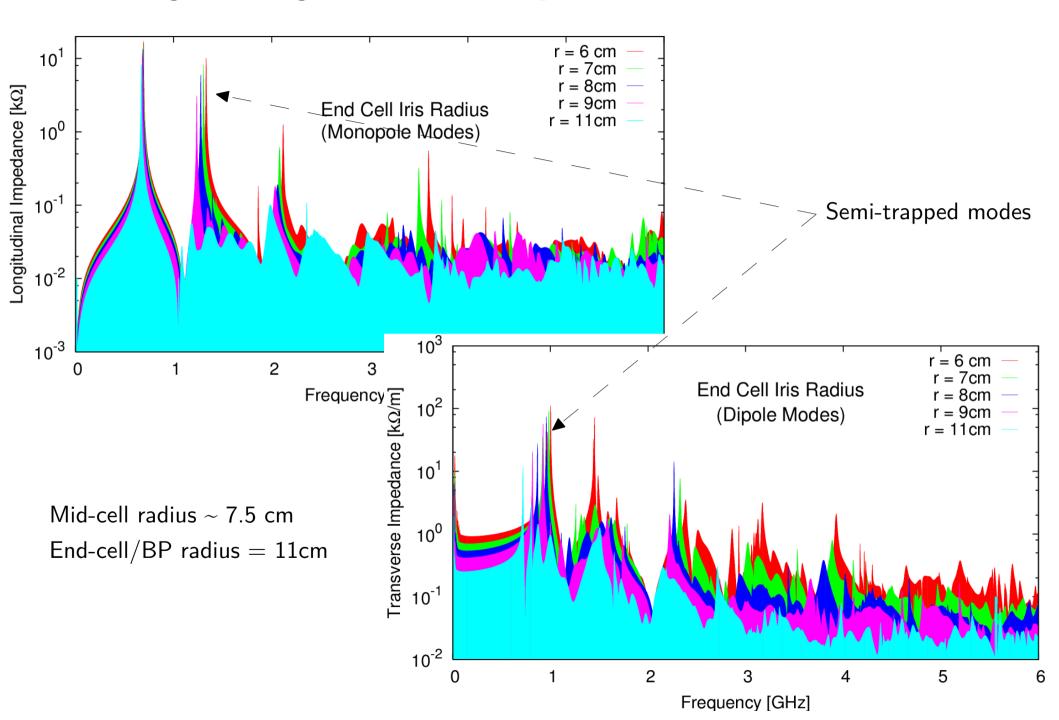


2.2

2.4

Parameter	BNL I	BNL II
	Mid & End Cell	Mid & End Cell
Frequency [MHz]	703.75	703.75
Iris Radius, R_{iris} [cm]	8.5	8.5
Wall Angle, α [deg]	25	{14,12}
Equatorial Ellipse, $R = \frac{B}{A}$	1.0	1.0
Iris Ellipse, $r = \frac{b}{a}$	1.1	1.2
Cavity wall to iris plane, d [cm]	2.5	$\{1.7,1.2\}$
Half Cell Length, $L = \frac{\lambda \beta}{4} [cm]$	10.65	10.65
$H = D - (R_{iris} + b + B)[cm]$	${4.195, 3.792}$	{19.7124,19.4034}
Cavity Beta, $\beta = \frac{v}{c}$	1.0	1.0

END-CELL OPTIMIZATION



HOM Passbands

Mode	Freq	[GHz]	Freq	[GHz]	R/Q	K_{mid}	K_{end}	Δf
	Е	В	Е	В	$[\Omega]$	[%]	[%]	[kHz]
1	0.683	0.704	0.694	0.704	169.7	3.0	1.4	1.1
2	1.277	1.346	1.264	1.295	105.2	5.3	2.4	1.3
3	1.415	1.496	1.438	1.486	0.2	5.6	3.3	2.3
4	1.788	1.991	1.831	1.801	23.7	10.7	1.7	4.3
5	1.978	2.088	1.992	2.027	106.3	5.4	1.7	1.4
6	2.105	2.293	2.103	2.279	3.9	8.6	8.0	0.2
7	2.425	2.616	2.349	2.542	36.8	7.6	7.9	7.6
8	2.528	2.645	2.497	2.613	3.3	4.5	4.5	3.1
9	2.710	-	2.616	2.751	24.6	-	5.0	9.4
10	2.801	-	2.736	2.946	0.9	-	7.4	6.5

Monopoles

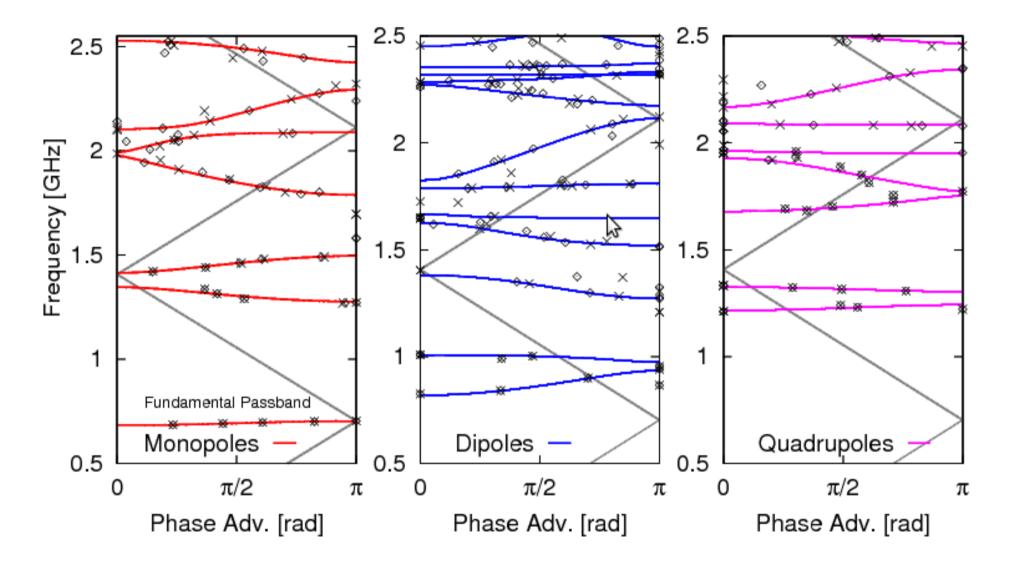
Mode	Freq	[GHz]	Freq	[GHz]	R/Q	K_{mid}	K_{end}	Δf
	E	В	E	В	$[\Omega]$	[%]	[%]	[kHz]
1	0.975	0.820	0.914	0.839	4.87	17.3	8.6	6.1
2	1.008	0.935	1.011	0.969	29.8	7.5	4.2	0.3
3	1.520	1.272	1.531	1.324	19.7	17.8	14.5	1.1
4	1.649	1.382	1.642	1.497	0.4	17.6	9.2	0.7
5	1.667	1.626	1.743	1.625	2.3	2.5	7.0	7.6
6	1.788	1.809	1.804	1.806	3.0	1.2	0.1	1.6
7	2.175	1.825	2.215	2.055	0.1	17.5	7.5	4.0
8	2.284	2.115	2.256	2.237	2.2	7.7	0.9	2.8
9	2.318	2.273	2.275	2.277	2.7	2.0	0.1	4.3
10	2.334	2.320	-	-	0.04	0.6	-	-
11	2.374	2.355	2.366	2.335	0.05	0.8	1.3	0.8
12	2.452	2.450	2.455	2.364	9.0	0.1	3.8	0.3
13	2.761	2.615	2.789	2.712	17.4	5.4	2.8	2.8
14	2.863	2.830	2.860	2.859	0.07	1.2	0.04	0.3
15	2.892	2.868	2.879	2.879	0.01	0.8	0.0	1.3

Dipoles

Quadrupoles

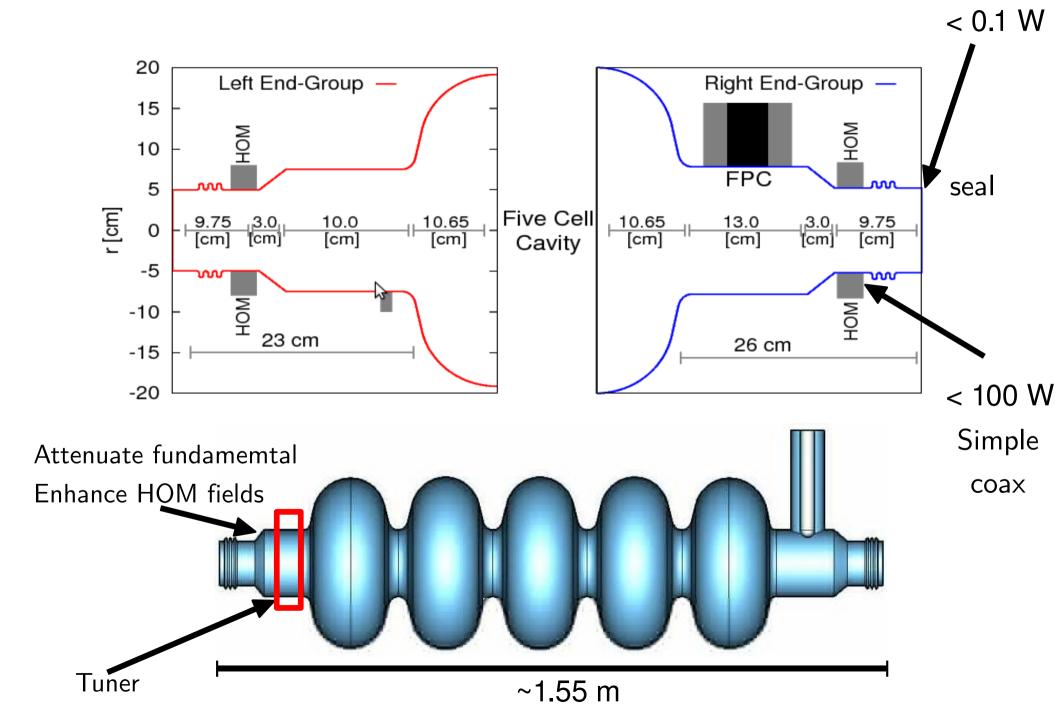
Mode	Freq	[GHz]	Freq	[GHz]	R/Q	K_{mid}	K_{end}	Δf
	Е	В	Е	В	$[\Omega]$	[%]	[%]	[kHz]
1	1.243	1.216	1.219	1.207	0.37	2.2	1.0	2.4
2	1.326	1.304	1.338	1.326	0.36	1.7	0.9	1.2
3	1.775	1.680	1.736	1.687	0.6	5.5	2.9	3.9
4	1.952	1.752	1.877	1.786	0.006	10.8	5.0	7.5
5	1.962	1.928	1.949	1.928	0.22	1.8	1.1	1.3
6	2.092	2.084	2.071	2.071	0.24	0.4	0.0	2.1
7	2.467	2.169	2.474	2.225	0.14	12.9	10.6	0.7
8	2.521	2.343	2.495	2.361	0.03	7.3	5.5	2.6
9	2.585	2.577	2.544	2.534	0.02	0.3	0.4	4.1
10	2.655	2.700	2.608	2.653	-	1.7	1.7	4.7
11	2.711	2.710	2.706	2.706	0.002	0.04	0.0	0.5
12	2.807	3.085	2.799	2.834	0.007	9.4	1.2	0.8

DISPERSION CURVES

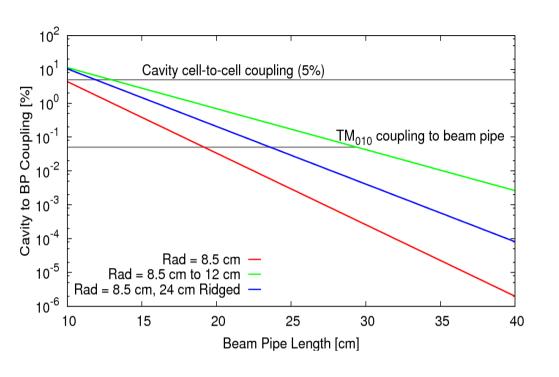


Modes with phase velocity = c are strongly excited (also high R/Q) HOM analysis and damping ongoing (also at Rostok)

TRANSITION SECTION



Transition Section



Length of transition:

Reduce fundamental field at flange Minimize cross talk

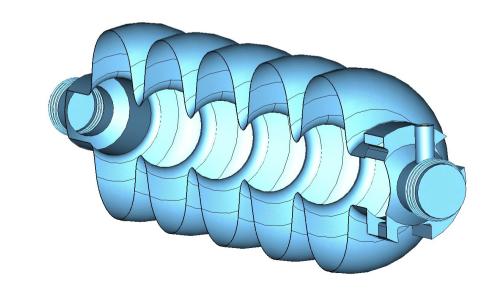
Two choices:

Straight pipe (or taper) - SPL Enlarged (or ridged) - eRHIC

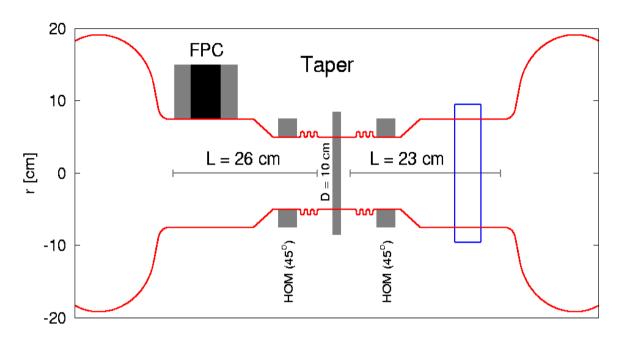
For eRHIC only

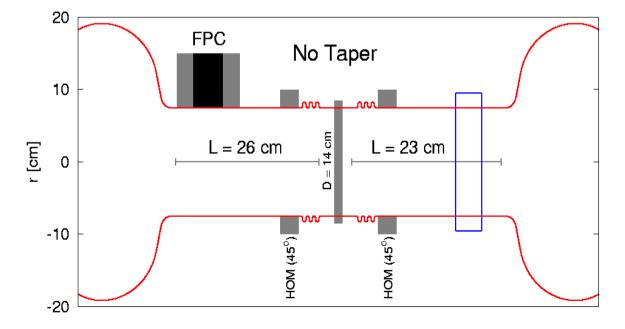
The use of ridges can improve HOM damping, modification to baseline design

Enlarged BP (old design) \rightarrow longer transitions



TRANSITION SECTION





Taper Advantages:

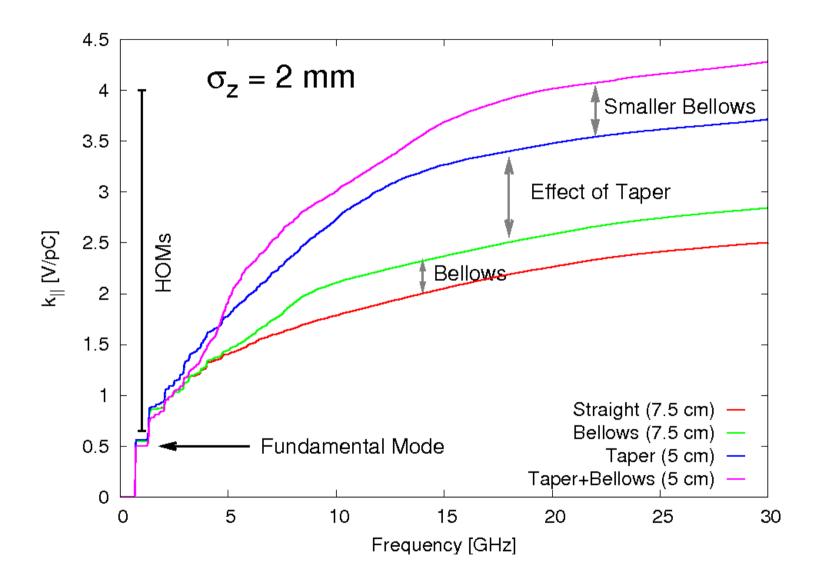
Damp fundamental mode Reduce cross talk

Disadvantages:

Increased cavity wakes
Aperture & activation
Low field multipacting

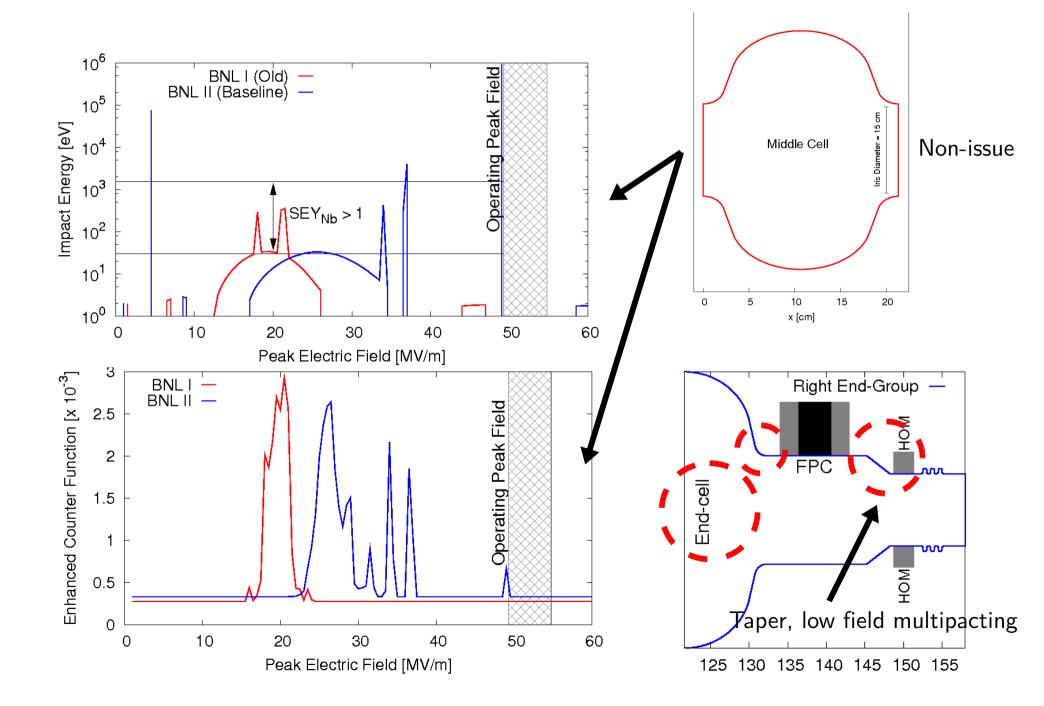
	k _L (V/pC)	k _T (V/pC/m)
Bellow	3.0	2.81
Taper	4.03	6.47
Taper+B	4.6	7.44

Longitudinal Loss Factor

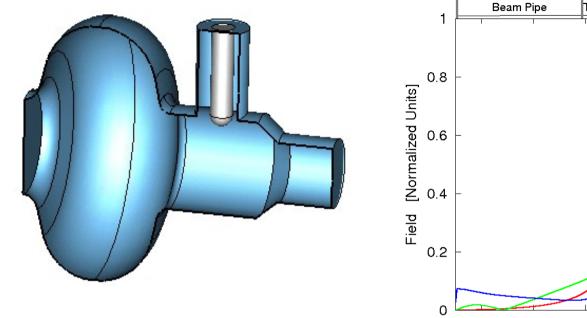


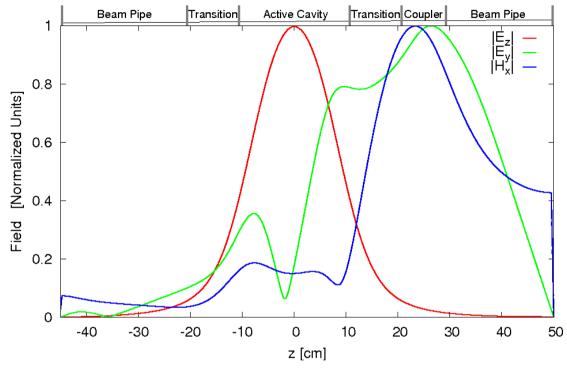
Energy loss & spread (RF, cavity wakes, resistive wall) $\delta E \sim Q k_{_{||}} \ (? \ MeV),$

CAVITY MULTIPACTING



Coupler Kicks





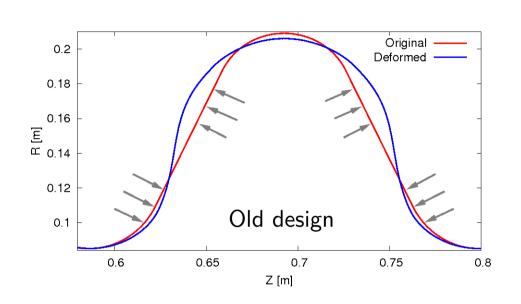
Coupler kicks cannot be neglected (not easy to have alternate couplers)

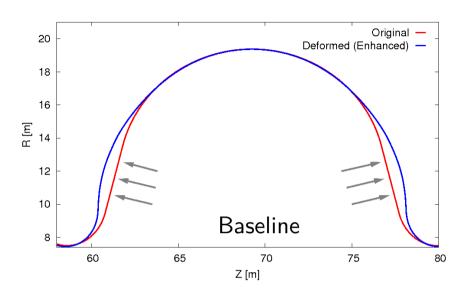
The kicks received and consequent emittance growth depends on Qext

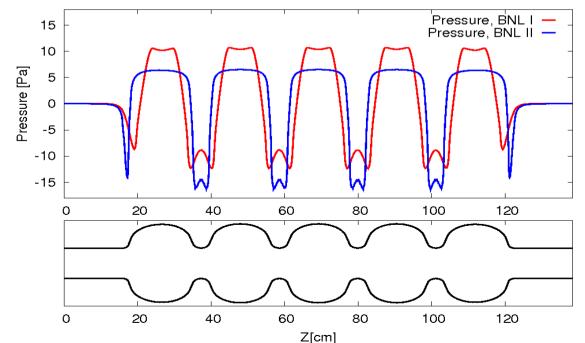
Iteration with optics & beam dynamics required

Partially remedy like symmetrizing studs could be useful

LORENTZ FORCE DETUNING







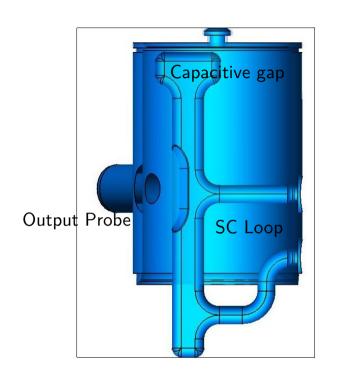
Work ongoing:

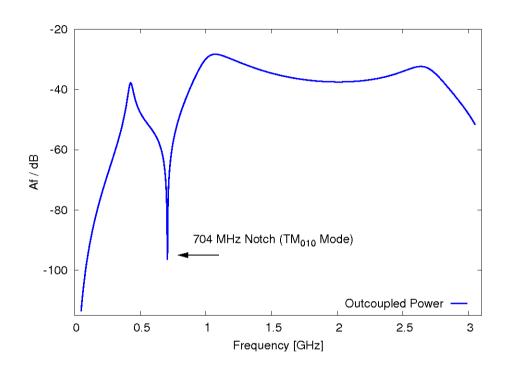
Structural differences from old design Stiffness $\times 2$ smaller from BNL I $(1.28 \text{ Hz/(MV/m})^2)$

Cavity stiffeners "may not" be needed

ANSYS: S. Bellavia

HOM COUPLERS





The "market standard" of tesla-type resonant filters possible but location is NOT in high-field region

Simple coaxial type or more broad-band is robust and appropriate (also BPMs)

Loss materials feasible, but particulates, out-gassing, charge deposition, 2K load

Some Comments

- Detailed cavity design & transition section complete
 - Engineering issues (He vessel, tuner etc..) needs to finalized
 - Mechanical & thermal analysis underway

- The decision of taper needs beam dynamics iteration
 - Taper section: $\underline{\mathbf{5cm}} \rightarrow \mathbf{suggestion}$ to CEA cavity
 - Or- a common flange radius if not taper

• Detailed HOM analysis and damping is being carried out