



## **News from beam-beam SixTrack development**

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WP2 meeting 23/5/2017

# Beam-beam kick recap.

- Strong beam is sliced in both 4D and 6D model according to the longitudinal charge distributions and centroid positions
  - 4D uncoupled beam-beam kick uses  $d_x$ ,  $d_y$ ,  $\Sigma_{xx}$ ,  $\Sigma_{yy}$  to calculate the kick in  $\Delta p_{x,y}$  for each weak particle
  - 6D beam-beam effects are introduced by the Synchro beam mapping such that
    - $\Delta p_{x,y}$  is calculated for the  $d_x$ ,  $d_y$ ,  $\Sigma_{xx}$ ,  $\Sigma_{yy}$  at the effective interaction point using  $(ct, p_x, p_y, \Sigma)$  at the reference IP
    - a  $\Delta p_t$  (emerging from the  $ct$  dependence) is also applied
    - with crossing angle a translation, rotation and a boost change the reference frame in which  $\langle p_{x,y} \rangle, X, Y, P_{x,y} = 0$
  - With coupling the uncoupled form is used in a rotated frame ( $ct$  dependent for the 6D kick)
1. 1976, "[Potential of a Three-Dimensional Gaussian Bunch](#)", S. Kheifets, PETRA Note 119, 3D electric potential
  2. 1980, "[Closed expression for the electrical field of a two-dimensional Gaussian charge](#)", M. Bassetti, A. Erskine, CERN-ISR-TH-80-06; 4D beam beam kick
  3. 1992, "[A Symplectic Beam-Beam Interaction with Energy Change](#)", K. Hirata, F. Ruggiero, SLAC-PUB-10055, KEK Preprint 92-117; Synchro beam mapping (SBM) for head-on beam-beam effects.
  4. 1994, "[Don't Be Afraid of Beam-Beam Interactions With a Large Crossing angle](#)", K. Hirata. SBM with crossing angle
  5. 2001, "[6D Beam-Beam Kick including Coupled Motion](#)", L.H.A. Leunissen, F. Schmidt, G. Ripken; SBM with crossing angle and coupling

# Options in Standard SixTrack BB interface

`lhc=0`, uses as input:

- position of the strong beam w.r.t the weak beam
- $\Sigma_{xx}$ ,  $\Sigma_{yy}$  and other  $\Sigma$  elements are calculated from the weak beam optics
- slicing is computed internally using as input number of slices, crossing angle (`xang`), and slices slope (`xstr`) [1];

`lhc=1`, as before but inverting x with y;

`lhc=2`, as `lhc=1` :

- $\Sigma_{xx}$ ,  $\Sigma_{yy}$  are taken as input in `fort.2` (generated by MadX from the values created by the beam-beam macros)
- other elements of  $\Sigma$  are computed like `lhc=1`;

[1] J. Barranco, [On-going SixTrack code development](#), 30/5/2013, LHC-Beam-beam meeting

# 6D Beam-Beam in SixTrack

## Timeline:

- 1996 [6D kick BCC code from Hirata](#)
- 2000 [6D code in SixTrack with coupling](#) (coupling not used in production)
- 9/2/2011 [lhc=2 option introduced by E. Laface for flat beam with 4D lenses](#)
- 30/12/2013 [lhc=2 fix for 6D and phi2 for effective crab angle by J. Barranco for 6D](#)
- **24/3/2014** **[discussion and decision to change 6D interface to fix 6D issues](#)**: go on with previous fix in the short term, then implement general solution
- 11/5/2014 lhc=2 option in SixTrack release for Boinc
- 11/9/2015 [sigma matrix calculation in MadX requested](#)
- 24/9/2015 [last test/code/manual sent by Javier and reviewed/integrated by Kyrre](#)
- 12/4/2017 [MadX production release with sigma matrix calculation available](#)
- 19/4/2017 [Javier code merged with new expert interface merged by Kyrre and Riccardo](#)
- 10/3/2017 [Gianni started verifying equations](#) from papers and code, bug in 6D boost identified and [fixed by Gianni and merged by Riccardo](#), likely bug in coupling angle sign and other numerical issues under investigations
- 5/5/2017 beam-beam macro beam being adapted by Dario
- 5/5/2017 [bug in sigma matrix calculation identified by Dario and corrected by Irina](#)
- 17/5/2017 impact of boosti bug assessed with a tune scan by Dario
- 17/5/2017 macro completed and mask updated and tested in SixDesk (studies on going) by Dario

## Generalization of the interface

Needed to simulate in 6D:

- flat optics without relying on weak optics information
- crab crossing or other complex strong charge distributions
- dynamic effects like separation collapse or strong orbit noise using DYNK (to do)

# EXPERT interface

- Position of the strong beam w.r.t the weak beam,  $\Sigma$  elements, crossing angle are taken as input and completely decoupled from weak beam.
- 1-slice 6D element supported to allow arbitrary longitudinal distribution and crab crossing with RF curvature via external slicing
- No special slice slope angle

New developments from release 4.6.16: [1]

- Standard and Expert method produces same results
- Standard and Expert interface now coexists and Expert input format is generated by SixTrack

[1] K. Sobjak, <https://github.com/SixTrack/SixTrack/pull/246>

# New Input Format for BB elements

## BEAM

**[ppb]**    $\epsilon_{n,x}$     $\epsilon_{n,y}$     $\sigma_z$ [m]    $\sigma_e$ [m]   **ibeco**   **ibtyp**   **lhc**   **ibbc**
Beam params

This variable still to be kept because was used for other purposes. (lh=9)

"Exact" BB kicks (ibtyp=1) and linear coupling (ibbc=1) NOT TESTED with these new inputs!!!

**name\_4D**   **nsli**    $\Sigma_{xx}$ [mm<sup>2</sup>]    $\Sigma_{yy}$ [mm<sup>2</sup>]   **Sep<sub>x</sub>**[mm]   **Sep<sub>y</sub>**[mm]   **strength-ratio**   **4D**

**name\_6D**   **nsli**    $\theta/2$  [rad]    $\phi$ [rad]   **Sep<sub>x</sub>**[mm]   **Sep<sub>y</sub>**[mm]

$\Sigma_{xx}$  [mm<sup>2</sup>]    $\Sigma_{xyp}$  [mm mrad]    $\Sigma_{xpxp}$  [mrad<sup>2</sup>]    $\Sigma_{yy}$  [mm<sup>2</sup>]    $\Sigma_{yyp}$  [mm mrad]

$\Sigma_{ypyp}$  [mrad<sup>2</sup>]    $\Sigma_{xy}$  [mm<sup>2</sup>]    $\Sigma_{xpy}$  [mm mrad]    $\Sigma_{xpyy}$  [mrad<sup>2</sup>]   **strength-ratio**   **6D**

## NEXT BEAM

Number of slices:  
 · 0 means 4D  
 · ≥ 1 means 6D

If a BB element is divided in several 4D or 6D different elements this variable sets the strength wrt to the total kick.

**2.2000E+11**   **2.5**   **2.5**   **7.5e-02**   **1.10e-04**   **1**   **0**   **0**   **0**   **Beam params**

**bb\_par.l5b1\_18**   **0**   **5.92e-06**   **2.45e-06**   **2.43e+01**   **3.83e-04**   **1**   **4D**

**bb\_ho1b1\_0**   **15**   **0.0**   **295e-03**   **9.69123123e-07**   **-1.37123123e-06**

**5.021231233e-05**   **-4.256123123e-09**   **3.069123123e-07**   **5.021231233e-05**   **3.007123123e-08**

**2.231123123e-03**   **4.075123123e-08**   **1.231123123e-07**   **-4.264123123e-07**   **2.236123123e-03**   **1**   **6D**

## NEXT

59th HiLumi WP2 Task Leader Meeting

J. Barranco, [Status of new input definition of the beam-beam lens in SixTrack](#), 13/11/2015, 59th WP2 meeting



# EXPERT interface (example)

## Standard

```
bb_ho5b1_0 20 9.111827660e-07 -1.350224489e-06 1.000000000e+00 5.026457379e-05 5.026457406e-05 0.000000000e+00
bb_ho1b1_0 20 9.669766338e-07 -1.378612898e-06 1.000000000e+00 5.026457379e-05 5.026457406e-05 0.000000000e+00
```

BEAM

```
2.2000e+11 2.5 2.5 7.5000e-02 1.1000e-04 1 0 0 0
```

```
bb_ho5b1_0 15 295e-6 0.0 295e-6
```

```
bb_ho1b1_0 15 295e-6 1.57 295e-6
```

NEXT

## Expert

```
bb_ho5b1_0 20 0.000000000e+00 0.000000000e+00 0.000000000e+00 0.000000000e+00 0.000000000e+00 0.000000000e+00
bb_ho1b1_0 20 0.000000000e+00 0.000000000e+00 0.000000000e+00 0.000000000e+00 0.000000000e+00 0.000000000e+00
```

BEAM

EXPERT

```
2.2000e+11 2.5 2.5 7.5000e-02 1.1000e-04 1 0 0 0
```

```
bb_ho5b1_0 15 2.9500000000001e-004 0.0000000000000e+000 9.1118276600001e-007 -1.3502244890000e-006
5.0034903462428e-005 -9.593556151459e-008 2.24428543738e-003 5.021051982892e-005 7.5280318127904e-007
2.2365333052480e-003 -1.663390341512e-009 -1.5308153223e-009 7.342199089562e-010 -6.517402396885e-009 1.000
```

```
bb_ho1b1_0 15 2.9500000000001e-004 1.5700000000001e+000 9.66976633800002e-007 -1.3786128980000e-006
5.0520079639196e-005 -6.010182490910e-007 2.22276103671e-003 5.028688389602e-005 7.7037643894229e-007
2.2330903791604e-003 -3.652801218428e-009 2.66101452881e-008 3.638680415249e-008 1.1594595769731e-007 1.000
```

NEXT

Expert input is also written by SixTrack in the standard output



# Update beam-beam macros

Former 4D beam-beam MadX macros from Stephane now write in the mask SixTrack Expert input by computing missing  $\Sigma$ -matrix elements for each slice

- centroid with crab effects and  $\Sigma_{11,33}$  were already computed
- first sanity checks shows good agreement with previous models (cannot be reproduced fully because they were inconsistent)
- Test on full studies on-going
- Tracking with Beam 4 under investigation

	mad/six	mad	sixtrack
sig11	1.00000002447	0.002246565358	0.00224656530302
sig12	1.00000002437	0.0001498270964	0.000149827092749
sig22	0.99999999265	6.00464297e-05	6.00464297441e-05
sig33	0.999999994158	0.01125155011	0.0112515501757
sig34	0.999999994116	-0.0007503841707	-0.000750384175115
sig44	0.999999999041	6.003852509e-05	6.00385251476e-05
sig13	1.00000001226	0.0001896193048	0.000189619302476
sig14	1.00000001153	-1.264601973e-05	-1.26460195841e-05
sig23	1.00000001153	1.264601973e-05	1.26460195842e-05
sig24	1.00000001202	-1.686933683e-06	-1.68693366273e-06

Mad vs SixTrack  
Sigma matrix calculations

# Differences old to new macros

## Old macros for 6D

- $\Sigma_{11,33}$  and  $x_{B2}, y_{B2}$  computed from an ideal machine
- $x_{B1}, y_{B1}$  add from imperfect orbit by MadX
- Crossing angle input manually
- $\Sigma_{12,22,34,44,13,14,23,24,34}$  computed by Sixtrack based B1 optics
- $\Sigma_{13,14,23,24,34}$  discarded

## New macros for 6D

- $\Sigma_{full}$  for and  $x, px, y, py$  for B1,2 computed from an ideal machine in MadX
- $\Sigma_{13,14,23,24,34}$  discarded pending verifications
- Input for Beam 1
- Beam 4 possible (under development)

# Review of the the 6D beam-beam routines

(Is the physics implemented correctly?)

# Review of the 6D beam-beam routines

Addressing two questions:

- **What is the code supposed to do?**
  - Mathematical derivation of the implemented numerical model
- **Is the code doing what it is supposed to do?**
  - Verify the implementation of the above numerical model

# Mathematical derivation

The code implements the **Synchro Beam Mapping** in the presence of:

- **Crossing angle** ( $\phi$ )
- Arbitrary **crossing plane** ( $\alpha$ )
- Optics at the IP described by a **general 4D correlation matrix** ( $\Sigma$ -matrix) → hour glass effect, elliptic beams, alphas, and linear coupling at the IP are included in the modeling)

This makes the **mathematical derivation quite heavy**

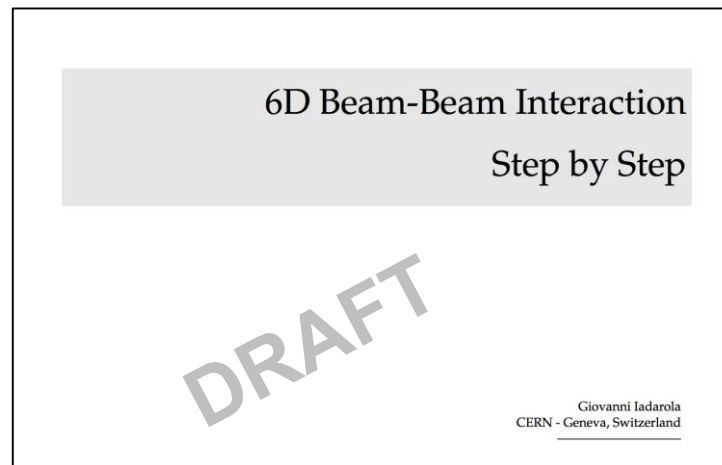
Implementation in Sixtrack in **largely based on:**

- [6D Beam-Beam Kick including Coupled Motion](#), L.H.A. Leunissen, F. Schmidt, G. Ripken, 2001

... but **important parts** (e.g. inverse boost, “optics de-coupling” including longitudinal derivatives) are **not reported in the paper nor anywhere else**, to our best knowledge...

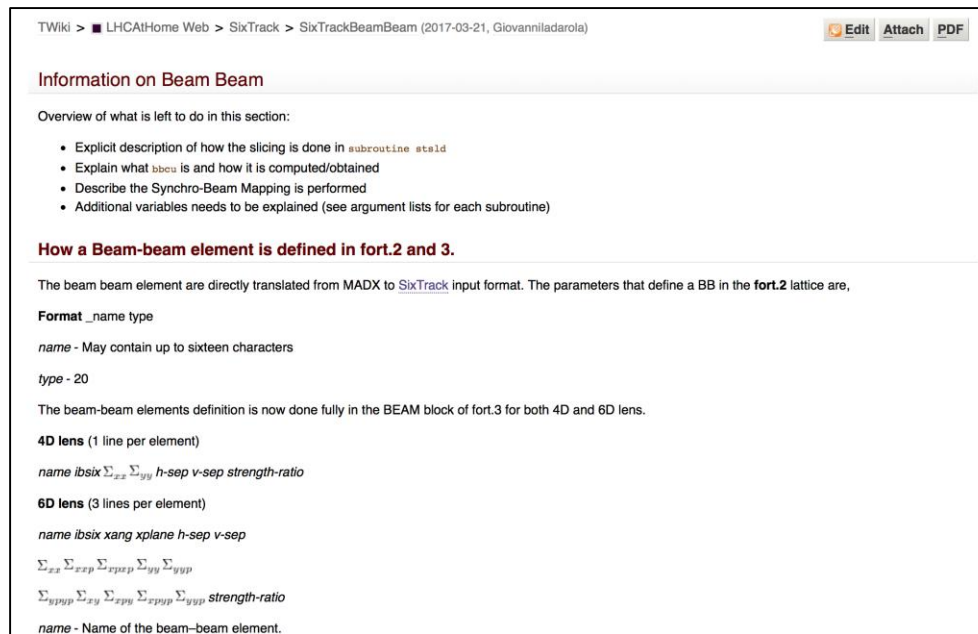
# Mathematical derivation

- Invested some time in **understanding and re-constructing the mathematical treatment** trying to use as little as possible the source code as a reference
  - **Independent reconstruction** of the equations to verify the implementation in Sixtrack and to be used as a basis for a modern implementation (GPU compatible, for example)
  - **Parts not available in literature** (mainly inverse Lorentz boost, and a large fraction of the coupling treatment) **had to be re-derived**
- Drafted a **document** including the full set of equation to enable a possible re-implementation (and avoid that somebody has to redo the same exercise in ten years)



# Verification of the implementation

- Started from **previous work** done by J. Barranco
  - Identified and described the **interface of the main functional blocks**
  - Built tables with the descriptions of the cumbersome **notation** used in the code



TWiki > LHCATHome Web > SixTrack > SixTrackBeamBeam (2017-03-21, Giovanniladarola) Edit Attach PDF

### Information on Beam Beam

Overview of what is left to do in this section:

- Explicit description of how the slicing is done in subroutine `steld`
- Explain what `sbscs` is and how it is computed/obtained
- Describe the Synchro-Beam Mapping is performed
- Additional variables needs to be explained (see argument lists for each subroutine)

### How a Beam-beam element is defined in fort.2 and 3.

The beam beam element are directly translated from MADX to SixTrack input format. The parameters that define a BB in the **fort.2** lattice are,

**Format** `_name` type

`name` - May contain up to sixteen characters

`type` - 20

The beam-beam elements definition is now done fully in the BEAM block of fort.3 for both 4D and 6D lens.

**4D lens** (1 line per element)

`name lbsix`  $\Sigma_{xx}$   $\Sigma_{yy}$  `h-sep` `v-sep` `strength-ratio`

**6D lens** (3 lines per element)

`name lbsix xang xplane` `h-sep` `v-sep`

$\Sigma_{xx}$   $\Sigma_{xpx}$   $\Sigma_{xpy}$   $\Sigma_{yxx}$   $\Sigma_{yy}$   $\Sigma_{yyp}$

$\Sigma_{yyp}$   $\Sigma_{xy}$   $\Sigma_{xpy}$   $\Sigma_{xpy}$   $\Sigma_{yyp}$  `strength-ratio`

`name` - Name of the beam-beam element.

- Moved to the understanding and testing of the source code...

# Verification of the implementation

- Very difficult to identify problems by using the full tracking simulations
  - Need to test the single routine **“on the bench”**
- **Procedure** being performed for each functional block
  - Built a **quick C/python implementation** from the equations in the document
  - Extracted the **corresponding sixtrack source code** and compiled as of a stand-alone python module (f2py)
  - **“Stress test”** performed on the two: consistency checks, comparison against each other



# Verification of the implementation

- **Present status** of the verification for the different functional blocks:

Module	Tests performed	Outcome
<b>Boost/anti-boost</b>	<ul style="list-style-type: none"><li>• Comparison Sixtrack vs C/python routine</li><li>• Checked that the two cancel each other</li></ul>	<b>Bug</b> identified and <b>corrected</b>
<b>Beam-beam forces</b> (with potential derivatives w.r.t. sigmas)	<ul style="list-style-type: none"><li>• Comparison sixtrack vs C/python routine</li><li>• Force compared against Finite Difference Poisson solved (PyPIC)</li><li>• Other derivatives compared against numerical integration/derivation</li></ul>	<b>All checks passed</b>
<b>Beam shape propagation and coupling treatment</b>	<ul style="list-style-type: none"><li>• Comparison Sixtrack vs C/python routine</li><li>• Comparison against MAD for a coupled beam line</li><li>• Crosscheck with numerical derivation</li></ul>	Ongoing: <ul style="list-style-type: none"><li>• <b>Uncoupled beams look OK</b></li><li>• <b>Coupling</b> under investigation: different <b>problems</b> already identified</li></ul>
<b>Computation of the kicks</b>	Still to be tested	Still to be tested
<b>Slicing</b>	Still to be tested	Still to be tested

- Complete review to be presented later this year

# Problem in the inverse boost

- Problem **identified with “bench-test”** (large crossing angle, test particle very off momentum and large  $p_x$ ,  $p_y$ )
- Boost and anti-boost should cancel each other exactly

## Error after boost + anti-boost

Python test routine		SixTrack routine	
<b>x</b>	4.3e-19	<b>x</b>	6.5e-19
<b>px</b>	0.0	<b>px</b>	0.065
<b>y</b>	4.3e-19	<b>y</b>	4.3e-19
<b>py</b>	3.e3-17	<b>py</b>	0.027
<b>sigma</b>	0.0	<b>sigma</b>	0.0
<b>delta</b>	1e-16	<b>delta</b>	2.0e-17

# Problem in the inverse boost

- Problem **identified with “bench-test”** (large crossing angle, test particle very off momentum and large  $p_x$ ,  $p_y$ )
- Boost and anti-boost should cancel each other exactly

**Discrepancy** found between in the anti-boost between derived equations and SixTrack source code:

$$p_x = p_x^* \cos \phi + h \cos \alpha \tan \phi \quad (95)$$

$$p_y = p_y^* \cos \phi + h \sin \alpha \tan \phi \quad (96)$$

```
TRACK (2) = (TRACK (2) + CALPHA * SPHI * H1) * CPHI
```

```
TRACK (4) = (TRACK (4) + SALPHA * SPHI * H1) * CPHI
```

The lines should be:

```
TRACK (2) = (TRACK (2) * CPHI + CALPHA * TPHI * H1)
```

```
TRACK (4) = (TRACK (4) * CPHI + SALPHA * TPHI * H1)
```

- Digging a bit we found out that the issue was already present in [Hirata's code](#) from 1996, on which the Sixtrack implementation is based

# Problem in the inverse boost

- Problem **identified with “bench-test”** (large crossing angle, test particle very off momentum and large  $p_x$ ,  $p_y$ )
- Boost and anti-boost should cancel each other exactly

## Error after boost + anti-boost

Python test routine		SixTrack routine		SixTrack corrected	
<b>x</b>	4.3e-19	<b>x</b>	6.5e-19	<b>x</b>	6.5e-19
<b>px</b>	0.0	<b>px</b>	0.065	<b>px</b>	5.55e-17
<b>y</b>	4.3e-19	<b>y</b>	4.3e-19	<b>y</b>	4.3e-19
<b>py</b>	3.e3-17	<b>py</b>	0.027	<b>py</b>	0.1e-19
<b>sigma</b>	0.0	<b>sigma</b>	0.0	<b>sigma</b>	0.0
<b>delta</b>	1e-16	<b>delta</b>	2.0e-17	<b>delta</b>	2.0e-17

# Problem in the inverse boost

- Problem confirmed by Riccardo simulating a beam-beam interaction with **zero intensity in the strong beam**

## Original implementation

### Coordinates before interaction

### Coordinates after interaction

dump_ip.dat							dump_bb.dat												
#	ID	turn	s[m]	x[mm]	xp[mrad]	y[mm]	yp[mrad]	dE/E[1]	ktrack	#	ID	turn	s[m]	x[mm]	xp[mrad]	y[mm]	yp[mrad]	dE/E[1]	ktrack
1	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973240618E-03			1	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973250177E-03		
2	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973240618E-03			2	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973250177E-03		
3	1	1	0.00000	2.169989354E-01	1.829089161E-02	1.931331047E-01	-1.627923509E-02			3	1	1	0.00000	2.169989354E-01	1.829089158E-02	1.931331047E-01	-1.627927274E-02		
4	1	1	0.00000	2.169989354E-01	1.829089161E-02	1.931331047E-01	-1.627923509E-02			4	1	1	0.00000	2.169989354E-01	1.829089158E-02	1.931331047E-01	-1.627927274E-02		
5	1	1	0.00000	2.894989354E-01	2.440193375E-02	3.628561362E-01	-3.058522956E-02			5	1	1	0.00000	2.894989354E-01	2.440193367E-02	3.628561362E-01	-3.058532567E-02		
6	1	1	0.00000	2.894989354E-01	2.440193375E-02	3.628561362E-01	-3.058522956E-02			6	1	1	0.00000	2.894989354E-01	2.440193367E-02	3.628561362E-01	-3.058532567E-02		
7	1	1	0.00000	3.619989354E-01	3.051297588E-02	5.325791676E-01	-4.489122400E-02			7	1	1	0.00000	3.619989354E-01	3.051297574E-02	5.325791676E-01	-4.489140898E-02		
8	1	1	0.00000	3.619989354E-01	3.051297588E-02	5.325791676E-01	-4.489122400E-02			8	1	1	0.00000	3.619989354E-01	3.051297574E-02	5.325791676E-01	-4.489140898E-02		
9	1	1	0.00000	4.344989354E-01	3.662401801E-02	7.023021991E-01	-5.919721844E-02			9	1	1	0.00000	4.344989354E-01	3.662401777E-02	7.023021991E-01	-5.919752266E-02		
10	1	1	0.00000	4.344989354E-01	3.662401801E-02	7.023021991E-01	-5.919721844E-02			10	1	1	0.00000	4.344989354E-01	3.662401777E-02	7.023021991E-01	-5.919752266E-02		
1	2	1	0.00000	1.308501246E-01	8.514045444E-03	-9.961266845E-03	3.153912424E-04			1	2	1	0.00000	1.308501246E-01	8.514045441E-03	-9.961266845E-03	3.153866850E-04		
2	2	1	0.00000	1.308501246E-01	8.514045444E-03	-9.961266845E-03	3.153912424E-04			2	2	1	0.00000	1.308501246E-01	8.514045441E-03	-9.961266845E-03	3.153866850E-04		
3	2	1	0.00000	1.041820622E-01	-1.200951763E-02	-8.217894405E-02	2.601833146E-03			3	2	1	0.00000	1.041820622E-01	-1.200951763E-02	-8.217894405E-02	2.601823666E-03		
4	2	1	0.00000	1.041820622E-01	-1.200951763E-02	-8.217894405E-02	2.601833146E-03			4	2	1	0.00000	1.041820622E-01	-1.200951763E-02	-8.217894405E-02	2.601823666E-03		
5	2	1	0.00000	7.751399978E-02	-3.253308068E-02	-1.543977321E-01	4.888831596E-03			5	2	1	0.00000	7.751399978E-02	-3.253308074E-02	-1.543977321E-01	4.888313646E-03		
6	2	1	0.00000	7.751399978E-02	-3.253308068E-02	-1.543977321E-01	4.888831596E-03			6	2	1	0.00000	7.751399978E-02	-3.253308074E-02	-1.543977321E-01	4.888313646E-03		
7	2	1	0.00000	5.084593752E-02	-5.305664373E-02	-2.266176309E-01	7.175036594E-03			7	2	1	0.00000	5.084593752E-02	-5.305664388E-02	-2.266176309E-01	7.174856626E-03		
8	2	1	0.00000	5.084593752E-02	-5.305664373E-02	-2.266176309E-01	7.175036594E-03			8	2	1	0.00000	5.084593752E-02	-5.305664388E-02	-2.266176309E-01	7.174856626E-03		
9	2	1	0.00000	2.417787538E-02	-7.358020677E-02	-2.988386405E-01	9.461798139E-03			9	2	1	0.00000	2.417787538E-02	-7.358020705E-02	-2.988386405E-01	9.461452606E-03		
10	2	1	0.00000	2.417787538E-02	-7.358020677E-02	-2.988386405E-01	9.461798139E-03			10	2	1	0.00000	2.417787538E-02	-7.358020705E-02	-2.988386405E-01	9.461452606E-03		

## Corrected implementation

### Coordinates before interaction

### Coordinates after interaction

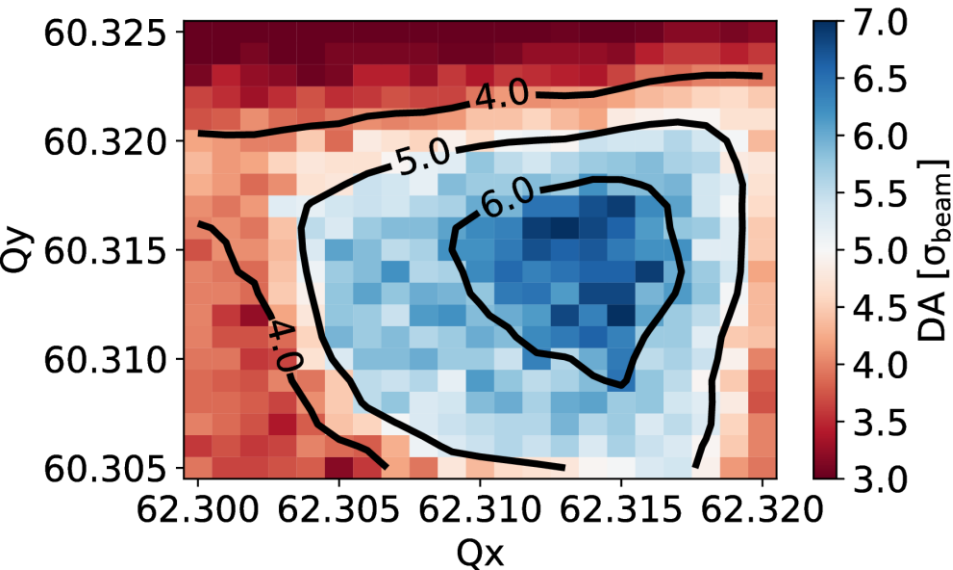
dump_ip.dat							dump_bb.dat												
ID	turn	s[m]	x[mm]	xp[mrad]	y[mm]	yp[mrad]	dE/E[1]	ktrack	ID	turn	s[m]	x[mm]	xp[mrad]	y[mm]	yp[mrad]	dE/E[1]	ktrack		
1	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973240618E-03			1	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973240618E-03		
2	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973240618E-03			2	1	1	0.00000	1.444989354E-01	1.217984946E-02	2.341007330E-02	-1.973240618E-03		
3	1	1	0.00000	2.169989354E-01	1.829089161E-02	1.931331047E-01	-1.627923509E-02			3	1	1	0.00000	2.169989354E-01	1.829089161E-02	1.931331047E-01	-1.627923509E-02		
4	1	1	0.00000	2.169989354E-01	1.829089161E-02	1.931331047E-01	-1.627923509E-02			4	1	1	0.00000	2.169989354E-01	1.829089161E-02	1.931331047E-01	-1.627923509E-02		
5	1	1	0.00000	2.894989354E-01	2.440193375E-02	3.628561362E-01	-3.058522956E-02			5	1	1	0.00000	2.894989354E-01	2.440193375E-02	3.628561362E-01	-3.058522956E-02		
6	1	1	0.00000	2.894989354E-01	2.440193375E-02	3.628561362E-01	-3.058522956E-02			6	1	1	0.00000	2.894989354E-01	2.440193375E-02	3.628561362E-01	-3.058522956E-02		
7	1	1	0.00000	3.619989354E-01	3.051297588E-02	5.325791676E-01	-4.489122400E-02			7	1	1	0.00000	3.619989354E-01	3.051297588E-02	5.325791676E-01	-4.489122400E-02		
8	1	1	0.00000	3.619989354E-01	3.051297588E-02	5.325791676E-01	-4.489122400E-02			8	1	1	0.00000	3.619989354E-01	3.051297588E-02	5.325791676E-01	-4.489122400E-02		
9	1	1	0.00000	4.344989354E-01	3.662401801E-02	7.023021991E-01	-5.919721844E-02			9	1	1	0.00000	4.344989354E-01	3.662401801E-02	7.023021991E-01	-5.919721844E-02		
10	1	1	0.00000	4.344989354E-01	3.662401801E-02	7.023021991E-01	-5.919721844E-02			10	1	1	0.00000	4.344989354E-01	3.662401801E-02	7.023021991E-01	-5.919721844E-02		
1	2	1	0.00000	1.308501247E-01	8.514045444E-03	-9.960917299E-03	3.153577120E-04			1	2	1	0.00000	1.308501247E-01	8.514045444E-03	-9.960917299E-03	3.153577120E-04		
2	2	1	0.00000	1.308501247E-01	8.514045444E-03	-9.960917299E-03	3.153577120E-04			2	2	1	0.00000	1.308501247E-01	8.514045444E-03	-9.960917299E-03	3.153577120E-04		
3	2	1	0.00000	1.041820623E-01	-1.200951763E-02	-8.217756745E-02	2.601701095E-03			3	2	1	0.00000	1.041820623E-01	-1.200951763E-02	-8.217756745E-02	2.601701095E-03		
4	2	1	0.00000	1.041820623E-01	-1.200951763E-02	-8.217756745E-02	2.601701095E-03			4	2	1	0.00000	1.041820623E-01	-1.200951763E-02	-8.217756745E-02	2.601701095E-03		
5	2	1	0.00000	7.751400004E-02	-3.253308069E-02	-1.543942171E-01	4.888044424E-03			5	2	1	0.00000	7.751400004E-02	-3.253308069E-02	-1.543942171E-01	4.888044424E-03		
6	2	1	0.00000	7.751400004E-02	-3.253308069E-02	-1.543942171E-01	4.888044424E-03			6	2	1	0.00000	7.751400004E-02	-3.253308069E-02	-1.543942171E-01	4.888044424E-03		
7	2	1	0.00000	5.084593802E-02	-5.305664374E-02	-2.266108663E-01	7.174387701E-03			7	2	1	0.00000	5.084593802E-02	-5.305664374E-02	-2.266108663E-01	7.174387701E-03		
8	2	1	0.00000	5.084593802E-02	-5.305664374E-02	-2.266108663E-01	7.174387701E-03			8	2	1	0.00000	5.084593802E-02	-5.305664374E-02	-2.266108663E-01	7.174387701E-03		
9	2	1	0.00000	2.417787621E-02	-7.358020679E-02	-2.988275150E-01	9.460730924E-03			9	2	1	0.00000	2.417787621E-02	-7.358020679E-02	-2.988275150E-01	9.460730924E-03		
10	2	1	0.00000	2.417787621E-02	-7.358020679E-02	-2.988275150E-01	9.460730924E-03			10	2	1	0.00000	2.417787621E-02	-7.358020679E-02	-2.988275150E-01	9.460730924E-03		

# Problem in the inverse boost

- Impact on **realistic simulation study** assessed by Dario
- Tune scans comparison with 2017 ATS optics show no dramatic change, but slightly worse DA

Old version

ATS Optics;  $\beta^* = 40$  cm;  $Q' = 15$ ;  $I_{MO} = 500$  A;  
 $\varepsilon = 2.5$   $\mu\text{m}$ ;  $I = 1.25 \cdot 10^{11}$  e;  $X = 150$   $\mu\text{rad}$ ; Min DA.



Corrected version

ATS Optics;  $\beta^* = 40$  cm;  $Q' = 15$ ;  $I_{MO} = 500$  A;  
 $\varepsilon = 2.5$   $\mu\text{m}$ ;  $I = 1.25 \cdot 10^{11}$  e;  $X = 150$   $\mu\text{rad}$ ; Min DA.

