



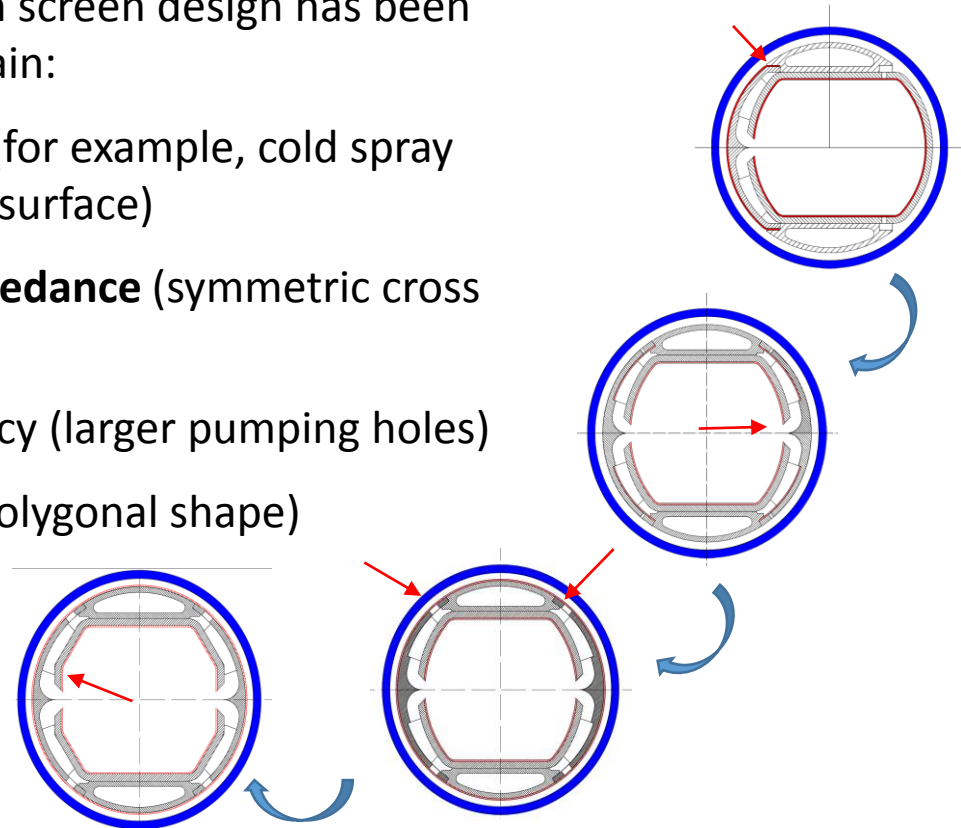
Progress with the cryogenic vacuum system of FCC-hh

Francis Perez (ALBA) and Paolo Chiggiato (CERN)
on behalf of EuroCirCol WP4

Progress with the FCC-hh beam screen design

- In the last two year, the beam screen design has been modified several times to attain:

- Improved **heat transfer** (for example, cold spray copper ring in the outer surface)
- Reduced transverse impedance** (symmetric cross section)
- Higher pumping efficiency** (larger pumping holes)
- Easier manufacturing** (polygonal shape)

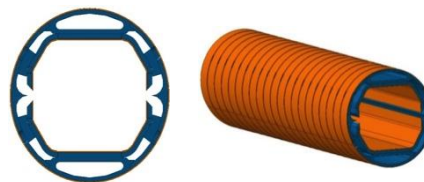


Progress with the FCC-hh beam screen design

Orsay 09/2015
3th WP4 meeting



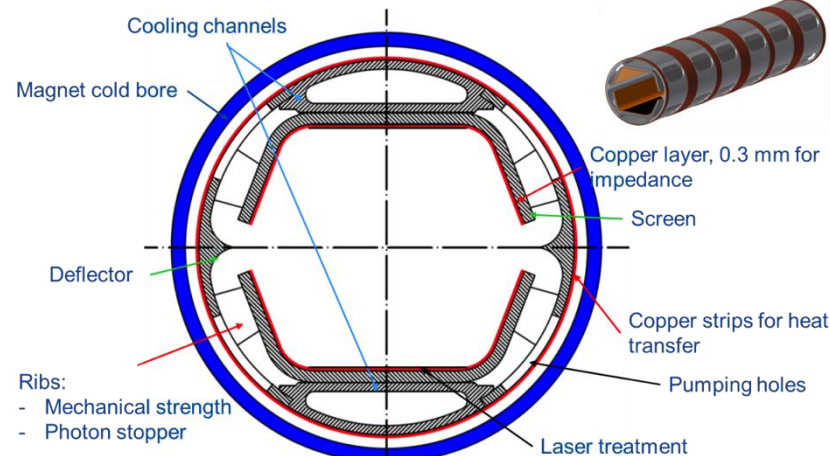
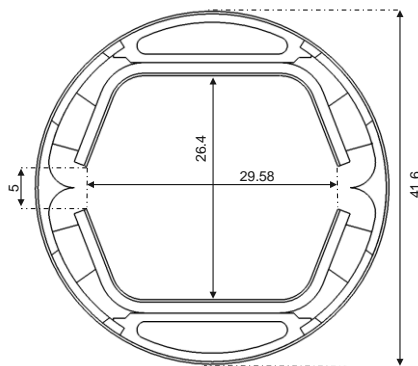
Geneva 06/2016
4th WP4 meeting



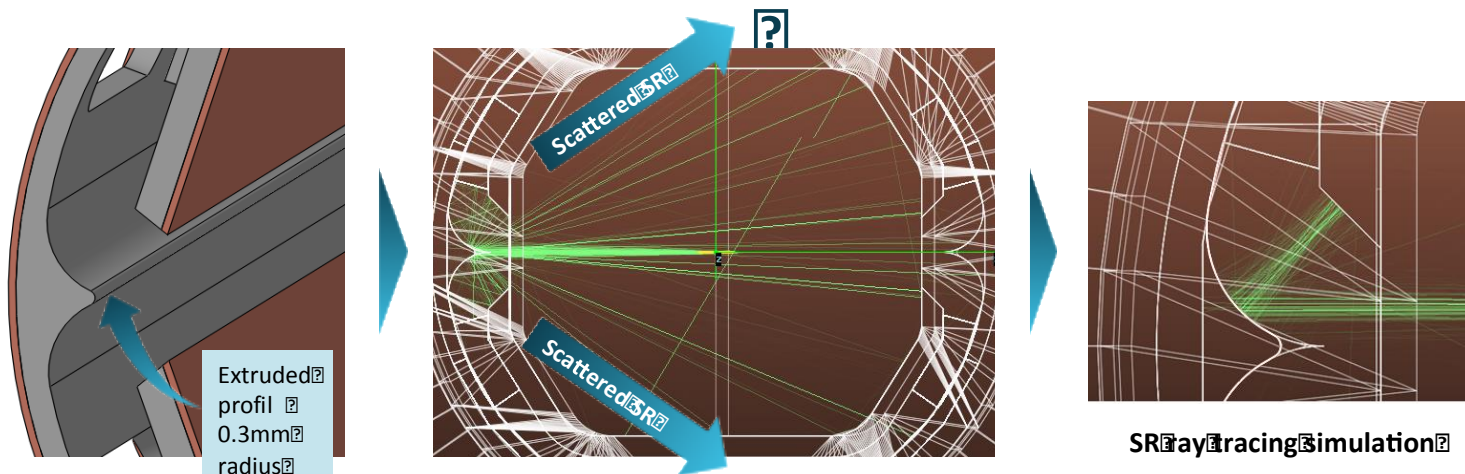
Barcelona 11/2016
5th WP4 meeting



Karlsruhe 04/2017
6th WP4 meeting



SR POWER REDIRECTION

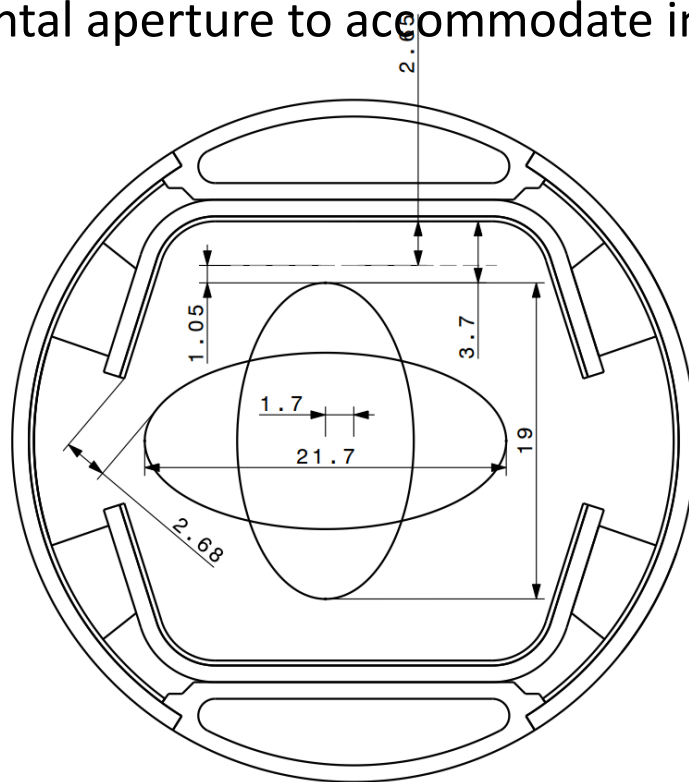


- The reflector, with a V-shape, was aimed to redirect the radiation towards the ribs, in order to avoid scattering photons back to the main chamber and to improve the conductance of molecules towards the cold bore.
- Nevertheless, the chosen manufacturing methodology (extrusion) would always leave a rounded edge instead of a perfectly sharp one. Even being as small as 0.3mm (best found supplier), if the beam is centered, and without machining it afterwards, it makes a huge amount of SR go back to the main chamber where it was originated.
- Besides, to work properly even being perfectly sharp, the beam can't be misaligned more than 1mm, otherwise the beam sees a flat surface. And, as previously studied it has to be very polished to work efficiently, rising the costs.

BEAM DYNAMICS REQUIRED LARGE APERTURES

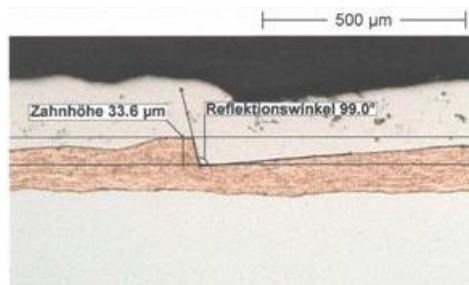
Large acceptance to accommodate vertical orbit error

Larger horizontal aperture to accommodate injection (15.5 sigma)



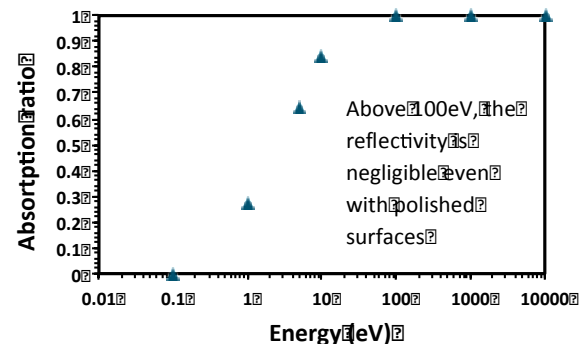
SAWTOOTH SURFACE PROPERTIES

- Owing to the difficulties of effectively reflect the synchrotron radiation with the reflector and within an affordable complexity, the approach has been changed to maximize the absorption on the first impact area, along the beam screen walls.
- For this, a sawtooth profile has been proposed, because of its proved efficacy in absorbing X-rays with a relatively low manufacturing cost whilst besides decreasing the photoelectron yield (PEY) and light scattering.
- According to the carried out simulations, even with a polished copper surface, it can absorb more than the 90% of the photon flux and 99.5% of the power coming from the bending magnets.

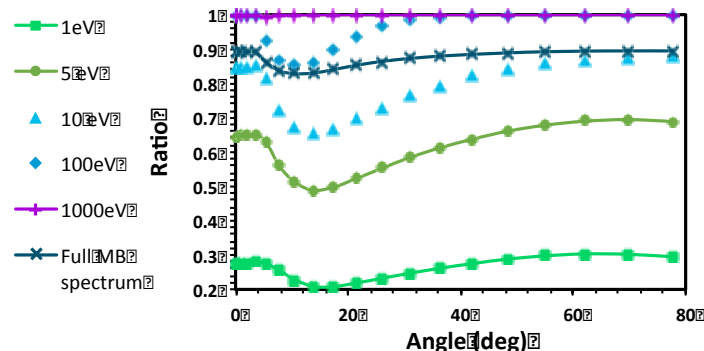


Sawtooth profile of the LHC's BS

Absorption Ratio vs photon Energy
0.057° Fe Sawtooth $T=0.036$

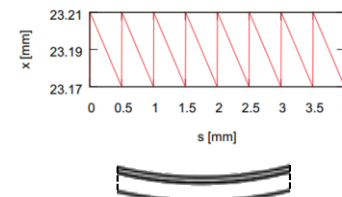
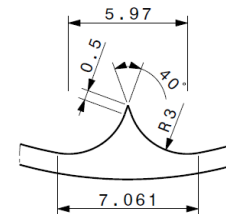
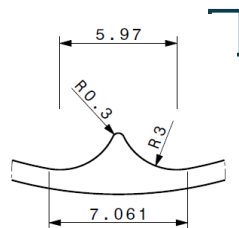


Absorption Ratio vs grazing angle
Fe Sawtooth $T=0.036$



REFLECTOR PROFILE COMPARISON

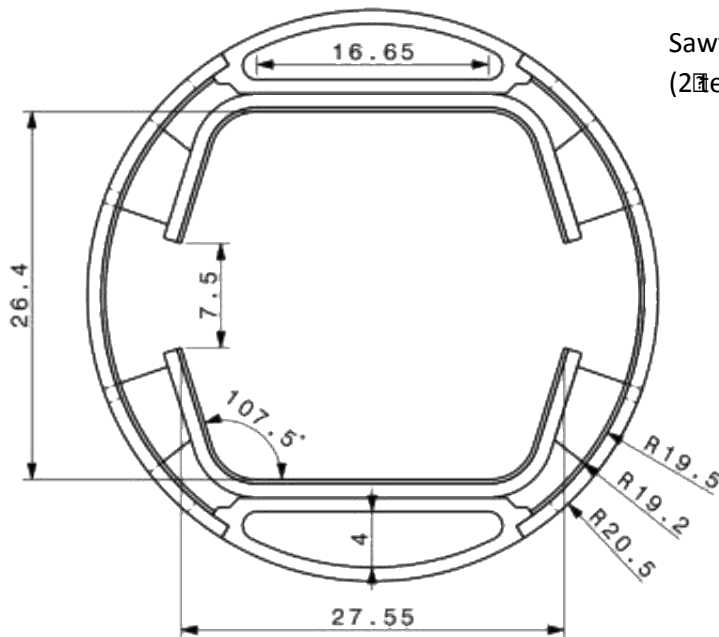
- With the former beam screen dimensions, a comparison of three possible reflector profiles has been performed, with polished surface and the beam aligned, for 50 TeV, 500 mA, SR > 4 eV



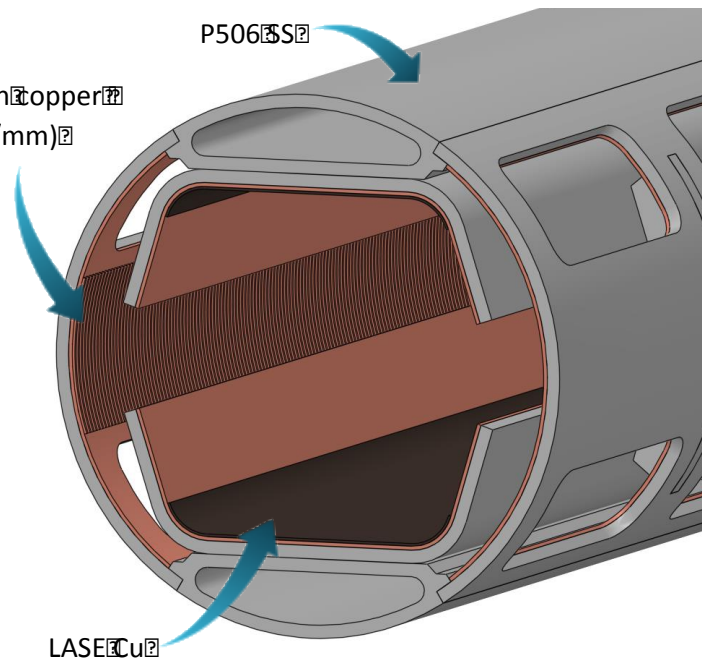
	Extruded profile	Extr.+machined profile	Cu sawtooth
Leaked SR power to cold mass ($\sigma=1$)	0.035 W	0.045 W	0.002 W
Inner beam Cu chamber SR power	80.1 W (16% of MB)	3.6 W (0.8% of MB)	0.18 W (0.04% of MB)
Power on flat area of the inner Cu	13.2 W (2.7% of MB)	0.3 W (0.06% of MB)	0.006 W (0.0013% of MB)
Leaked % SR power through main slot	20%	1%	0.01%
Ribs SR absorbed power	25 W	91.2 W	0.0025 W
% Power absorption on the reflector	49%	49%	99.5%
H ₂ molecular density PSD 36 A·h	$1.7 \cdot 10^{14}$ H ₂ /m ³	$1.2 \cdot 10^{14}$ H ₂ /m ³	$4.8 \cdot 10^{13}$ H ₂ /m ³
Manufacturing complexity	Low	Medium	High

- Best numbers are given by the sawtooth profile in all critical fields, redirecting 400 times less power to the inner Cu chamber, also lowering the total PSD generated outgassing. Shown numbers are per MB, for the previous design

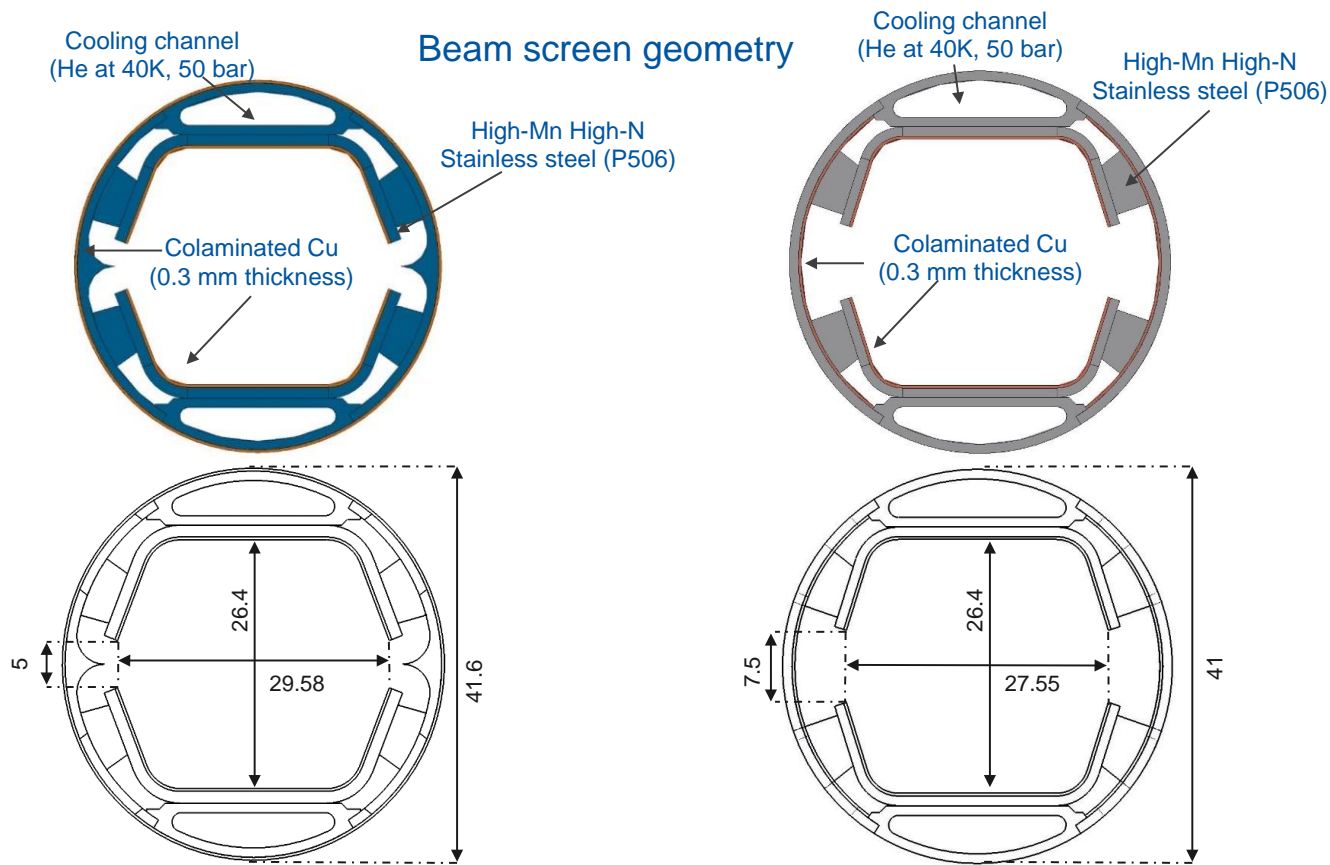
NEW BEAM SCREEN PROPOSAL



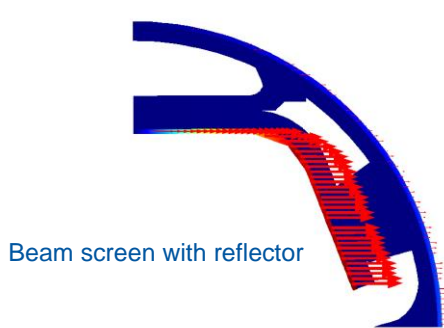
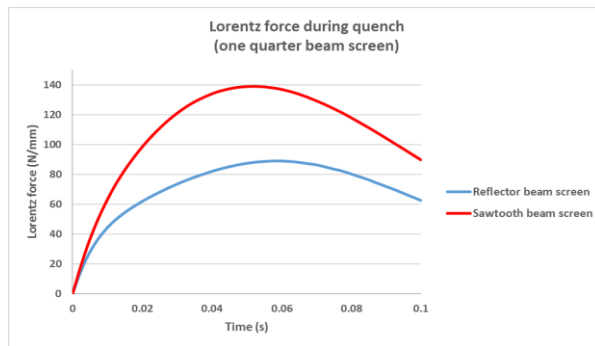
Sawtooth Copper
(21 teeth/mm)



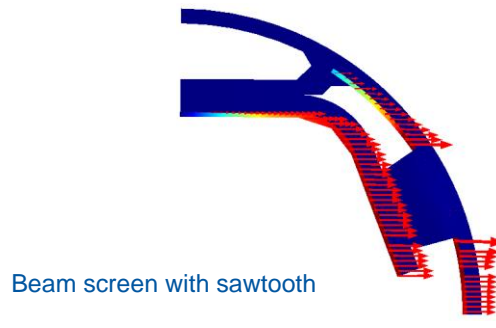
Beam Screen Design



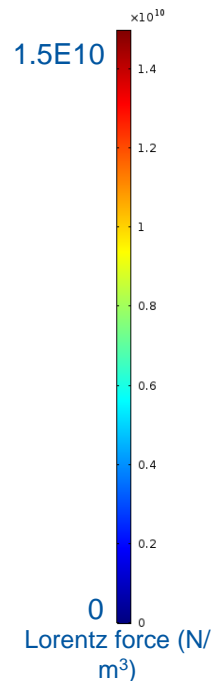
Lorentz forces



Beam screen with reflector



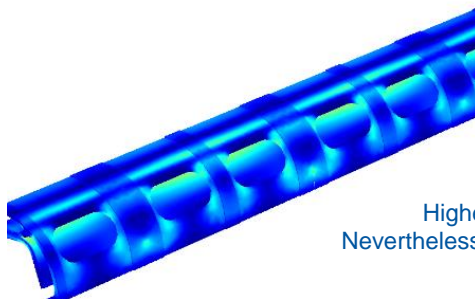
Beam screen with sawtooth



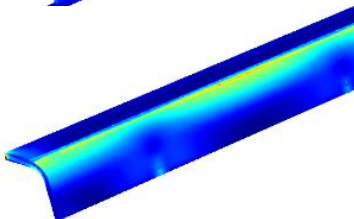
New copper part increases 57% Lorentz force.
High copper electrical conductivity produces more induced currents, thus, more Lorentz force during quench.

Mechanical Design

Stress analysis



Higher stress with new co-laminated copper.
Nevertheless, plasticity was not reached in any of its points.

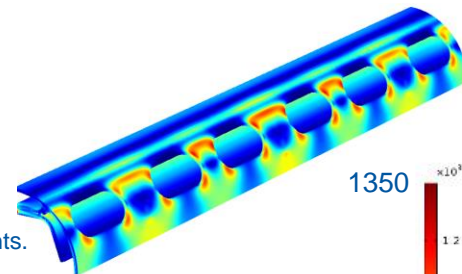


Welding lines must be studied in detail to ensure its strength.

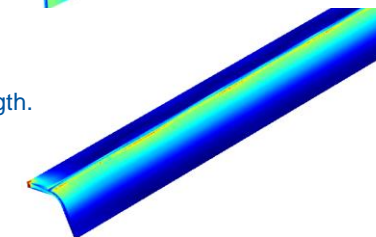


Max stress: 700 MPa

Max displacement exterior beam screen: 0.35 mm



1350 $\times 10^3$



Max stress: 1200 MPa

Max displacement exterior beam screen: 0.6 mm

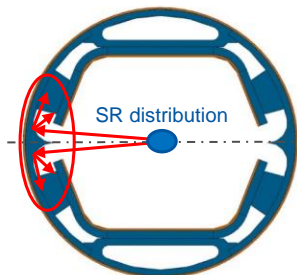
Von Mises Stress (MPa)

0

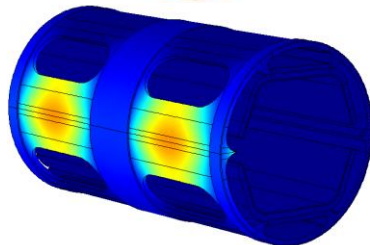
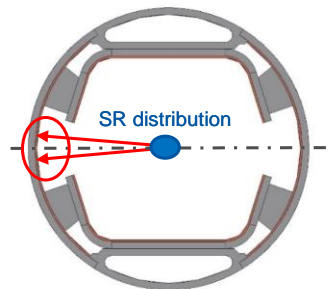


Thermal analysis

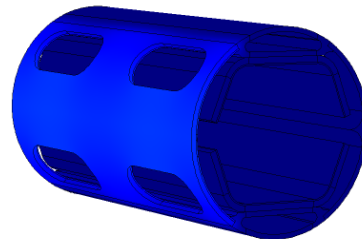
Synchrotron radiation impact



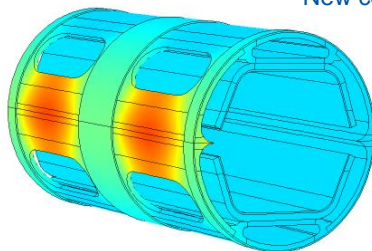
SR distribution changes with sawtooth.
Different heat load.



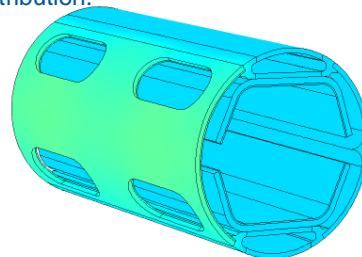
Helium inlet conditions
40 K, 5000 W/m²K, 50 bar



New copper layer produces different temperature distribution.



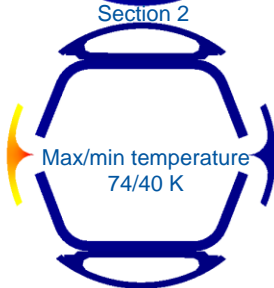
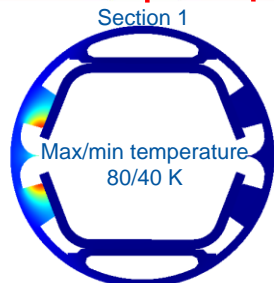
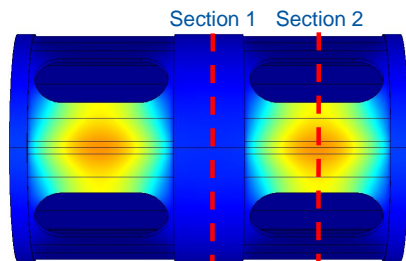
Helium outlet conditions
57 K, 5000 W/m²K, 50 bar



Thermal analysis

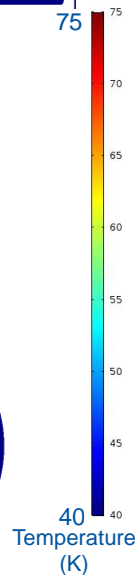
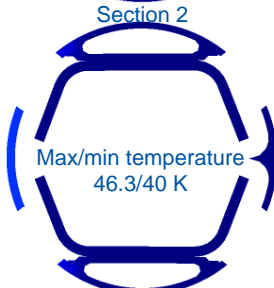
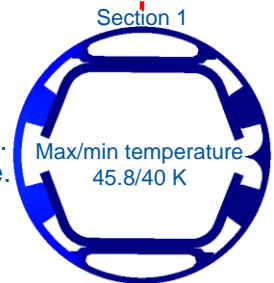
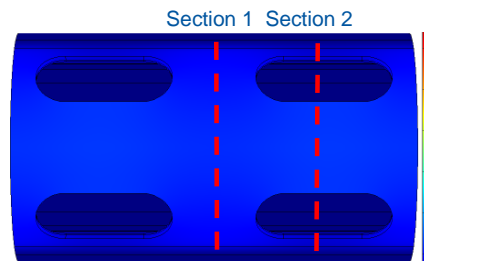
Synchrotron radiation impact

Helium inlet conditions
40 K, 5000 W/m²K, 50 bar



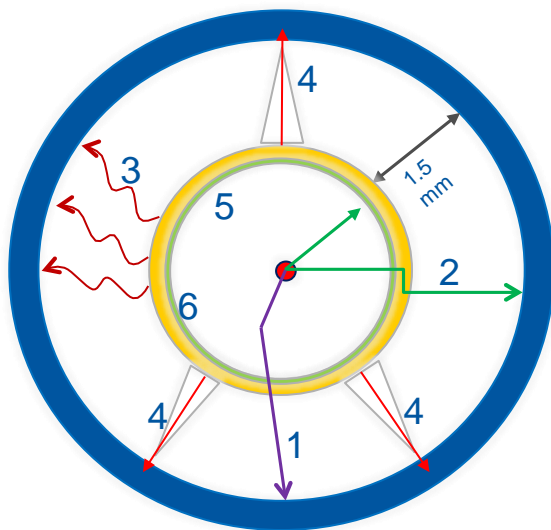
Most of the radiation is absorbed by the sawtooth.
Stiffeners don't act as a photon stoppers anymore.

High thermal conductivity in copper sawtooth
layer helps to reduce temperatures



Thermal analysis

Heat transferred to cold bore



		<u>Reflector</u>	<u>Sawtooth</u>
1	• Nuclear scattering:	191 mW/m	191 mW/m
2	• Synchrotron radiation:	2.4 mW/m	0.5 mW/m
3	• Thermal radiation:	1 mW/m	0.6 mW/m
4	• Beam screen supports:	100 mW/m	75 mW/m
5	• Image currents		
6	• Electron cloud effect		

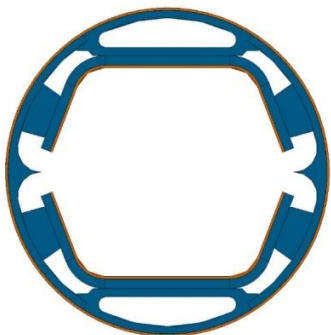
Max power allowed: 300 mW/m

Total thermal load transferred to cold bore with sawtooth: 267.1 mW/m

Beam Screen Design

Beam screen evolution

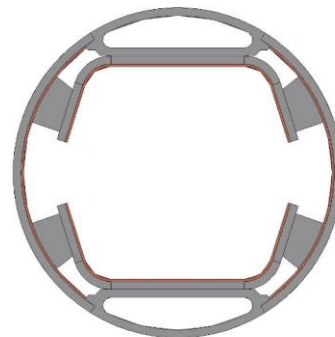
Berlin 05/2017
FCC week



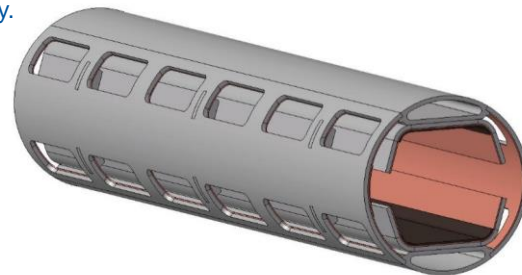
1. Reflectors have been changed by an co-laminated copper coating and sawtooth synchrotron radiation absorber.



Geneva 10/2017
WP4 meeting

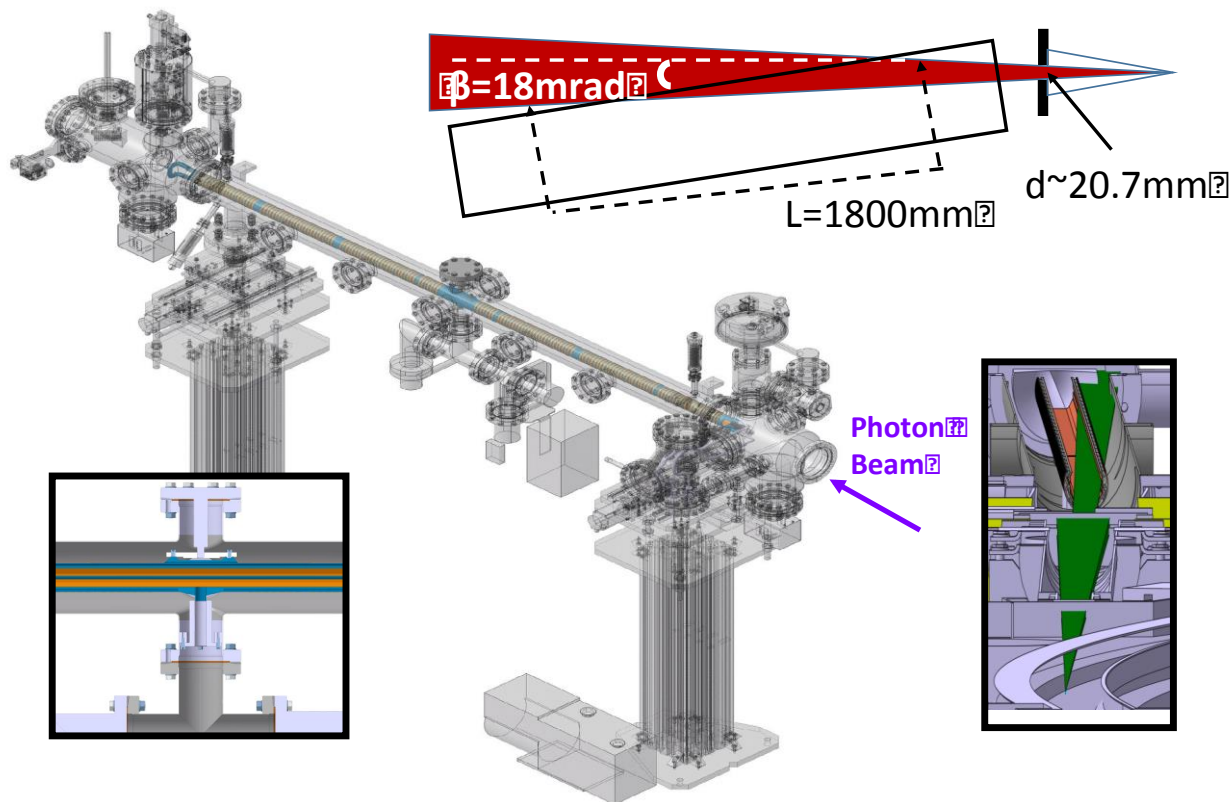


2. Copper strips have been eliminated since copper coating increases thermal efficiency.



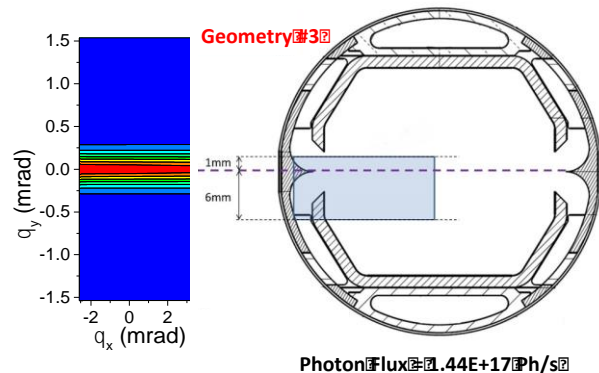
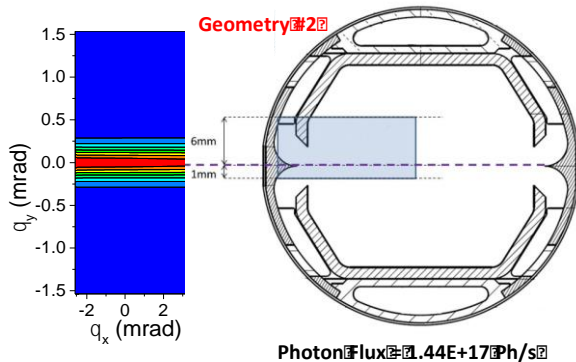
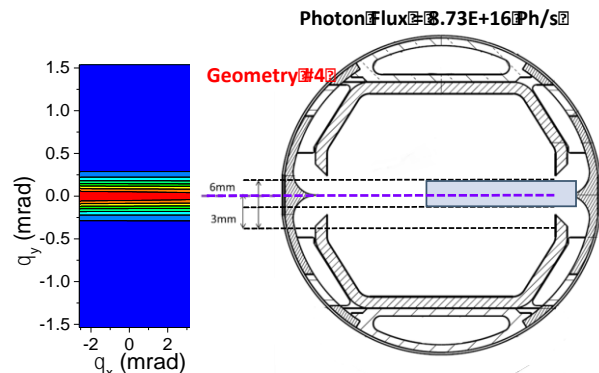
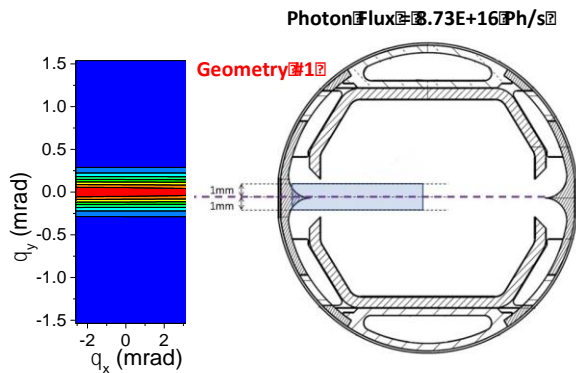
KARA (Karlsruhe Research Accelerator - Ex-ANKA)

BESTEX (BEam Screen Testbench EXperiment)



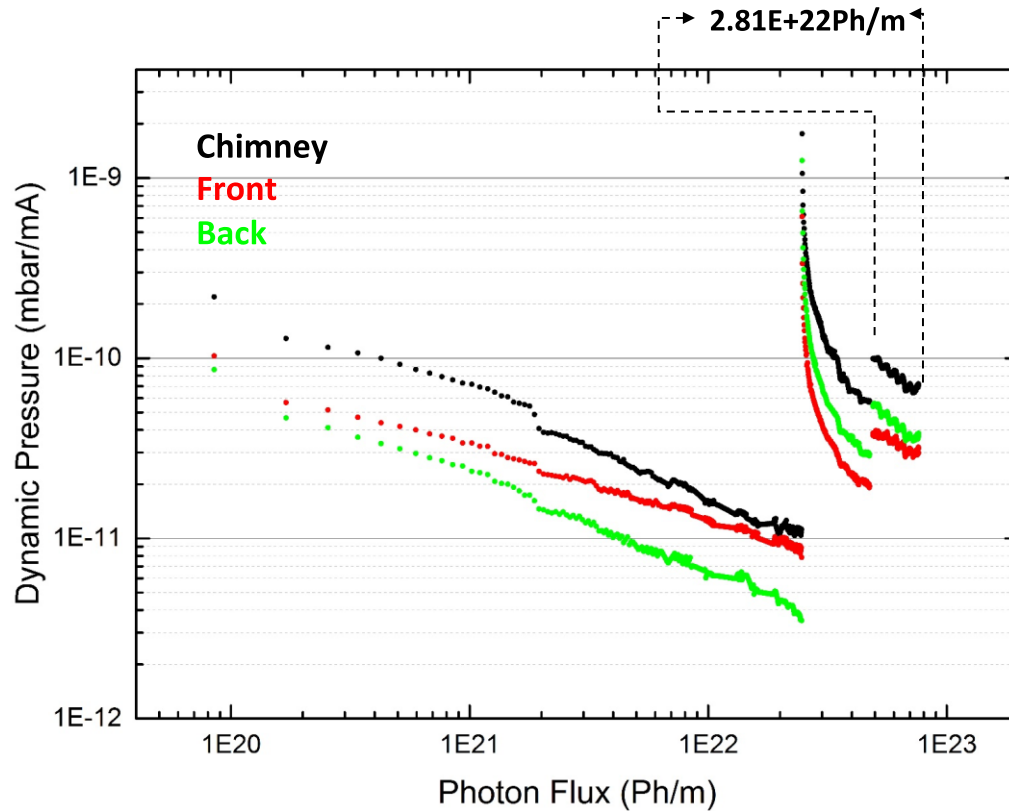
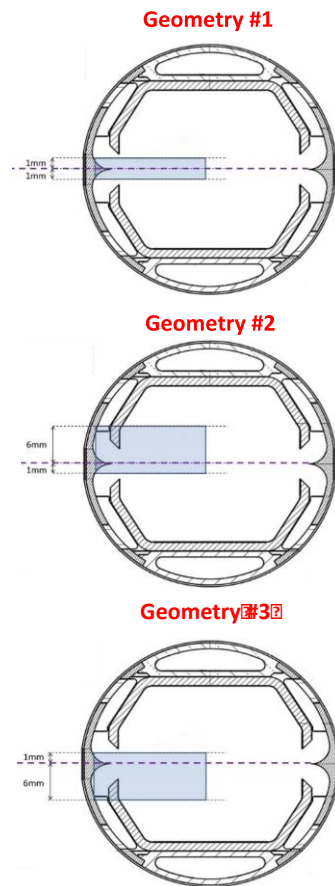
1st Prototype Measurements

Experimental Configurations



1st Prototype Measurements:

Pressure Evolution Results



1st Prototype Measurements: Comparison with Simulations

Pressures (mbar)

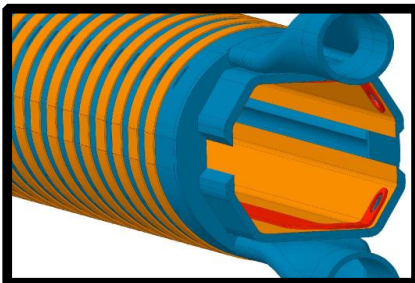
	2.5GeV/130mA					
	3Ah			9.5Ah		
	Experiment	Simulations	Rel Discrepancy %	Experiment	Simulations	Rel Discrepancy %
Middle	7.25E-09	2.30E-08	68.5%	3.71E-09	1.20E-08	69.0%
Front	3.87E-09	4.70E-09	17.7%	2.44E-09	2.80E-09	12.9%
Back	2.42E-09	3.80E-09	36.4%	1.39E-09	2.00E-09	30.3%

RGA masses

	3Ah		9Ah	
	Experiment	Simulations	Experiment	Simulations
H2	72.0%	29.8%	71.6%	36.4%
CO	24.5%	28.9%	24.5%	27.1%
CO2	1.9%	33.6%	2.4%	28.8%
CH4	1.6%	7.7%	1.5%	7.7%

2st Prototype Installation:

Planning



#2:#1 + electrodes for photoelectron current measurements

Irradiation 4th config

Disassemble SetUp and transport outside the ring

Assembly and comitioning Outside the ring

October				November			
Day	Week	Shift 9-18	19-8	Day	Week	Shift 9-18	19-8
				1	44	Allerheiligen	NO
				2			NO
				3			NO
1				4			
2	40	NO	NO	5			
3		Tag d. deutsch	NO	6	45	NO	St
4		NO	NO	7		UO	UO
5		NO	NO	8		UO	UO
6		NO	NO	9		UO	UO
7				10		UO	UO
8				11			
9	41	NO	St	12			
10		UO	UO	13	46	NO	MP
11		UO	UO	14		MP	MP
12		UO	UO	15		SUO	SUO
13		UO	UO	16		SUO	SUO
14				17		MP	MP
15				18			
16	42	NO	MP	19			
17		MP	MP	20	47	NO	St
18		SUO	SUO	21		UO	UO
19		SUO	SUO	22		UO	UO
20		MP	MP	23		UO	UO
21				24		UO	UO
22				25			
23	43	NO	St	26			
24		UO	UO	27	48	NO	St
25		UO	UO	28		UO	UO
26		UO	UO	29		UO	UO
27		UO	UO	30		UO	UO
28							
29							
30	44		NO				
31		Reformationsta	NO				

Beam Screen Proto 2



Transport inside the ring
Commissioning

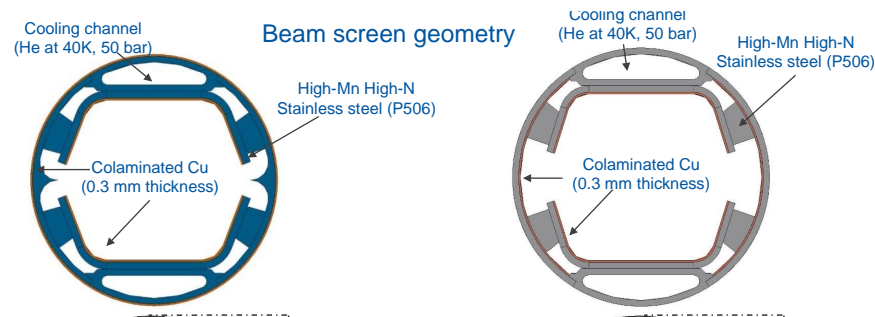
Bake out
Conditioning

Irradiation
2nd Prototype

Next prototypes:

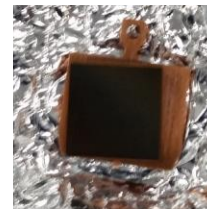
Considering several options:

Work in parallel with LASE, deflector &/or sawtooth
Final decision before welding (April 18 – July 18)

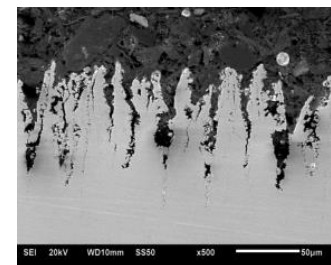
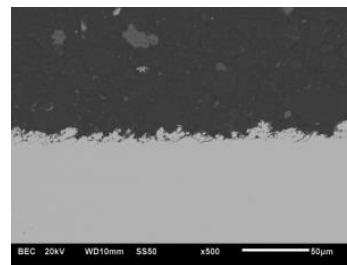
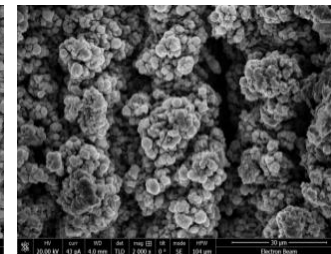
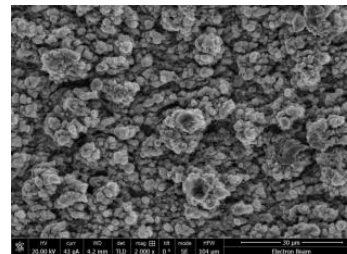


4th prototype: Sawtooth (& electrode) ??

Laser Treated Copper



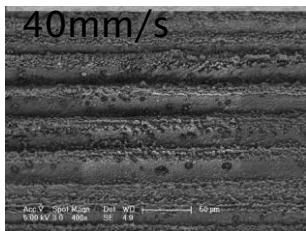
- Surfaces have a micro and nanostructure
- Optically black
- Various laser parameters can be varied to change the topology
- Images (left) are of different scan speeds, 180 mm/s and 30 mm/s shown



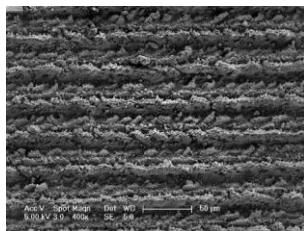
Varying power and scan speed at 1064 nm

$\lambda = 1064 \text{ nm}$
 $P = 20 \text{ and } 10.5 \text{ W}$
 $\tau = 2 \text{ ns}$
 $F = 40 \text{ kHz}$
 $H = 0.02 \text{ } \mu\text{m}$
 $v = 80 \text{ and } 40 \text{ mm/s}$

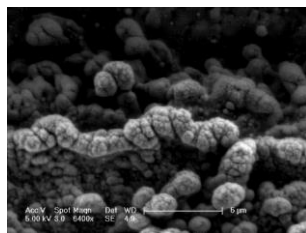
Produced With Micronanics



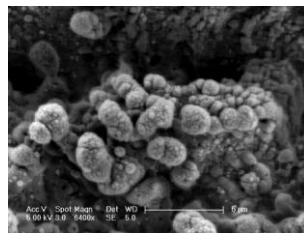
100 μm



100 μm

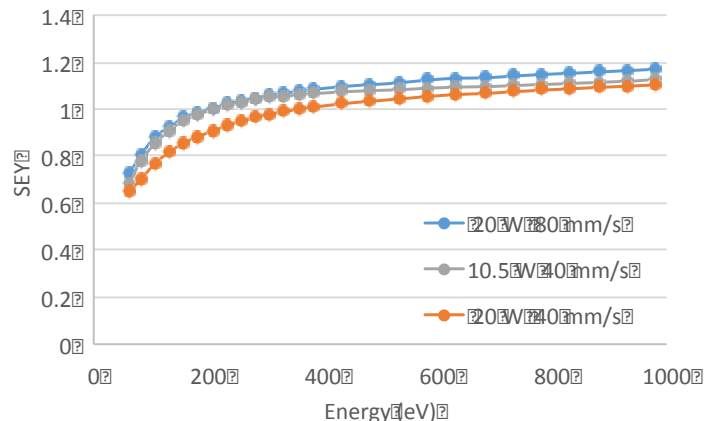


10 μm
20 W 80 mm/s



10 μm
10.5 W 40 mm/s

Varying Power and Scan speed

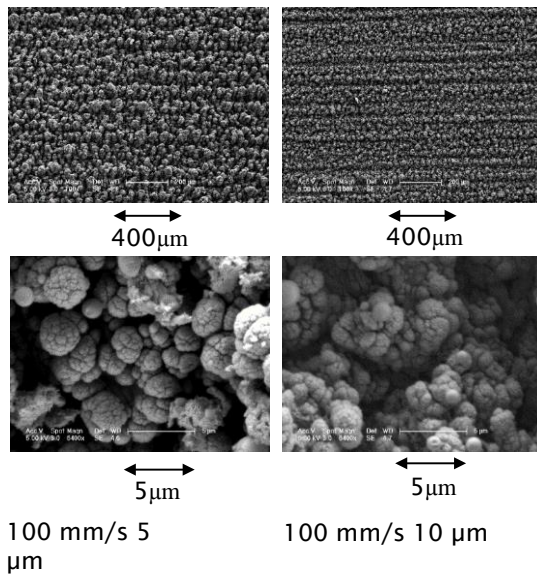


- Power normalised by scan speed give similar results within parameters explored

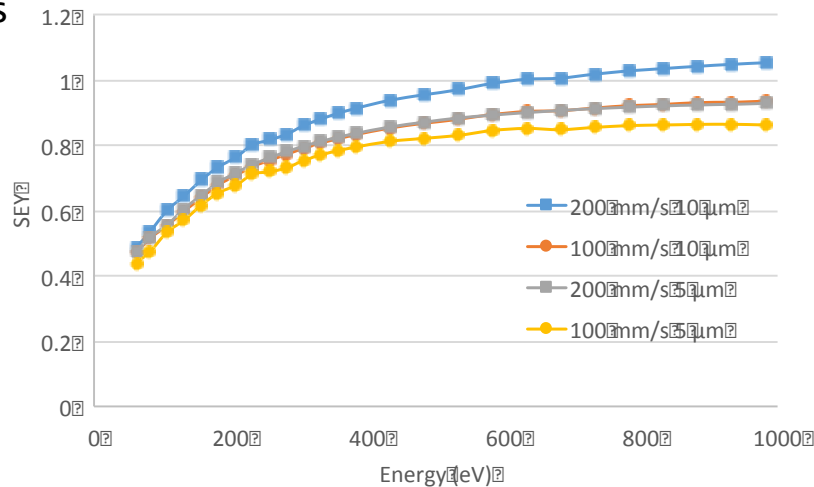
Varying speed and pitch

$\lambda = 1064 \text{ nm}$
 $P = 5 \text{ W}$
 $\tau = 70 \text{ ns}$
 $F = 100 \text{ kHz}$
 $H = 5 \text{ and } 10 \text{ } \mu\text{m}$
 $v = 100 \text{ and } 200 \text{ mm/s}$

Produced
with
Micronanics



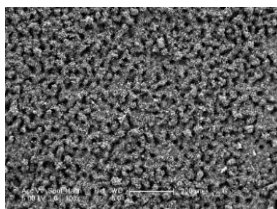
Optimising speed and pitch



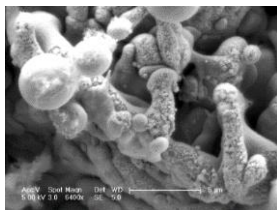
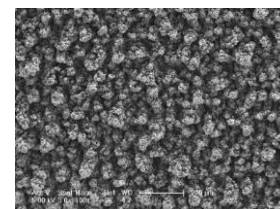
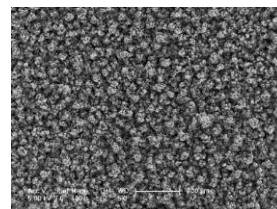
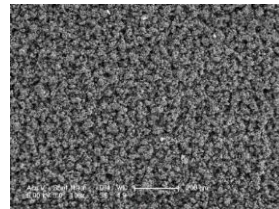
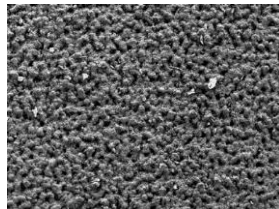
- Same SEY observed for faster scan speed when matched with a smaller pitch

SEM

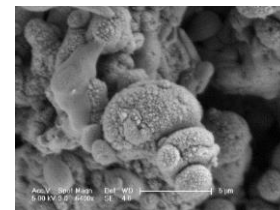
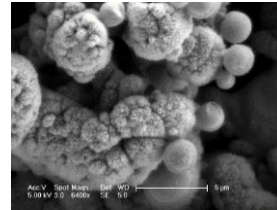
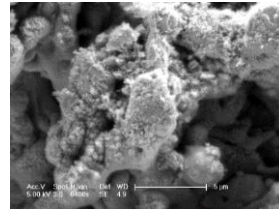
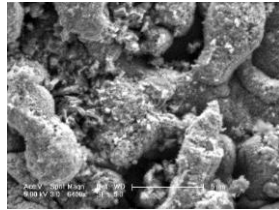
Highest SEY → Lowest SEY



400µm



5µm



Compressed air with glass

Pumped flow with glass

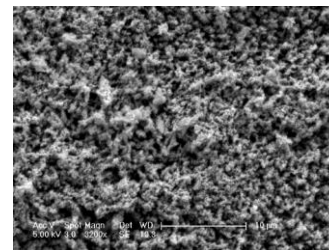
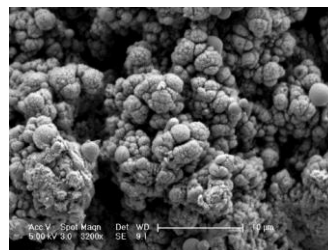
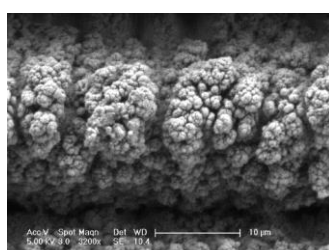
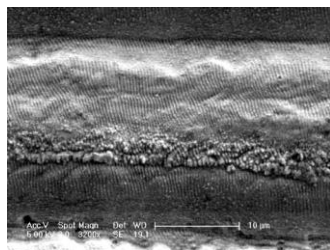
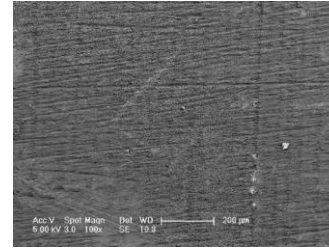
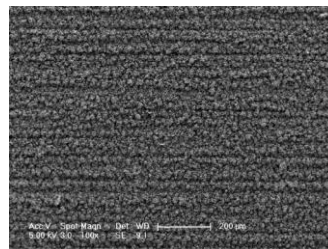
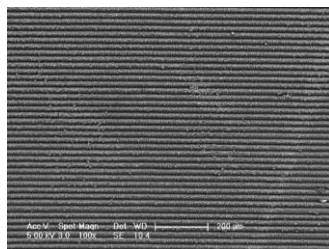
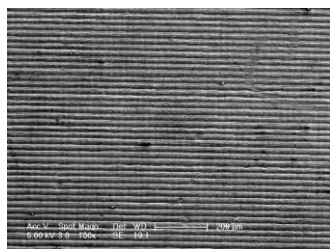
Air, no glass

Compressed air, no glass

Pumped flow, no glass

Various structures

- Can make various shapes with different structures all with different properties and SEY



NEG coating studies

Current work:

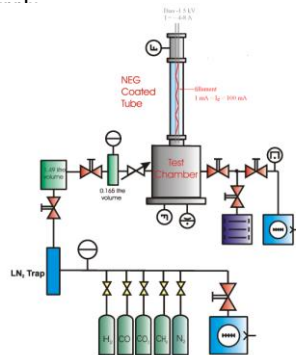
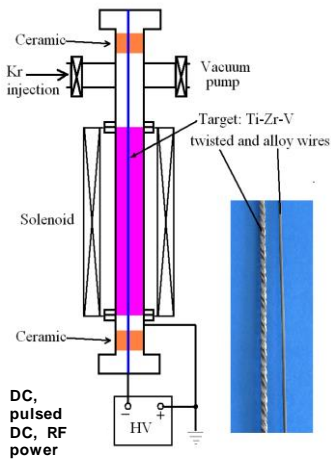
- MOLFLOW modelling of the test facility - completed
- Deposition of Zr on a sample tube, ESD and pumping measurements
 - Sample 1 (dense film) – measurements are completed, data analysis in progress
 - Sample 2 (dense film) – measurements are completed, data analysis in progress
 - Sample 3 (columnar film) – pumping property measurements are completed, ESD measurements have started

Next Steps:

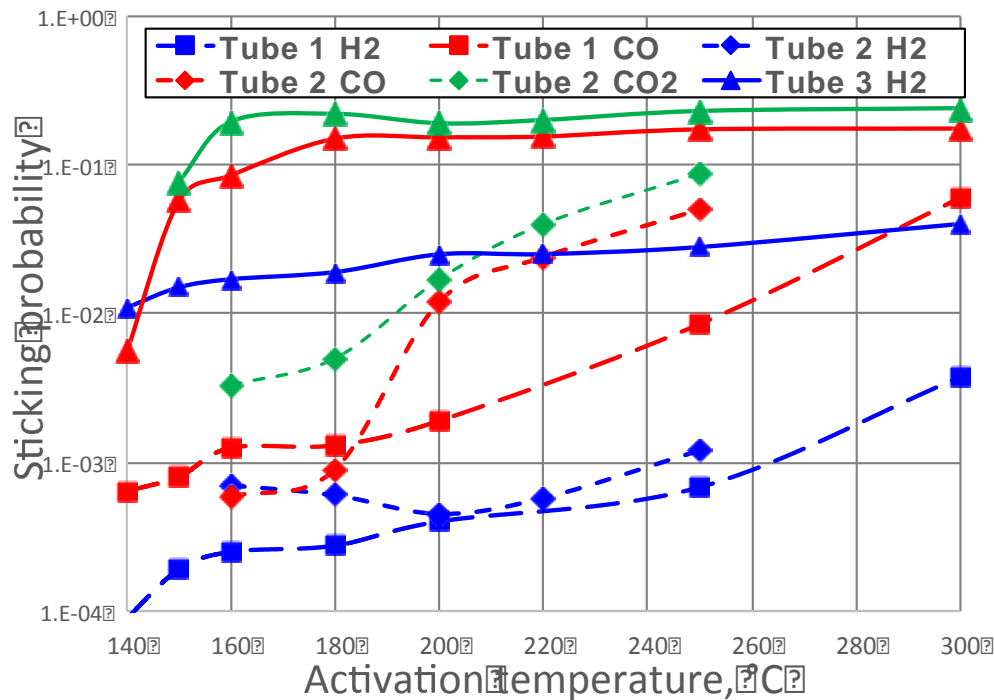
- Modifying a facility for measurements with LN_2
- Ti-Zr-Hf-V film to be deposited and measured at temperatures between room temperature and LN_2
- Design of a facility for cryogenic (dry system $4\text{ K} < T < 80\text{ K}$) measurements
- Analysis of the experimental results

Showstoppers

- None at this stage

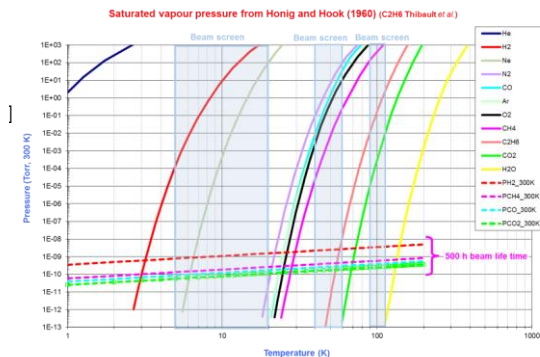
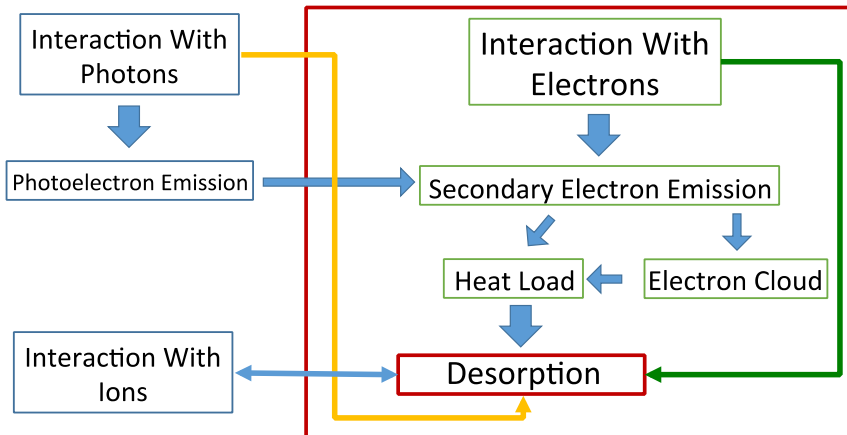


Samples 1&2 - dense Zr, sample 3 - columnar Zr



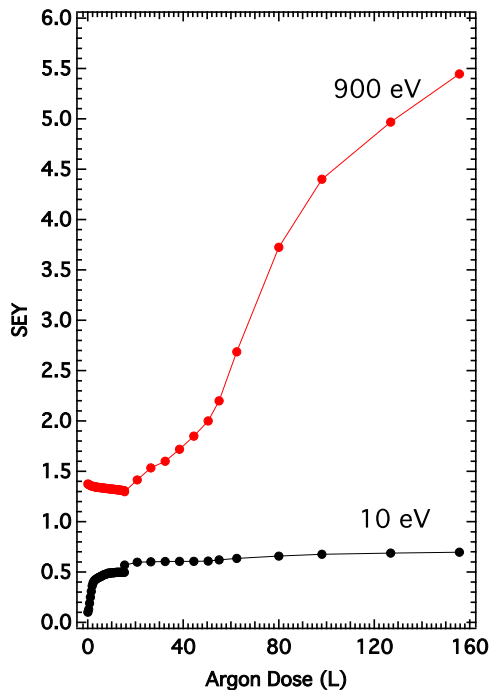
- Pure Zr coated tube with a columnar structure demonstrated good pumping properties after activation to 150°C.
- ESD - to be analysed

Gas adsorption/desorption dynamics and SEY

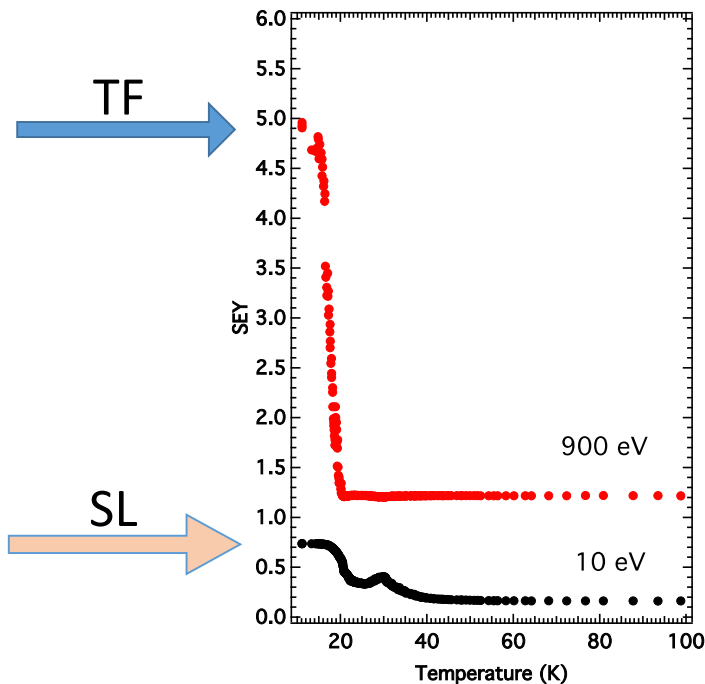


Argon Desorption (SEY)

Adsorption



Desorption

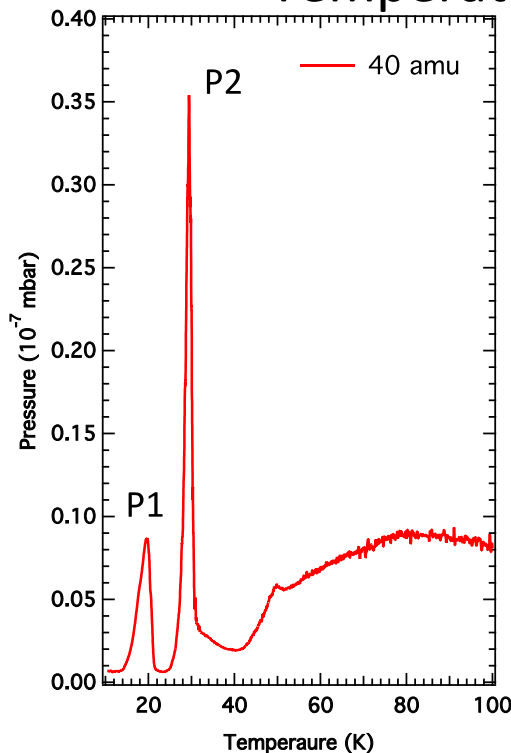


TF

SL

Argon Desorption (TPD)

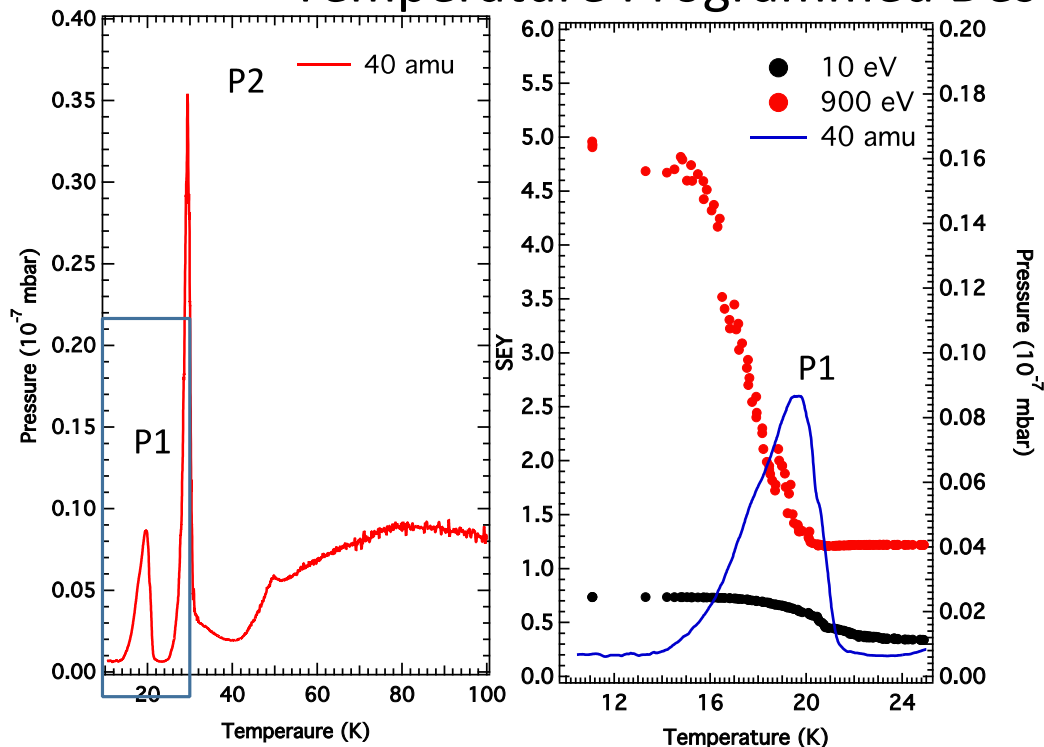
Temperature Programmed Desorption (TPD)



- Characteristic desorption behaviour
- First desorption process around 20 K (P1)
- Second desorption process @ 30 K (P2)
- Other desorption after 50 K

Argon Desorption (TPD)

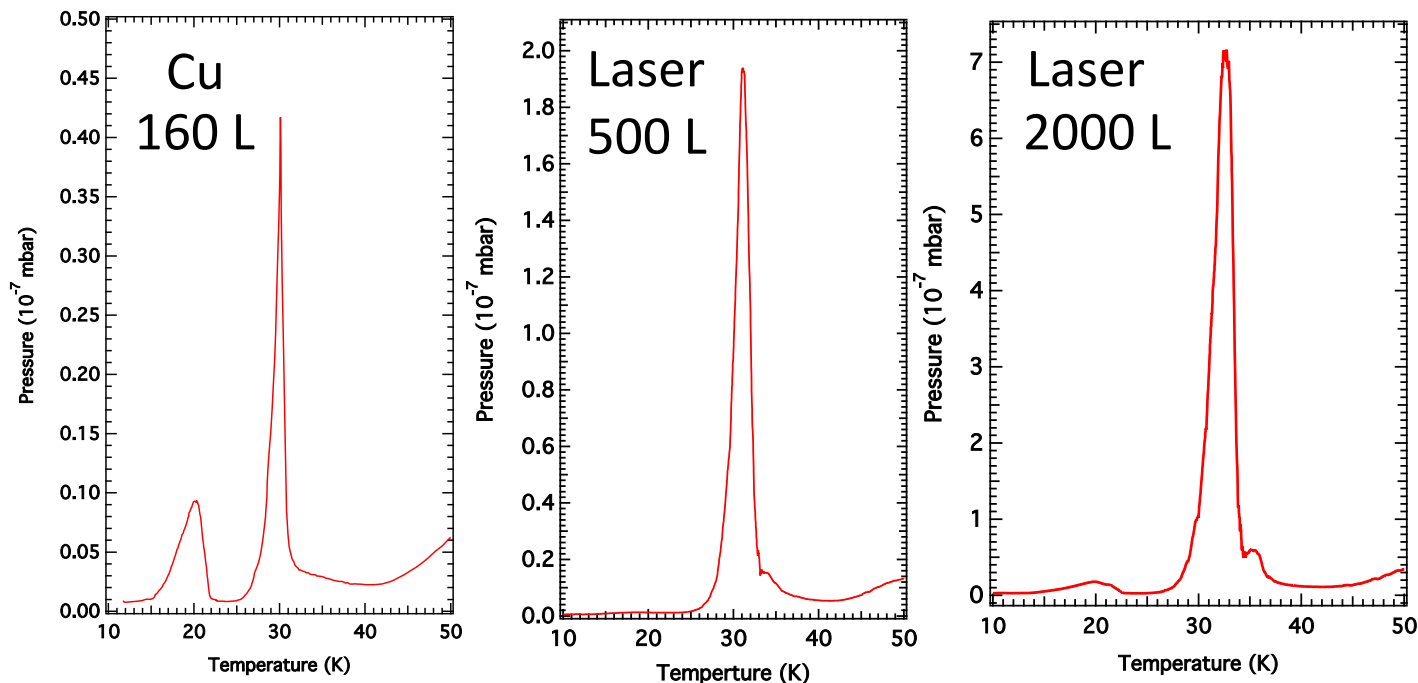
Temperature Programmed Desorption (TPD)



Correlation
between P1 and
SEY signals

Laser Treated Sample

Temperature Programmed Desorption (TPD)





Conclusion

Impressive work by the team

Thanks