

Marx prototype pulse generator design and initial results

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Outline

Parameters of injection system

Pulse power generators for kicker magnets

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- Application: kicker system
- Marx generator concept & specifications
- Marx single switch unit measurements
- One & four Marx stage measurements
- Ongoing R&D
- Conclusions

Parameters of injection system

Hardware parameter	Unit	Kicker
Deflection	mrad	0.18
Integrated field	T∙m	2.0
Field rise time	μs	0.43
Magnet single way delay	μs	0.355
System impedance	Ω	6.25
Magnet current	kA	2.4
Generator pulse rise time	ns	75
Generator output voltage	kV	15
Flattop length	μs	2.0
Flattop stability	%	±0.5



- Injection kicker system must be highly reliable;
- > The baseline injection energy for the FCC-hh is 3.3 TeV;
- For machine protection reasons, a maximum of 80-100 bunches can be accepted by the injection protection system and hence safely transferred into FCC at a time;
- > Each ring will be filled with 130 batches of **80** bunches (separated by 25 ns) \Rightarrow **2** μ s pulse.

Oral presentation: FCC-hh transfer line and injection design, E. Renner, 11/04/2018, 15:30hrs.

Pulse power generators for kicker magnets



- Many kicker systems today use thyratron (gas tube) switches and pulse forming networks/lines (PFNs/PFLs);
 - Long-term availability of thyratrons is a real concern;
 - Thyratrons can exhibit unwanted, spontaneous, turn-on;
 - Thyratrons require a PFN/PFL: the **long-term availability of high-voltage PFL technology is a concern**.
- Solid-state technology and topologies show great promise for kicker application e.g.:
 - Inductive Adder (Oral presentation: "Inductive adder prototype pulse generator for FCC-hh kickers", D. Woog, 11/04/2018, 11:10hrs);
 - Marx Generator.

Goal: to achieve reliable, fast-switch technologies based on semiconductor devices. Both the Inductive Adder (<3us pulse width) and Marx Generator technologies are being actively pursued.

Motivation & challenges

Semiconductor switches, such as SiC MOSFETs (metal-oxide-semiconductor field-effect transistors), can potentially be used in fast high current pulsed power accelerator applications to replace thyratrons and PFLs.

Versus:

Thyratrons

- + Generally reliable
- + Robust (fault tolerant)
- + Relatively high voltage
- + Relatively high current
- Long term availability
- Spontaneous turn on
- Can only be turned on

MOSFETs

- + Cost-effective
- + Easy to use
- + Off-the-shelf
- + Flexible
- + Modular
- + Maintainability
- + Can be turned on and off (thus PFL/PFN is not required)
- Relatively low voltage
- Relatively low current

But.... Semiconductors have limited voltage and current rating. Hence, requires **series** and parallel connection of power semiconductors to achieve high pulsed power.

Solid-state Marx generator (1)

Electrical circuit first described by Erwin Otto Marx in 1924 – until recently the Marx did <u>not</u> use semiconductor switches.

Concept: generate a high-voltage pulse from a low-voltage DC supply and components.

The circuit operates by (1) charging capacitors in parallel, then subsequently connecting them in series to generate a high-voltage output pulse.

STEP 1

1a) All the odd numbered MOSFETs/IGBTs (i.e. $M_1, M_3, M_5, ...$) are off.

1b) The capacitors $(C_1, C_2, ..., C_5)$ are charged in parallel, from *Vdc*, by turning-on all the even numbered MOSFETs/IGBTs (i.e. $M_2, M_4, M_6, ...)$ [$V_{Marx} \approx 0$ V]:



Solid-state Marx generator (2)

The circuit operates by charging capacitors in parallel, then (2) subsequently connecting them in series to generate a high-voltage output pulse.

<u>STEP 2</u>

2a) Capacitors $C_1, C_2, ..., C_5$ have been charged to V_{dc} in step (1b). All the even numbered MOSFETs/IGBTs (i.e. $M_2, M_4, M_6, ...$) are then turned off. 2b) All the odd numbered MOSFETs/IGBTs (i.e. $M_1, M_3, M_5, ...$) are then turned on, to connect the capacitors in <u>series</u>. Here: $V_{MARX} \approx 5 \cdot V_{dc}$



For fast, rectangular, pulses MOSFET technology is required.

Marx generator solid-state modular concept

package, with separate emitter for gate voltage (C3M0065100J, 1000V, now available) C3M0065090J data sheet parameter Value Min. Drain-Source Breakdown Voltage 900 V Pulsed current 90 A On-State Resistance 65 mΩ Rise time (90 - 10 %) 9 ns Fall time (10 - 90 %) 7.5 ns

One MOSFET tested to date: CREE SiC MOSFET C3M0065090J, 900V, SiC MOSFET, in D2PAK-7L



- Each switch unit consists of a pulse capacitor and 3 SiC MOSFETs in parallel
- *n* staked (series) stages. Each stage consists of 8 switch units



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Marx MOSFET switch unit: measurements

Switch unit: 3 parallel MOSFETs with a 60µF capacitor:

Switch unit: current sharing of 3 parallel MOSFETs:

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M1	166 A (33%)
M2	152 A (31%)
M3	182 A (36%)



750 V pulse across 1.5Ω (500 A)



One MOSFET Marx stage: measurements

Operating conditions: *U*dc=800V, *R*load=0.25 $\Omega \Rightarrow ^{2}3200$ A expected:



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Four MOSFET Marx stages: measurements

*U*dc=800V, *R*load≈1.175Ω \Rightarrow ~2700 A expected:



Circuit time constant of 24 ns with a load of 1.175 $\Omega \Rightarrow$ four stage Marx circuit inductance of ~28 nH (~7nH/stage).

- ✓ Current magnitude (2.7kA) meets specification (2.4kA),
- ✓ Current rise time (53ns, 10-90%) is in the right "ball-park" (75ns);

 $\checkmark\,$ Current flattop duration close to requirement (2µs).

11/04/2018, FCC Week

Solid-state Marx: ongoing R&D/challenges



- Studies to reduce flattop droop to within ±0.5%...
- Low inductance is achieved with four return wires on each side of Marx, close to "go" current paths: higher voltage is more clearance reqd. for insulation is higher circuit inductance
 increased rise time
- Study of fault conditions (e.g. short-circuit in magnet) and limitation of current
- Study of possible failure modes of Marx generator
- Long-term reliability
- ▶

Conclusions

ISEL & EPS have made very good progress carrying out R&D for a solid-state Marx generator for possible application to kicker systems:

- SiC MOSFETs, connected in parallel, can be used in fast high current pulsed power applications: good current sharing.
- Preliminary measurements with a solid-state Marx generator topology, with SiC MOSFETs, show that it is a promising candidate for generating fast, high current, pulses for kicker systems:
 - One stage @ 800V ⇒ 3200A
 - Four stages @ 3200V ⇒ 2700A: measurements show good performance (rise and fall).
- The Marx generator topology is a promising candidate for replacing thyratrons and PFLs in kicker applications.
- Future:
 - Assemble and test more stages and investigate the overall performance and reliability.
 - Long term operation with higher frequency;
 - Behaviour under fault conditions (e.g. short circuit).

Questions?

Thank you for your attention !

Questions ?



Bibliography

- J.A. Casey, F.O. Arntz, M.P.J. Gaudreau and M. Kempes, Solid-State Marx bank modulator for the Next Linear Collider, Pulsed Power Conference, 15–18 June 2003, pp. 641–644, https://doi.org/10.1109/PPC.2003.1277791.
- A. Krasnykh, R. Akre, S. Gold and R. Koontz, A Solid-state Marx type modulator for driving a TWT, Power Modulator Symposium, 2000. Conference Record of the 2000 Twenty-Fourth International, Norfolk, VA, USA, 26–29 June 2000.
- R. Phillips, M.P.J. Gaudreau, M. Kempkes, K. Ostlund and J. Casey, Affordable, short pulse Marx modulator, IEEE International Vacuum Electronics Conference, 22–24 April 2014, Monterey, CA, pp. 455–456.
- S.C. Glidden and H.D. Sanders, Solid state Marx generator, Power Modulator Conference, Arlington, VA, USA, 14–18 May 2006, Arlington, https://doi.org/10.1109/MODSYM.2006.365246.
- T. Beukers, C. Burkhart, M. Kemp, R. Larsen, M. Nguyen J. Olsen and T. Tang., P1-Marx modulator for the ILC, IEEE Power Modulator and High Voltage Conference, 23-27 May 2010, pp. 21–22.
- M.A. Kemp, A. Benwell, C. Burkhart, D. MacNair and M. Nguyen, The SLAC P2 Marx, IEEE Power Modulator and High Voltage Conference, 2012, pp. 1721–1728.
- L.M. Redondo and J. Fernando Silva, IEEE Trans. Plasma Sci., 37 (2009) 1632. https://doi.org/10.1109/TPS.2009.2023221.
- L.M. Redondo, A. Kandratsyeu, M.J. Barnes, S. Calatroni and W. Wuensch, Solid-state Marx generator for CLIC breakdown studies, to be published in Proc. 2016 IEEE Power Modulator and High Voltage Conference, San Francisco, CA, USA, 5–9 July 2016, https://doi.org/10.1109/IPMHVC.2016.8012824.
- L.M. Redondo, A. Kandratsyeu and M.J. Barnes, Marx generator prototype for kicker magnets based on SiC MOSFETs, IEEE Transactions on Plasma Science, 2018, DOI: 10.1109/TPS.2018.2808194.