

# Hi-Lumi LHC Twin Aperture Orbit Correctors Update Development , Cold Test, Next models

G. A. Kirby

13<sup>th</sup> Sep 2017

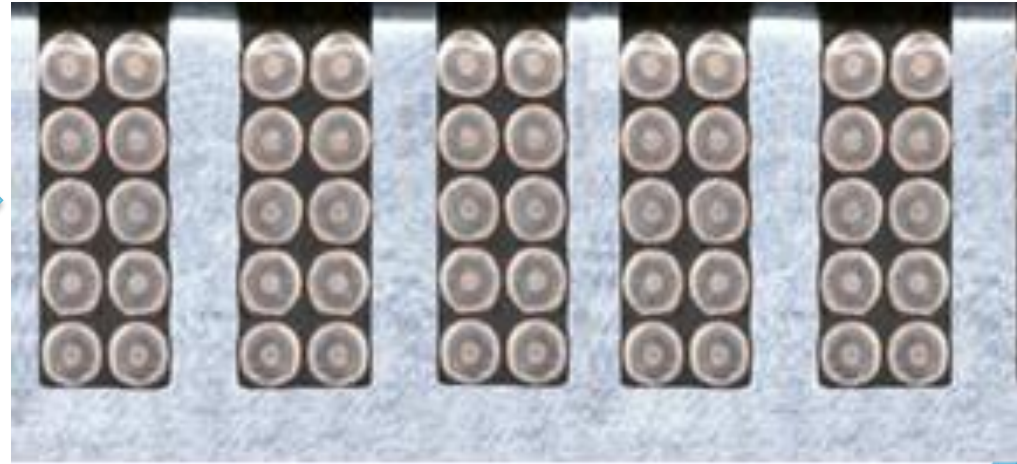
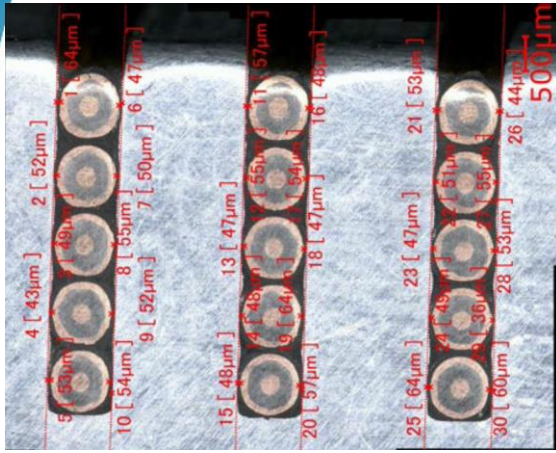


# Talk Over View

- CCT aperture development
- Coil and former design
- Impregnation tooling
- Quench analysis
- Heat extraction
- 0.5m coil test over view
- The improved magnet design
- Planning



# Machined former development

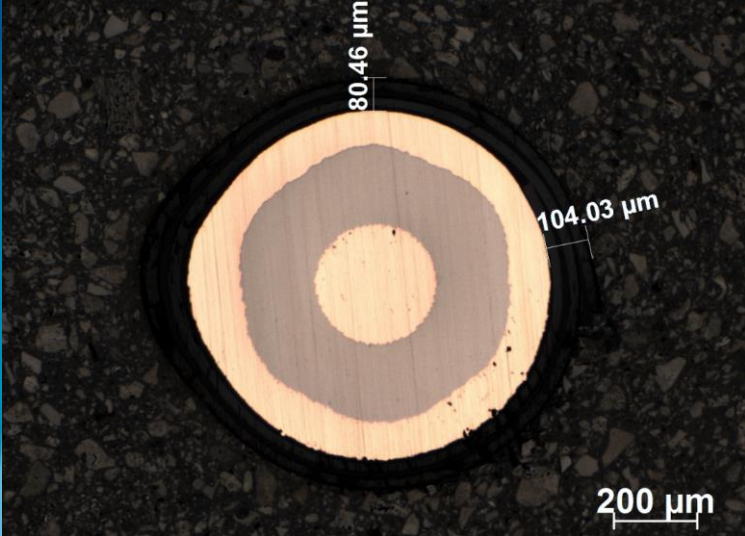


The 1mm wide x 5mm deep channel **could not be machined** over the 128 m long 0.5m former!

Moving to a 2 mm wide slot, the cutting tool is much stronger!

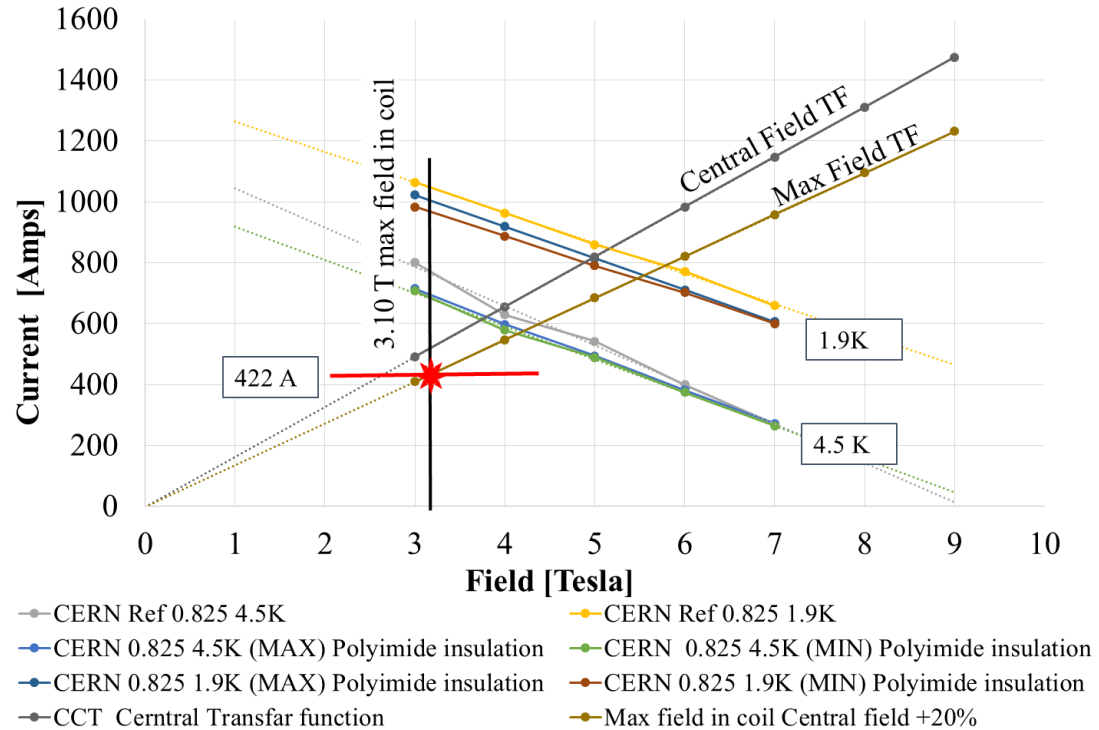
The machining time / cost to machine the channel is reduced!

# Wire Performance

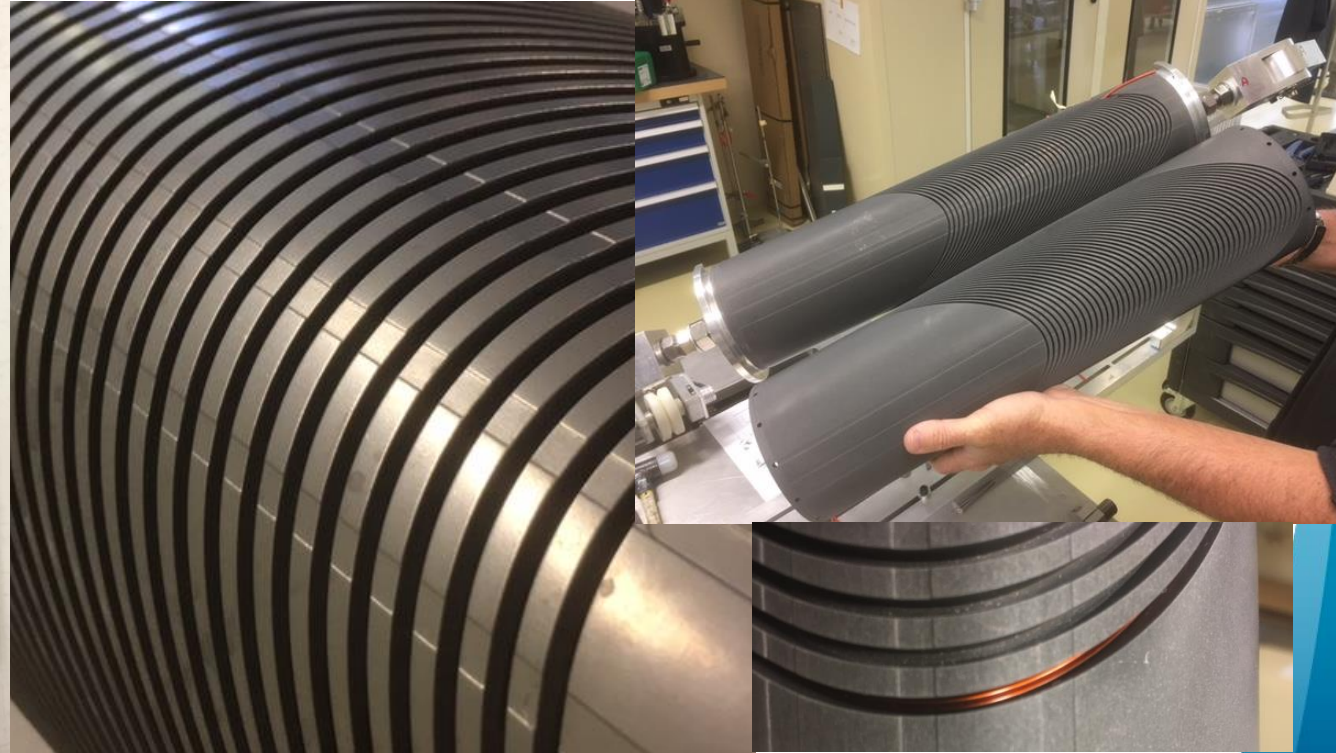


6 mm wide tape 50 to 55 % polyimide wrapped insulation .  
 Insulation curing temperature 420°C for 30 sec degraded the wire  $I_c$  by 10%.  
 Magnet merging is still high at 55 % SS

Test insulation 12 kV min



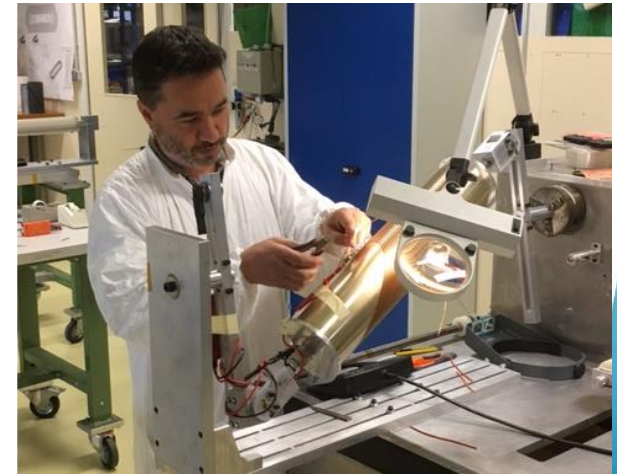
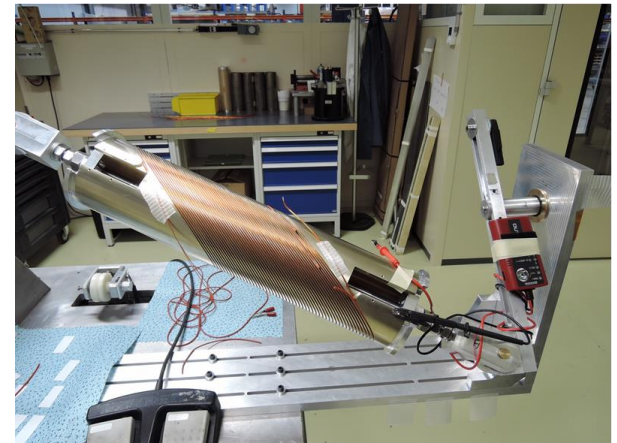
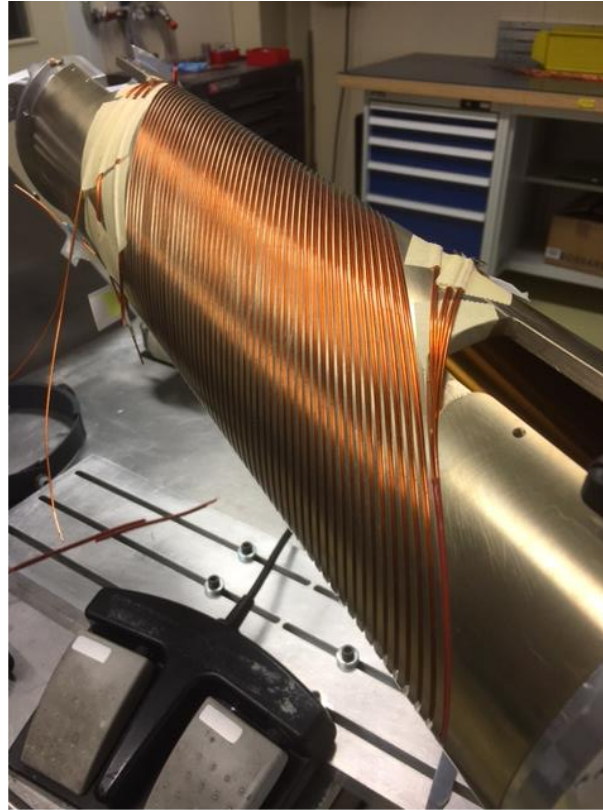
# Aluminium formers 6082-T6 polishing test to de-burr? and then Hard Anodization (Micro-Machining)



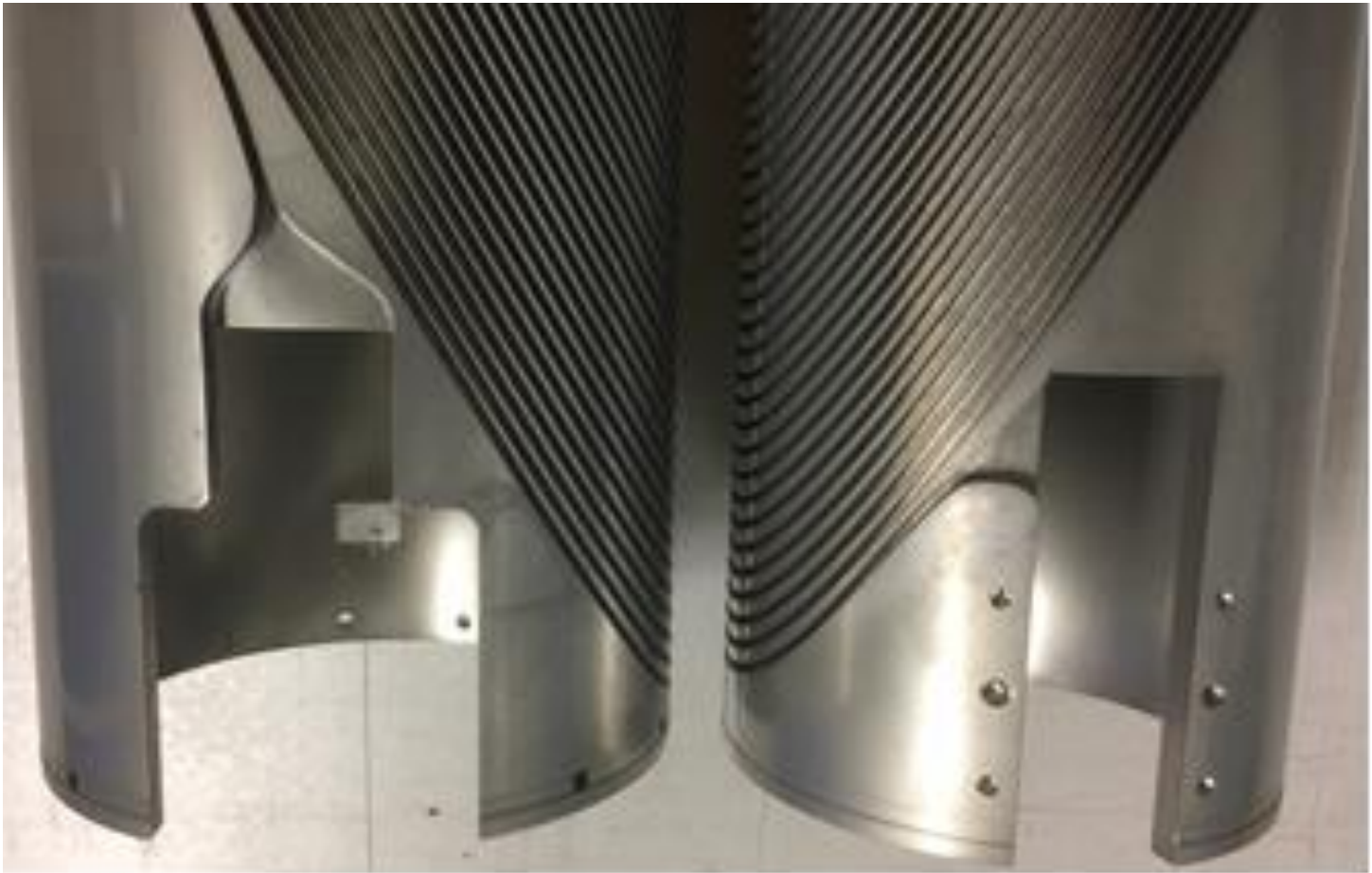
Example of polishing to remove burrs



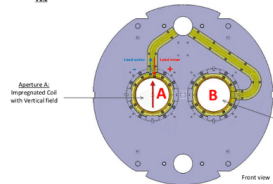
# Coil Winding



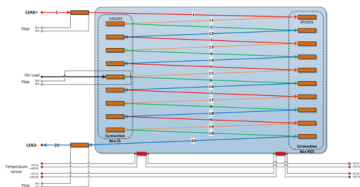
Two wires are wound at the same time, with low tension.  
This is repeated until we have the full 2 wide by 5 high coil.



Wiring Diagram  
CCT Model # LCT(MMS)  
VSL

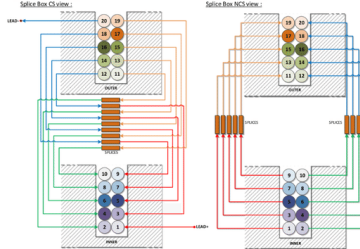


Aperture A:

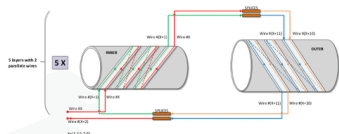


Transversal cross-section Solenoid Box CI view:

Transversal cross-section Solenoid Box NCK view:

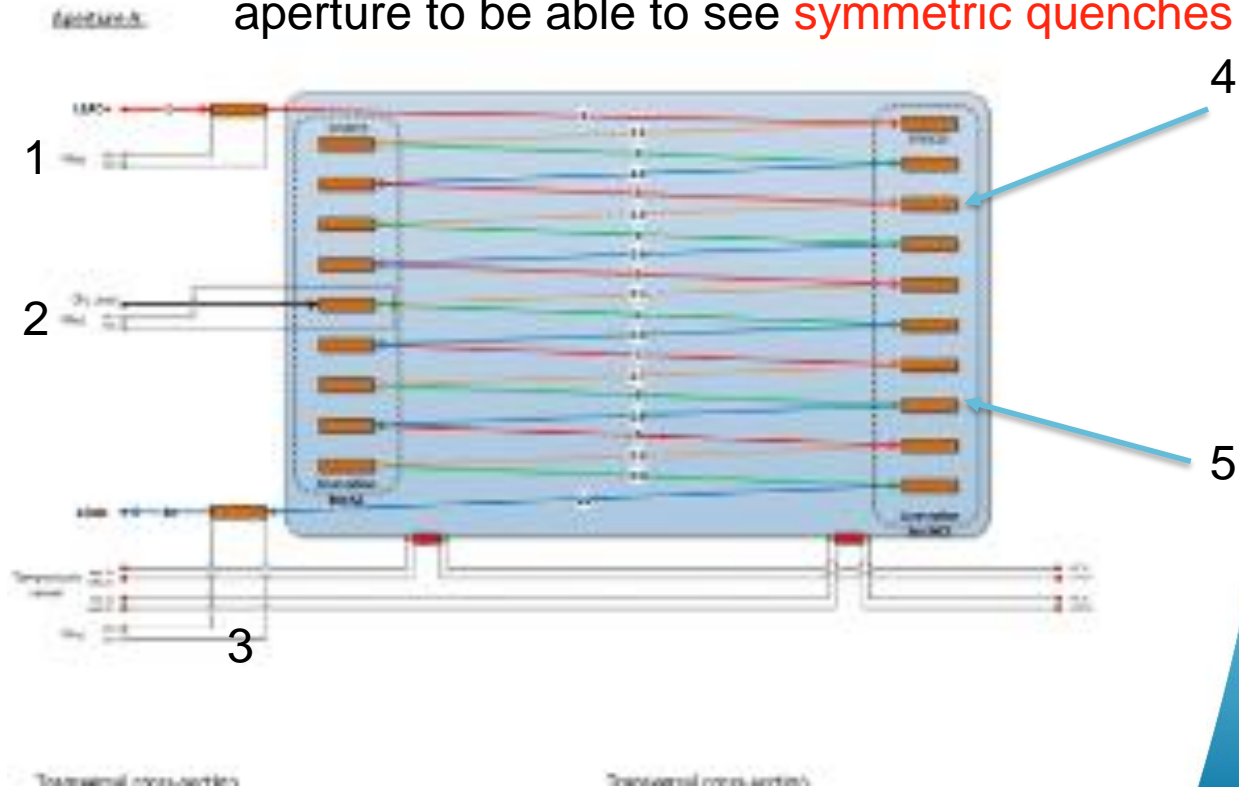


Laser winding details:



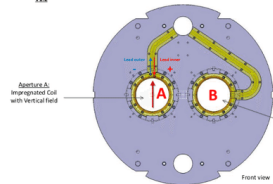
# Wiring

We may need 5 sets of voltage taps on each aperture to be able to see **symmetric quenches**

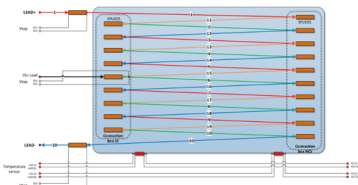




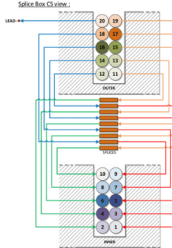
Wiring Diagram  
CCT Model # LCT(MMS)  
VSL



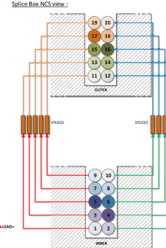
Assemble A:



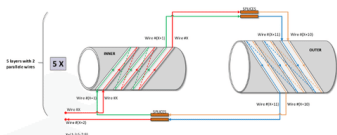
Transversal cross-section Solenoid Box CI view:



Transversal cross-section Solenoid Box NCK view:



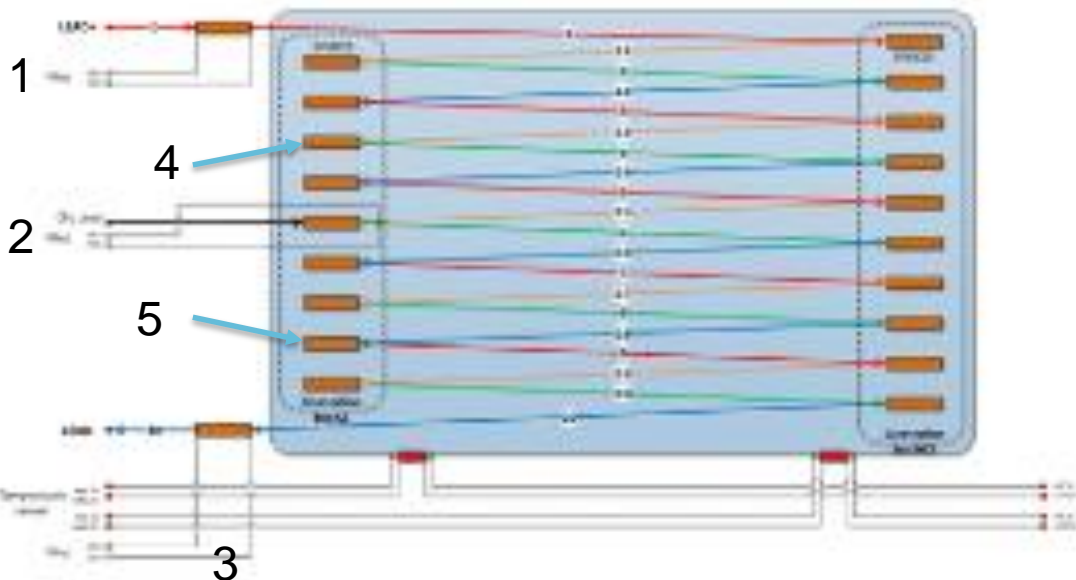
Laser winding details:



# Wiring

Would be better to have all instrumentation exiting at the lead end! So 4&5 should move.

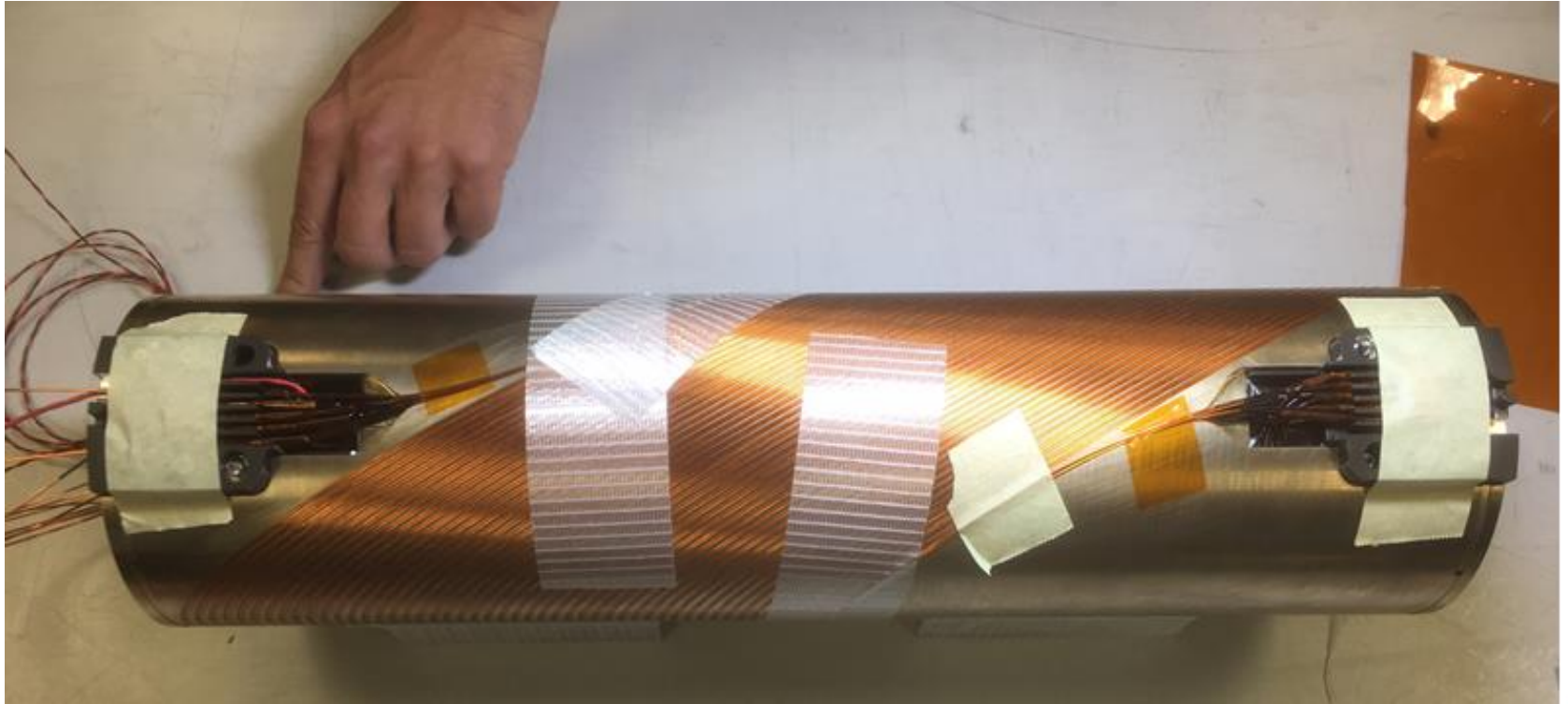
Assemble A:



Transversal cross-section:

Transversal cross-section:

# Joints at both end in the magnet former

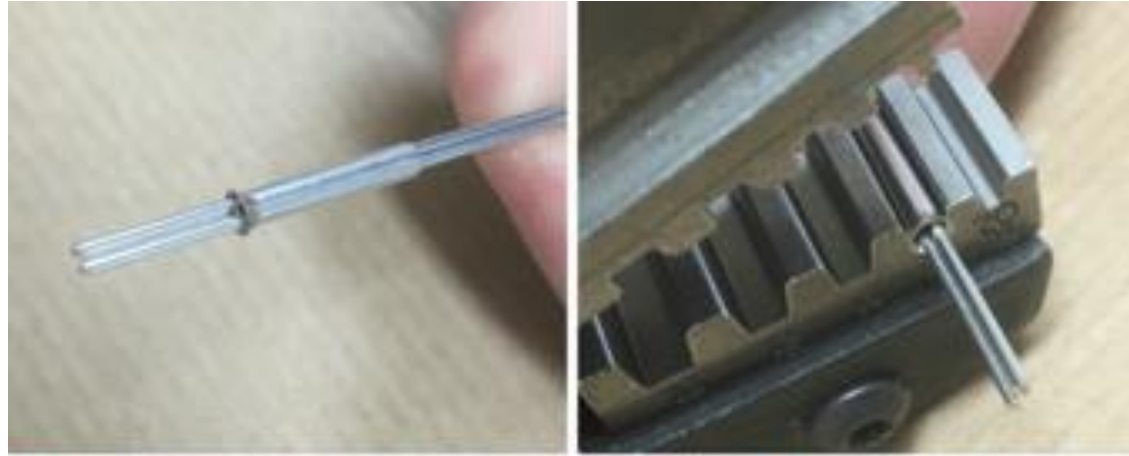
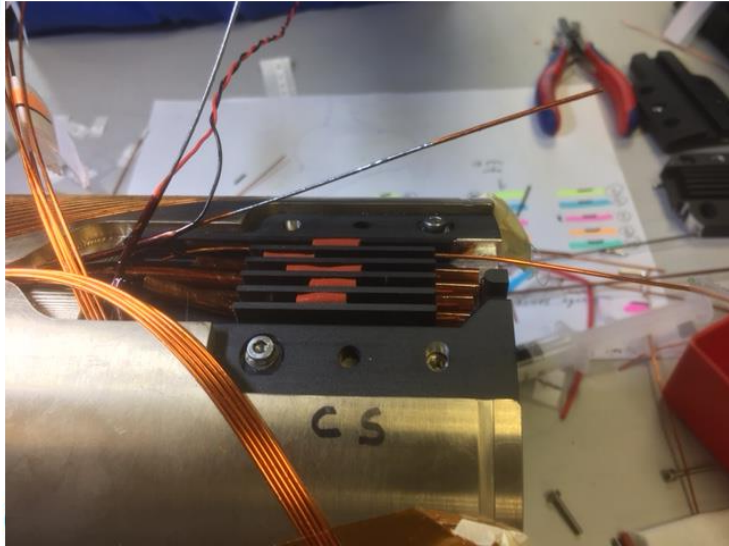


# Jointing

Jointing system:

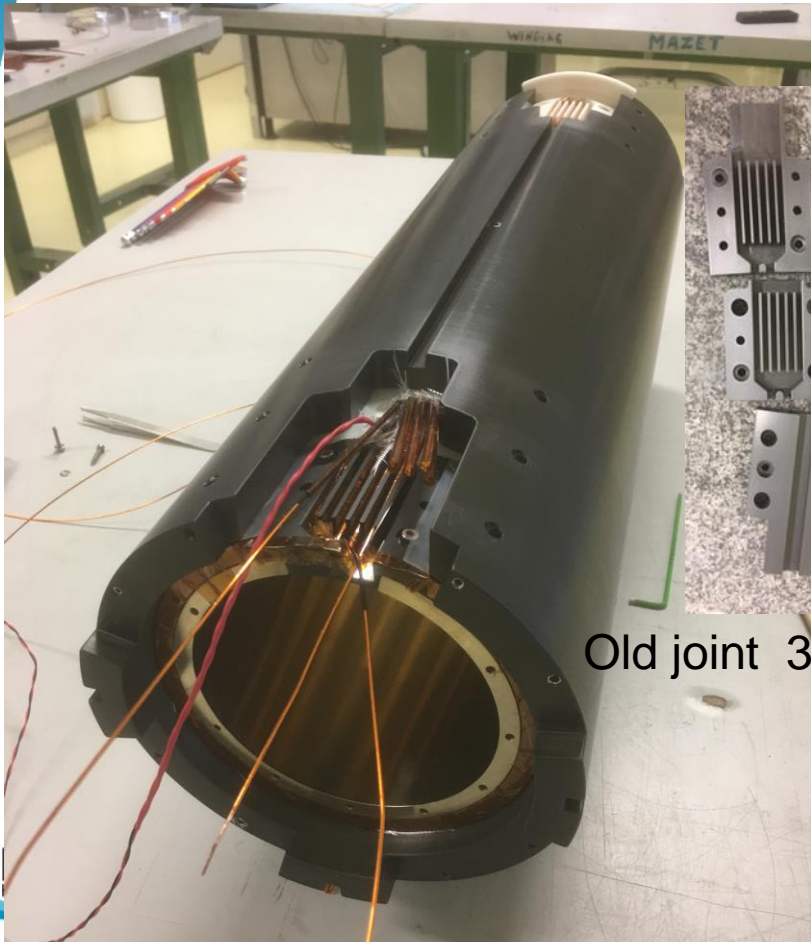
- 1) Tin wires,
- 2) Copper tube
- 3) Crimp for mechanical support
- 4) Solder
- 5) Insulation

~6 nOhm's

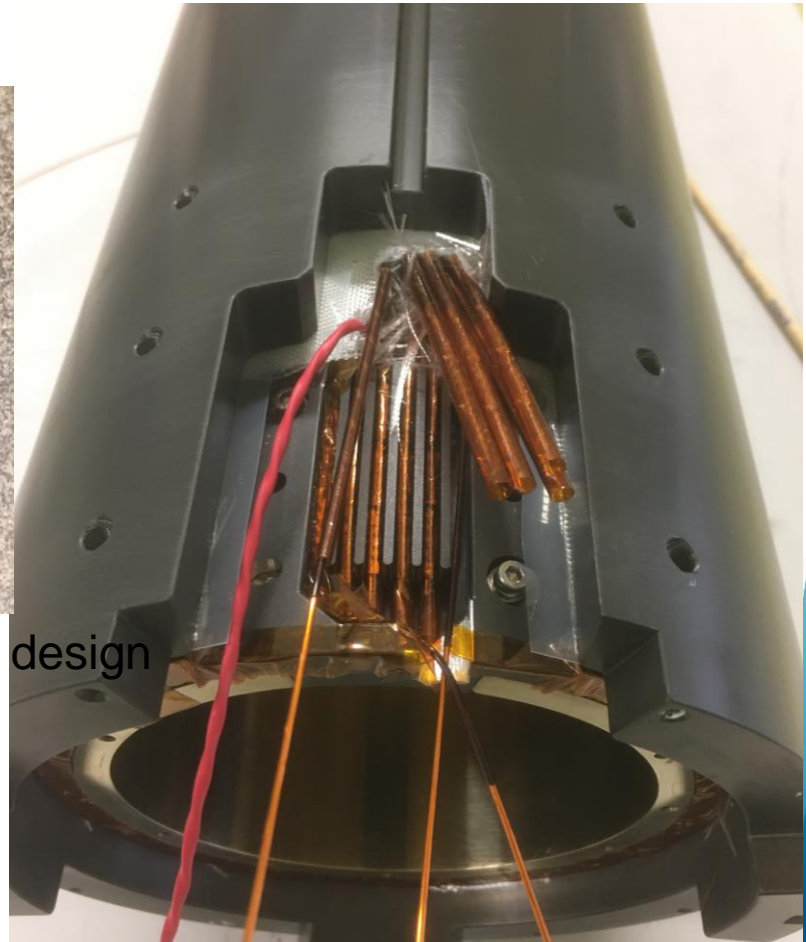




# Joint box

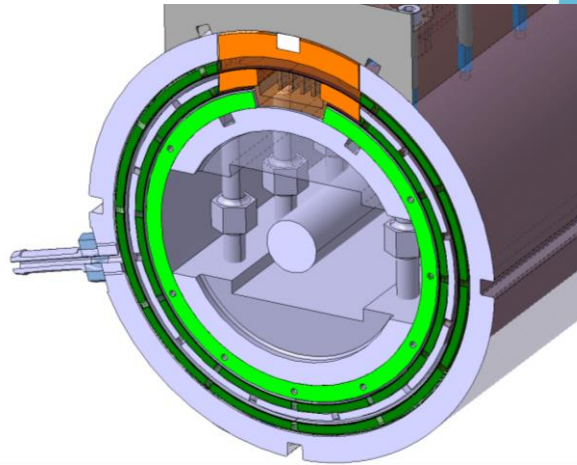
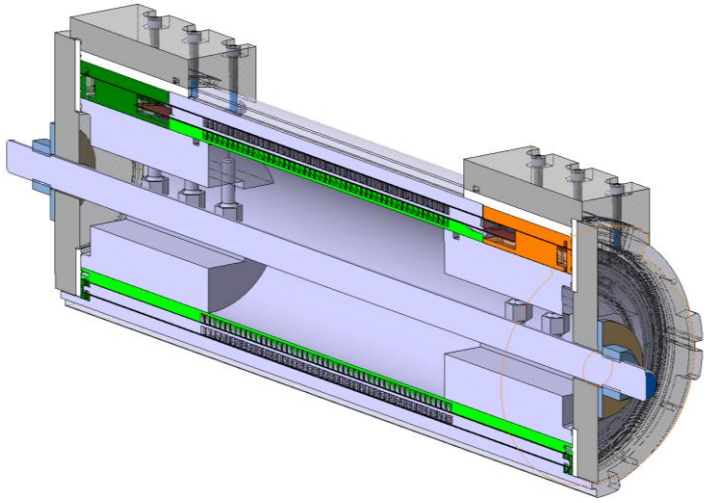
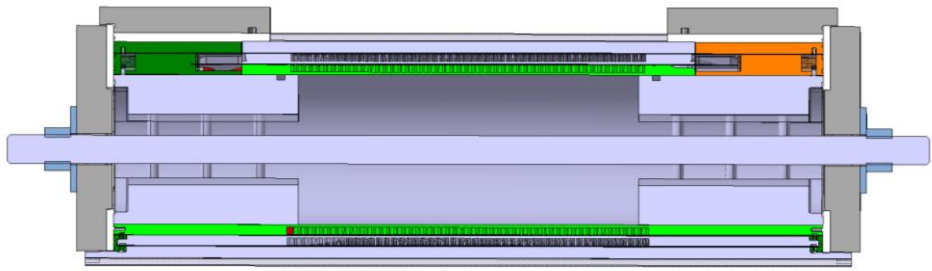
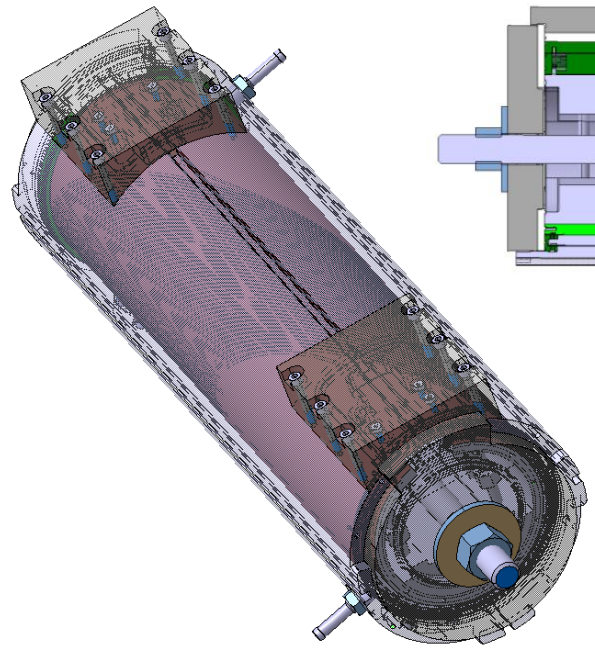


Old joint 3 part box design



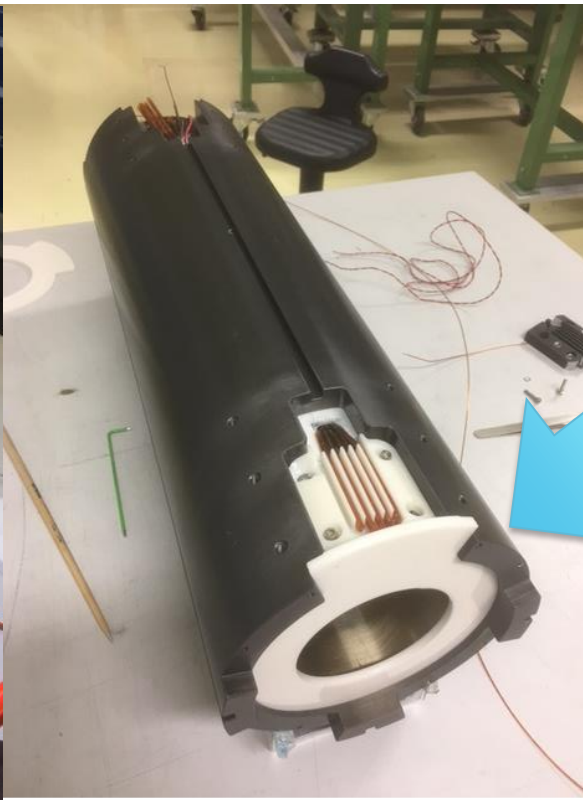
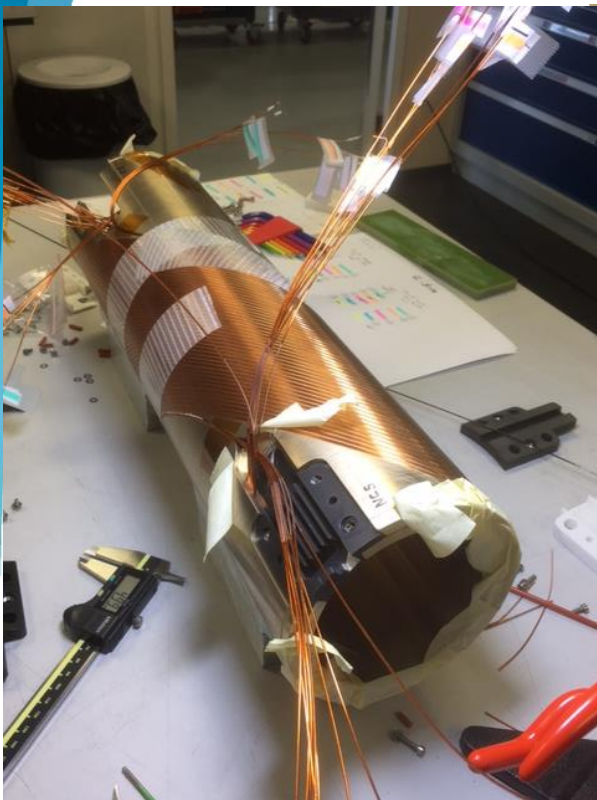
# Impregnation

This is the only specialist tooling that is needed to build the magnet, along with the winding machine and impregnation equipment.





# Coils impregnated inside the magnet outer support tube



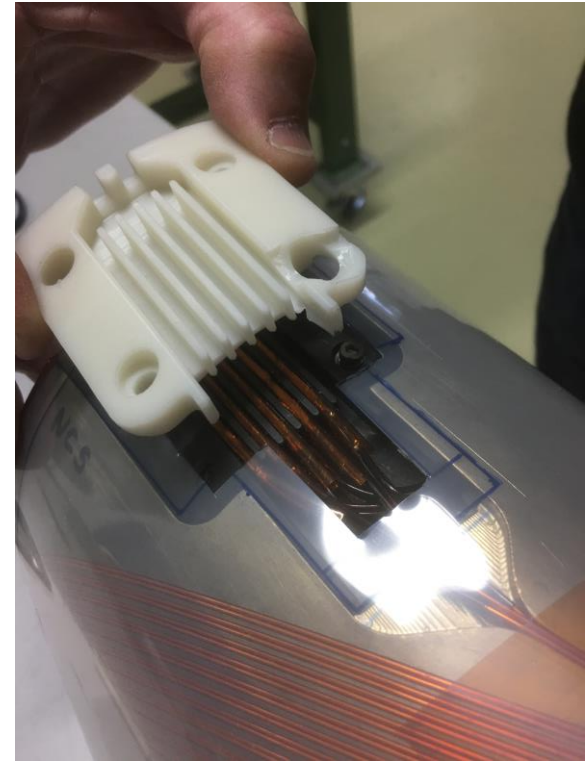
Vacuum / pressure Impregnation seal



Seal mechanical support

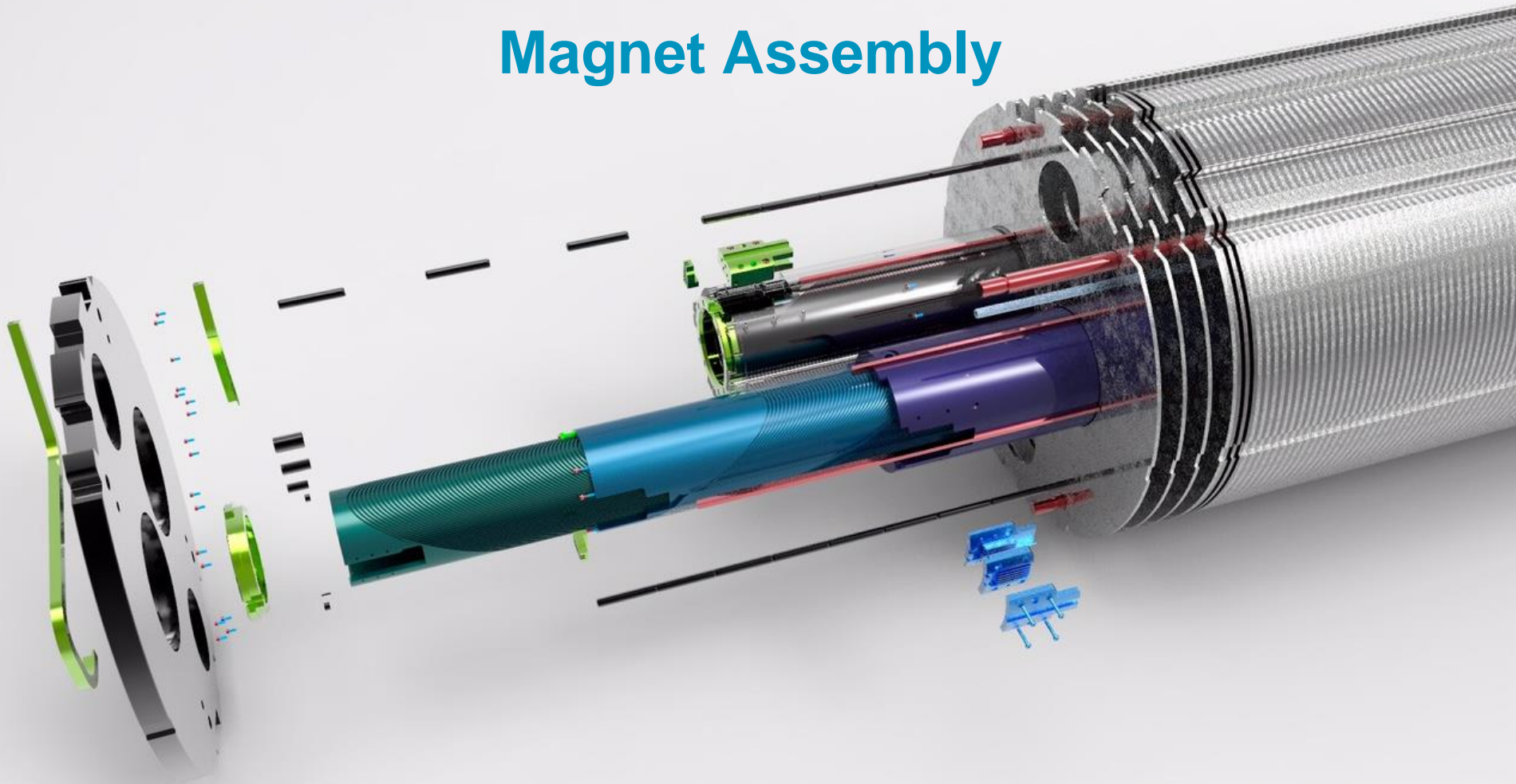


# Insulation between the two layers



Two layers of insulation with min  
4mm brake down distance for

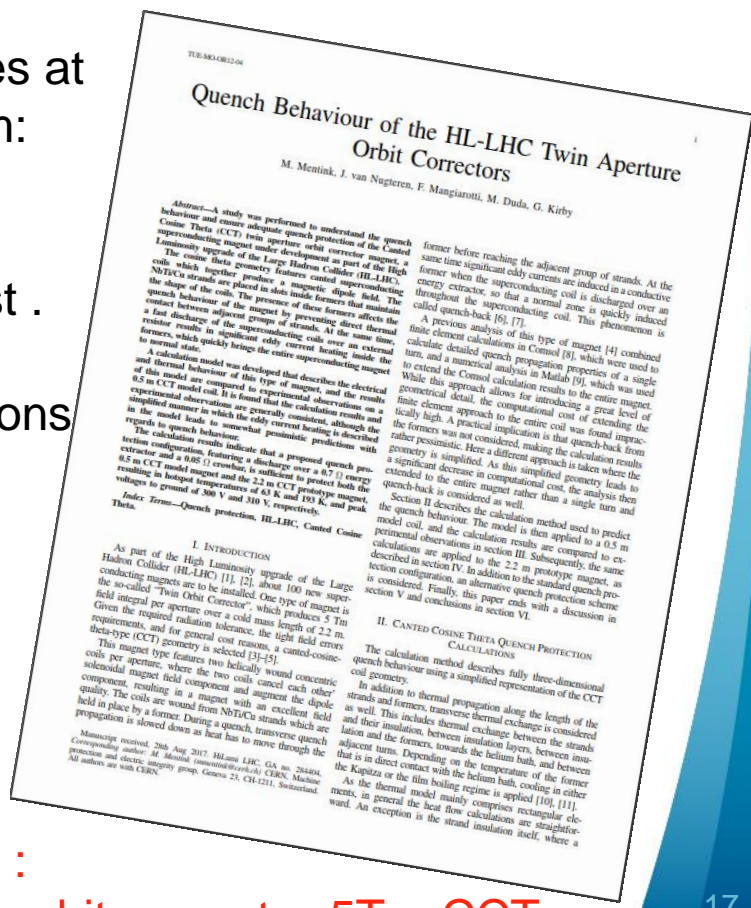
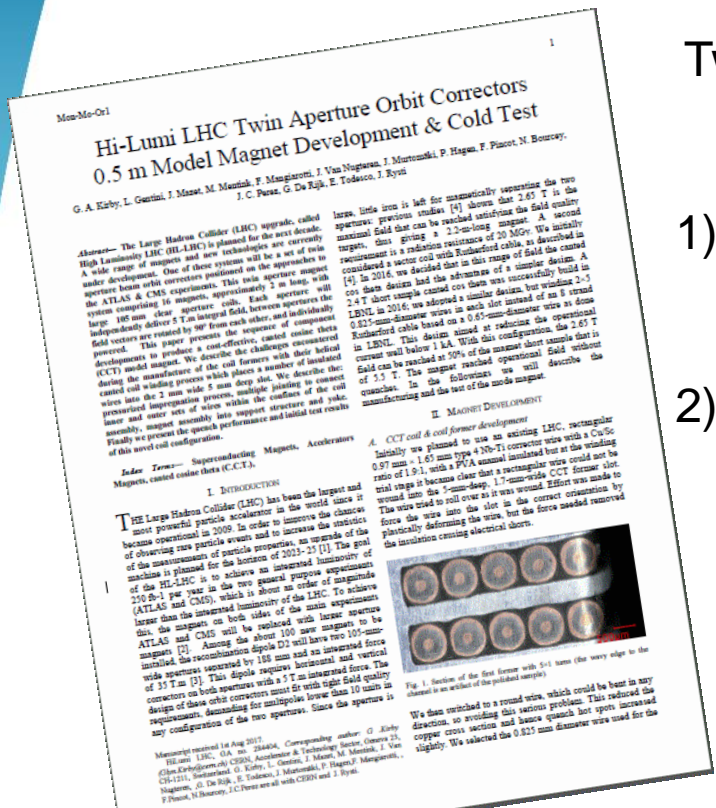
# Magnet Assembly



# MT25 Papers

## Two papers publishes at MT 25 Amsterdam:

- 1) 0.5 m model assembly and test .
- 2) Quench Calculations

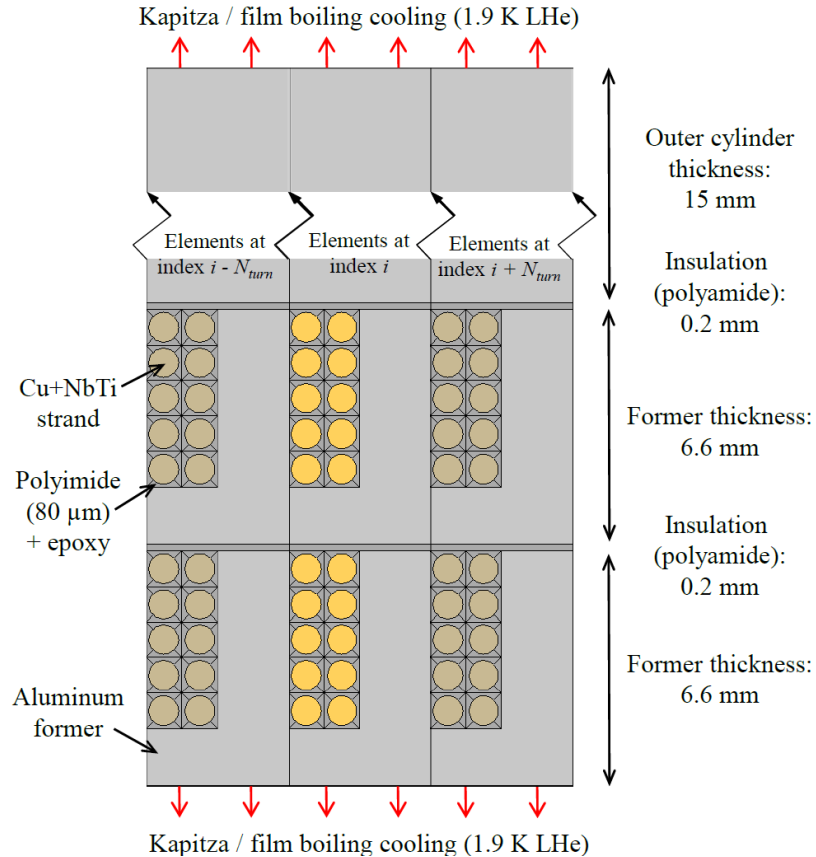


Pre-prints are available at :

<https://www.researchgate.net/project/LHC-hi-Lumi-orbit-corrector-5Tm-CCT>

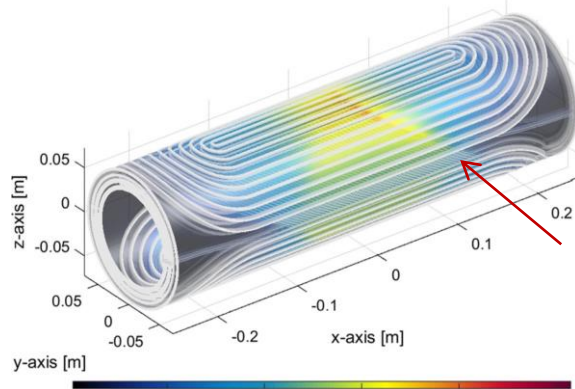
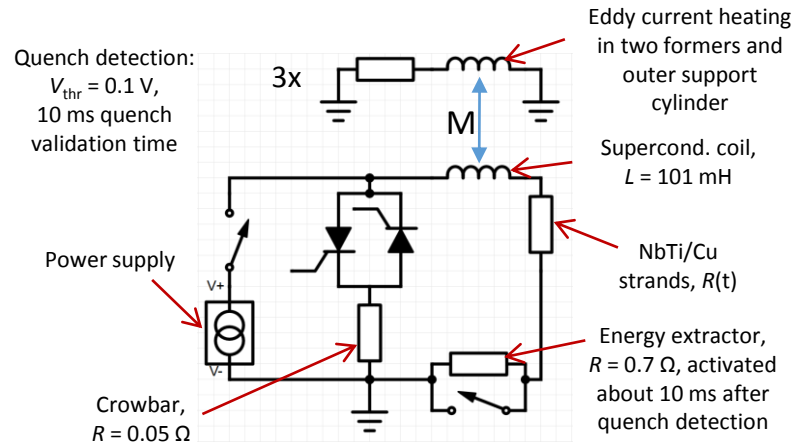


# Simulation model: Thermal aspects



- Incorporates a simplified three-dimensional thermal layout
- Longitudinal thermal exchange along strands and formers
- Transverse thermal exchange
  - Between strands, insulation, formers, former insulation, and outer support cylinder
  - Between adjacent turns
  - To 1.9 K helium bath (Kapitza / film boiling)

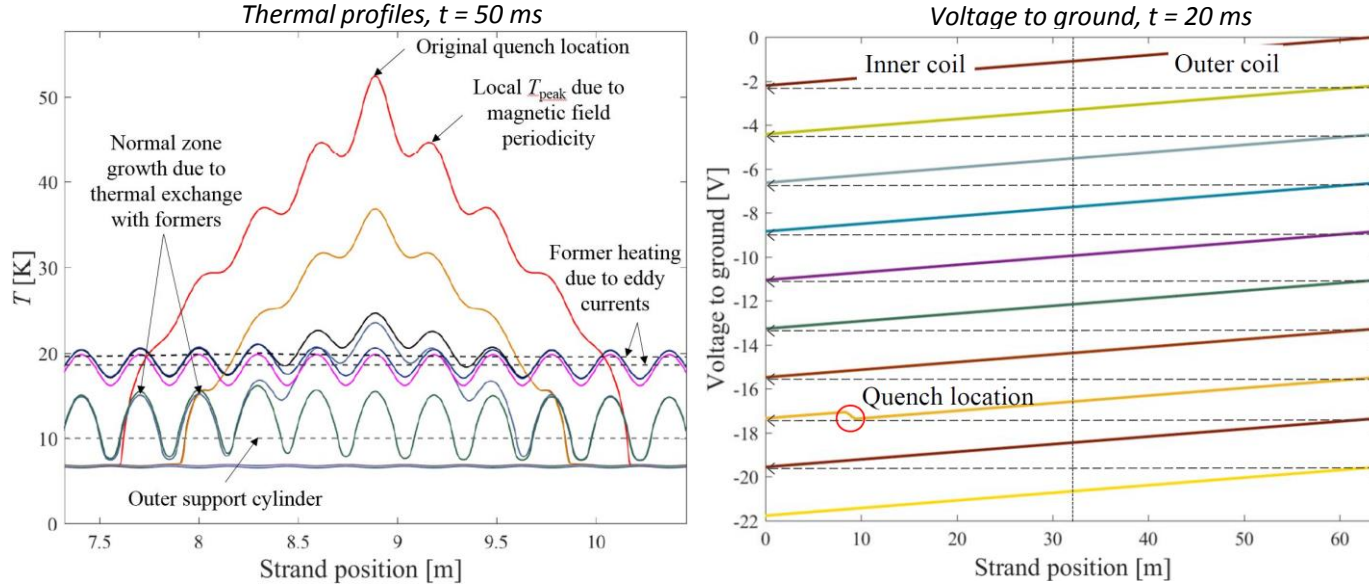
# Simulation model: Electro-magnetic aspects



Simplified  
assumption: Eddy  
currents follow  
particular path with  
homogeneous  
current distribution

- Magnet assumed to be powered by a typical LHC 600 A circuit, including a crowbar and an energy extractor
- Eddy currents in the formers and outer support cylinder: Assumed to follow specific path with homogeneous current density (= simplified assumption)
- Inductances and magnetic field distributions calculated with Field simulation package

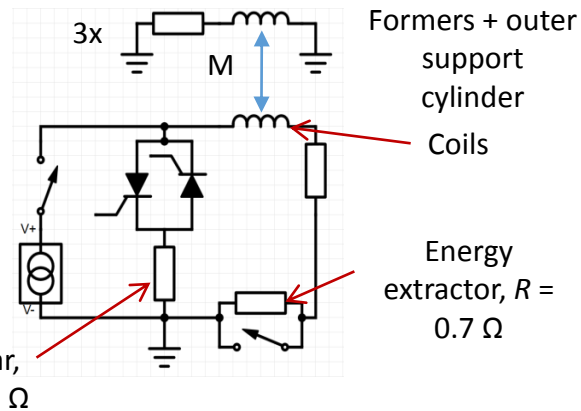
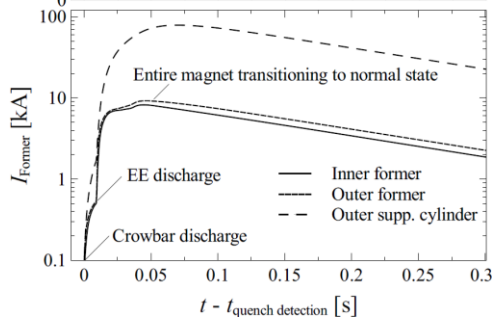
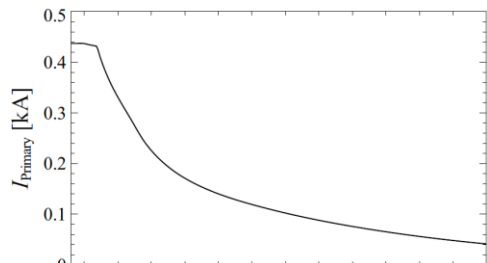
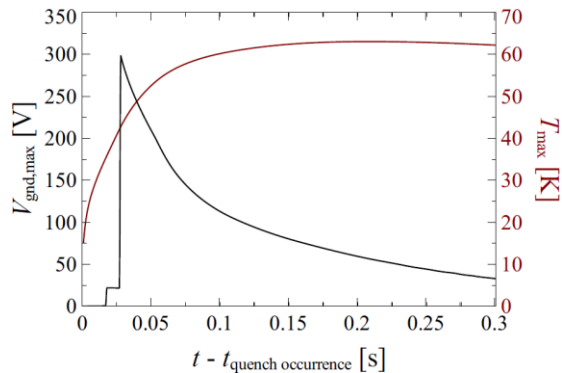
## 0.5 m CCT model magnet, calculation results 1/2



- Initial operating current: 438 A
- After quench detection and validation, magnet is discharged over 0.05  $\Omega$  crowbar + 0.7  $\Omega$  energy extractor (10 ms after quench detection + validation)
- Eddy current heating --> Normal zone spreads throughout magnet
- Peak voltage to ground dominated by external resistors

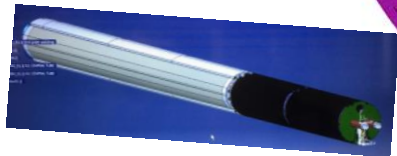
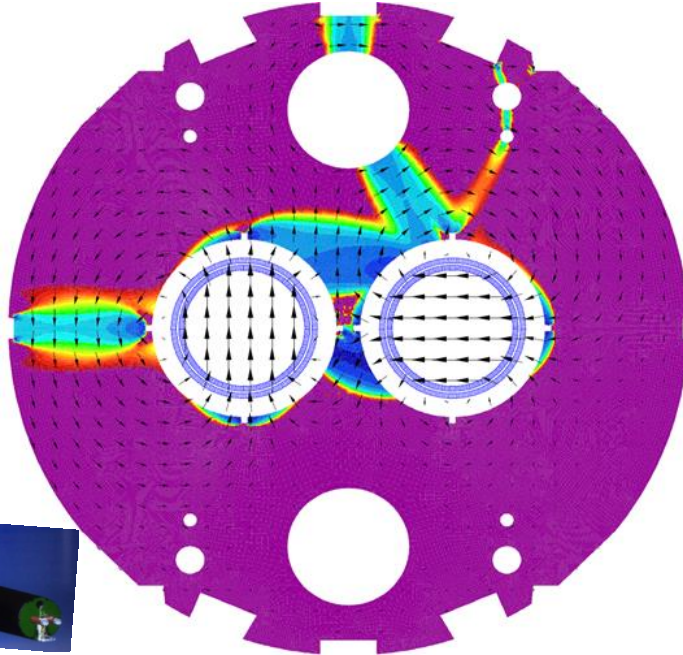


# 0.5 m CCT model magnet, calculation results 2/2

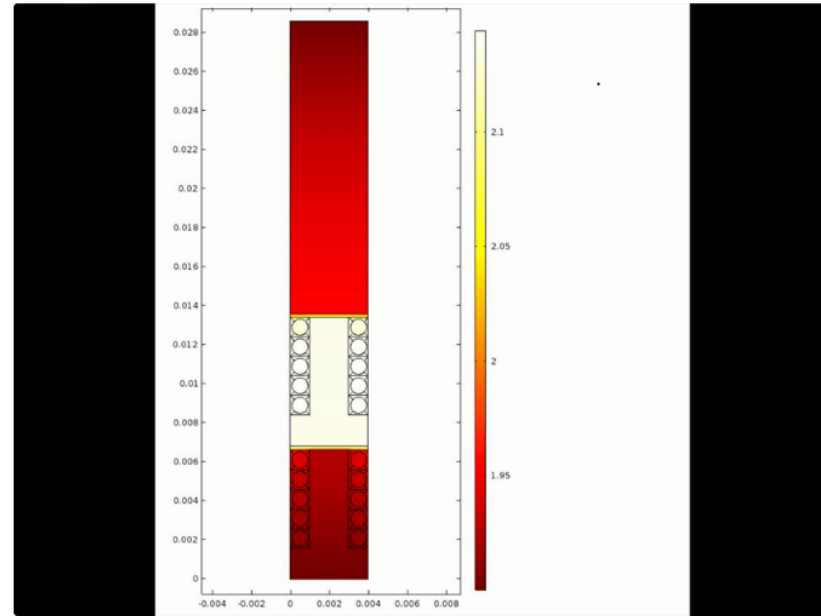


- Quench detection (0.1 V threshold) + 10 ms validation --> 17 ms in total
- Initial discharge over crowbar, followed by discharge over energy extractor (10ms later)
- Peak temperature: 63 K
- Peak voltage to ground: 300 Volts
- For the 2.2m coils, extrapolating from the test results we expect:
  - Hot spot 193 K
  - Max voltage 330 Volts

# Beam heating calculations and heat extraction through cold mass



Large holes to extract heat from D2  
through the corrector to the cold  
point  $225 \text{ cm}^2$



Heat load from radiation.  $1 \text{ mW/cm}^3$  ( $1000 \text{ W/m}^3$ ) was applied to the full cross section? and fixed the former boundaries (i.e. the interface with the helium) at  $1.9 \text{ K}$ .

The result of this calculation is that the peak temperature is  $2.15 \text{ K}$ . This number is mainly determined by the thickness of the polyimide insulation separating the middle former from the innermost and outermost former. Here I assume a polyimide insulation thickness of  $0.2 \text{ mm}$  and a thermal conductivity of  $0.0037 \text{ W/(m}^*\text{K)}$ .

The heat load towards the helium is rather low; I find an average load of  $14 \text{ W/m}^2$ , well below the Kapitza limit of  $35000 \text{ W/m}^2$ .

to conclude the temperature in the coil will not increase above the lambda point. However boundaries are in perfect contact this may not be the case in the magnet.

# Magnet Test

Tested to 1.9K

RRR of wire measured at 253, high!

No quench up to 422 A nominal

One quench at 438 A (hot spot 57K)

Then No quench up to 460 A ultimate design value

Thermal cycle no quench.

Nominal ramp rate 4.2 A/s.

Max tested ramp rate with no quench 40 A/s

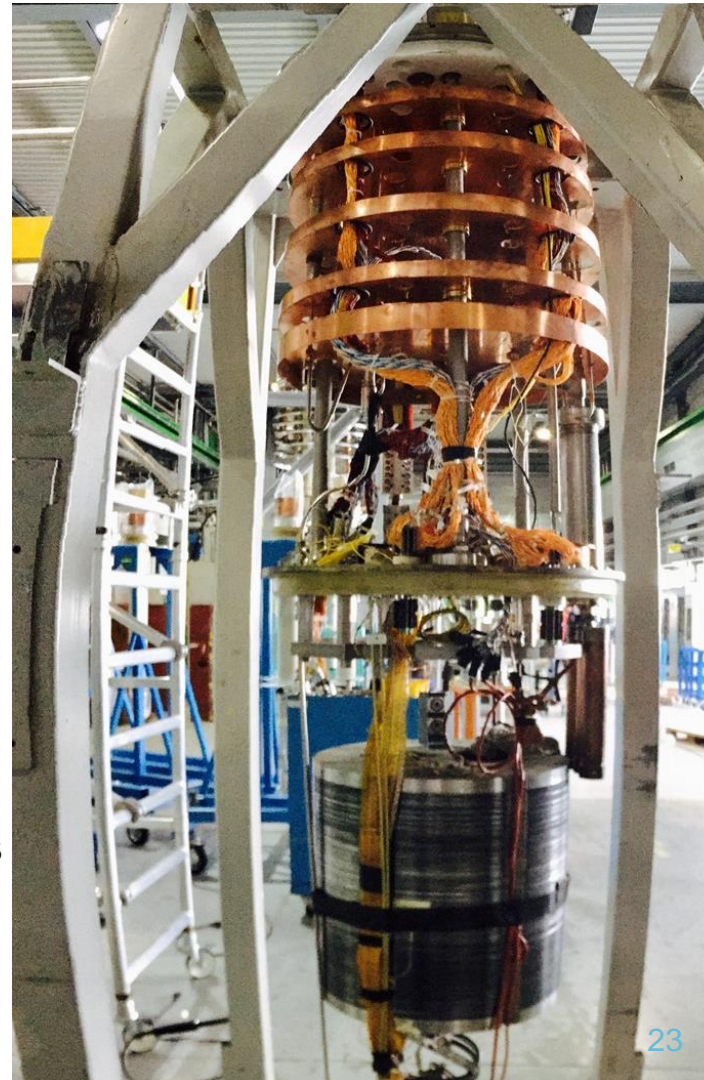
Joint resistances: Average 5.7 nOhm's

120 +/- 20 nΩ over one aperture.

Energy distribution during quench : with 0.7 Ω dump:

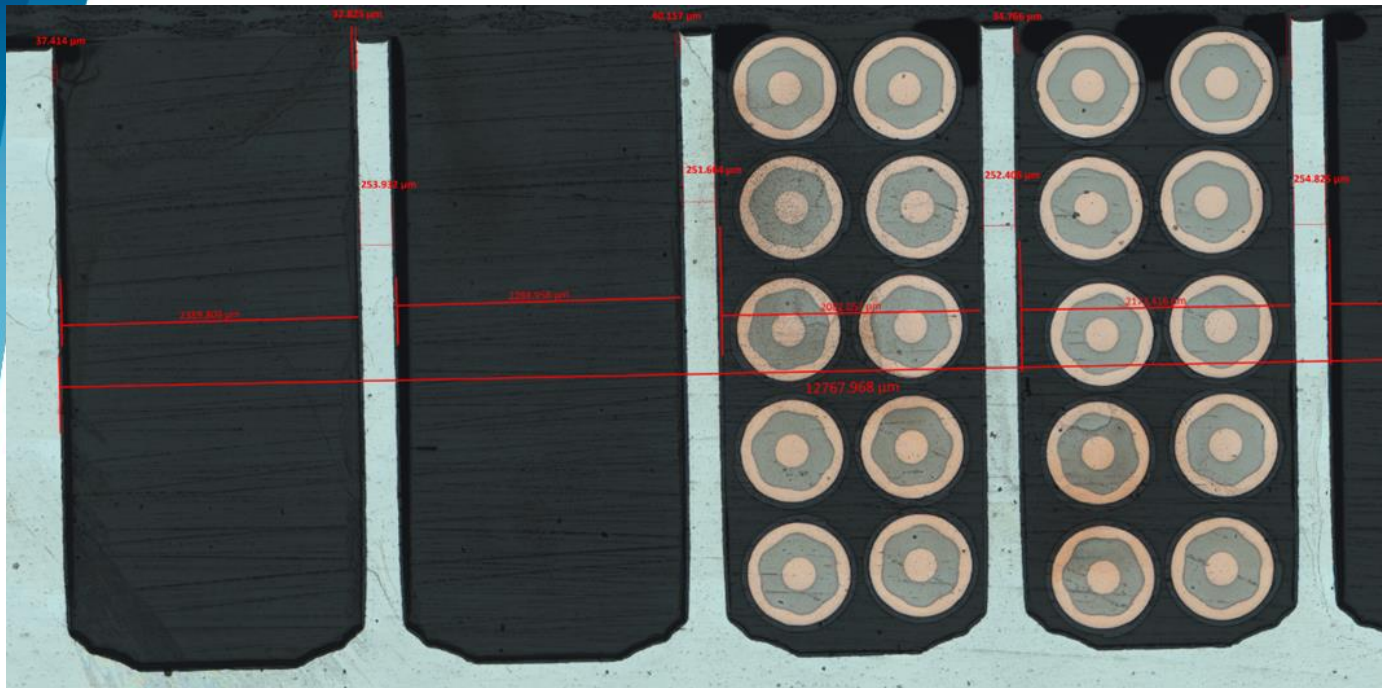
Coil 13%, Dump 59%,aluminium support tube and formers

28%





- Next model



### Channel width machining test.

A number of different channel widths were machined  
(2.1, 2.2, 2.3, 2.4 mm)

The aluminium block was then hard-anodized with a 0.02 mm build-up of anodization layer. The insulated wires were then impregnated into the channels

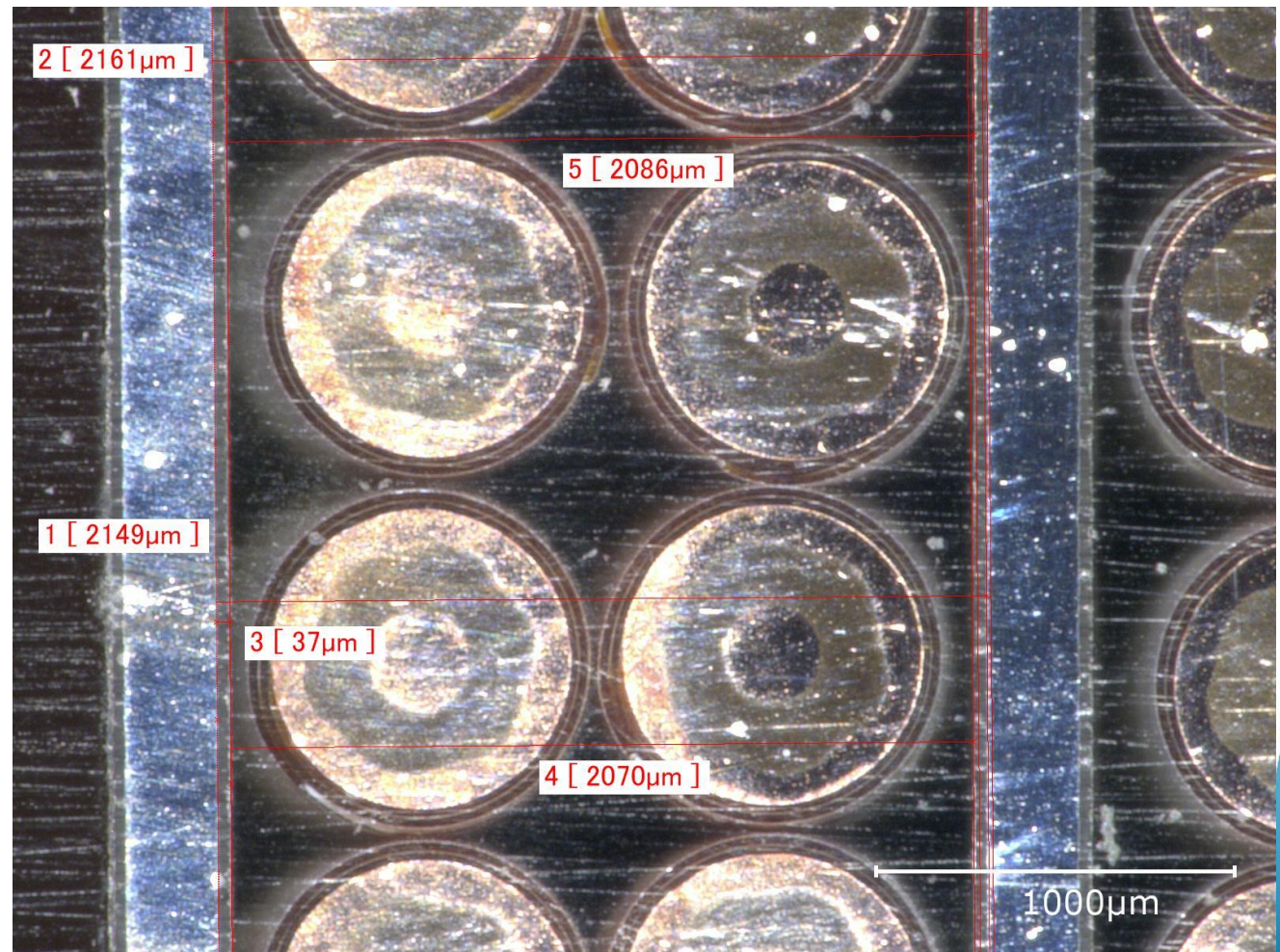
## Channel Width Test

We see the:

Anodized later on the  
aluminium former,

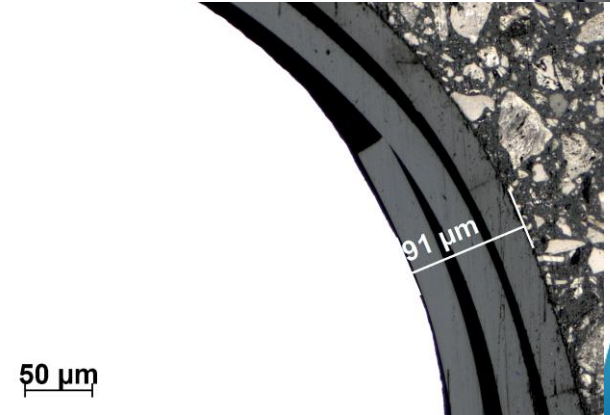
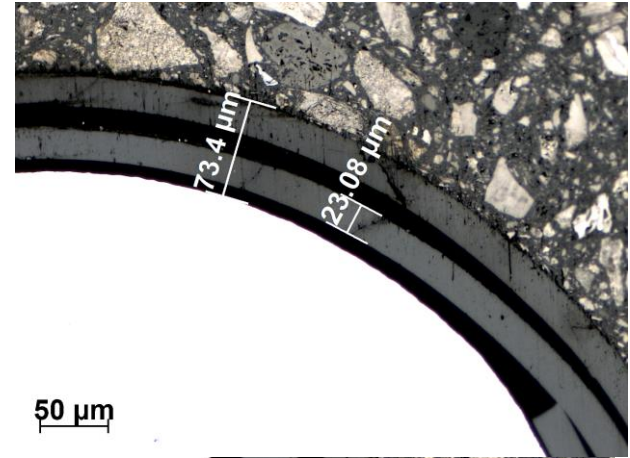
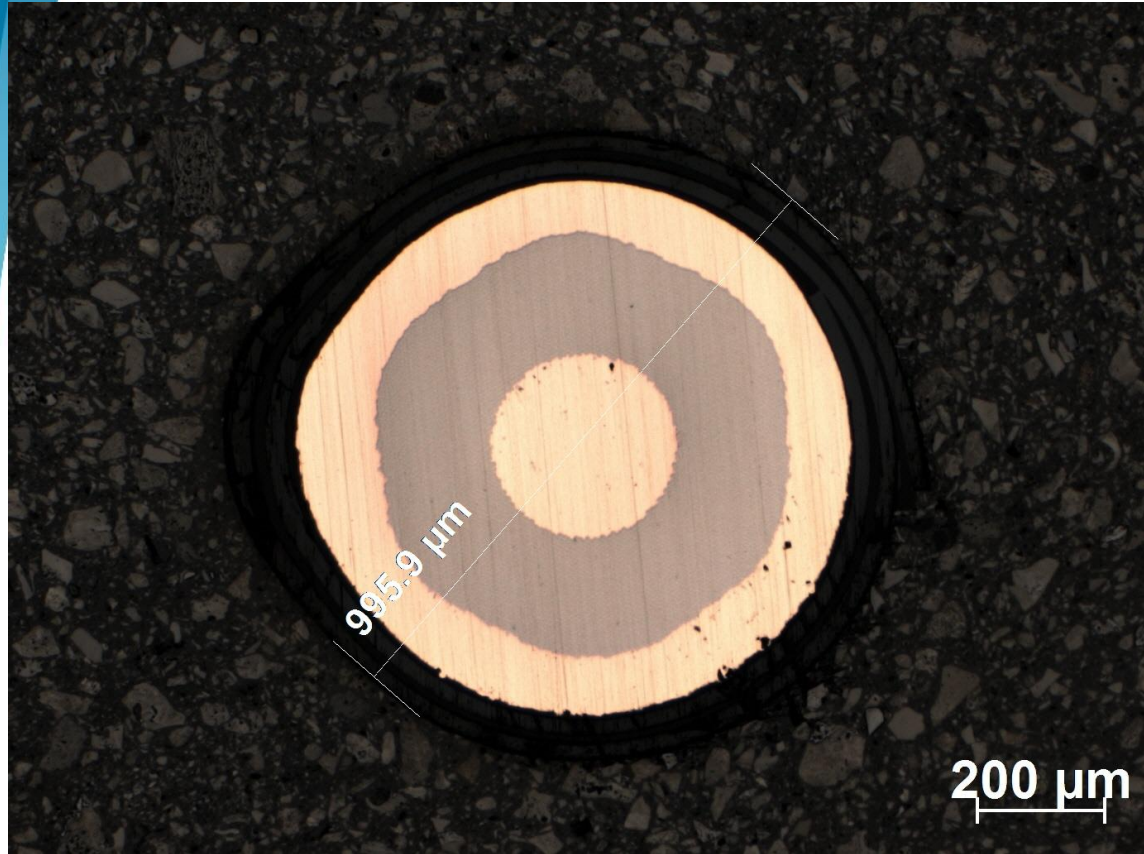
Insulated wires,

Resin filling the space  
between wires and  
former.

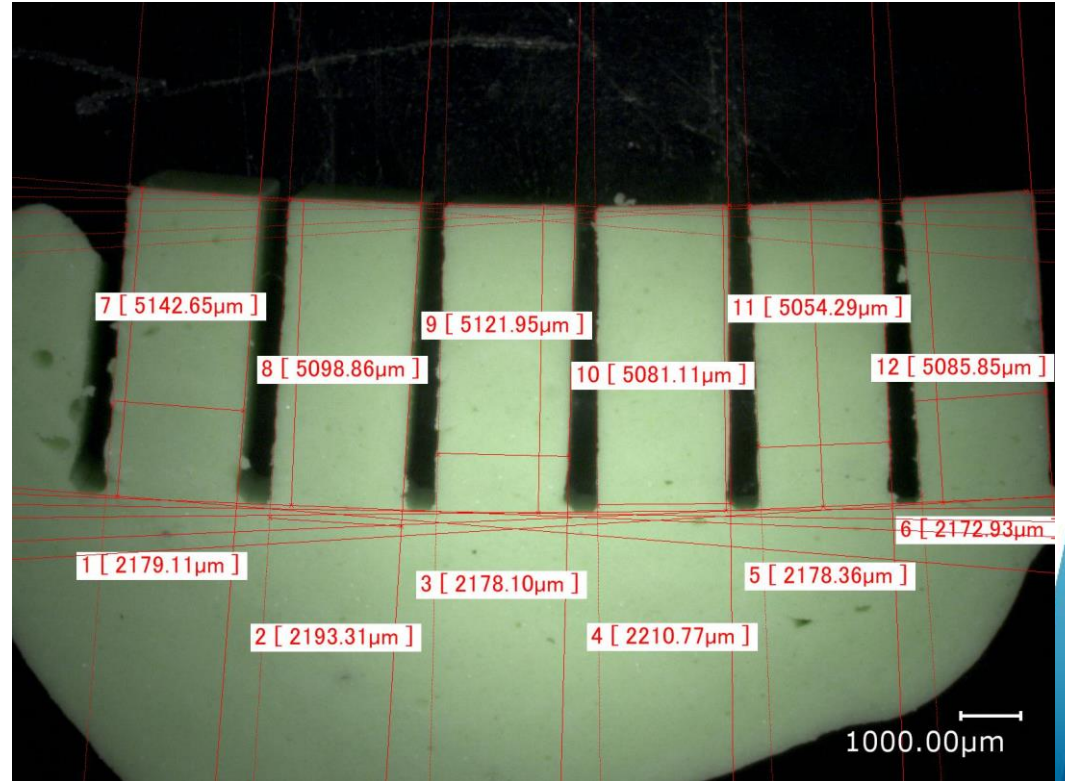




# Insulation design in the magnet that was tested



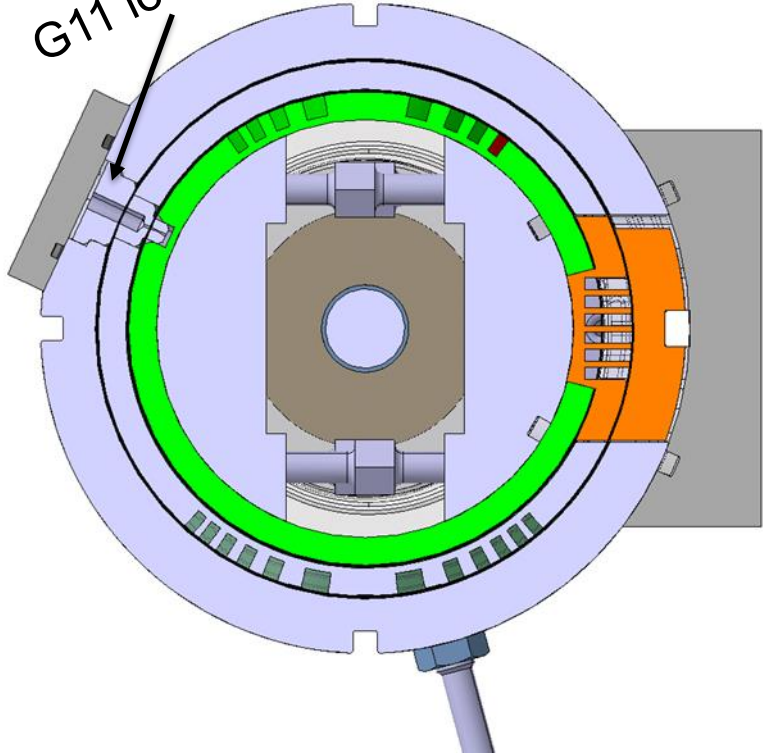
# Test cut for firm that will machine the 2.2 m formers



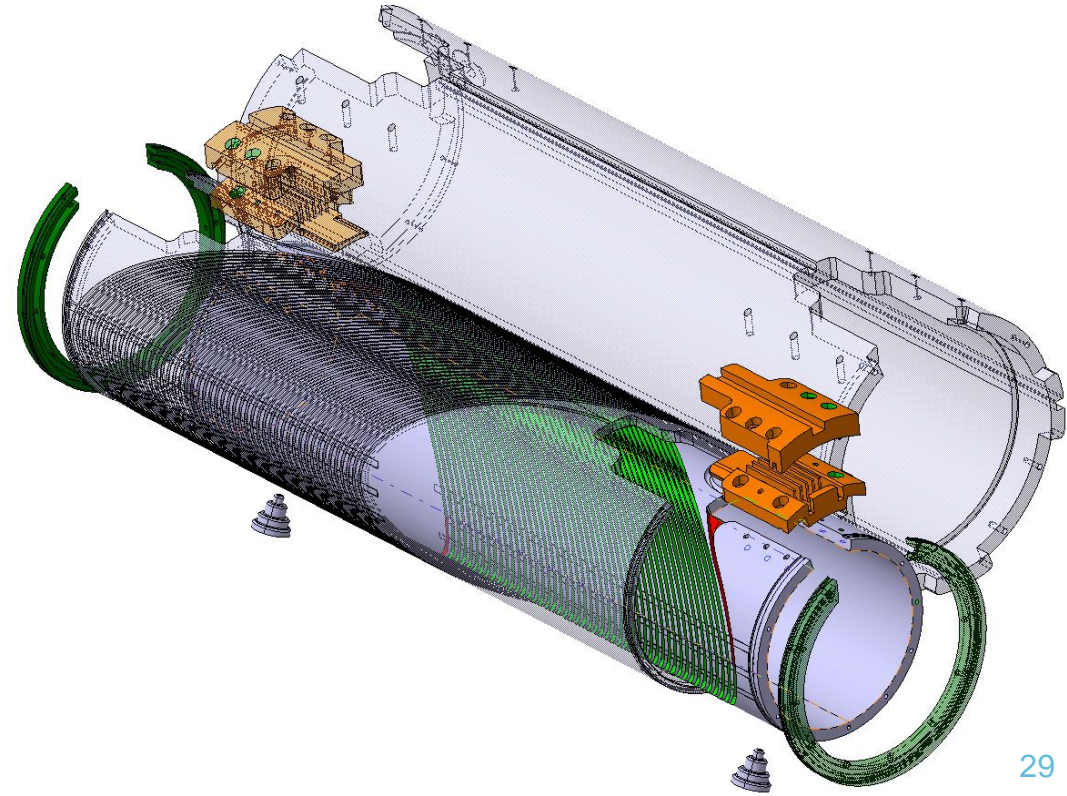


# Improved design

G11 locking pins



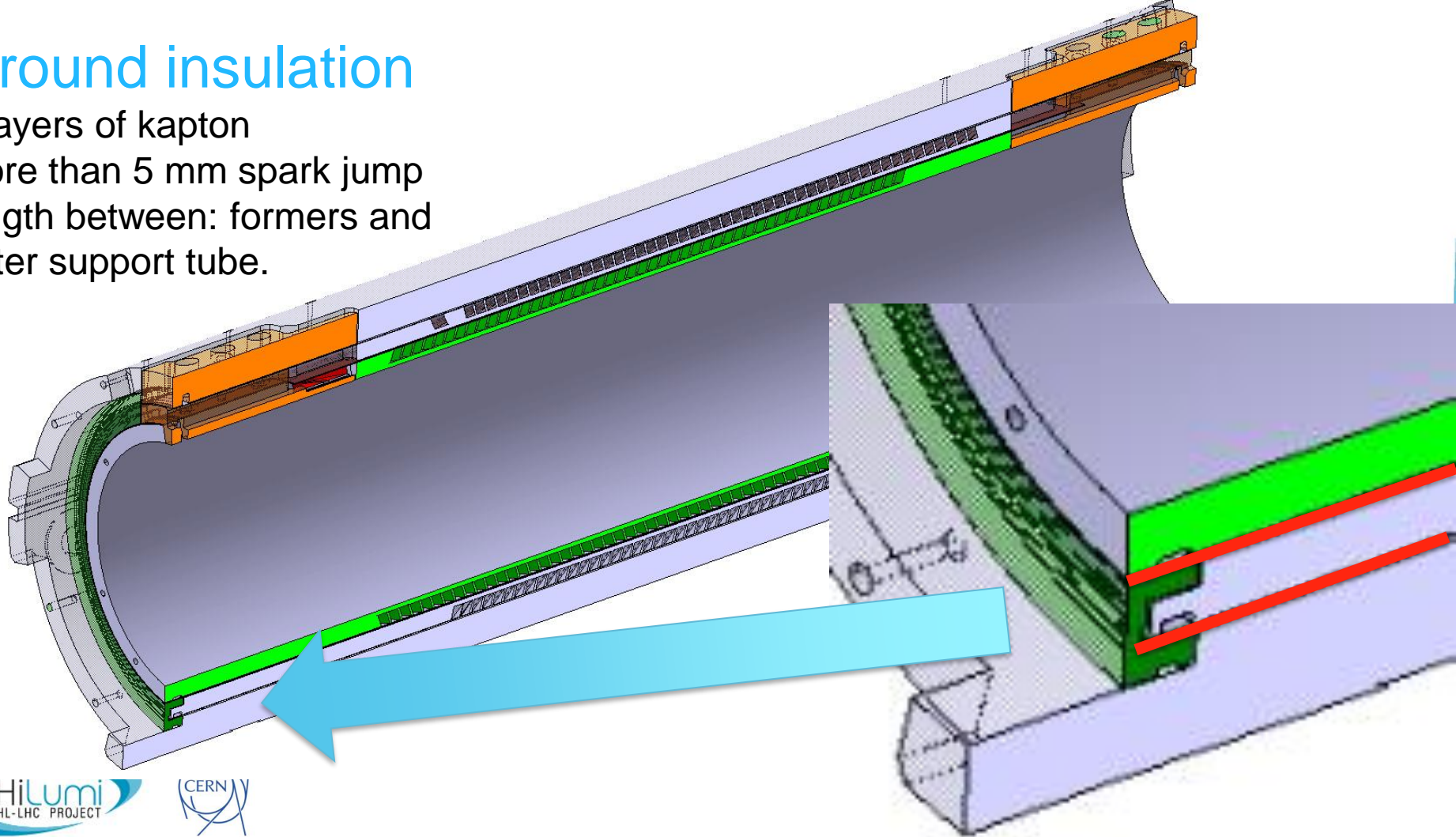
Less components  
Improved access for impregnation



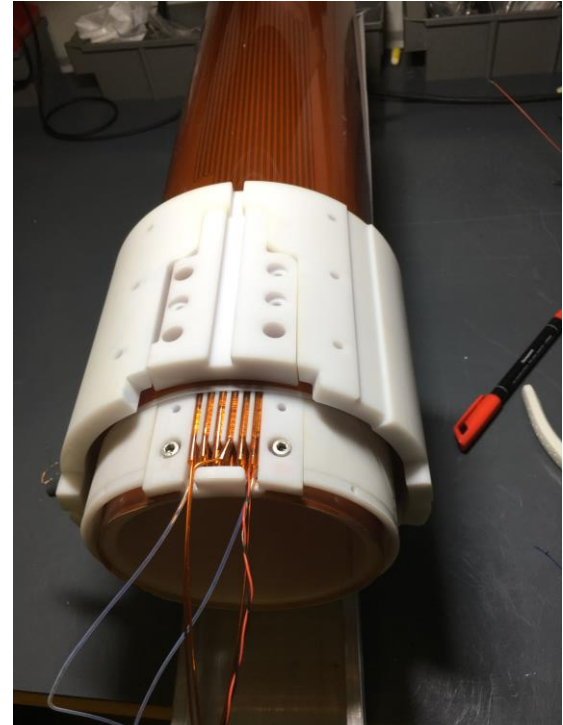
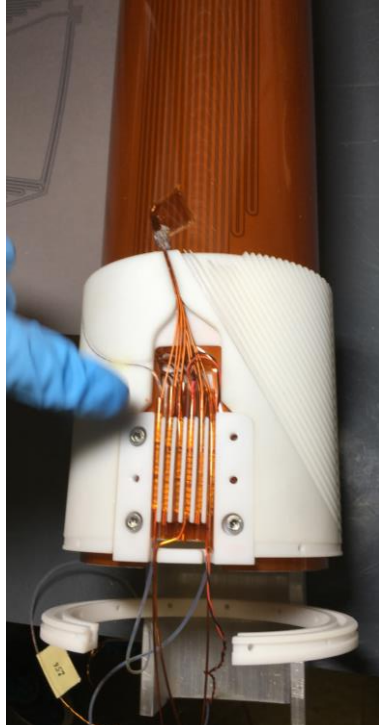


# Ground insulation

2 layers of kapton  
More than 5 mm spark jump length between: formers and outer support tube.

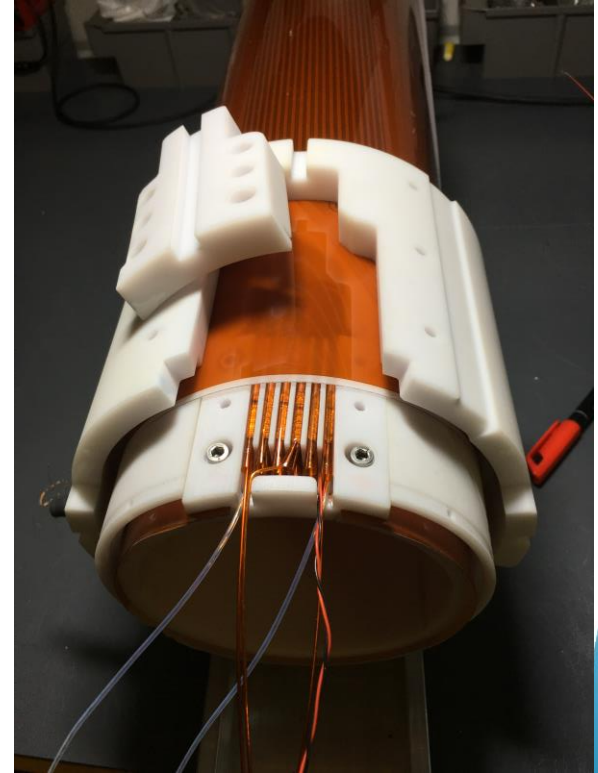
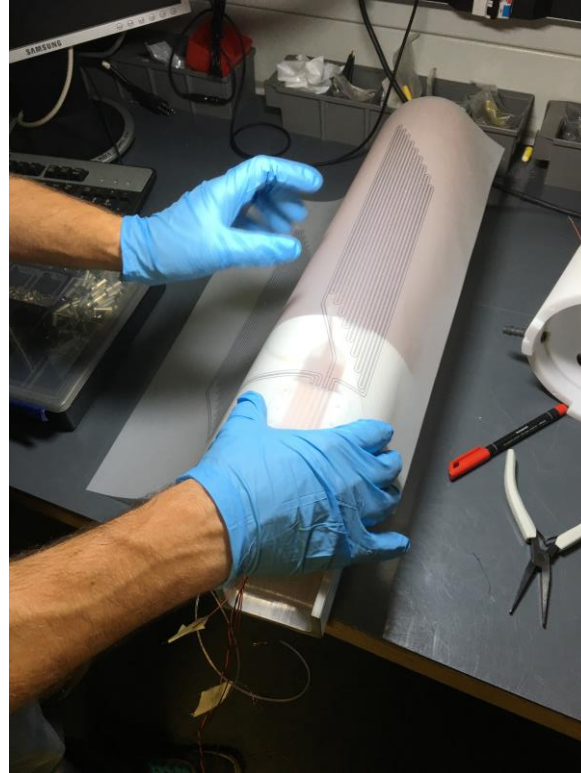
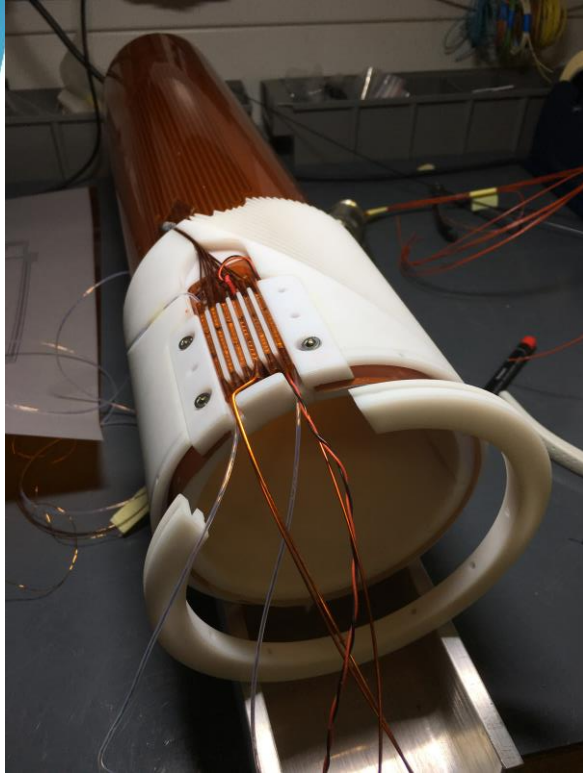


# New design: less parts, improved ground insulation, channels for instrumentation



The joint box, joint support plate was simplified from two parts to one, channels for voltage taps and temperature sensor wiring was improved. We are now considering deleting the joint box cover plate.

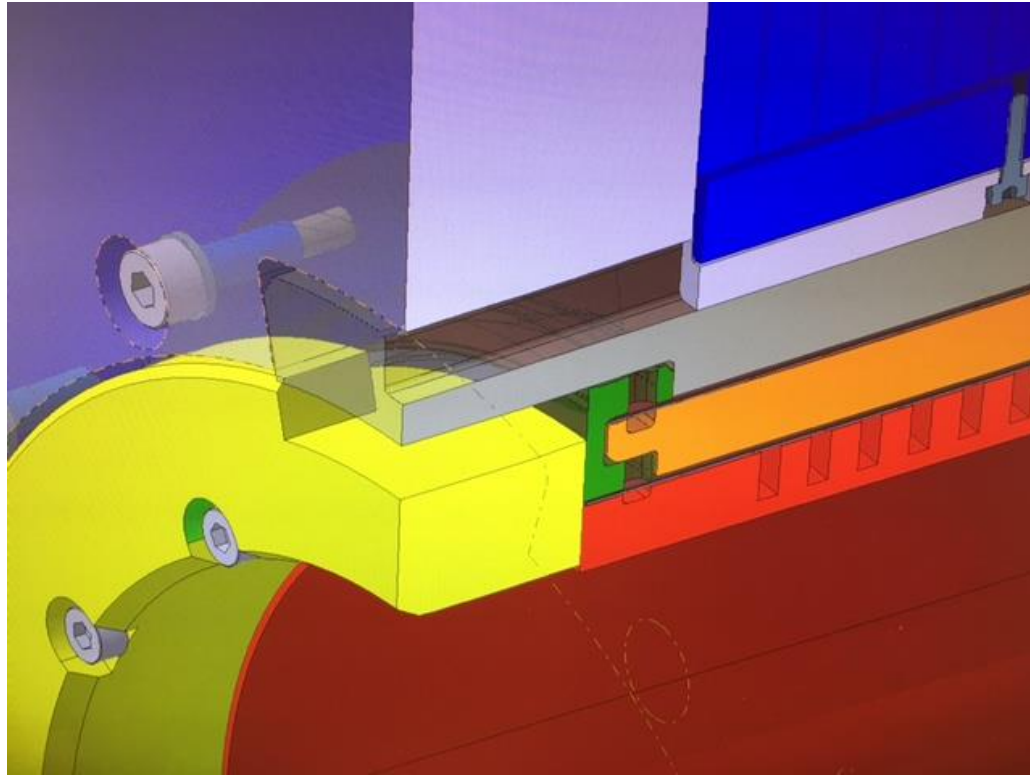
# Beam simulation heaters in trace part of insulation.



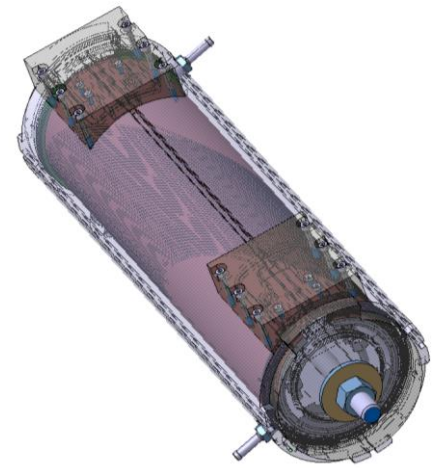
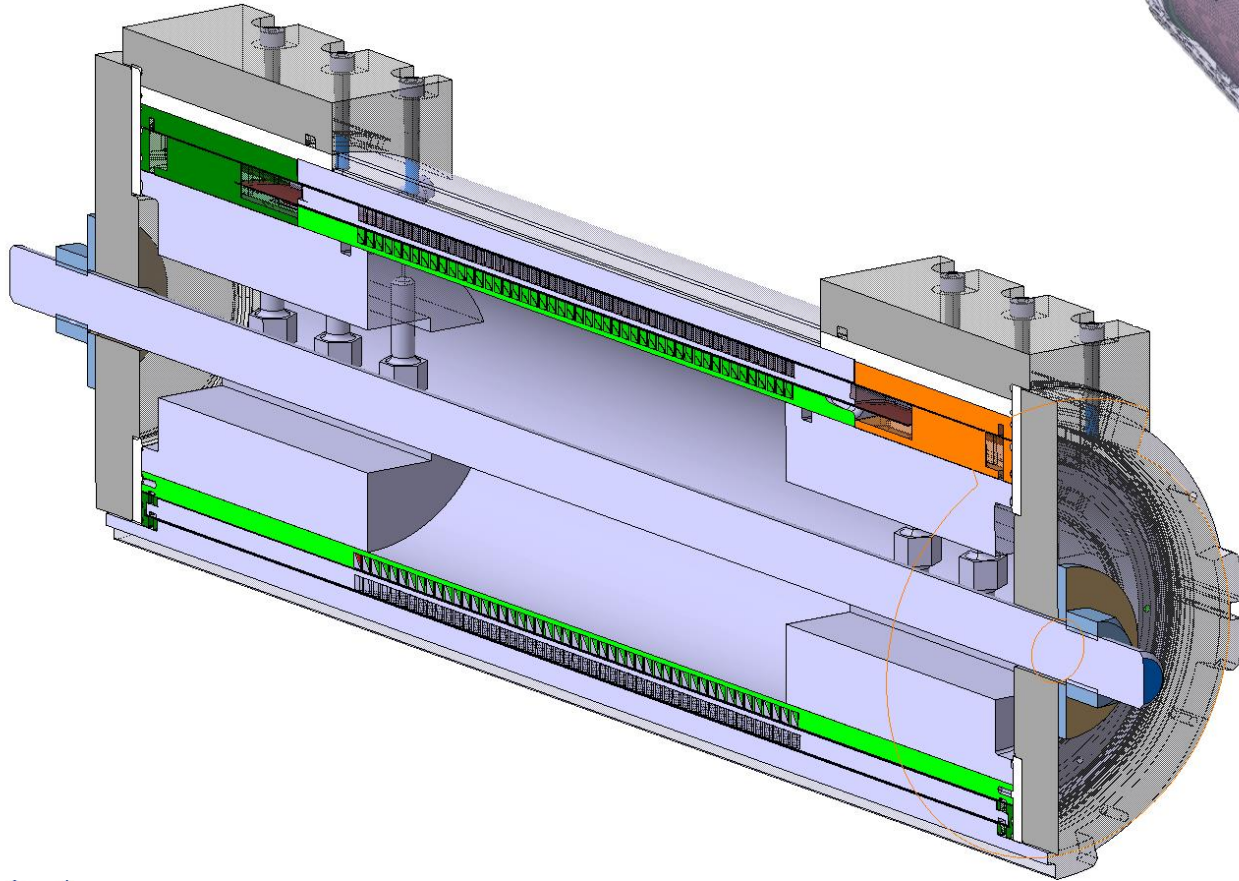
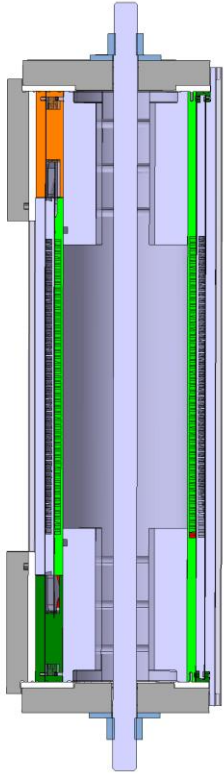
Beam simulation heaters cover inner and outer former, over low field volume where beam heating will be distributed. Only mounted on models



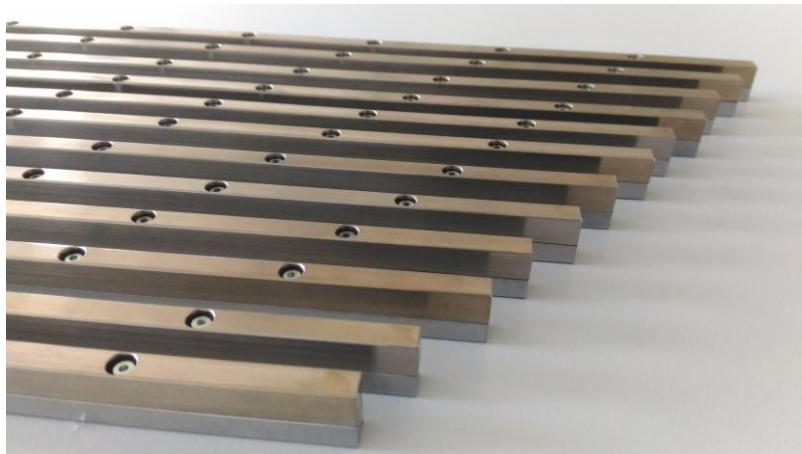
# Ongoing development / improvements



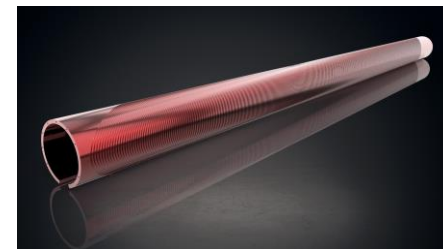
# Impregnation tooling



## 2.2m prototype components arriving



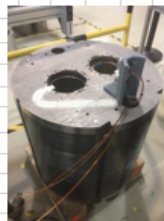
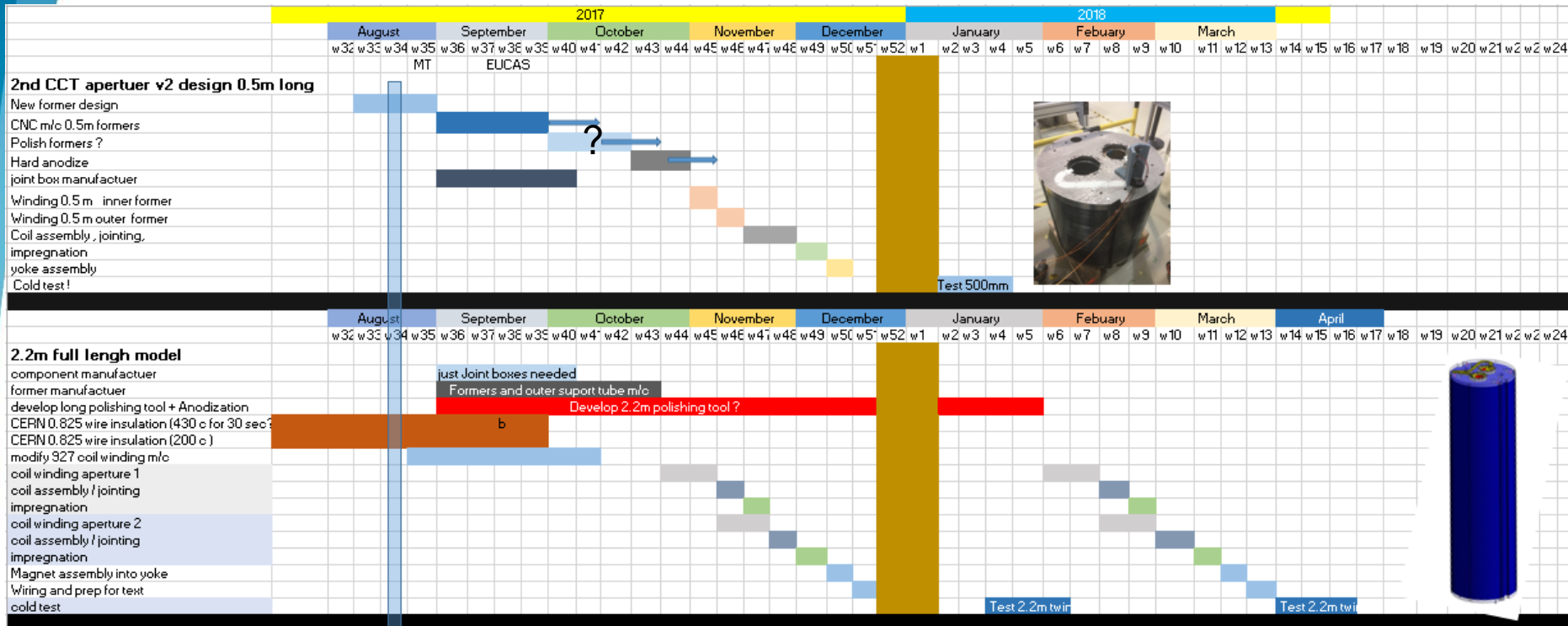
All other components are CERN



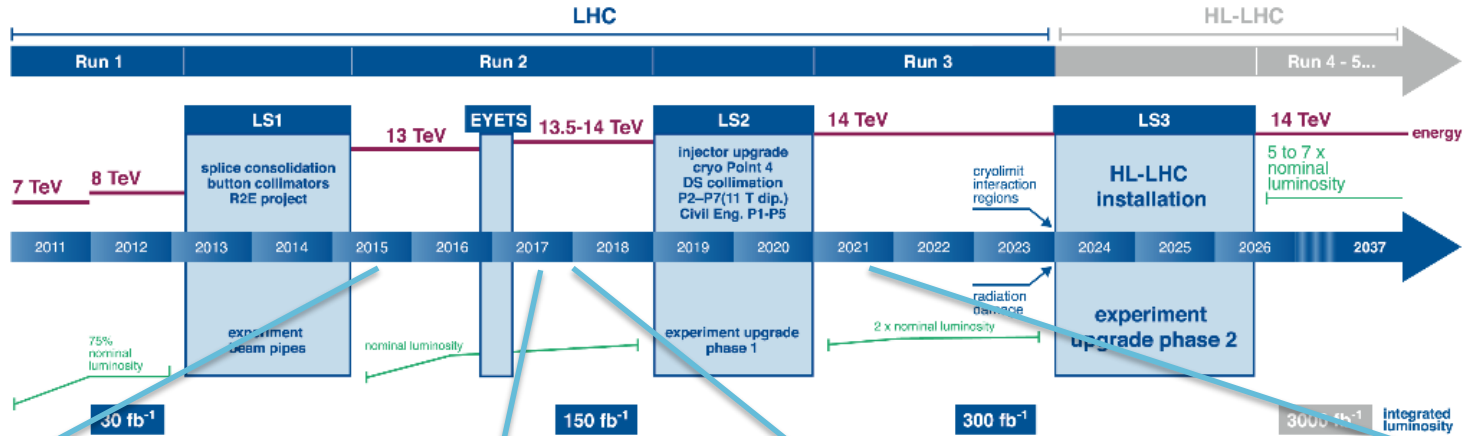
We have just finished the new long coil design: formers , outer support tube and joint boxes and hope to order soon



# Model planning

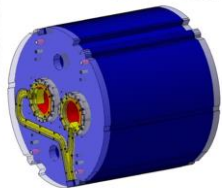


# LHC / HL-LHC Plan

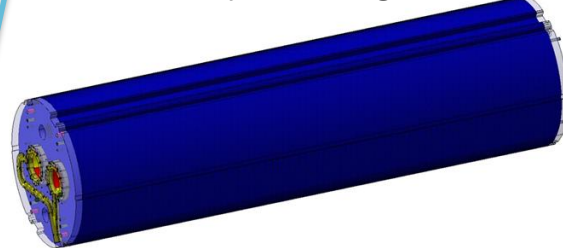


LHC/ HL-LHC Plan (last update 22.02.2016)

0.5m model tested  
Summer 2017



Full size prototype  
Assembly during 2018



18 - 20 off twin aperture  
magnets production  
delivery ~ 2020



***Thank you for your attention***



<https://www.researchgate.net/project/LHC-hi-Lumi-orbit-corrector-5Tm-CCT>