

# AC Loss and inter-strand resistance in Impregnated *ReBCO* Roebel cables

P. Gao, M. Dhalle, H. Norder, B. van Nugteren, K. Yagotintsev, S. Wessel, A. Nijhuis  
*University of Twente, Faculty of Science & Technology, 7522 NB Enschede, The Netherlands*

A. Kario, S. Otten, W. Goldacker  
*KIT, ITP, Karlsruhe, Germany*

L. Bottura, J. van Nugteren, G. Kirby, S. Tavares, S. Clement, L. Rossi and H. H.J. ten Kate  
*CERN, Geneva, Switzerland*



# Outline of this presentation:

1.

**Motivation**

2.

Introduction

3.

Inter-strand resistance of impregnated Roebel cable

4.

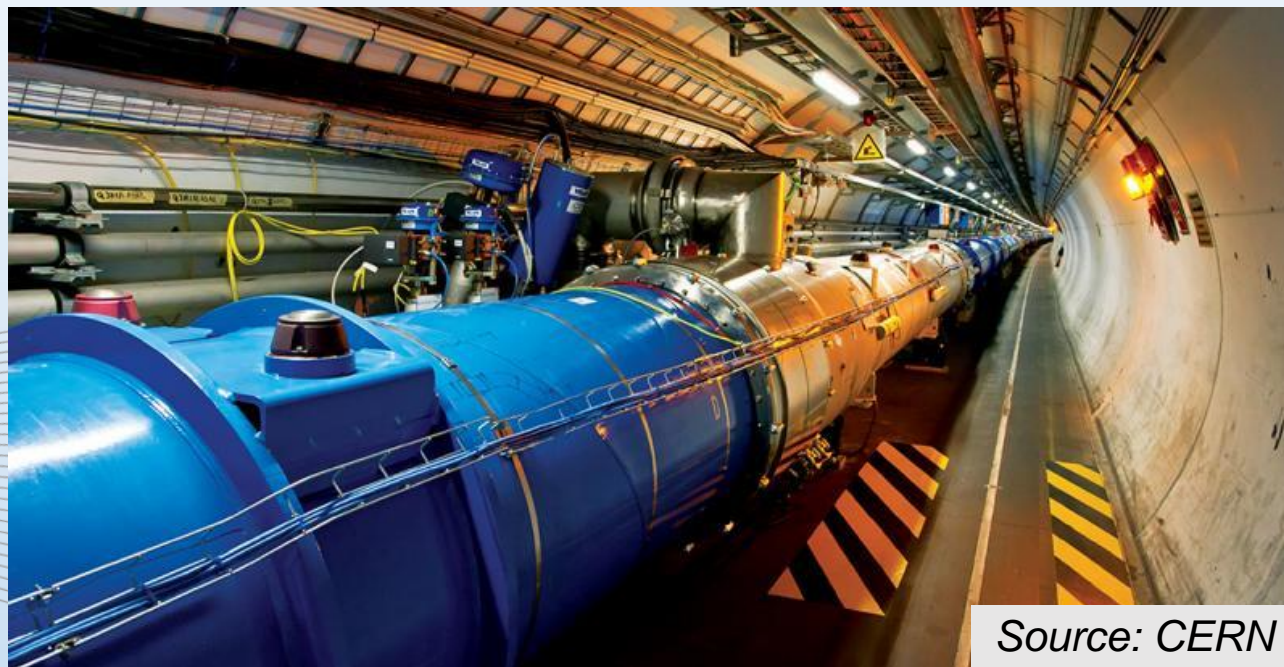
AC losses of impregnated Roebel cable

5.

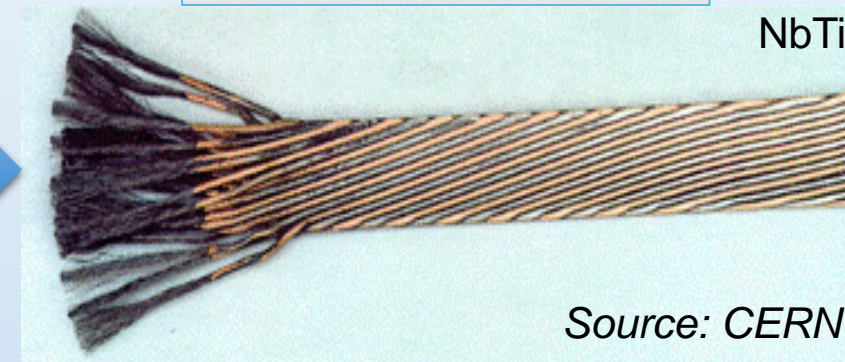
Conclusions



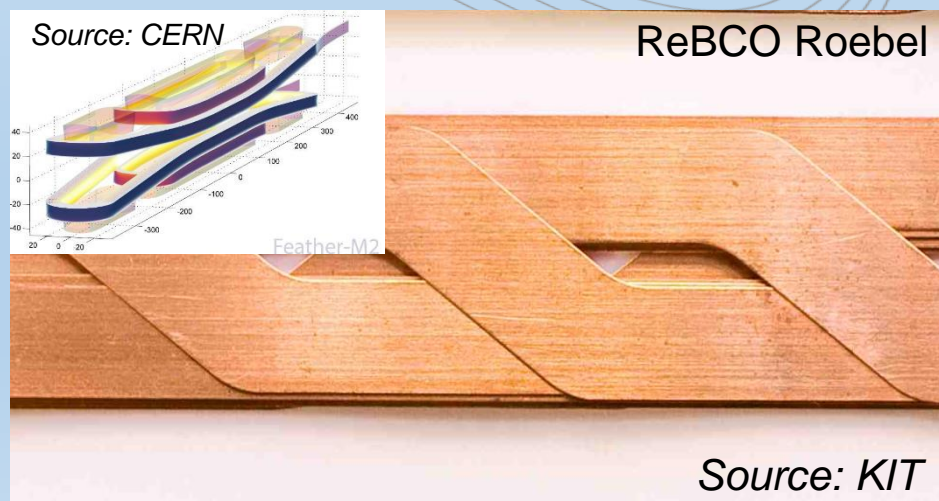
# 1. Motivation



**LHC 8.3T**

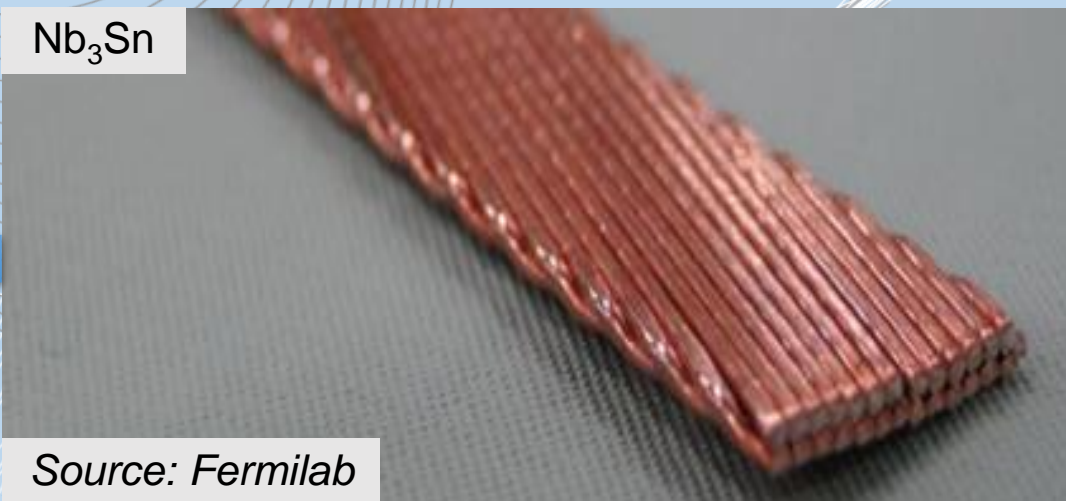


**EuCARD-2  $\geq 20$ T**



**HL-LHC 11T**

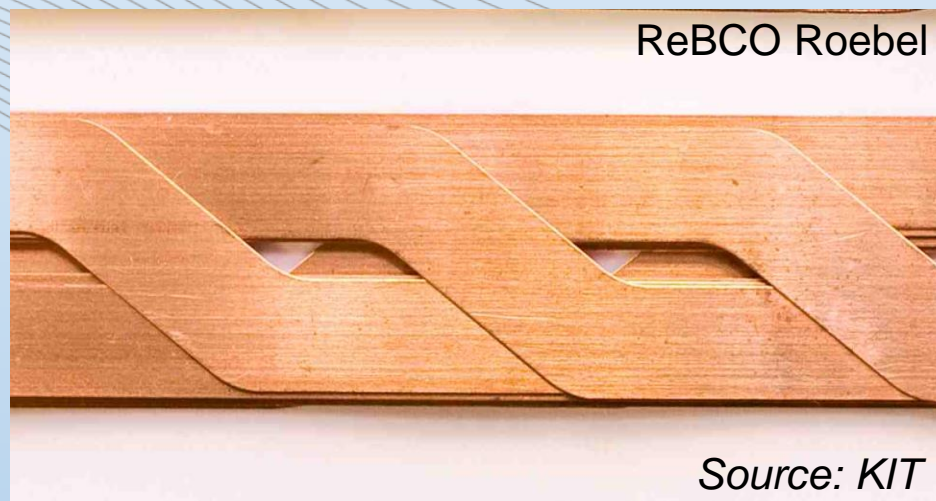
**FCC-EuroCirCol 16T**



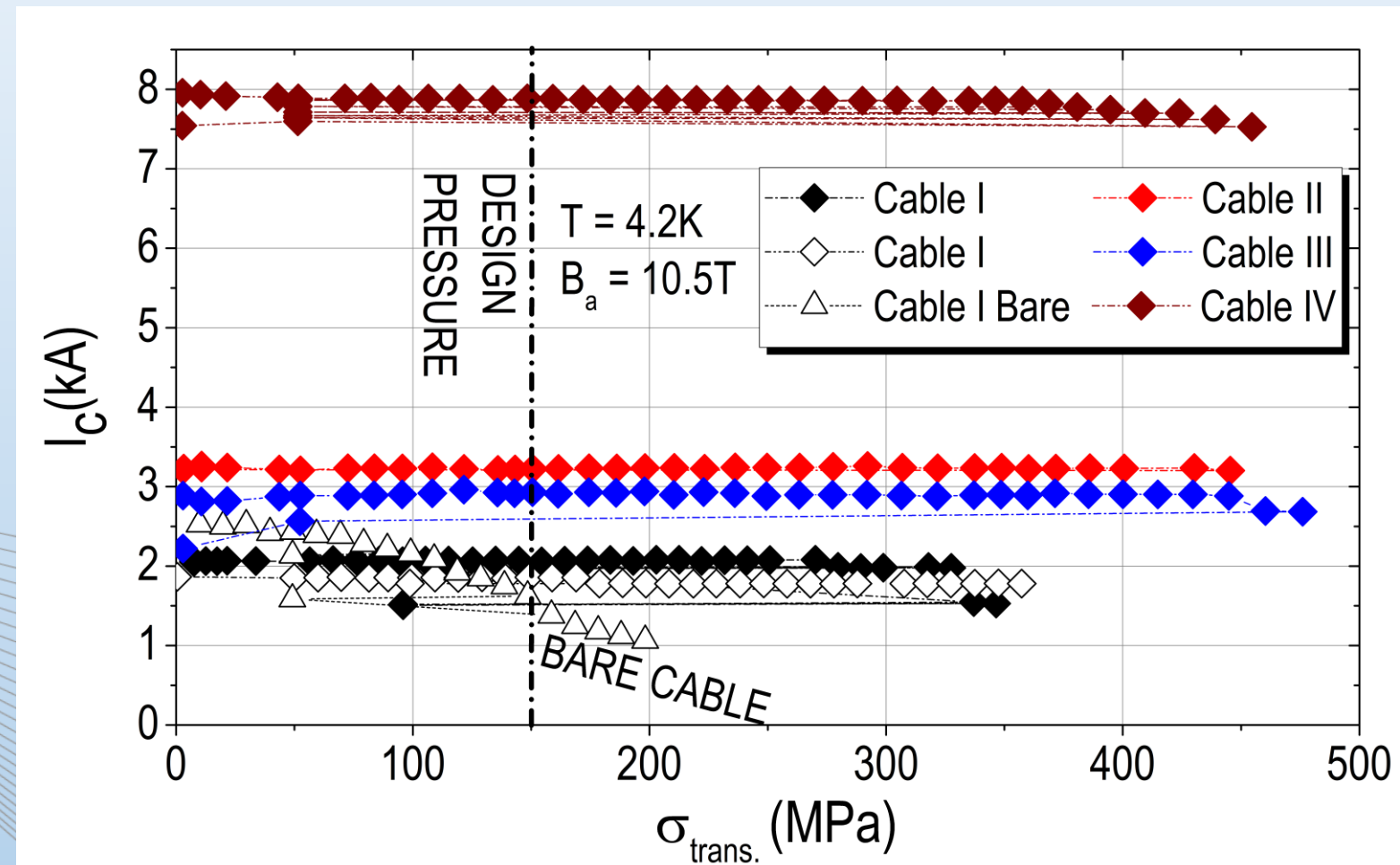


# 1. Motivation

**EuCARD-2  $\geq 20\text{T}$**



## Transverse pressure tolerance?



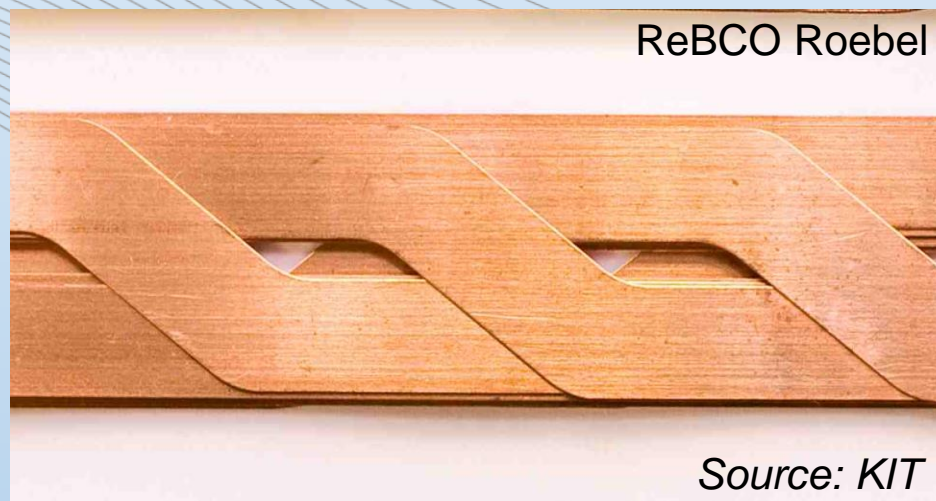
**Impregnation  $\Rightarrow \sigma_{\text{trans}} > 400\text{MPa}$  !**

Source: *P. Gao, M. Dhallé et.al. "The effect of tape layout and impregnation method on transverse pressure dependence of critical current in REBCO Roebel cables", to be published*

# 1. Motivation

## Inter-strand resistance?

**EuCARD-2  $\geq 20\text{T}$**



**Current redistribution**

**Field Quality**

**$R_c ?$**

**AC loss**

**Stability**



1.

Motivation

2.

Introduction

3.

Inter-strand resistance of impregnated Roebel cable

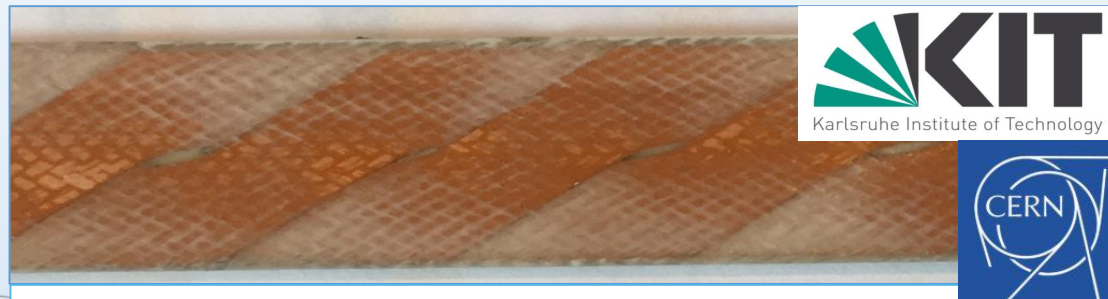
4.

AC losses of impregnated Roebel cable

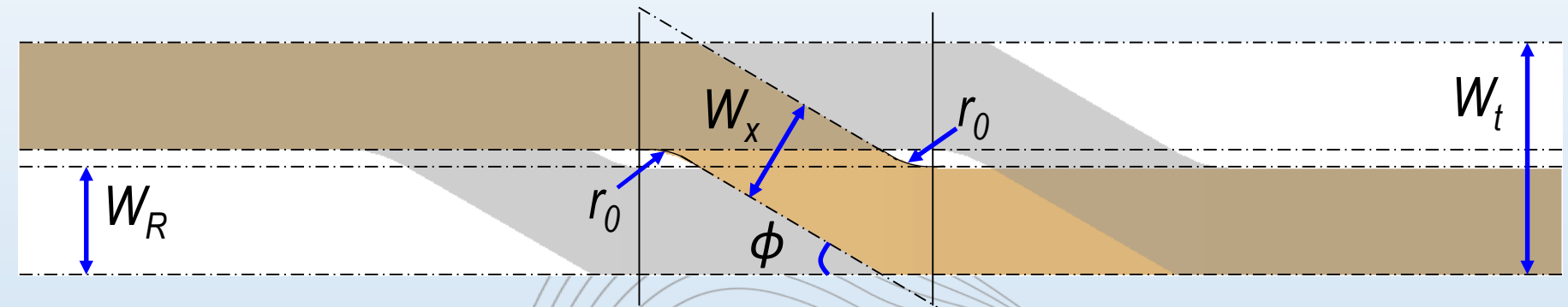
5.

Conclusions

## 2. Introduction : samples



CABLE I (KIT),  
impregnated with CTD101G, filled with  
alumina powder, 5MPa (CERN)



CABLE II (KIT),  
impregnated with CTD101K 5MPa (CERN)



Symbol	Value	Description
$N_s$	15	Number of strands
$d_s$	0.1 mm	Strand thickness
$d_c$	0.8 mm	Cable total thickness
$d_i$	0.1 mm	Insulation thickness
$W_r$	5.5 mm	Strand width
$W_t$	12.0 mm	Cable width
$W_x$	5.5 mm	Cross over width
$W_c$	1.0 mm	Channel width
$\phi$	30°	Cross over angle
$L_{tn}$	226 mm	Transposition pitch
$r_i$	6.0 mm	Inner radius
$r_o$	6.0 mm	Outer radius



# Outline of this presentation:

1.

Motivation

2.

Introduction

3.

**Inter-strand resistance of impregnated Roebel cable**

4.

AC losses of impregnated Roebel cable

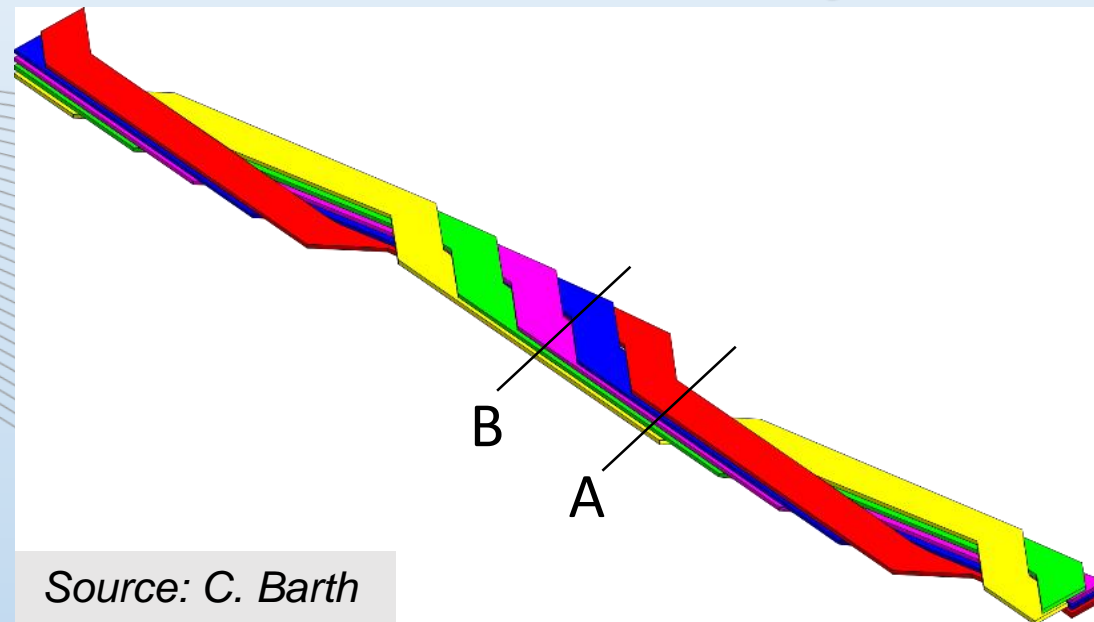
5.

Conclusions

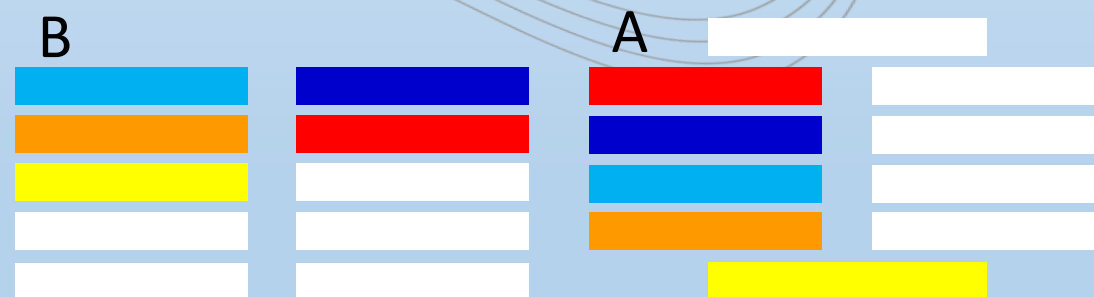
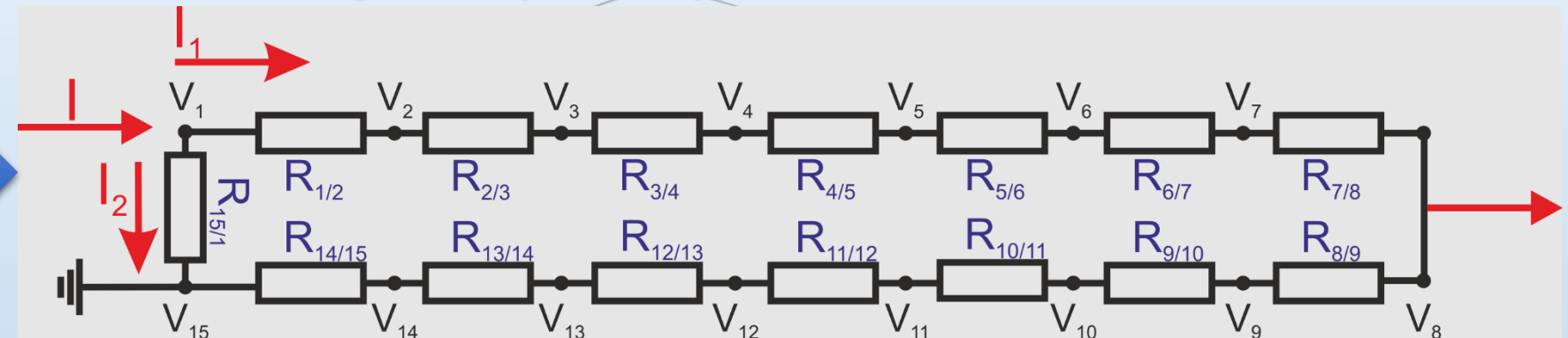


### 3. $R_c$ of impregnated Roebel cable

## Schematic of strands layout

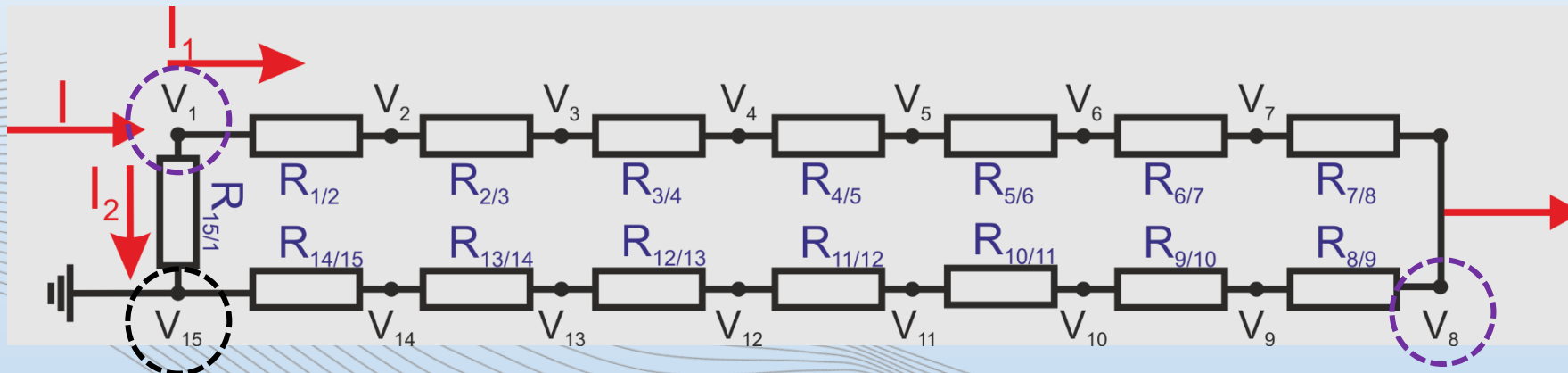


## Circuit diagram (15str.)



- 2 neighbors per stand
- 15 soldered contact taps
- $V_1 \sim V_{15}$ : equipotential (S.C. layer)
- $R_{i/j}$ : contact resistance between neighboring stands i & j

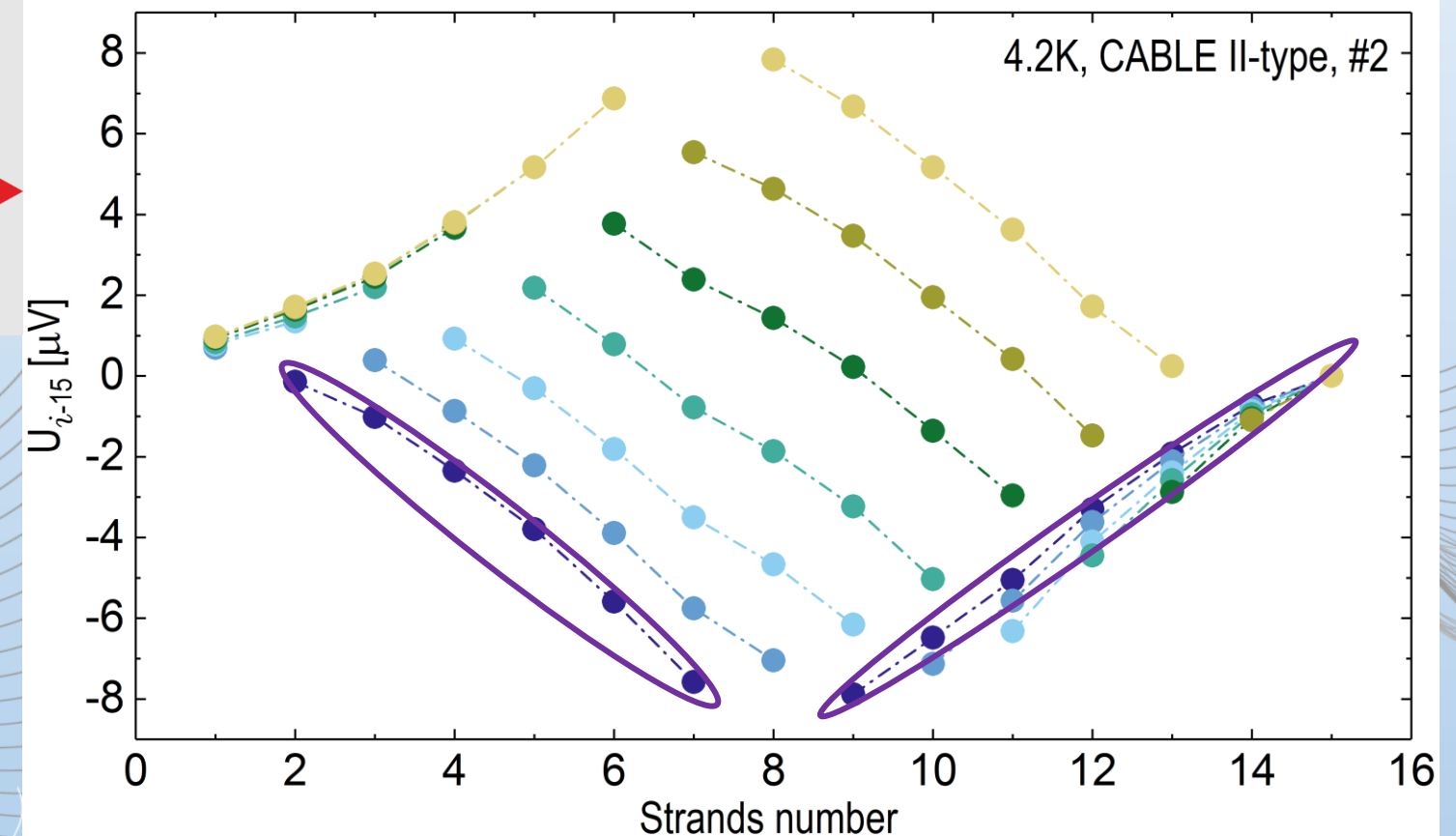
# 3. $R_c$ of impregnated Roebel cable



## Method:

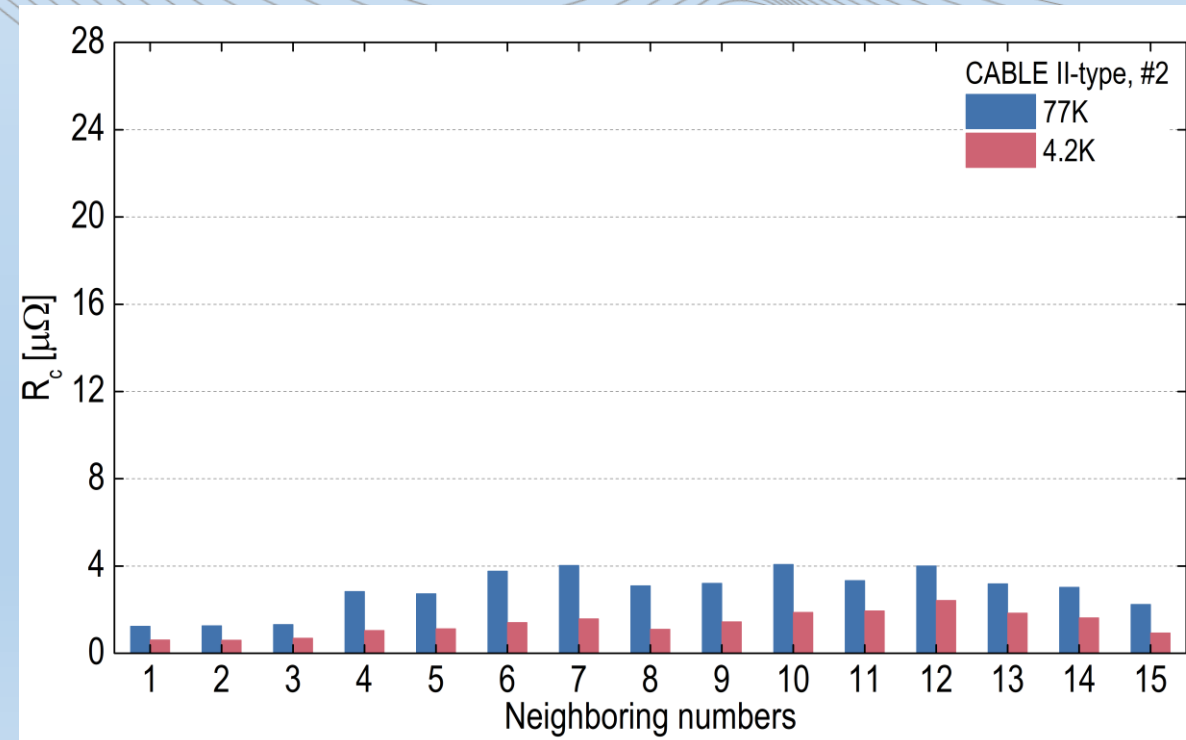
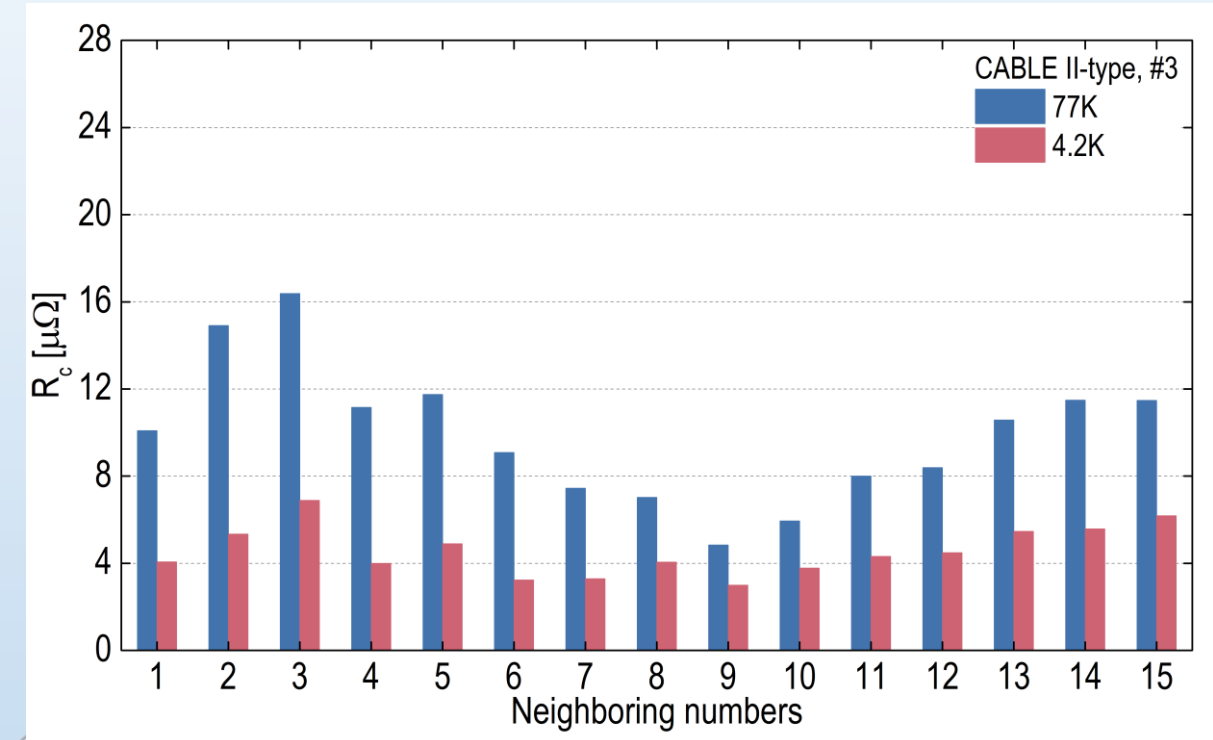
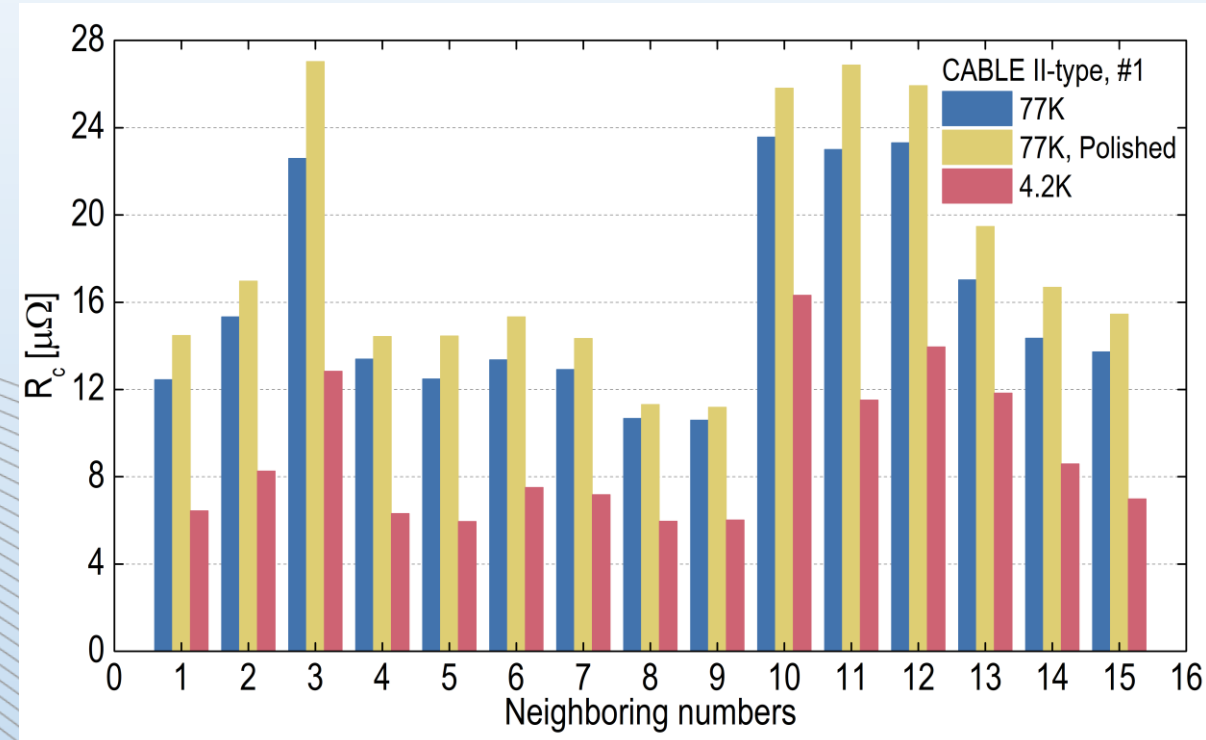
- 2 taps as current lead (e.g. 1 and 8)
- $V_{15}$  is grounded, as a ref. volt. potential
- $U_{i/15}$  are measured (e.g. purple data)
- cycle current lead position

$R_{i/j}$  can then be calculated by solving system of equations





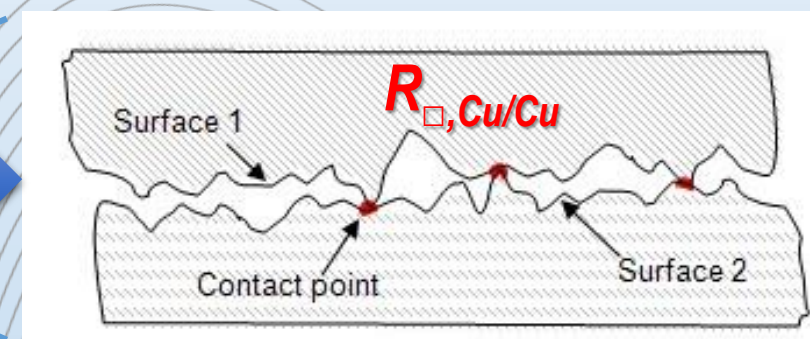
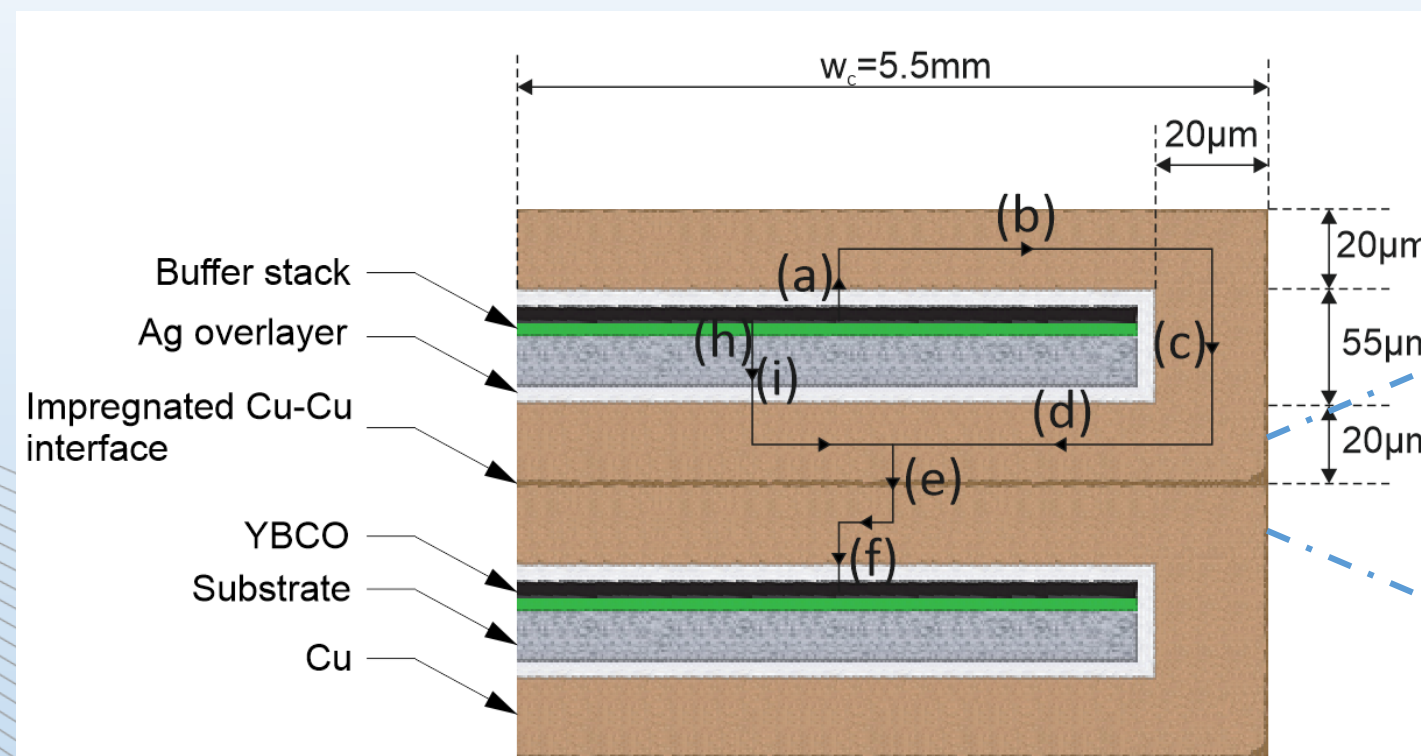
# 3. $R_c$ of impregnated Roebel cables



**Avg.  $R_c$  between neighbors**

$T$	# 1 $R_c(\mu\Omega)$	# 2 $R_c(\mu\Omega)$	# 3 $R_c(\mu\Omega)$
77K	15.9	2.9	9.9
77K polished	18.0	-	-
<b>4.2K</b>	<b>9.1</b>	<b>1.4</b>	<b>4.6</b>
$R_c(77K)/R_c(4.2K)$	1.8 ~ 2.0	2.1	2.2

# 3. $R_c$ of impregnated Roebel cable



$$R = \frac{\rho l}{A}$$

$$R = \frac{R_{\square}}{A}$$

Current path: ReBCO  $\rightarrow$  Ag  $\rightarrow$  Cu(b)  $\rightarrow$  Cu(c)  $\rightarrow$  **Cu(d)  $\rightarrow$  Cu-Cu(e)**  $\rightarrow$  Cu(f)  $\rightarrow$  Ag  $\rightarrow$  ReBCO

$T$	$R_{c, S.C./Ag} (\mu\Omega)$	$R_{c, S.C./Ag/Cu(b)} (\mu\Omega)$	$R_{c, Cu(c)} (\mu\Omega)$	$R_{c, Cu(d)+Cu-Cu(e)} (\mu\Omega)$	$R_{c, Cu(c)} (\mu\Omega)$	$R_{c, Cu(c)/Ag/S.C.} (\mu\Omega)$
77K	0.31~0.44	0.11~0.15	8.5E-2		6.5E-5	2.3E-3~4.7E-3
4.2K	1.6E-3~1.6E-2	4.4E-3~4.4E-2	3.6E-2		2.8E-5	9.3E-5~9.3E-4

Ref.: **C. Zhou**, "Intra wire resistance and strain affecting the transport properties of  $Nb_3Sn$  strands in Cable-in-Conduit Conductors", PhD dissertation, University of Twente, 2014

**T. Holúbek, M. Dhallé and P. Kováč**, "Current transfer in  $MgB_2$  wires with different sheath materials", University of Twente, SUST, 20, 2007

Assuming

$$R_{\square, Cu/Cu} (77K) \sim 10 \text{ to } 20 \text{ n}\Omega \cdot \text{m}^2$$

$$R_{\square, Cu/Cu} (4.2K) \sim 0.5 \text{ to } 10 \text{ n}\Omega \cdot \text{m}^2$$



# Outline of this presentation:

1.

Motivation

2.

Introduction

3.

Inter-strand resistance of impregnated Roebel cable

4.

**AC losses of impregnated Roebel cable**

5.

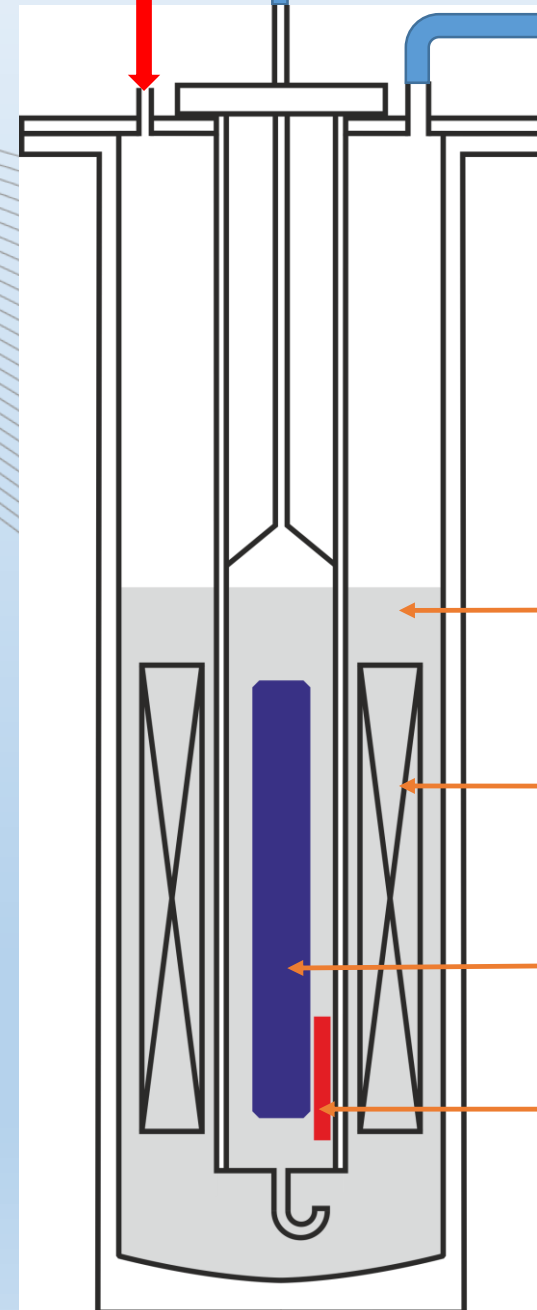
Conclusions

# 4. AC losses : Instrumentation

From He flow meter

to He flow meter

to He cycling system



Liquid He bath

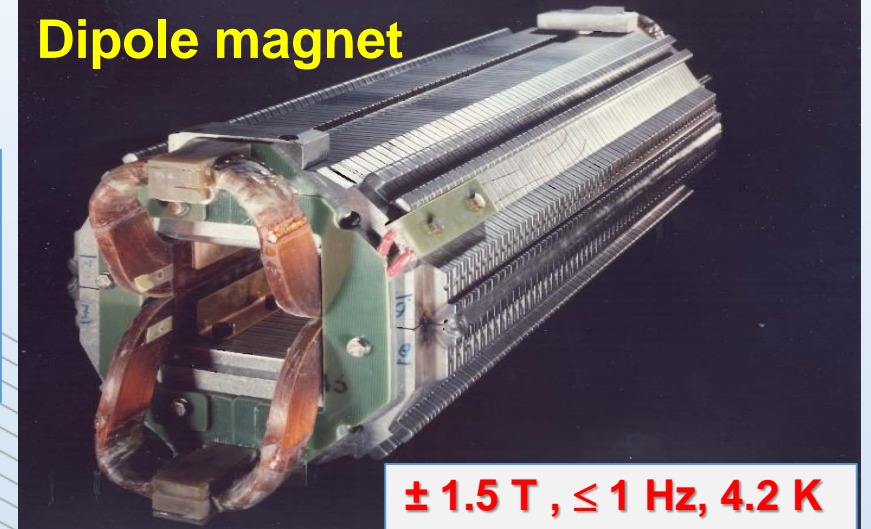
Superconducting dipole/solenoidal magnet

Sample chamber

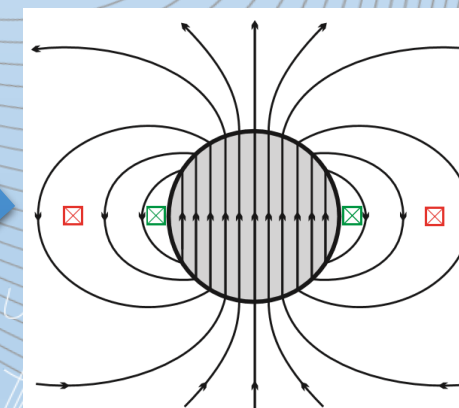
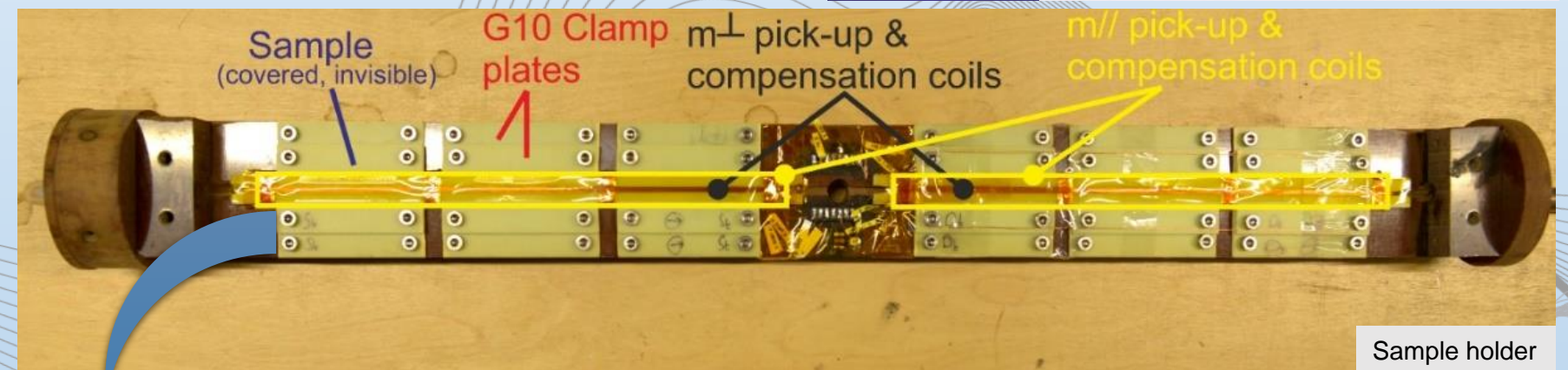
Heater for calibration

AC loss measured by gas flow **calorimetry** and **magnetisation** methods.

**Dipole magnet**

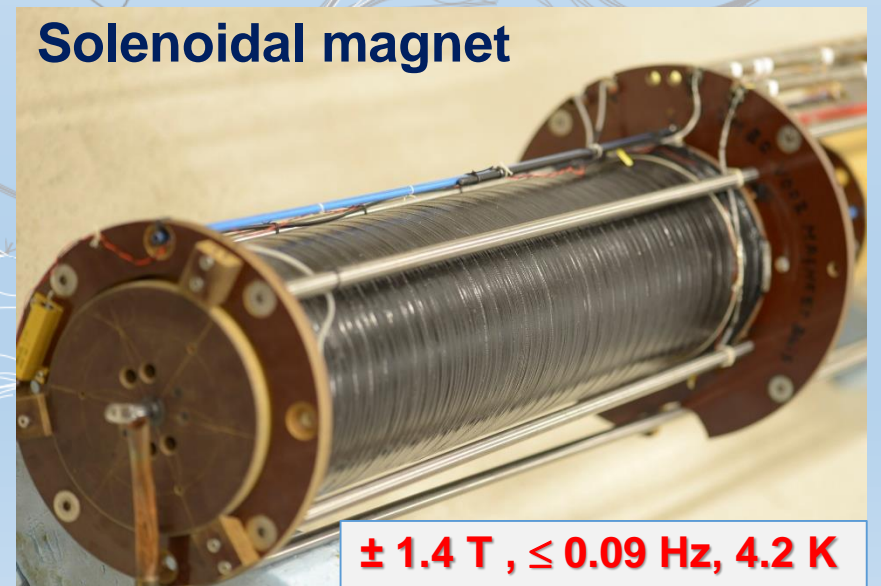


$\pm 1.5 \text{ T}, \leq 1 \text{ Hz}, 4.2 \text{ K}$



Filling factor effect

**Solenoidal magnet**

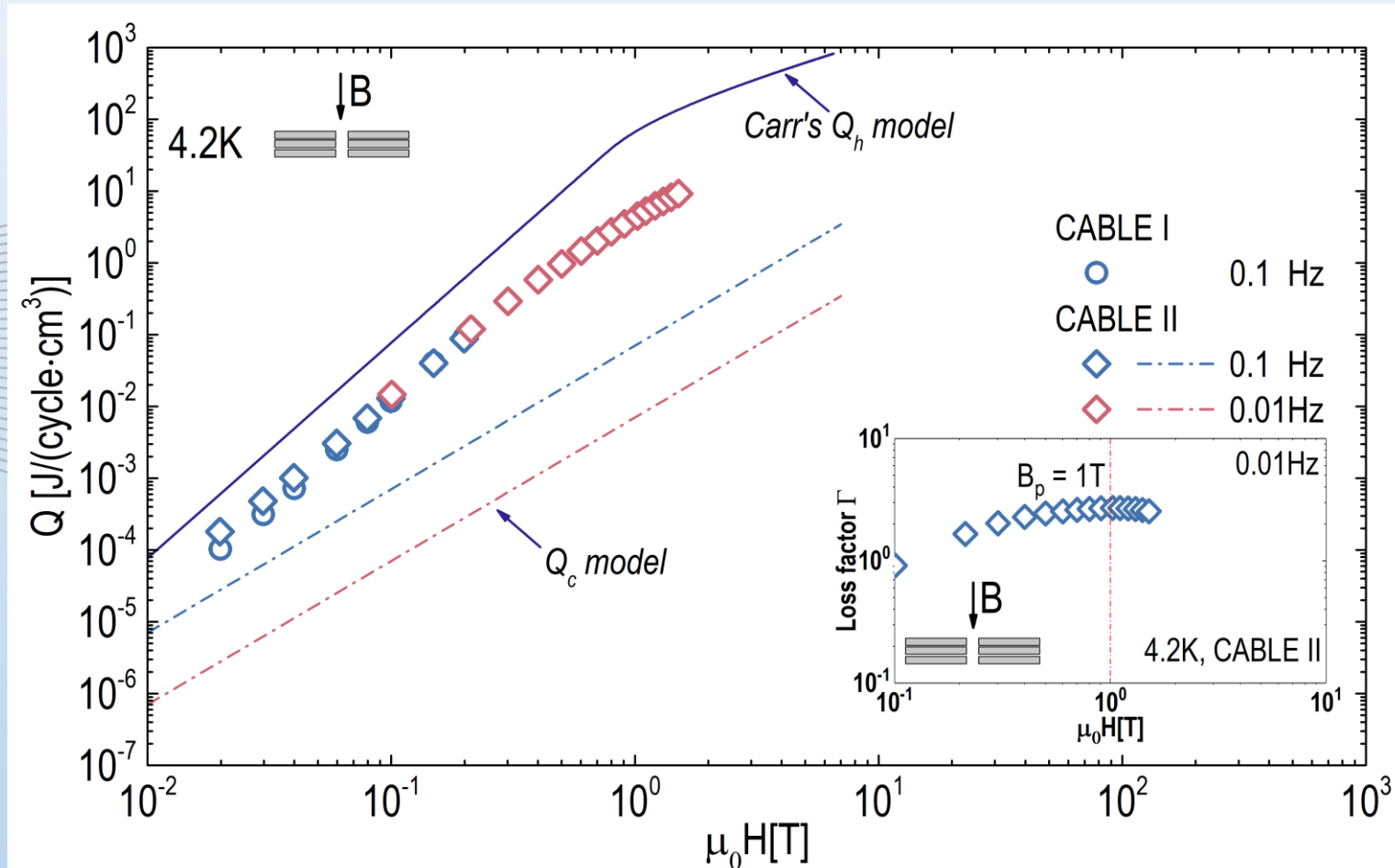


$\pm 1.4 \text{ T}, \leq 0.09 \text{ Hz}, 4.2 \text{ K}$

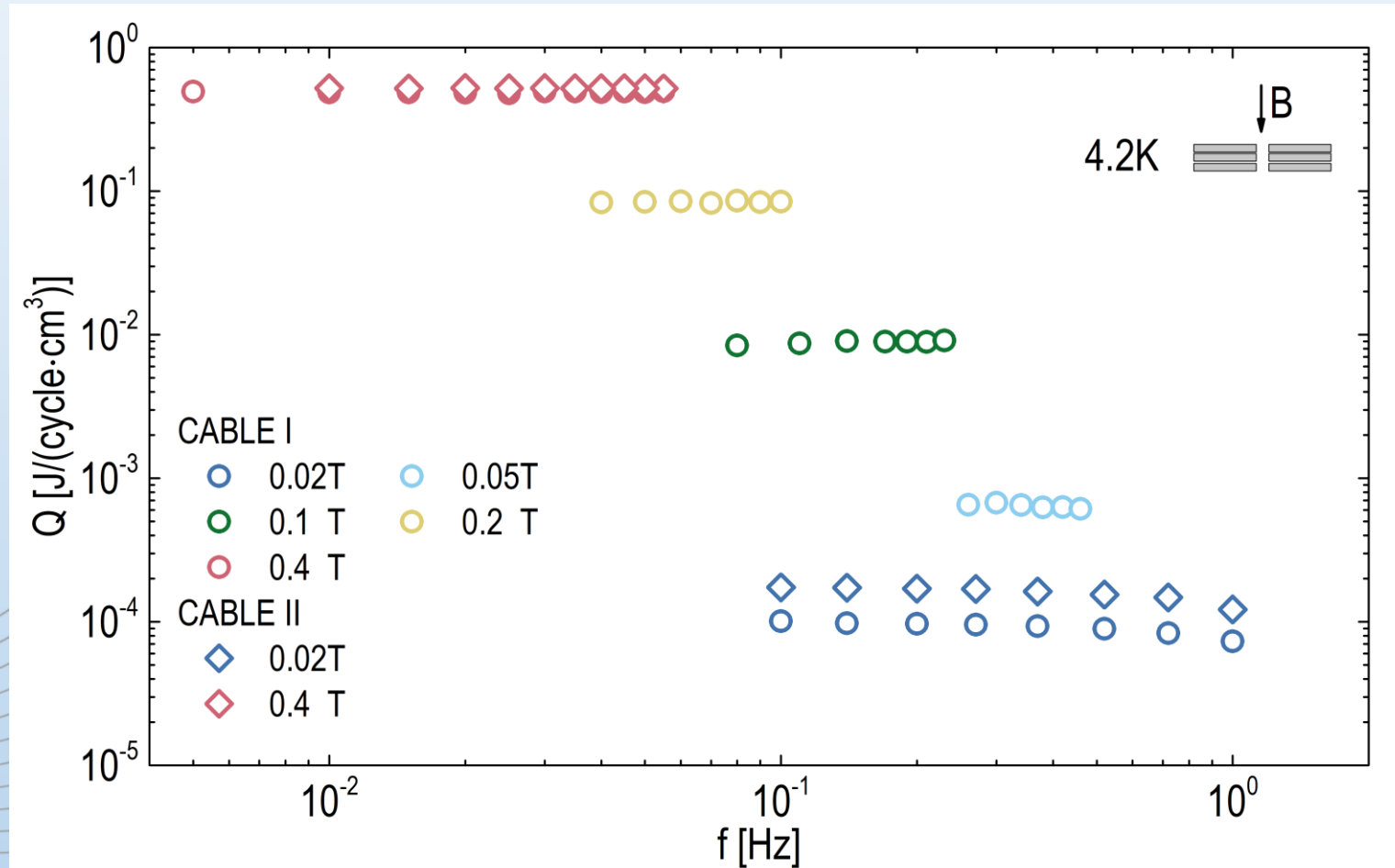


# 4. AC losses @ $B_{\perp}$ , 4.2K

## Amplitude dependence



## Frequency dependence



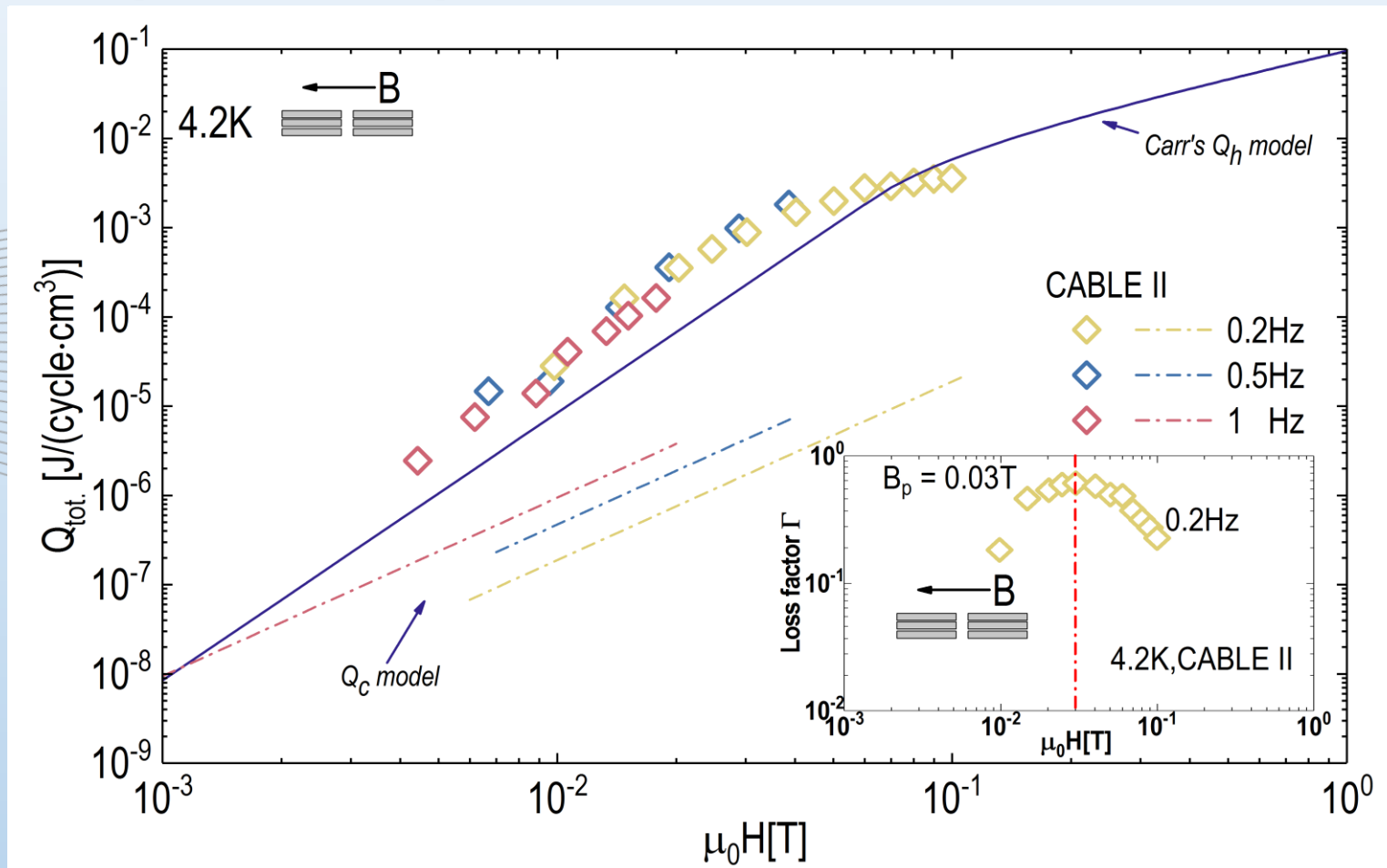
- AC losses are dominated by hysteresis
- No coupling losses are observed in exp. window
- Tested :  $B_{p\perp} \approx 1T$ ; Modelling:  $B_{p\perp} = 0.769T$

➔ Both in model prediction & experiment

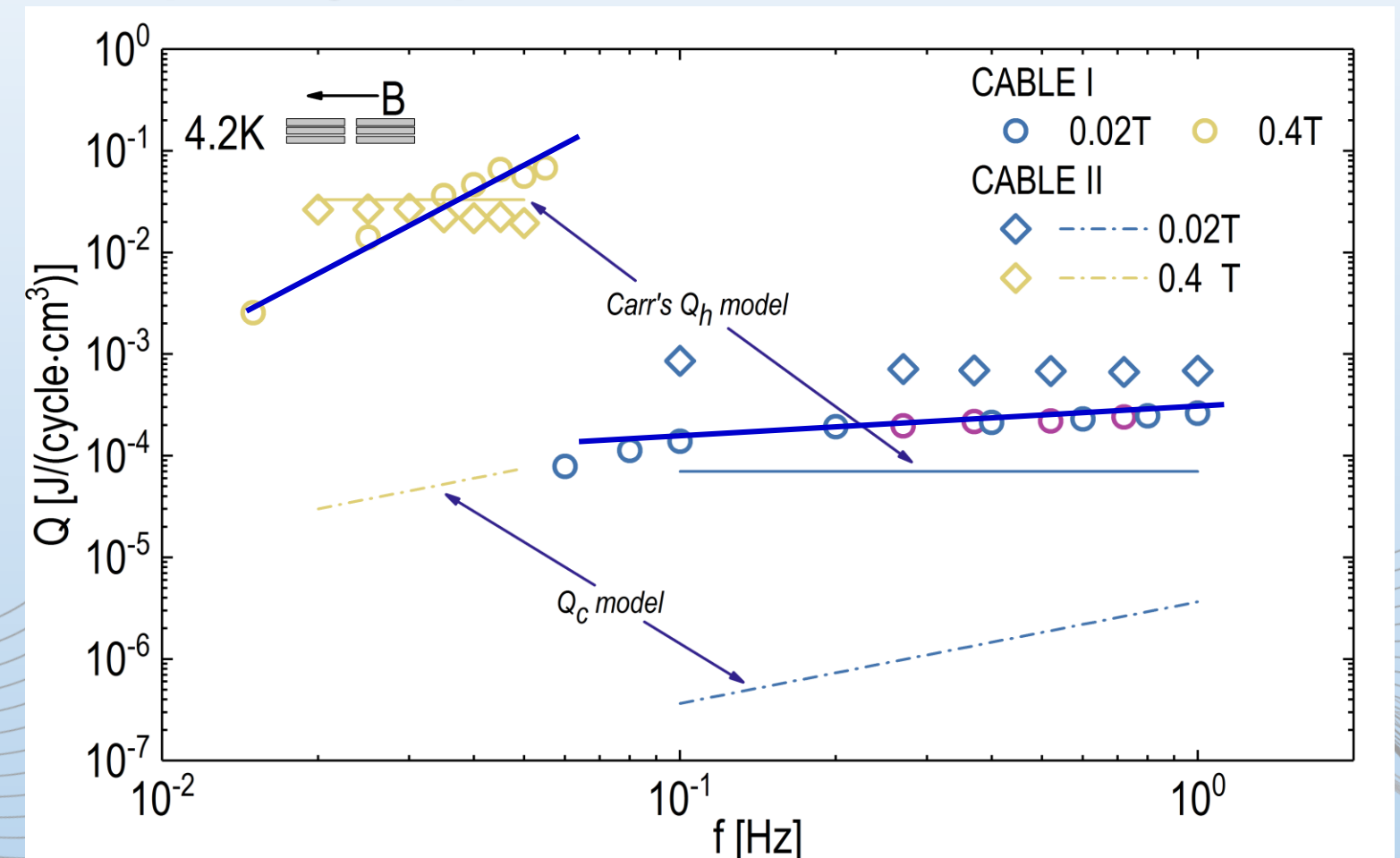
Carr's  $Q_h$  model, ref. : **W. J. Carr. Jr.** "AC Loss and Macroscopic Theory of Superconductors", CRC Press, 5 Jul 2001, USA

# 4. AC losses @ **B**<sub>//</sub>, 4.2K

## Amplitude dependence



## Frequency dependence



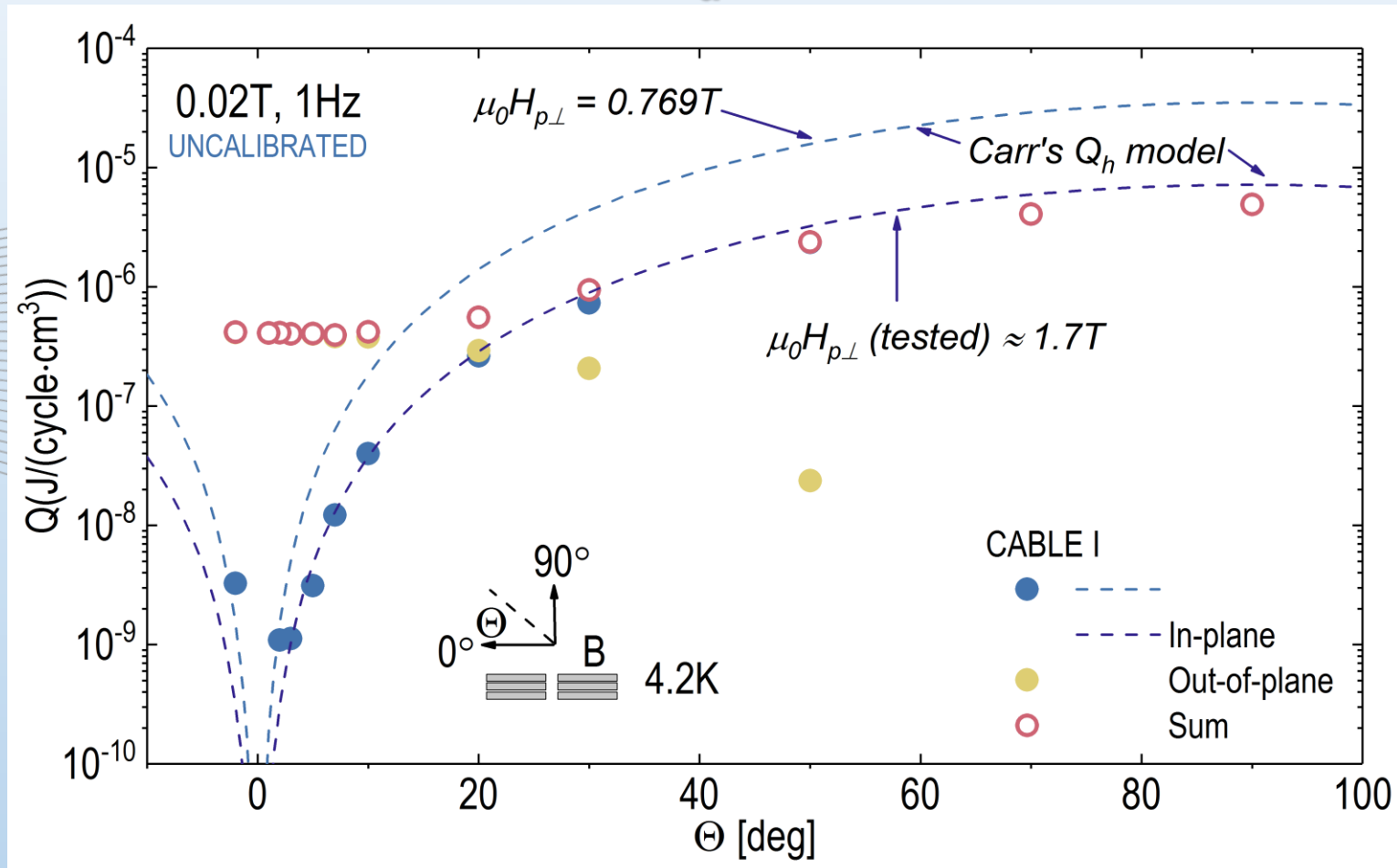
### CABLE II

- AC losses are dominated by hysteresis
- No coupling losses are observed in exp. window
- Tested:  $B_{p//} \approx 0.03$  T; Modelling  $B_{p//} = 0.06$  T
- $Q_c$  is much lower than measured  $Q_h$  in exp. window, which is identical with modelling estimation



# 3. AC losses @ $B_a = \pm 0.02T(\theta)$ , $f=1\text{Hz}$ , $4.2\text{K}$

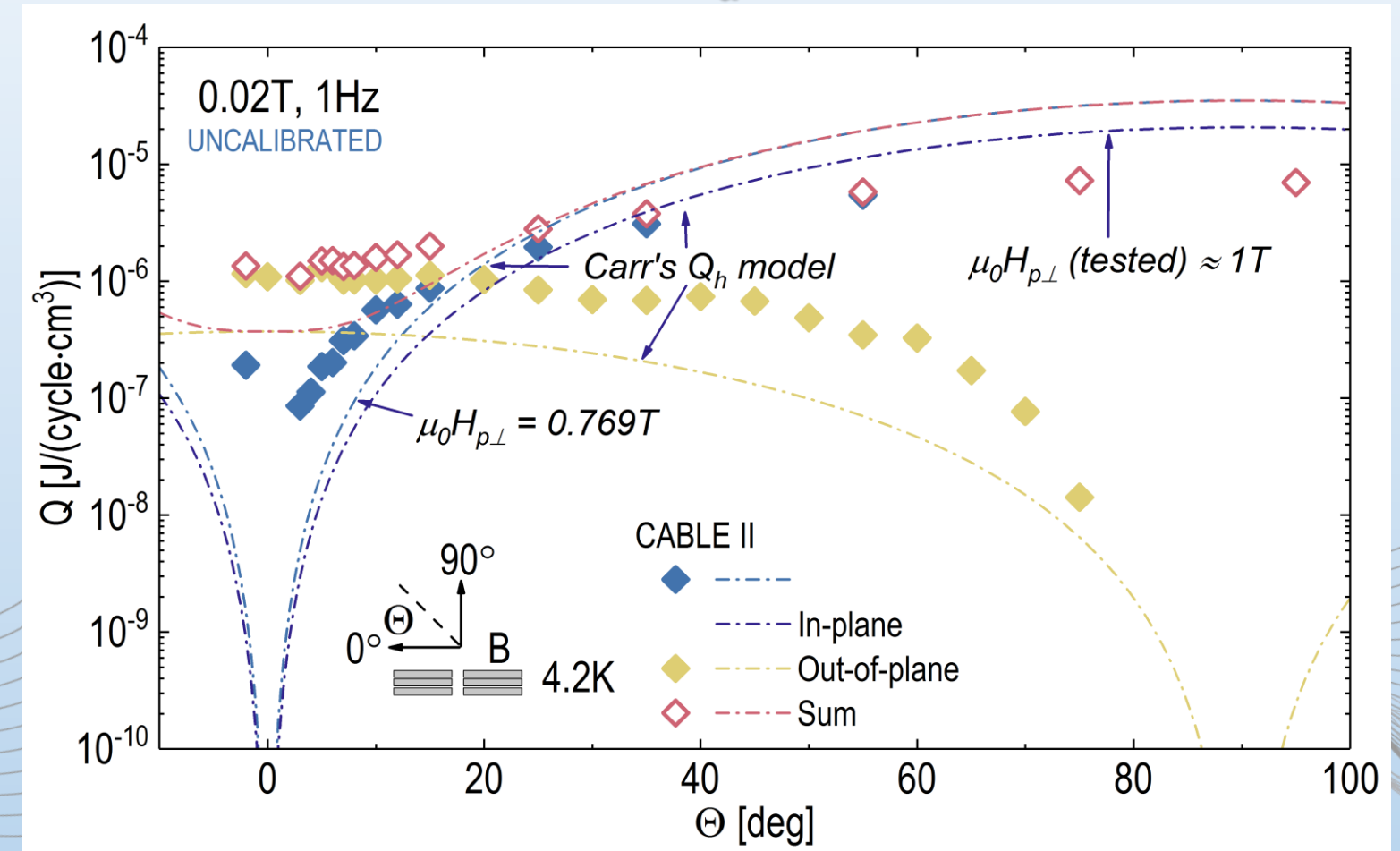
## CABLE I: AC losses- $B_a$ angle $\theta$



- The predominant role of AC losses: from **Coupling** to **Hysteresis** with the **increase  $\theta(0^\circ \sim 90^\circ)$**
- $Q_h$  model fits well with data when use  **$\mu_0 H_{p\perp} \approx 1.7T$**

Tested  $\mu_0 H_{p\perp} \approx 1.7T$ , ref. : J. Pelegrin, I. Falorio, E. A. Young, Y. Yang et.al. University of Southampton.

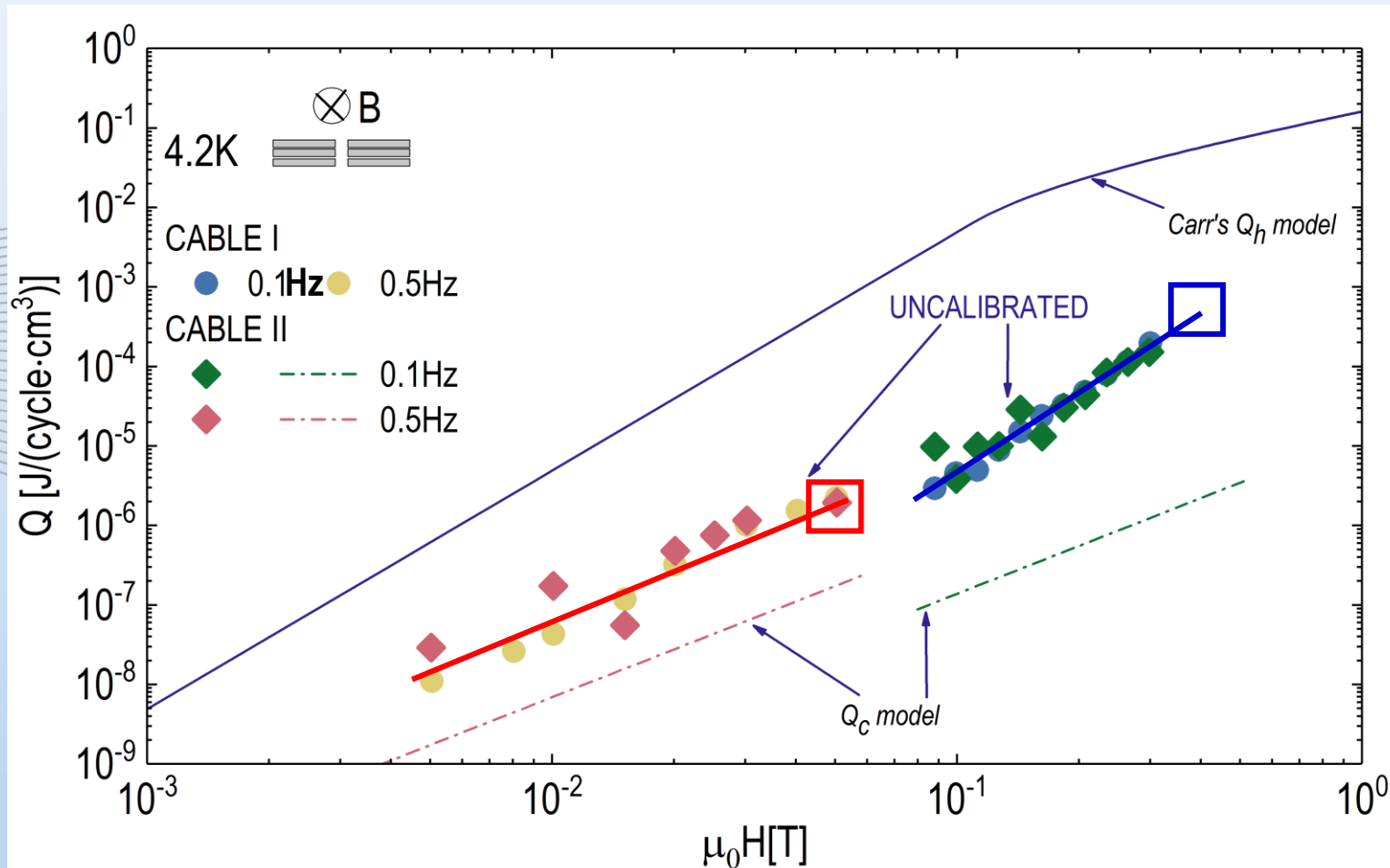
## CABLE II: AC losses- $B_a$ angle $\theta$



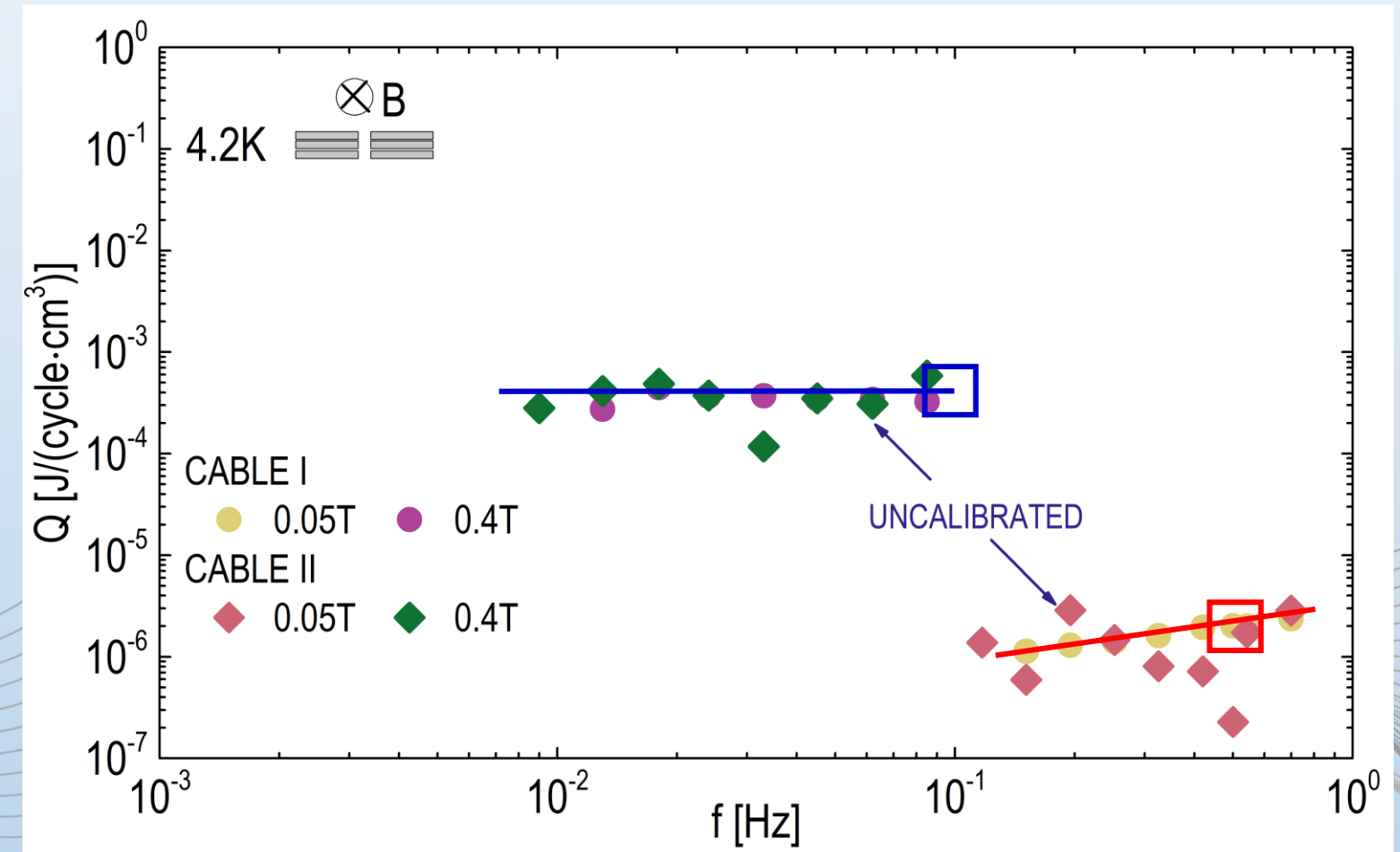
- AC losses are dominated by hysteresis
- $Q_h$  model doesn't fit well with exp. data, but the observed & predicted trends do correspond

# 4. AC loss @ $B_{\uparrow}$ , 4.2K

## Amplitude dependence



## Frequency dependence



- Coupling losses are observed in the exp. window  $5 \text{ mT} \leq \mu_0 H_0 \leq 50 \text{ mT}$
- Hysteresis losses are observed in the exp. window  $80 \text{ mT} \leq \mu_0 H_0 \leq 0.4 \text{ T}$
- Modelling:  $B_{p\uparrow} \approx 0.11 \text{ T}$



# Outline of this presentation:

1.

Motivation

2.

Introduction

3.

Inter-strand resistance of impregnated Roebel cable

4.

AC losses of impregnated Roebel cable

5.

Conclusions

# 5. Summary

- $R_c$  of Roebel cables ( $L_{tp}=226\text{mm}$ ) at **4.2 K** is around **1.5 – 10  $\mu\Omega$** , at **77 K** is about **3 – 20  $\mu\Omega$** , with about 30% variation within a cable and up to a factor 6 variation from cable-to-cable
- Coupling losses **can be predicted by** using the measured  $R_c$  values
- The inter-strand resistance is dominated by the contact resistance of the **Cu-Cu interface**
- AC losses are dominated by **hysteresis @  $B_{\perp}$** , at 4.2 K,  $B_{p\perp} \approx 1 \text{ T} \sim 1.7 \text{ T}$
- **Coupling** losses **might be** observed **@  $B_{\parallel}$**  and  **$B_{\uparrow}$** , at 4.2 K, depending on impregnation details;  $B_{p\parallel} \approx 0.03 \text{ T}$
- AC losses @ inclined field mostly ( $\theta \geq \sim 15^\circ$ ) **dominated** by the **perpendicular** field component
- Analytical models show same trends as measured data, a better fit probably requires numerical modelling



UNIVERSITY  
OF TWENTE,



Thanks for your attention