

# Quench propagation in MgB<sub>2</sub> Rutherford cables

A Cubero<sup>1</sup>, E Martínez<sup>1</sup>, R Navarro<sup>1</sup>, P Kováčč<sup>2</sup> and L. Kopera<sup>2</sup>

<sup>1</sup>Instituto de Ciencia de Materiales de Aragón (ICMA), CSIC – Universidad de Zaragoza, Zaragoza, Spain

<sup>2</sup>Institute of Electrical Engineering, Slovak Academy of Sciences, Bratislava, Slovakia

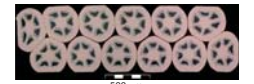
## Introduction

Rutherford cables offer several advantages over single conductors for different foreseen applications, since they are more flexible and may achieve a reduction of the AC losses by using appropriate transposition length and inter-strand electrical resistance. Furthermore, the optimization of these cables should also achieve the required thermal stability.

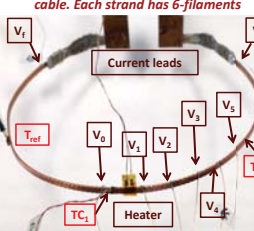
Two different configurations of 12-strand Rutherford cables have been analysed. The cables were assembled by IEE using a back-twist cabling machine with transposition length of 25 mm and have rectangular cross-section with final dimensions of 2.7 mm width and 0.7 mm thickness. The strands are 390 μm-diameter wires from HyperTech Research, Inc. and have Cu or Cu10Ni sheath, and Nb barrier to minimise the chemical reaction between the precursor powders and the sheath during the *in situ* formation of the MgB<sub>2</sub> phase.

Quench propagation has been measured and analysed in self-field conditions. These experiments were performed in vacuum and cooled by thermal conduction using a cryocooler.

## Case 1: Cu-sheathed wire



500 μm  
Cross-section of 12-strand Rutherford cable. Each strand has 6-filaments

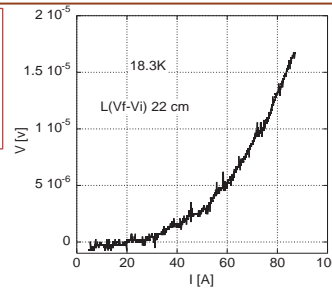


Heat pulses of variable duration were used to trigger the quench.

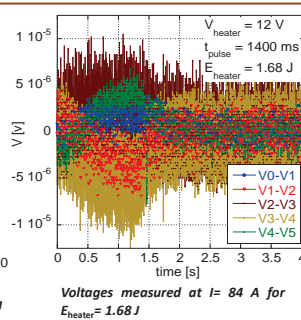
Heater: A strain gage of electric resistance,  $R=120 \Omega$ , was glued to the sample. Maximum heat power without damaging the heater is about 1.5 W.

### Sample prepared for quench analysis

- L: 25 cm
- Distance between  $V_i$  and  $V_j$  is 22 cm
- The heater was placed between  $V_0$  and  $V_1$  (1 cm separation).
- Additional voltage taps:  $V_2 \dots V_5$  (1.5 cm separation) to measure quench development and propagation.
- 2 Thermocouples (TC) were soldered.



I-V curve of the Cu-sheathed cable showing very low  $n$ -value ( $\sim 2.5$ ). Similar  $n$ -values were measured in the wires (before cable manufacturing).



For this test, sample is initially at  $T_{ref} = 18.3$  K.

Maximum temperatures:  $TC_1 \sim 25.3$  K and  $TC_2 \sim 21.4$  K.

➤ Voltages lower than 10 μV were measured for all energy pulses:  $E_{pulse} < MQE$ .

➤ Some voltages are positive and other negative. This reflects small I-V differences among strands.

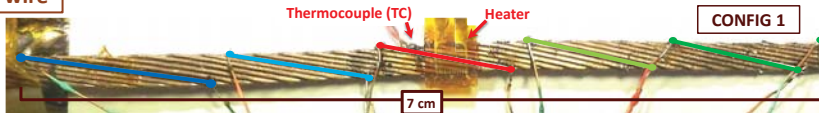
➤ Due to the very low  $n$ -values and the high thermal conductivity of the Cu-sheath, we were not able to induce a quench in this cable.

➤ In all cases, recovery after the heat pulse is observed.

## Case 2: Cu10Ni-sheathed wire



500 μm  
Cross-section of 12-strand Rutherford cable. Each strand is monocoire



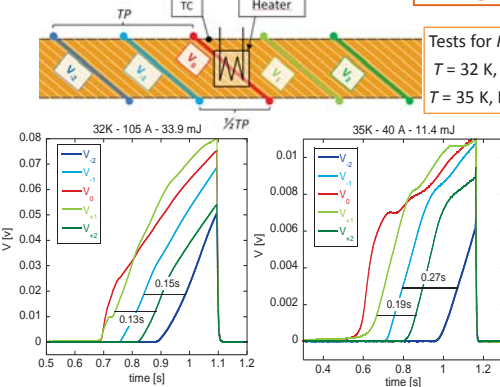
In **configuration 1** voltage taps were placed every half-twist pitch ( $TP/2$ ). Time delay between voltages  $V_{-1}$  and  $V_{-2}$  and  $V_1$  and  $V_2$  were used to estimate quench propagation velocities. In **configuration 2**, the separation between voltage taps was lower than  $TP/2$ .

I-V curve could not be measured for this cable. Instead, quench current,  $I_q(T)$ , was defined as the current that induces a quench without any external heat source (in self-field). It is always above local  $I_c$ .

Measurements were done at 32 K and 35 K.

Different voltage taps configurations were used.

### Configuration 1

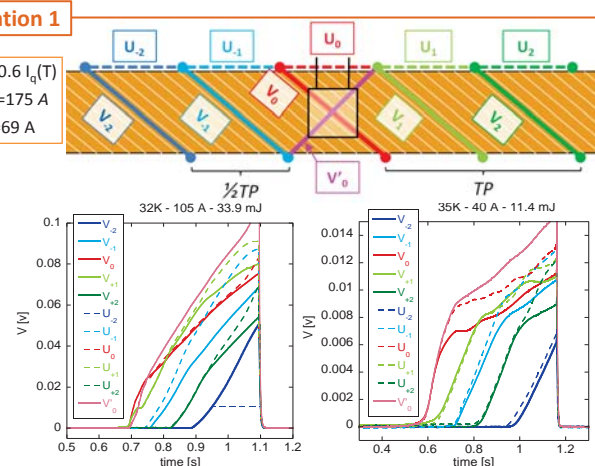


Quench development is not symmetric around the heater.

In some conditions,  $V_1$  signal starts at the same time than  $V_0$  (which measures voltage of the strand placed under the heater). This suggests that some parts of this cable (in the right part of the heater) would have lower  $I_c$ .

Estimated quench propagation velocities ( $v_p$ ) in [cm/s]

	$T = 32$ K	$T = 35$ K
$I = 0.6 I_q$	10.0-10.1	5.6-6.8
$I = 0.7 I_q$	10.1-12.7	6.4-7.4



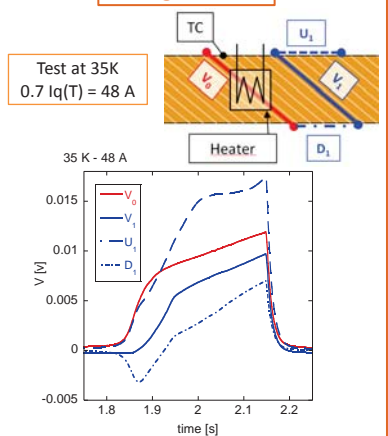
Voltages measured for the same conditions, but here also voltages  $U_i$  (see scheme) are plotted.

$V'_0$ , which measures the voltage of the strand in the opposite face of the cable, beneath the heater, is similar to  $V_0$ , but slightly higher (longer length).

In this configuration, measured "intra-strand" voltages,  $V_i$ , and corresponding "inter-strand" voltages,  $U_i$ , are similar but not equal.

Under these conditions maximum temperatures registered by TC were: 64.8 K at 32 K test and 47.7 K at 35 K. Note:  $U_2$  signal at 32 K test saturates at  $t > 0.95$  s.

### Configuration 2



For this voltage-tap configuration, large differences were observed between measured voltages  $U_1$ ,  $V_1$  and  $D_1$ .

This is caused by inhomogeneous local I-V characteristics among strands in this area. Current sharing between strands is difficult due to the high electrical contact resistance between strands in this cable.

## Conclusions

We have analysed experimentally the thermal and electrical behaviour of different MgB<sub>2</sub> Rutherford cables under hot-spot conditions. The quench behaviour strongly depends on the metal sheath.

**Cable consisting of strands of multifilamentary Cu-sheathed wires** has very low  $n$ -value, which is also measured for the individual wires. So, it is not caused by damage during cable assembling. Low  $n$ -values together with high thermal conductivity of the Cu-sheath make this cable very stable against local thermal disturbances and it is difficult to trigger a quench.

**Cable made with Cu10Ni-sheathed monocoire wires** presents some inhomogeneities in the local I-V of the different strands in some parts of the cable.

Different voltage-tap configurations have been analysed to understand the quench development and propagation in this cable. More experiments are currently underway.

**Acknowledgments:** This work was supported by the Spanish Ministerio de Economía y Competitividad and the European FEDER Program (project ENE-2014-52105-R) and by the Gobierno de Aragón (research group T12).