Tensile and bending stress tolerance on MgB₂ wire made by in situ PIT process

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4MP2-02

4MP2-09

1. Introduction

- \blacksquare It is important to understand how much strong strain leads to I_c degradation on reacted MgB₂ wires at room temperature for fabricating coils by React & Wind.
- The agreement between the critical tensile and bending strain was shown with ex situ tape wire [1].
- \blacksquare In this paper, we have studied the details of I_c degradation of the *in situ* round wire and compared the critical tensile strain at room temperature and the critical bending strain. The Young's module of filament using mechanical milled powder was compared with other type of MgB₂ filament.

	Analysis of I_c degradation	Improvement of		
	and mechanical properties	mechanical property		
Previous	Stress-Strain curve	> High strength metal sheath [2]		
studies	Young's modulus, E	High strength filaments		
	$> I_{\rm c}/I_{\rm c0}$	● IMD [3] ● CHPD [4]		
	$(I_{c0} = I_{c} \text{ of non-stressed wire})$	Mechanical alloyed powder [5]		
This	Stress-Strain curve	> High strength filaments		
study	\triangleright Young's modulus, E	 Mechanical milled powder [6] 		
	$> I_{\rm c}/I_{\rm c0}$	Related oral 4MO2-02		
	Shape of I-V curve	presentation		

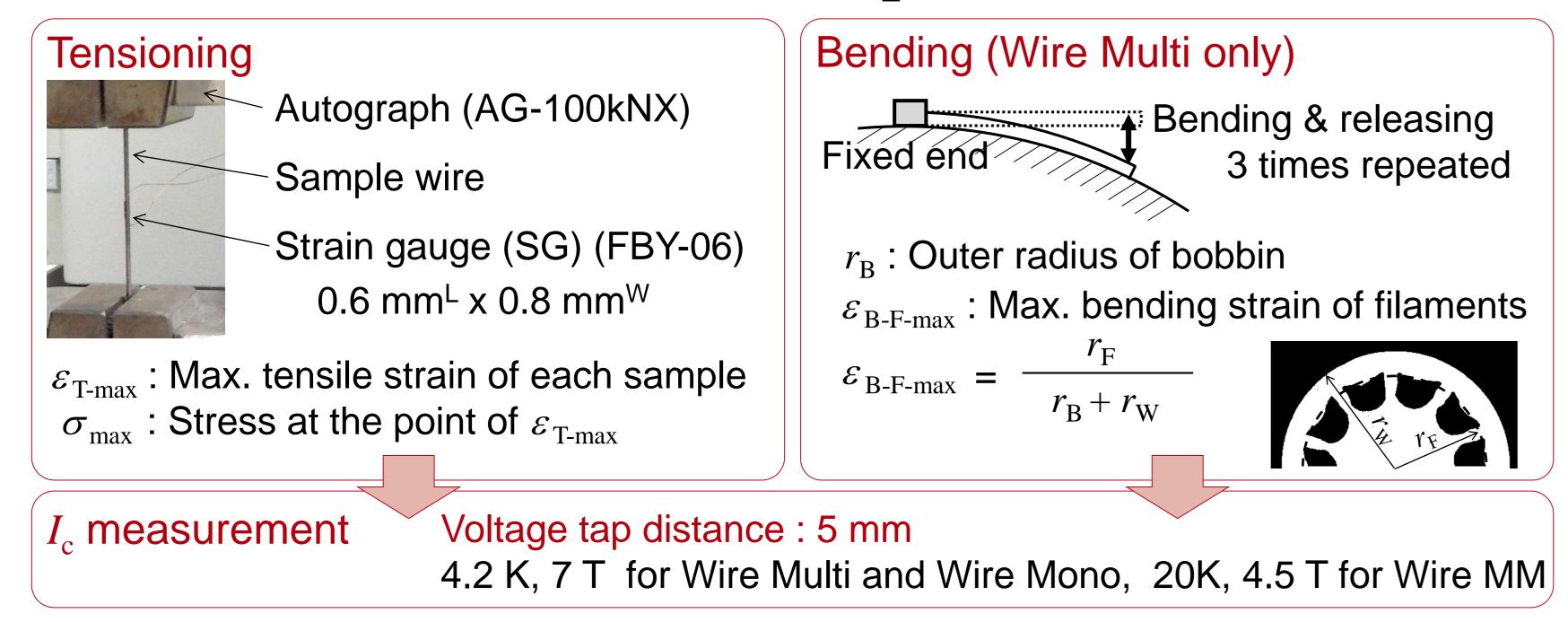
2. Experimental Details

2-1. Sample Wires (made by ourselves)

		Wire Multi [7] *	Wire Mono	Wire MM [6]
Milling		Ball	Ball	Mechanical
Dopant		Coronene	N/A	Coronene
Outer diameter		1.5 mm	1.3 mm	0.5 mm
Volume fraction	Fe	37%	32%	39%
	Cu	21%	34%	_
	Monel	18%	-	_
	MgB ₂	24%	34%	61%
Heat treatment		600 °C x 12 hr	600 °C x 6 hr	600 °C x 3 hr

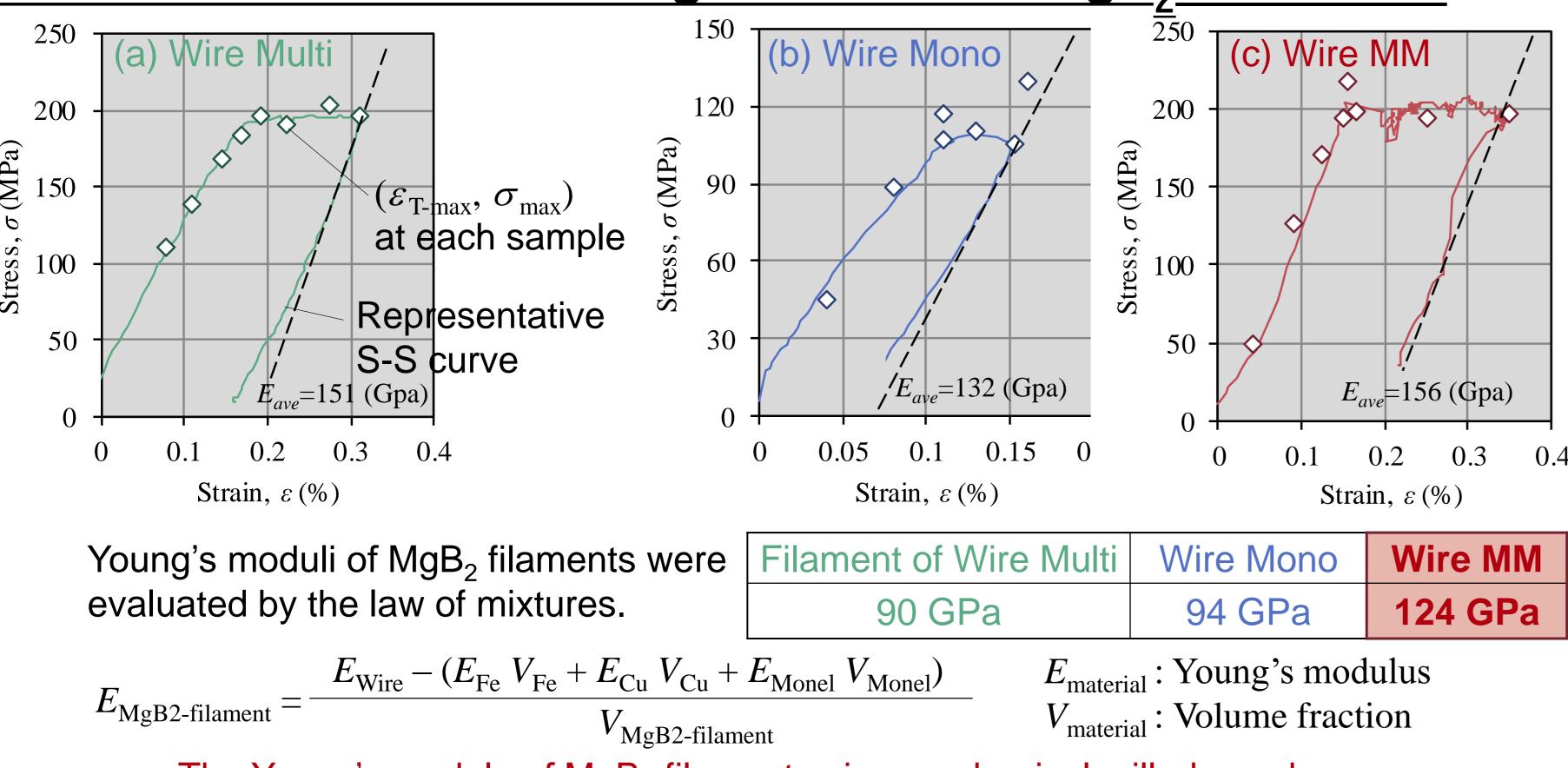
* Wire Multi prefers to W&R

2-2. Tensioning or Bending at RT and I. Measurement



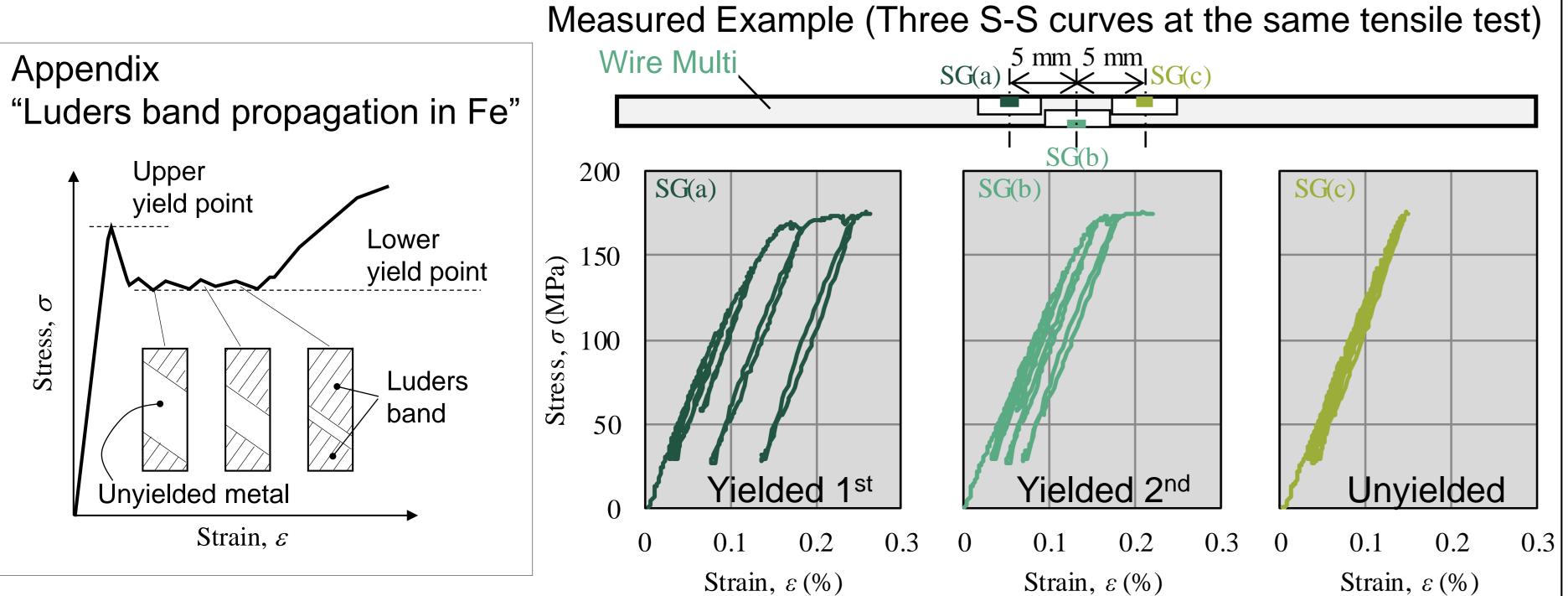
3. Results and Discussion

3-1. S-S Curves and Young's Moduli of MgB₂ Filaments



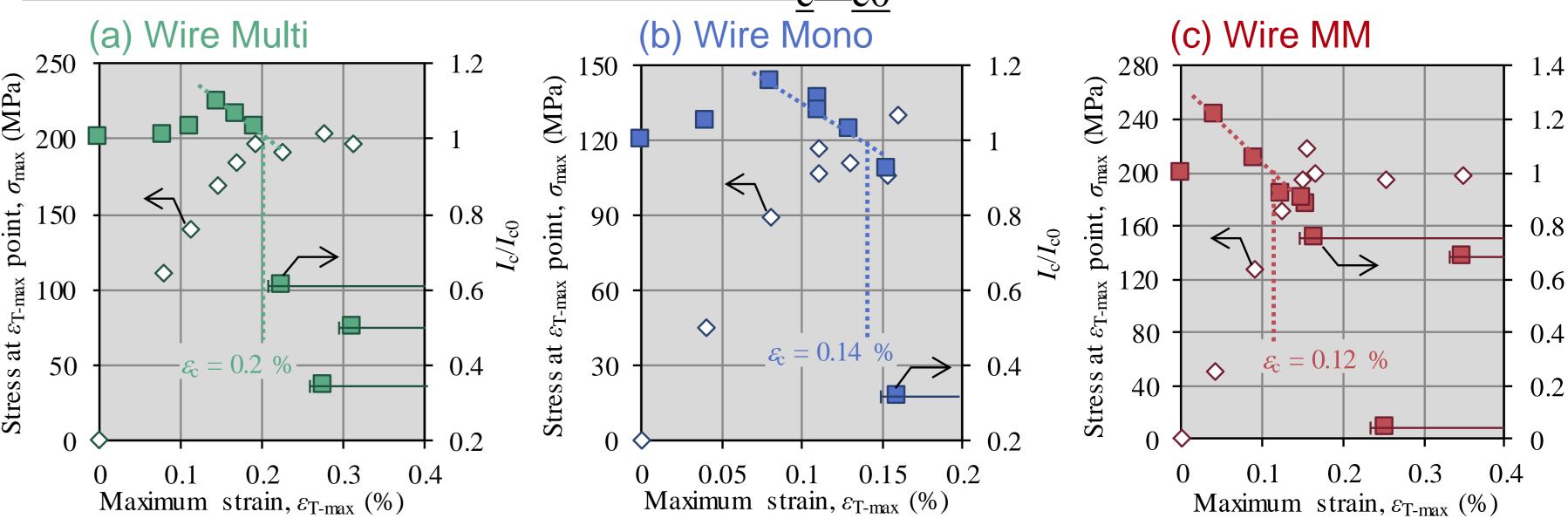
The Young's module of MgB₂ filament using mechanical milled powder was higher than that of ball milled powder.

3-2. Strain Measurement Error by Luders Band Propagation



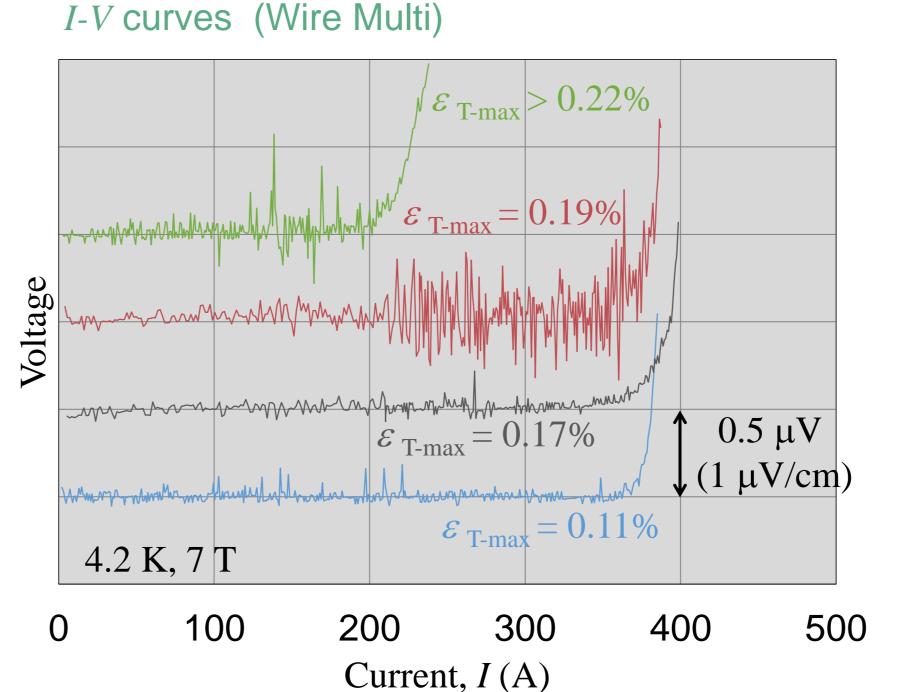
3. Results and Discussion (continued)

3-3. Tensile Strain at RT vs I_c/I_{c0}



We can measure the critical tensile strain at $I_c = I_{c0}$ as the threshold of I_c degradation from the results of $I_c > I_{c0}$, but ...

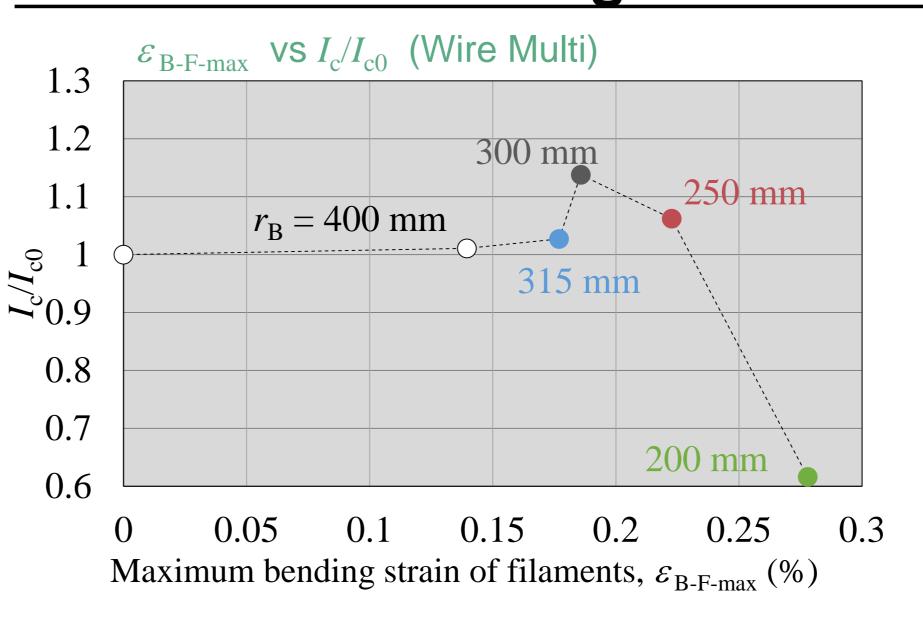
3-4. Critical Tensile Strain at RT Evaluated from *I-V* Curve

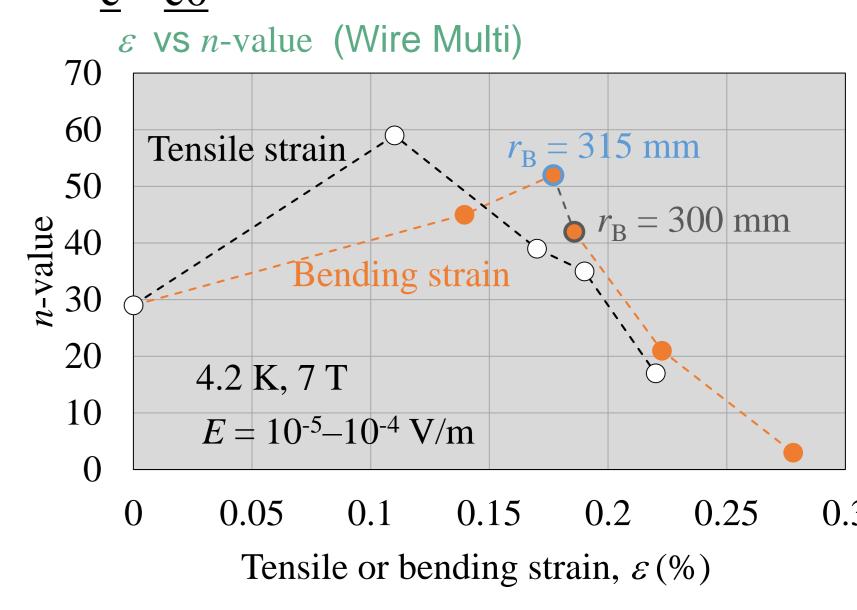


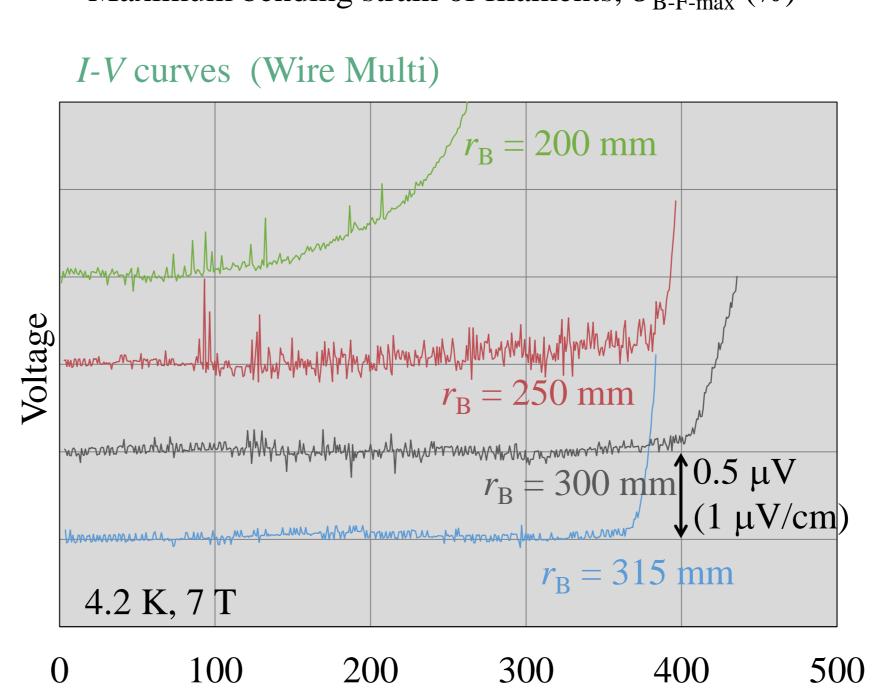
- *I-V* curve of $\varepsilon_{\text{T-max}}$ =0.19% was very noisy.
- It can be estimated that a small part of MgB₂ filaments of $\varepsilon_{\text{T-max}} = 0.19\%$ was damaged by tensile stress.
- It can be also thought that the noisy I-Vcurve was caused by the current distribution from some partly damaged filaments to some undamaged filaments.

The critical tensile strain at RT of Wire Multi was evaluated to be 0.17%–0.19%.

3-5. Critical Bending Strain from I/I and I-V Curve







Current, I(A)

- From I_c/I_{c0} , the critical bending radius seems to be 200–250 mm, but...
- $r_{\rm R} = 250 \, {\rm mm}$
 - *I-V* curve was noisy like over tensioned wire.
- $r_{\rm B} = 300 \; {\rm mm}$
- *I-V* curve was not so noisy.
- *n*-value begun to decrease.
- $r_{\rm R} = 315 \, {\rm mm}$

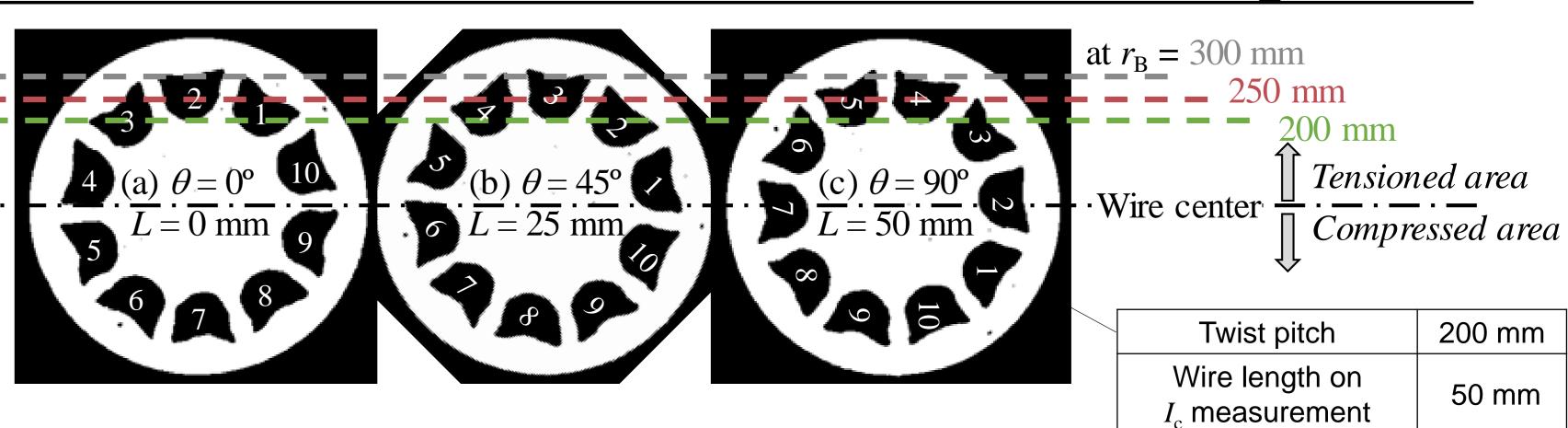
I-V curve seemed to be perfect.

The critical bending strain of Wire Multi at RT was evaluated to be 0.18%-0.19%.

200 mm

50 mm

3-6. Confirmation of Threshold Line of Bending Strain



 Threshold line was calculated with critical strain = 0.19%. The distribution of these lines agrees experimental results. e.g. $r_{\rm R}$ = 300 mm was close value as critical radius. Five filaments were damaged deeply in $r_{\rm R}$ = 200 mm.

4. Conclusions

- (1) The Young's module of MgB₂ filament using mechanical milled powder was higher than that of ball milled powder as expected.
- The critical tensile strain at room temperature and the critical bending strain of Wire Multi were agreed well each other and evaluated to be 0.18%-0.19%.
- (3) To find the threshold of I_c degradation, we should pay attention to not only the I_c/I_{c0} value but also the shape (noise and n-value) of I-V curve.
- (4) The stressed filament has a possibility of being partly damaged even if $I_c > I_{c0}$, and we can find it from noisy *I-V* curve.

5. References

- [1] P. Kováč, *SuST* (2015) 6200607
- [2] P. Kováč, *SuST* (2013) 105028
- [3] G. Nishijima *SuST* (2012) 054012 [4] C. Zhou, SuST (2014) 075002
- [5] P. Kováč, *SuST* (2009) 075026
- [6] M. Kodama, *SuST* (2017) 044006
- [7] H. Tanaka, IEEE Trans. Appl. Supercond. (2016) 4600904

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We could not measure the correct strain value of the entire area of the I_c measurement after iron began yielding, but the strains measured from the unyielded sample wires were correct.