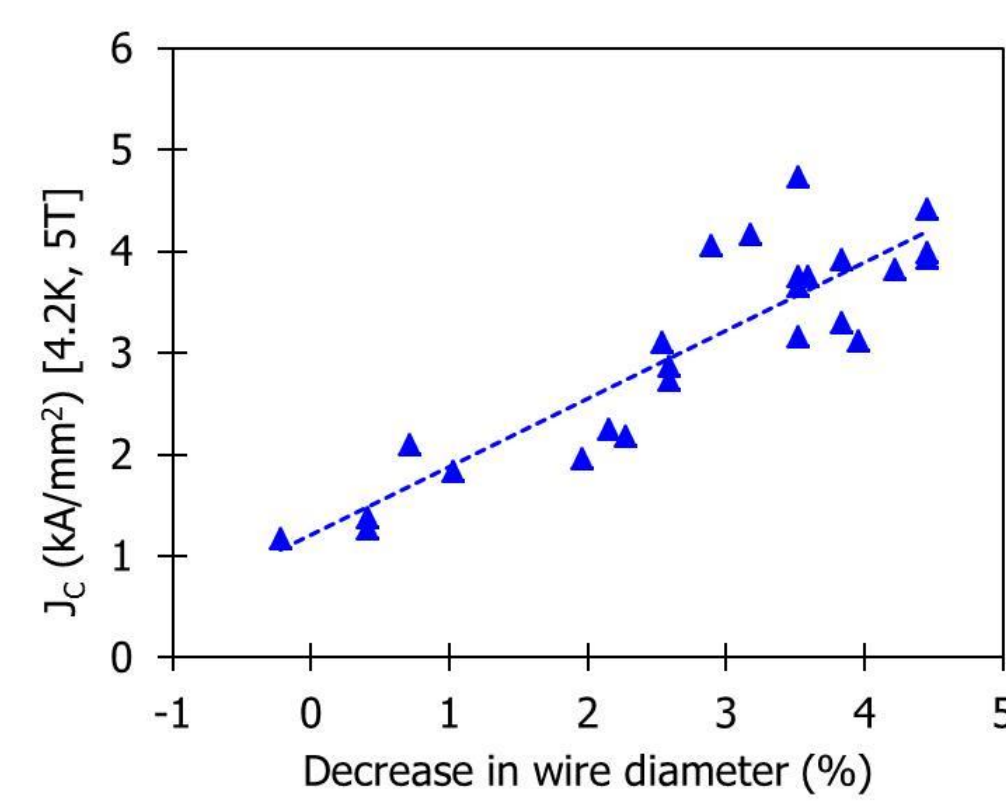


Motivation: 3.8 % wire shrinkage during coil OP processing

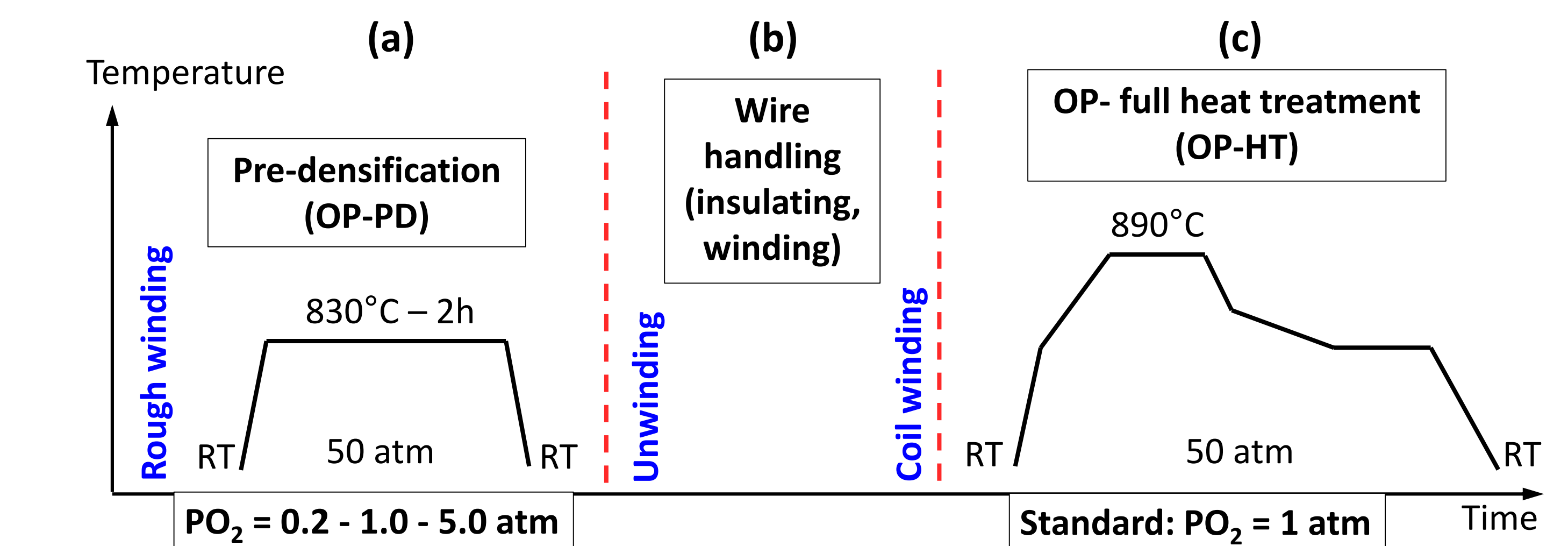
- To reach high J_c , $\text{Bi}_2\text{Sr}_2\text{CaCu}_2\text{O}_x$ (2212) has to be isostatically compressed with overpressure (OP) up to 50 atm during the partial-melt heat treatment (OP-HT) to reduce filament porosity. It results in about 3.8 % decrease in wire diameter.
- The decrease in wire diameter leads to a loose winding pack in solenoid magnets and may cause motion and deformation during the OP heat treatment.



We describe and study a process to pre-densify the wire before winding and heat treat the coil with pressure. We found that:

- the process reduces wire diameter shrinkage to 0.7 % during OP-HT.
- Dense wire can be wound into 10 mm diameter coil with no 2212 leak after OP-HT and no J_c degradation
- J_c was increased by 22% by increasing PO_2 during OP-PD

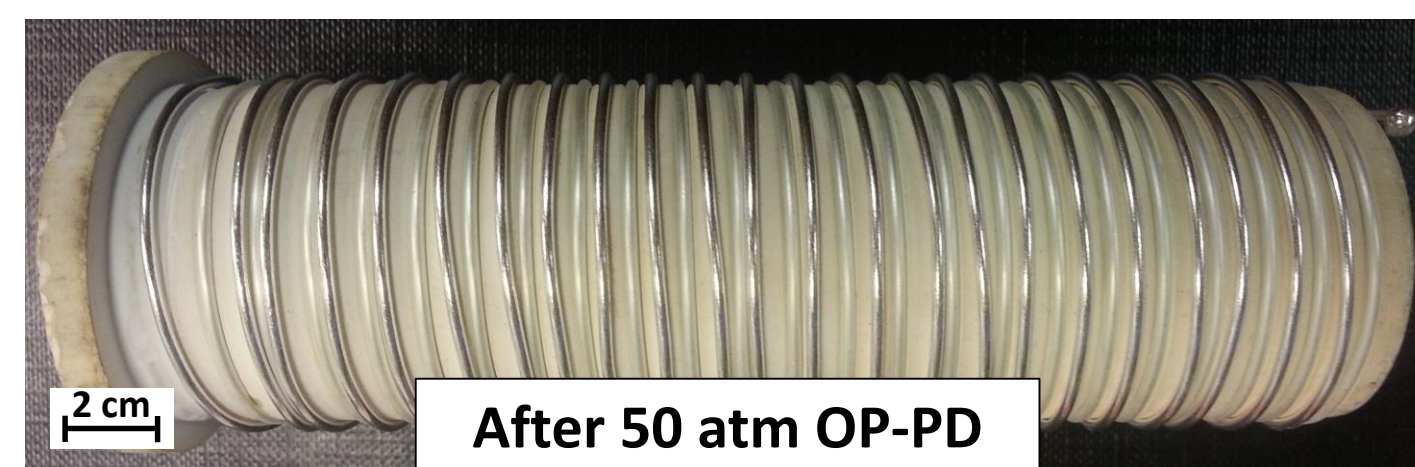
Process to densify 2212 wire before coil winding



- (a) OP-PD:
- 50 atm with $\text{PO}_2 = 0.2, 1, \text{ or } 5 \text{ atm}$
 - Powder doesn't melt

Ø 1.2 mm Ag-Mg and Ag-sheathed wire

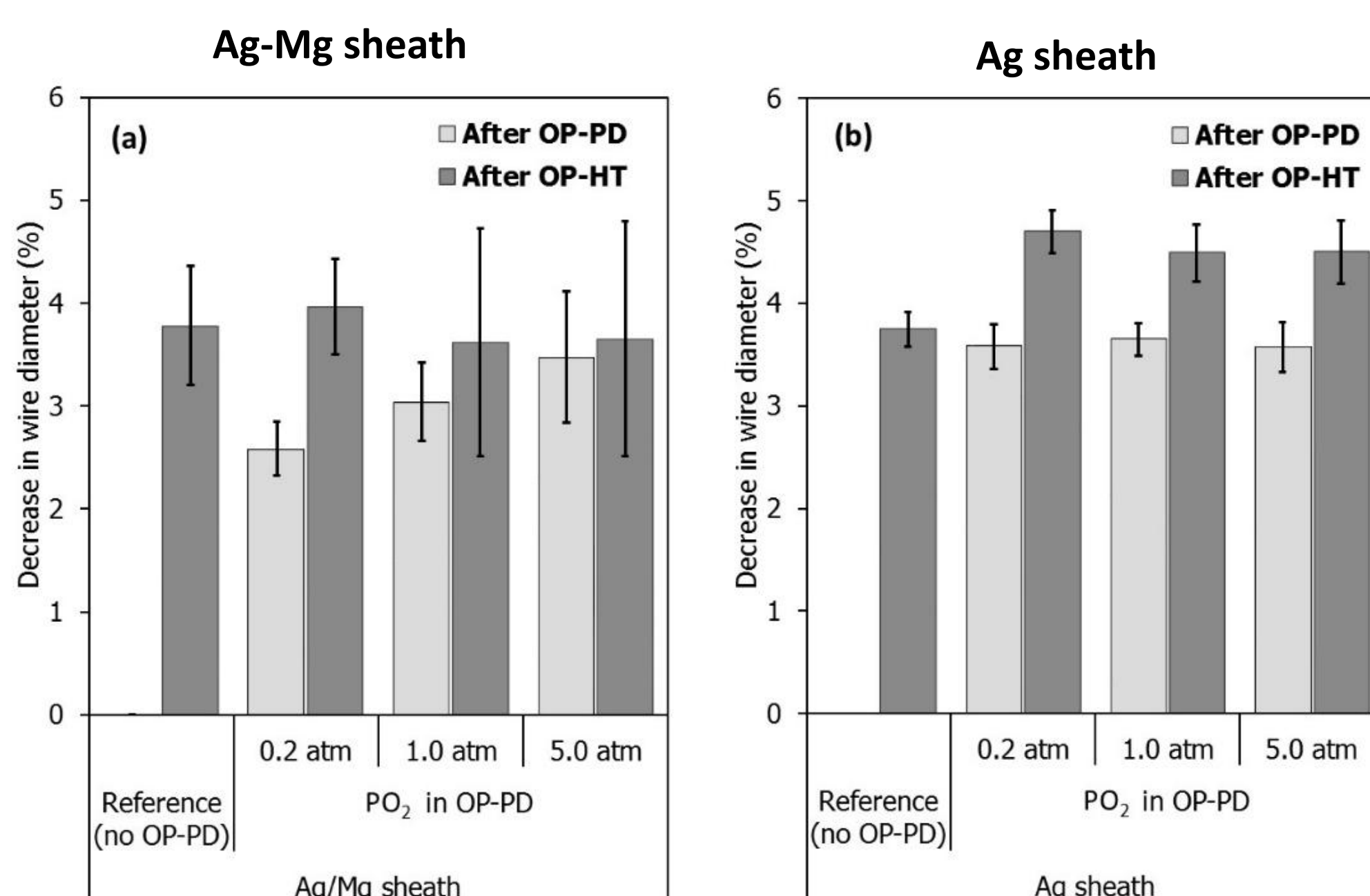
- (b) Wire handling and coil winding:
- Diameter measurement of dense wire (winding over five 15 cm dia. pulleys)
 - Dense wire was cut into four 50 cm sections and wound into 5, 10, 20 and 30 mm diameter coils.



- (c) OP-HT:
- The coils of dense wire were sealed and OP-HT at 50 atm with $\text{PO}_2 = 1 \text{ atm}$.



Successful process: after OP-PD wire shrinks by 0.7 % in OP-HT



Change in wire diameter

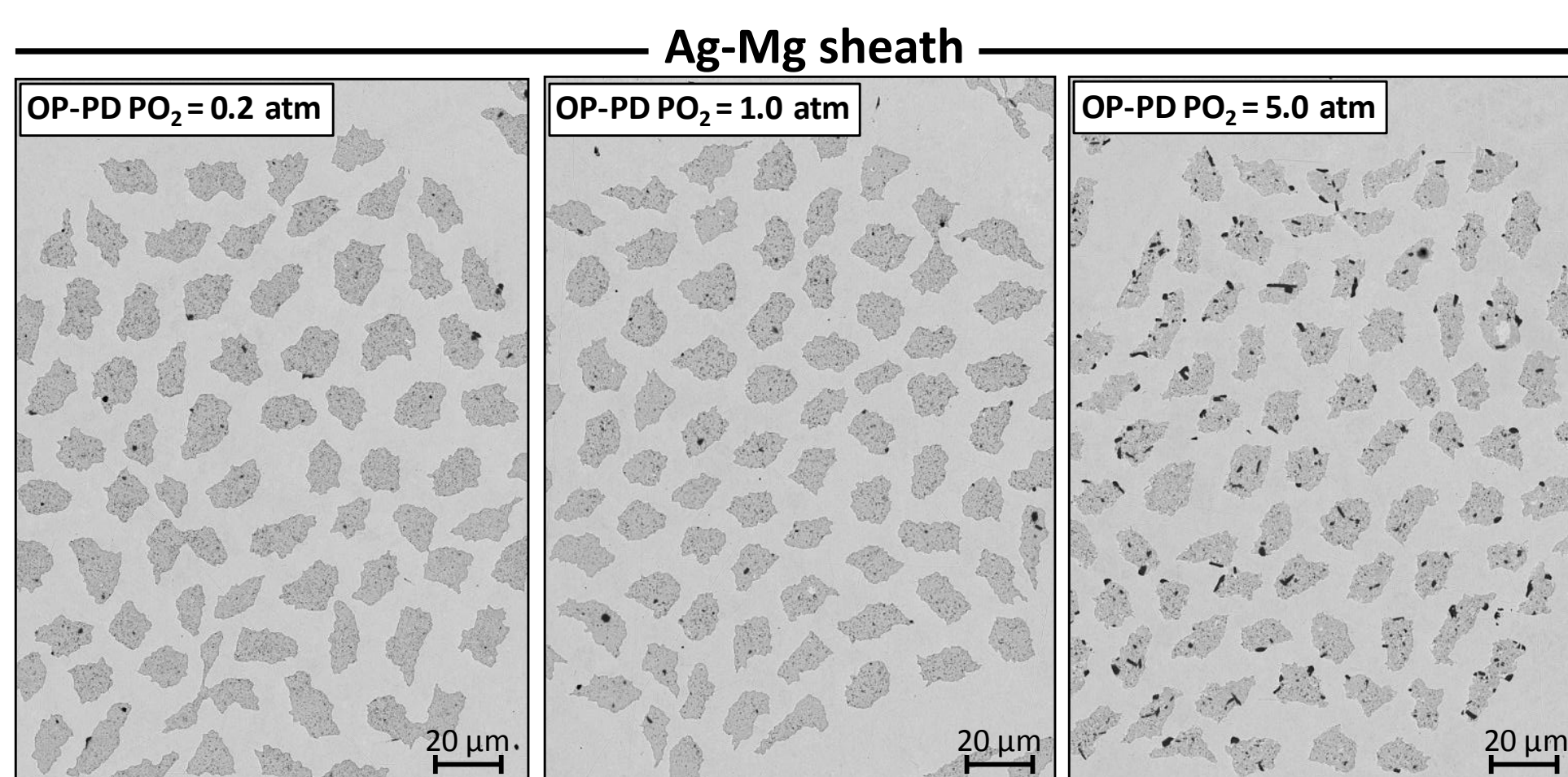
Ag-Mg sheathed wire:

- OP-PD: $\Delta\phi = -3.1 \pm 0.6 \%$
- OP-HT: $\Delta\phi = -3.8 \pm 1.0 \%$
- $\Delta\phi_{\text{OP-PD}} - \Delta\phi_{\text{OP-HT}} = 0.7 \%$

Ag sheathed wire:

- OP-PD: $\Delta\phi = -3.6 \pm 0.2 \%$
- OP-HT: $\Delta\phi = -4.6 \pm 0.3 \%$
- $\Delta\phi_{\text{OP-PD}} - \Delta\phi_{\text{OP-HT}} = 1.0 \%$

- 2212 decomposition is observed after OP-PD with $\text{PO}_2 = 5 \text{ atm}$.
- Similar results are observed with Ag-sheathed wire



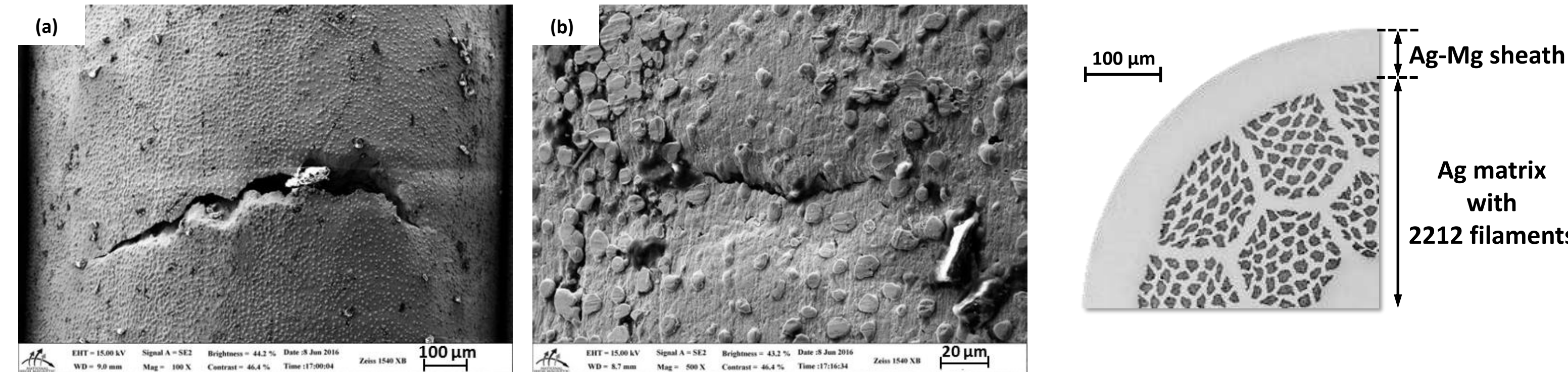
Dense wire winding ability depends on PO_2 during OP-PD

Dense Ag-Mg sheathed wire shows higher ductility with increasing PO_2 during OP-PD

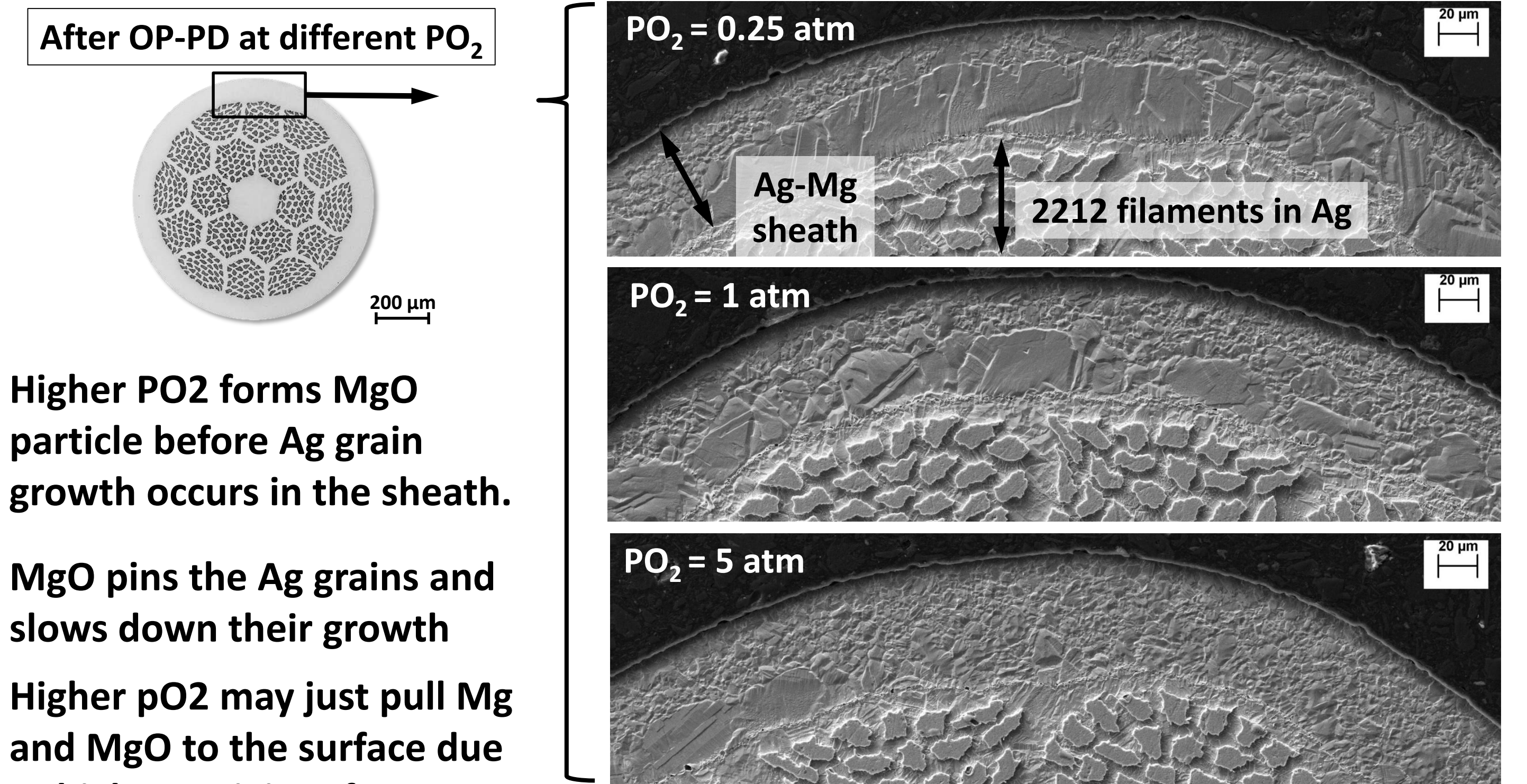
| Wire sheath | PO_2 for OP-PD | Can the OP-PD wire be wound into a coil? | | | | Is the coil leak-free after OP-HT? | | | |
|-------------|-------------------------|--|---|---|---|------------------------------------|----|---|---|
| | | Coil diameter (mm) | | | | Coil diameter (mm) | | | |
| Ag-Mg | Reference (no OP-PD) | Y | Y | Y | Y | Y | Y | Y | Y |
| | 0.2 atm | No | Y | Y | Y | * | Y | Y | ? |
| | 1.0 atm | No | Y | Y | Y | * | No | Y | Y |
| | 5.0 atm | Y | Y | Y | Y | No | Y | Y | Y |
| Ag | Reference (no OP-PD) | Y | Y | Y | Y | Y | Y | Y | Y |
| | 0.2 atm | Y | Y | Y | Y | Y | Y | Y | ? |
| | 1.0 atm | Y | Y | Y | Y | Y | Y | Y | Y |
| | 5.0 atm | Y | Y | Y | Y | No | Y | Y | Y |

* Coils were not OP-HTed

Macro and micro cracks form in sheath of dense Ag-Mg 2212 wire OP-PD with 0.2 atm PO_2



Increasing PO_2 during OP-PD decreases the grain size of the sheath



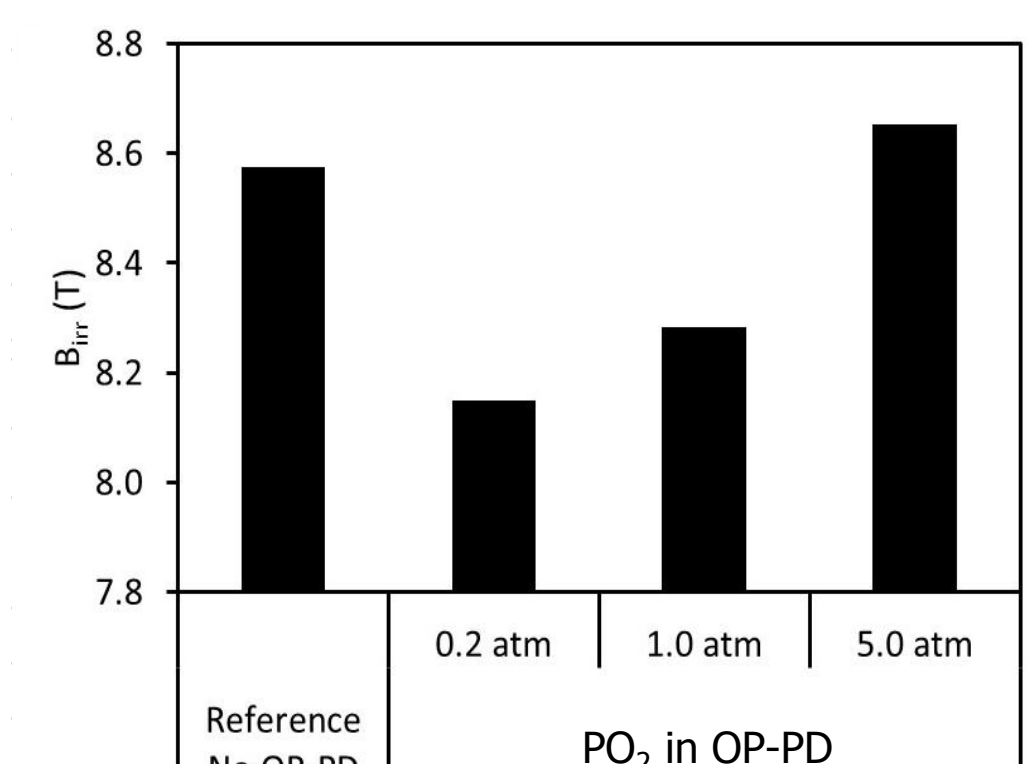
- Higher PO_2 forms MgO particle before Ag grain growth occurs in the sheath.
- MgO pins the Ag grains and slows down their growth
- Higher PO_2 may just pull Mg and MgO to the surface due to higher activity of O

Scanning electron microscope images of chemically etched wire cross section

No J_c degradation (+22 % J_c with $\text{PO}_2 = 5 \text{ atm}$ during OP-PD)

| Ag-Mg sheathed wire | | | |
|----------------------------|-----------------------|----------------|--|
| PO_2 during OP-PD | $\Delta J_c (\%)$ | | |
| | Straight section | Curved section | |
| 0.2 atm | -31.7 | -38.0 | |
| 1.0 atm | 2.1 | -1.3 | |
| 5.0 atm | 22.0 | 22.8 | |
| PO_2 during OP-PD | $J_c (\text{A/mm}^2)$ | | |
| | Straight section | Curved section | |
| Reference (no OP-PD) | 4303.5 | 4262.9 | |
| 0.2 atm | 2939.0 | 2667.7 | |
| 1.0 atm | 4394.9 | 4249.1 | |
| 5.0 atm | 5248.4 | 5282.9 | |

| Ag sheathed wire | | | |
|----------------------------|-----------------------|----------------|--|
| PO_2 during OP-PD | $\Delta J_c (\%)$ | | |
| | Straight section | Curved section | |
| 0.2 atm | -6.7 | -8.3 | |
| 1.0 atm | 3.0 | 7.9 | |
| 5.0 atm | 9.3 | 3.7 | |
| PO_2 during OP-PD | $J_c (\text{A/mm}^2)$ | | |
| | Straight section | Curved section | |
| Reference (no OP-PD) | 4219.8 | 4266.5 | |
| 0.2 atm | 3935.1 | 3870.1 | |
| 1.0 atm | 4346.6 | 4555.0 | |
| 5.0 atm | 4614.3 | 4376.2 | |



- J_c of wires OP-PD with $\text{PO}_2 = 1 \text{ atm}$ are identical
- Ag-sheathed wire shows no clear dependence on PO_2 during OP-PD
- Ag-Mg-sheathed wire shows a strong increase in J_c with increasing PO_2
- Ag-Mg sheathed wire shows an increase in H_{irr} after 5 atm PO_2 OP-PD + OP-HT suggesting an increase in oxygen concentration in 2212

Conclusions

- Densification before winding process has been successfully demonstrated:
 - Decrease in wire diameter during OP-HT is reduced from 3.8 % to 0.7 %.
 - Dense wire can be wound into coils as small as 20 mm in diameter without cracking or 2212 leaks after OP-HT.
 - J_c is not decreased by the process ($\text{PO}_2 = 1 \text{ atm}$)
- Ag-Mg-sheathed wire:
 - increasing PO_2 in the OP-PD increases J_c significantly (up to 22% with $\text{PO}_2 = 5 \text{ atm}$ compared to wire without OP-PD).
 - The increase in J_c with increasing PO_2 in OP-PD seems to be linked to the oxide dispersion strengthening mechanism (that varies with PO_2)
 - OP-PD with 5 atm PO_2 might be added to Ag-Mg sheathed 2212 coil OP processing since it to increased J_c by up to 22 % in these experiments.
- Ag-sheathed wire: Densification and J_c do not vary with PO_2 used in OP-PD.