

# 4EP2-23: Critical current scattering in series arrays of HTS SQUIDs based on ion-damaged barrier Josephson junctions

Denis Cr  t  <sup>1</sup>, Eliana Recoba Pawlowski<sup>1</sup>, Julien Kermorvant<sup>2</sup>, Yves Lema  tre<sup>1</sup>, Bruno Marcilhac<sup>1</sup>, Christian Ulysse<sup>3</sup>

<sup>1</sup>Unit   Mixte de Physique CNRS-THALES, Univ. Paris-Sud, Univ. Paris-Saclay, Palaiseau, France  
<sup>2</sup>THALES Com. and Security, France,  
<sup>3</sup>Labo. Photonique & Nanostructures, CNRS, Marcoussis, France



## Abstract

Characterization of scattering for an HTS Josephson junction (JJ) technology is usually based on critical current  $I_C$  (and normal resistance  $R_n$ ) defined by the Resistively Shunted Junction (RSJ) model. Accounting for thermal noise e.g. using Ambegaokar and Halperin (AH) model [1] is necessary but time consuming and not always sufficient.

We propose the thermal noise voltage (TNV) criterion for the determination of critical current, using AH model. At  $I=I_C$ ,  $\langle V \rangle$  is related to the junction parameters  $I_C$ ,  $R_n$  and  $\gamma = \hbar I_C / 2\pi k_B T$  where  $T$  is the physical temperature. An empirical analytical function has been found to fit the normalized thermal-noise/voltage relation given by AH.

We present the results of the TNV criterion on JJ based on the ion damage barrier technology described in [2] and compare it to the usual "predefined voltage threshold" (PVT) method.

[1] Ambegaokar V. and Halperin B.J., Phys. Rev. Lett., 22, 1364-1366 (1969)  
[2] App. Phys. Lett. 87, 102502 (2005) ; 89, 112515 (2006) ; 91, 142506 (2007) ; 91, 262508 (2007).

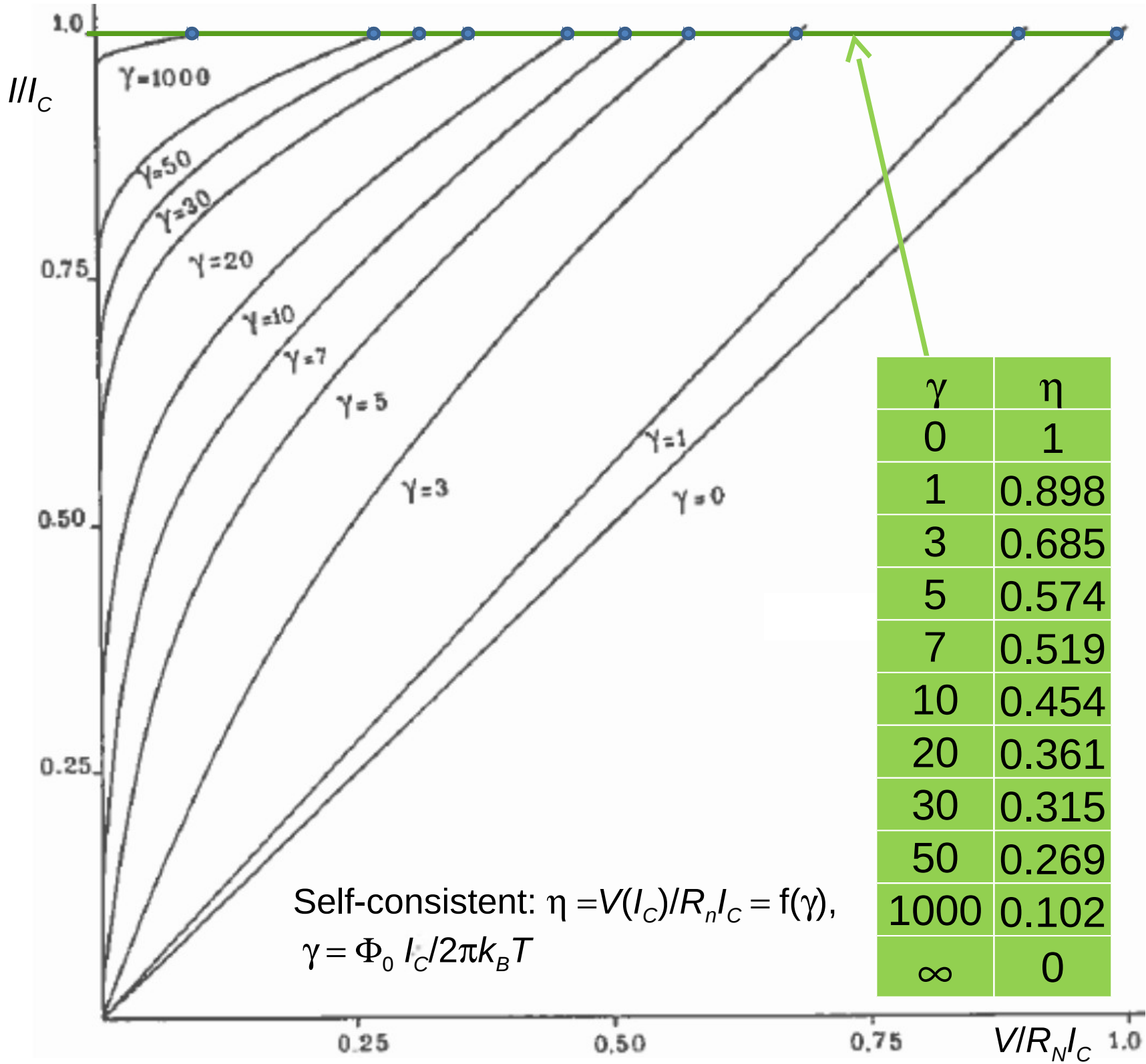
## Classical $I_C$ determination methods

Fixed Voltage Threshold (FV):  $I_C = I(V = V_{thres})$   
+ Simple (typ.  $V_{thres} = 1\mu V$ )  
+ For  $N$  JJ series array  $I_C = I(N \cdot V_{thres})$   
+ widely used (easy comparison)  
- The extracted value of  $I_C$  is lowered by thermal noise  
- In case of  $I_C$  scattering, TM essentially probes the JJ with the smallest critical current.

Ambegaokar & Halperin (AH):  
Adjust the full  $V(I)$  curve  $V(I, I_C, R_n, T)$   
+ No hypothesis made on any of the parameter ( $T = T_{noise}$ )  
+ In principle, applicable to JJ arrays, but ...  
- Very sensitive to deviation from RSJ model (and scattering)  
- Computation time is longer (and convergence is not guaranteed)

Ambegaokar & Halperin (limited to very small  $I_C$ ):  
 $I_C = f(T, R_{do}/R_n)$  where  $R_{do}$  is the dynamic resistance at  $I=0$   
+ Simple  
- Not applicable when Josephson energy  $> k_B T$

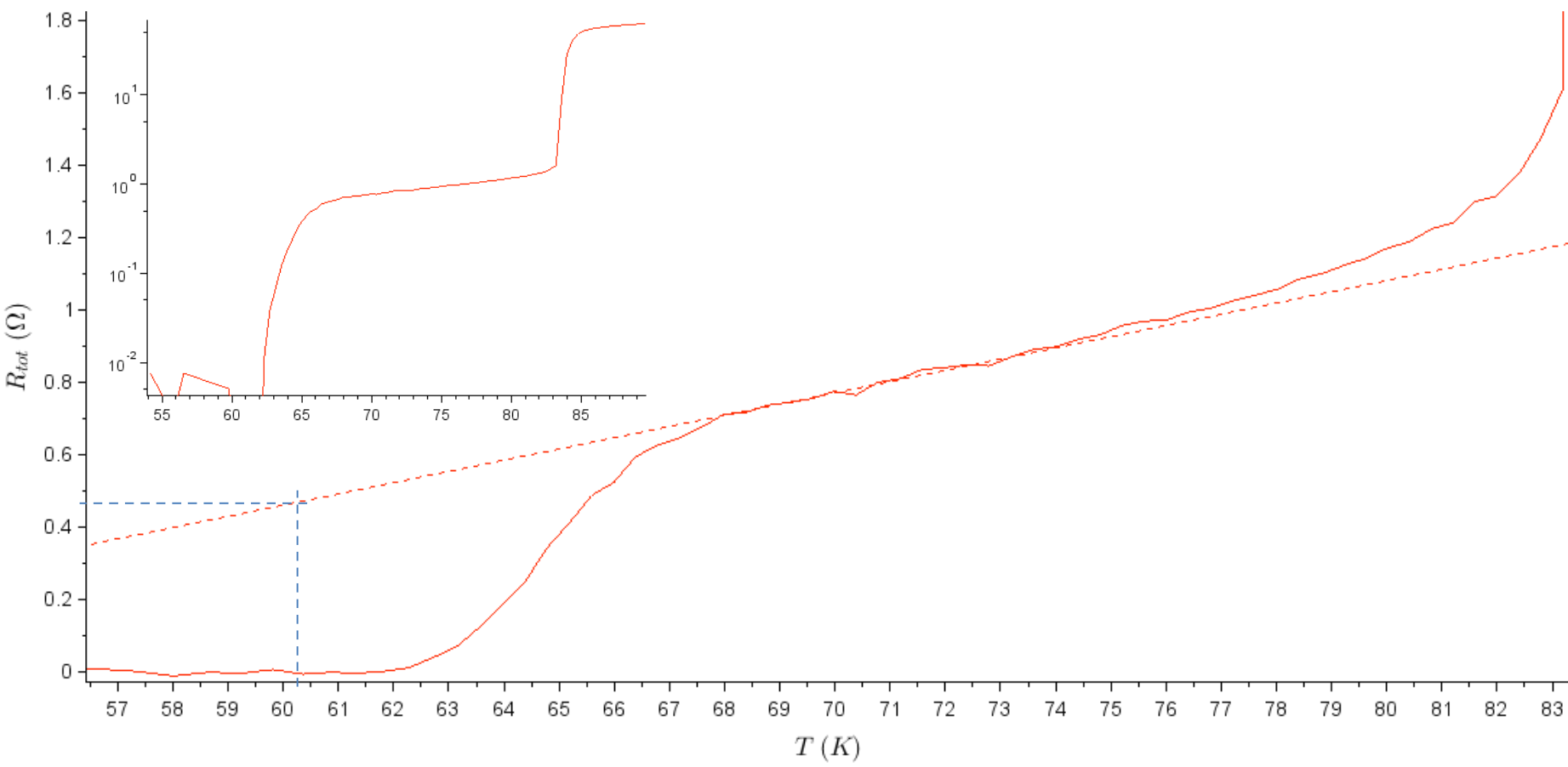
##    Thermal noise voltage    (TNV) method



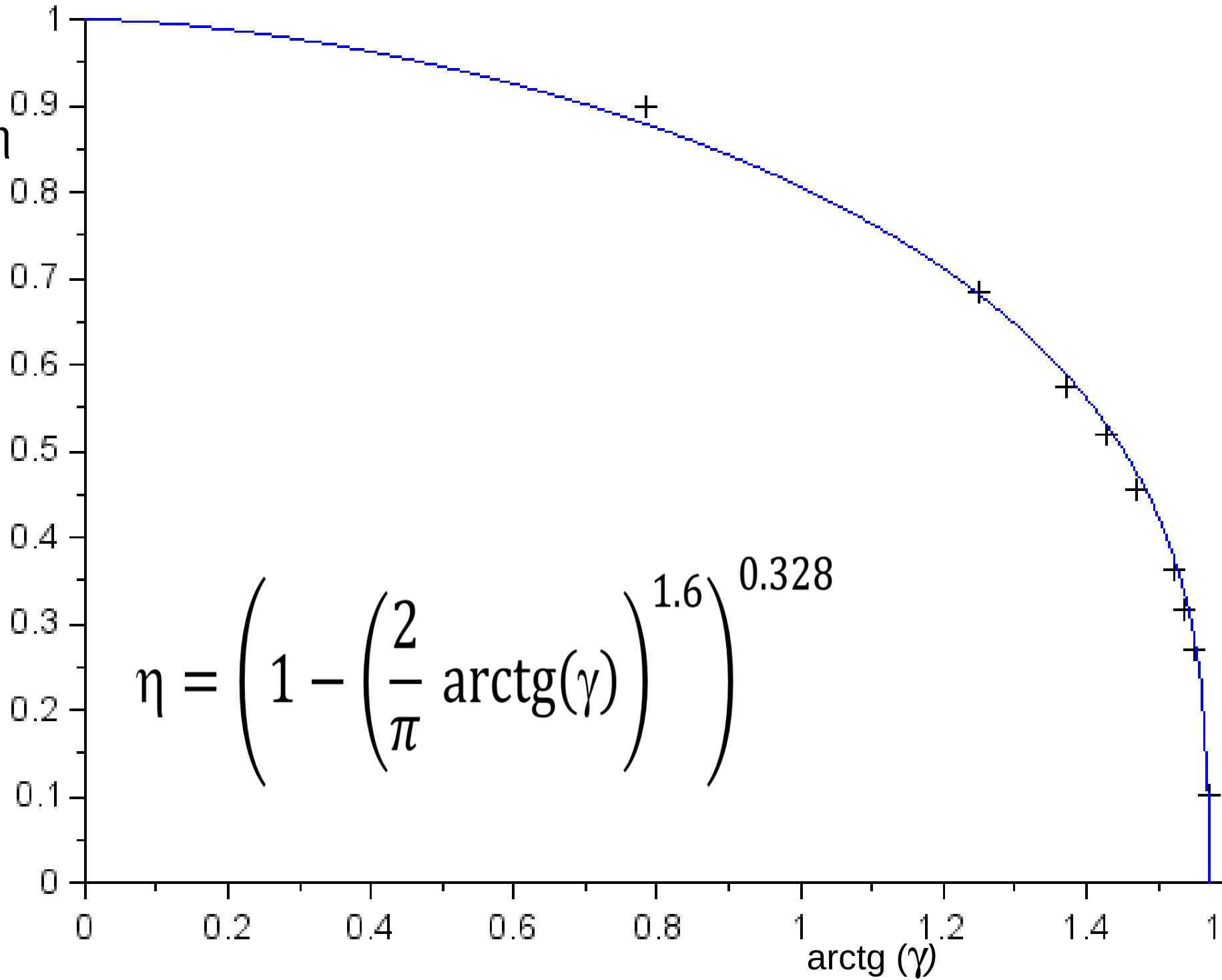
$V(I)$  curves of RSJ model in reduced coordinates for different values of  $\gamma$  (Ambegaokar & Halperin). For each  $\gamma$ , only the point at  $I=I_C$  is used

## Application of TNV method: determination of $R_n$

- Requires  $R_n$  : usually determined by the slope of  $V(I)$ . However, a few JJ types do not allow this method, e.g. ion-damaged barriers  
   Extrapolation of  $I(T)$  from above the Josephson coupling range (and of course below  $T_C$ ).



## Analytical approximation of $f(\gamma)$



Variation of the reduced    thermal noise voltage     $\eta$  versus  $\text{atan}(\gamma)$ . Crosses represent tabulated values, and the blue curve is the analytical approximation.

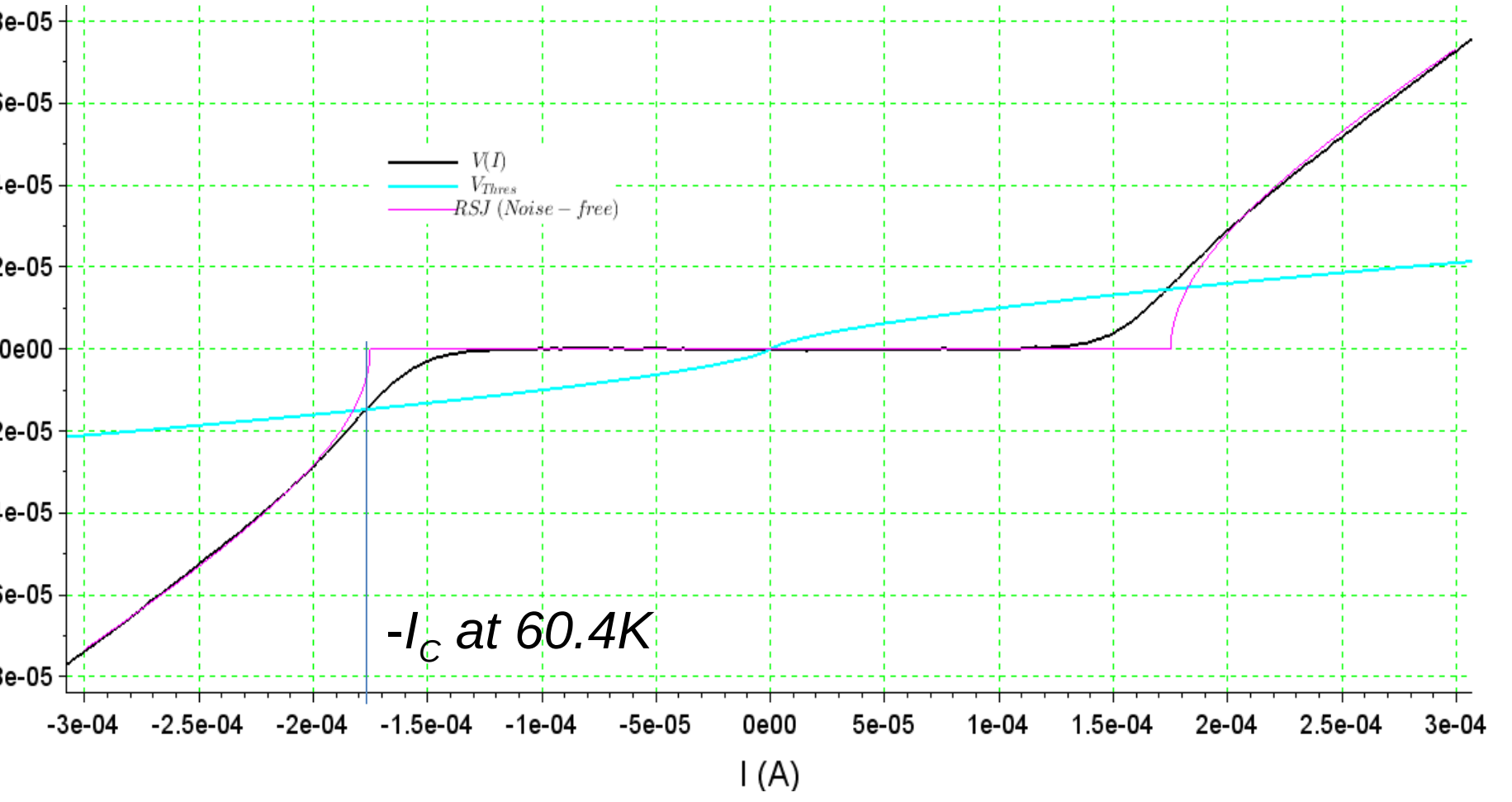
## Asymptotic behaviour

$$\text{arctg}\left(\frac{\Phi_0 I_C}{2\pi k_B T}\right) = \frac{\pi}{2} \left(1 - \left(\frac{V(I_C)}{R_n I_C}\right)^{3.08}\right)^{0.63}$$

-  $I_C/T \sim \left(\frac{V(I_C)}{R_n I_C}\right)^{-3.08}$  when  $\eta \rightarrow 0$   
  
- But  $I_C \sim (1 - \eta)^{0.63}$  when  $\eta \rightarrow 1$  instead of  $I_C \sim 1 - \eta$ . It only impacts at high temperatures when the  $V(I)$  curves are nearly linear.

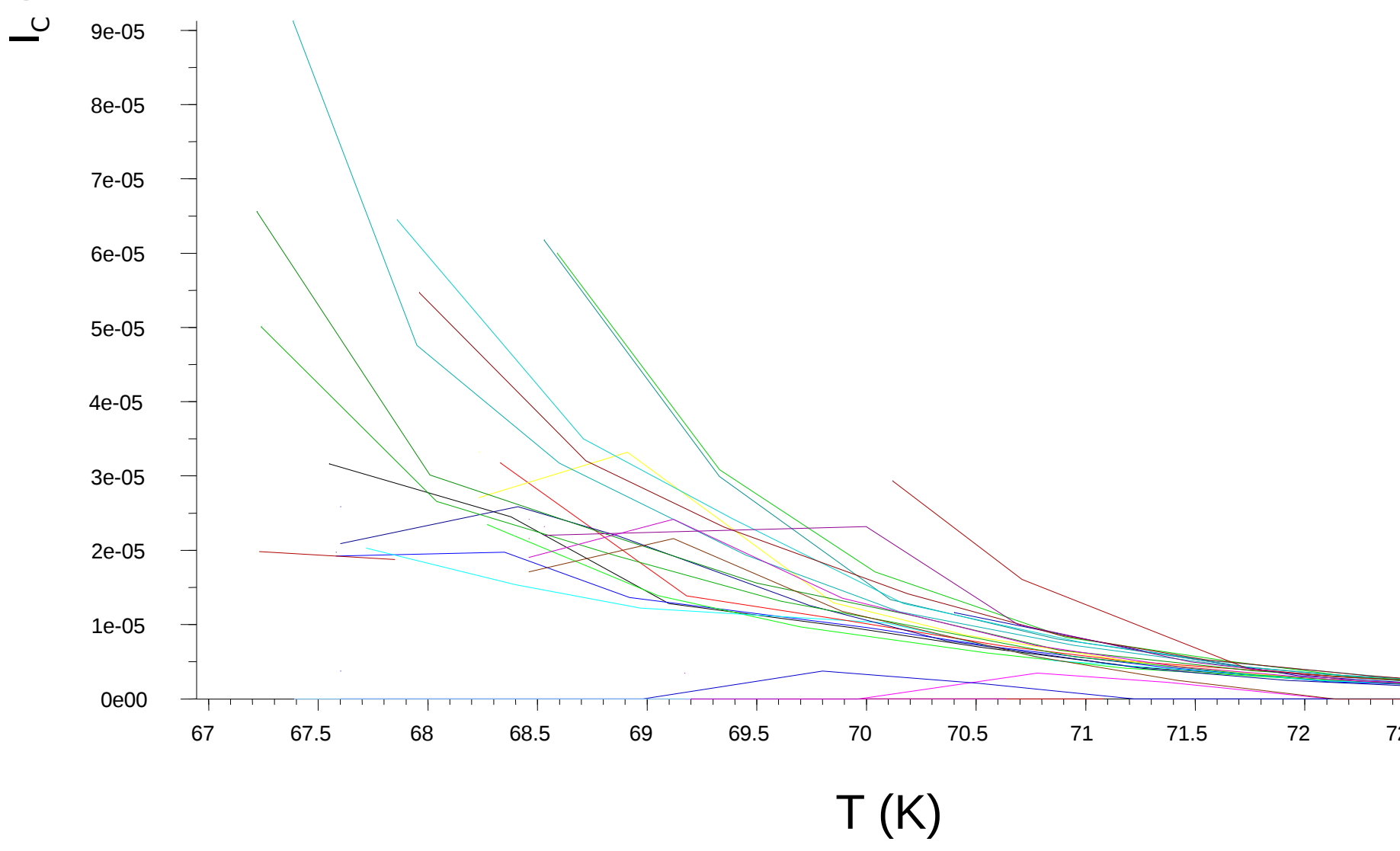
## Application of TNV method

$g_i = \Phi_0 / (2k_B T_{noise})$ ; // with  $T_{noise} = T_{physical}$   
 $V_{Thres} = R_n \cdot I \cdot (1 - (2/\pi \cdot \text{atan}(g_i \cdot I))^{1/0.63})^{1/3.08}$   
 $I_C = I(\text{find}(V >= V_{Thres}, 1))$ ; //    floor    value with sampling resolution

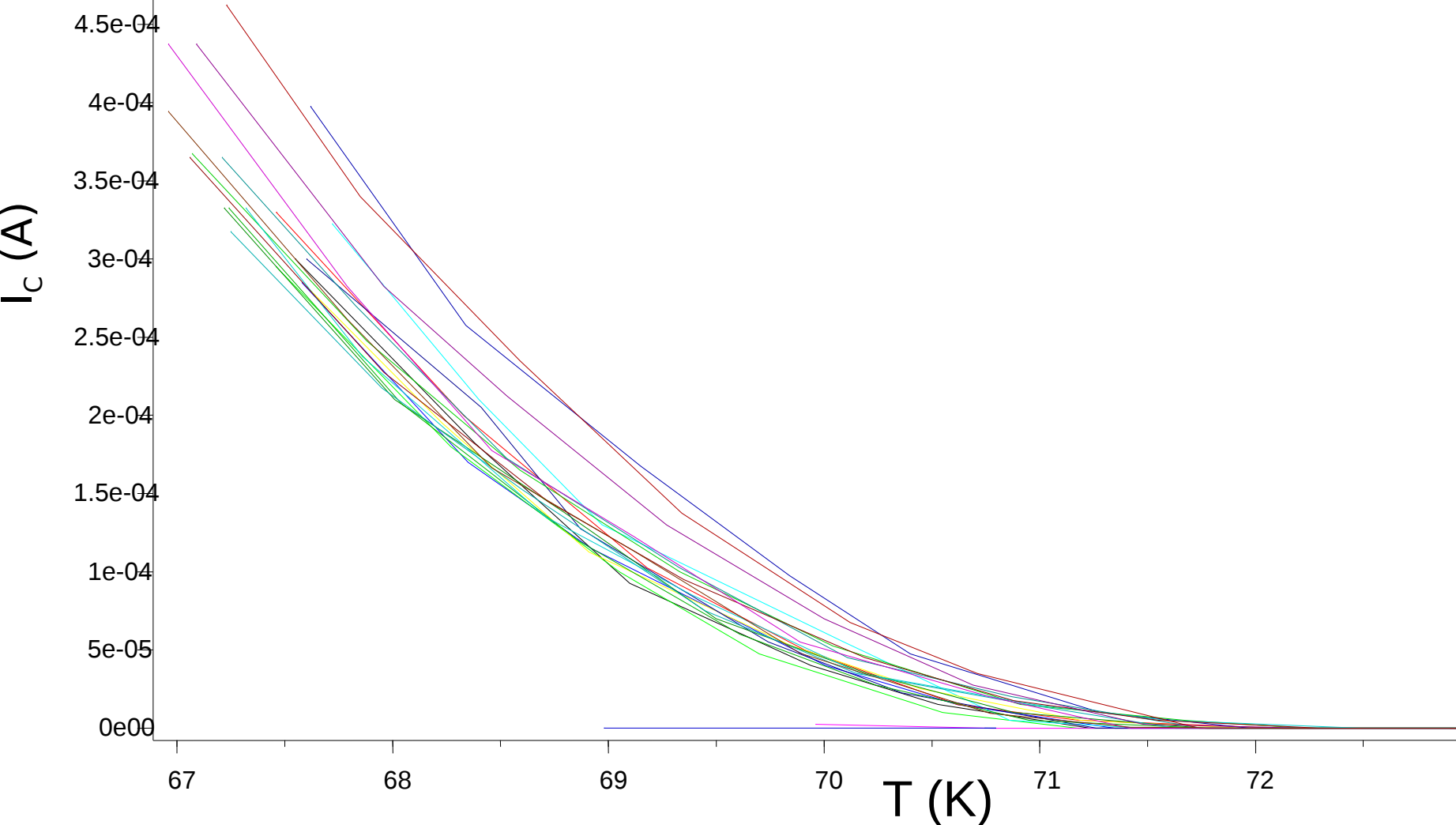


## Comparison of FV and TNV methods (on a collection of SQUIDs within same chip)

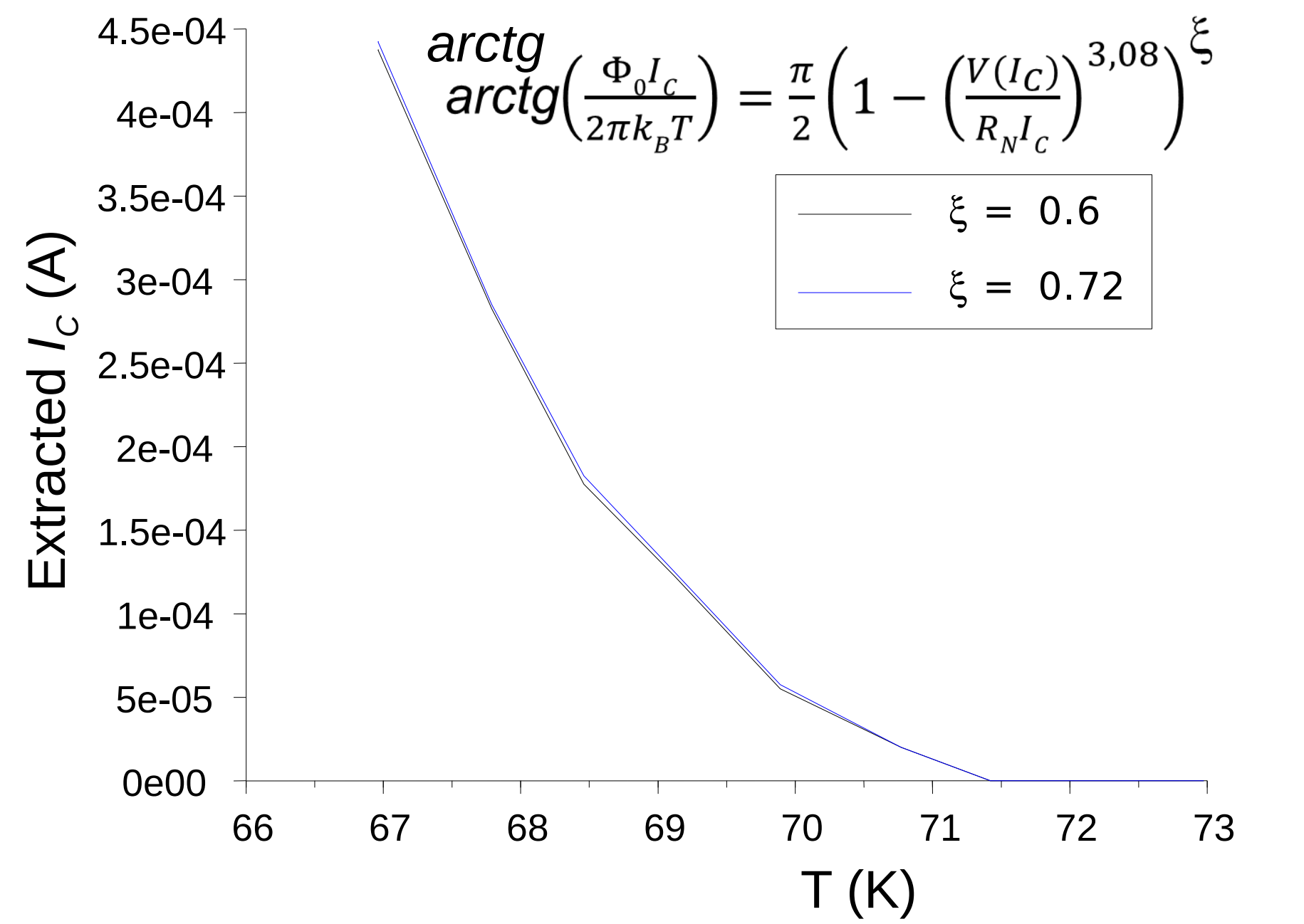
### Fixed Voltage Threshold



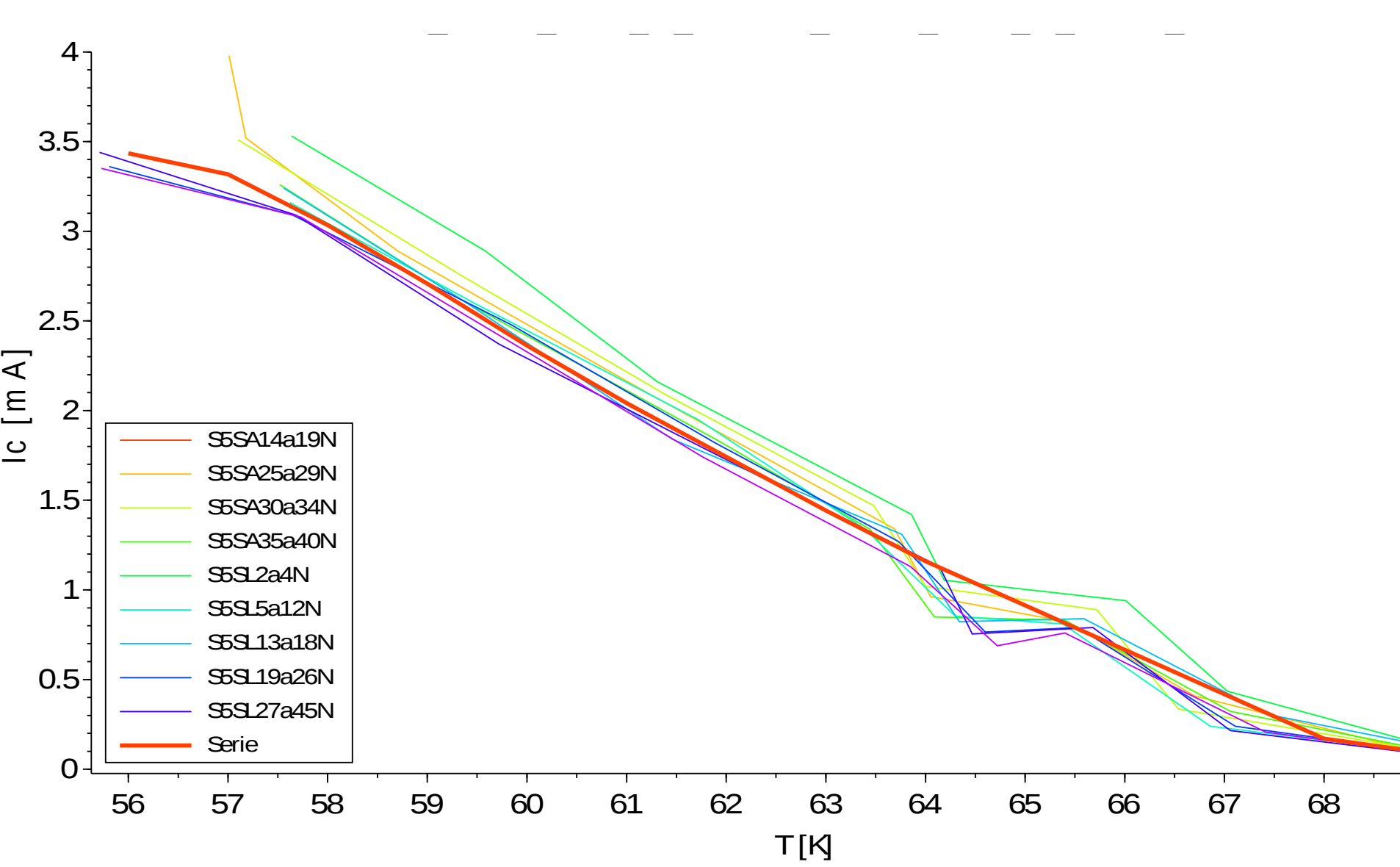
### Thermal Noise Voltage Threshold



## Moderate dependance of extracted $I_C$ values on $\xi$



## TNV method and scattering



The extracted  $I_C$  value for a series array is an average lying in the lower range of the  $I_{C_s}$  of its constituents (but larger than the minimum  $I_C$ , due to the larger voltage threshold).

## Conclusion

The expression we propose for the voltage measured at the terminals of an RSJ device biased at its critical current (TNV) is:

- analytical (fast),
- accurate (to within ~1% for a purely RSJ device),
-    tunable    with 2 parameters,
- useful for critical current determination from experimental results (provided  $R_n$  and  $T$  are known),
- basically robust against noise,
- applicable when either  $I_C=0$  or when the noise is very small.

It can be applied to series, parallel and 2D arrays of JJ.

Scattering in JJ parameters results in a weighted average of the critical current. This    average    is useful for choosing the bias point for operation of an array.