

UHV characterization of advanced materials and their coatings

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1st Workshop of ARIES PowerMat (WP17)

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ENGINEERING
DEPARTMENT

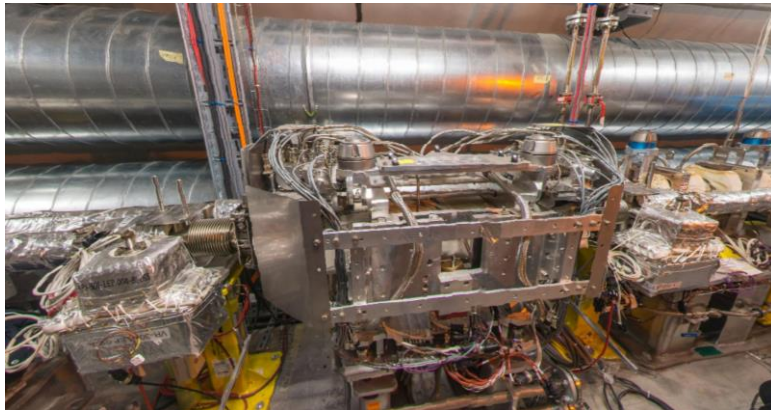
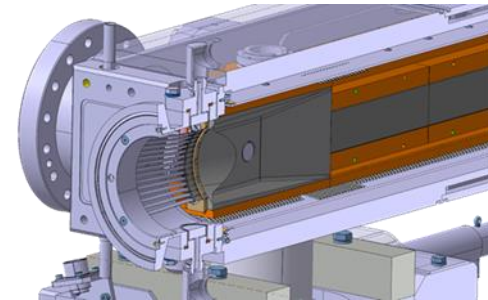


Outline

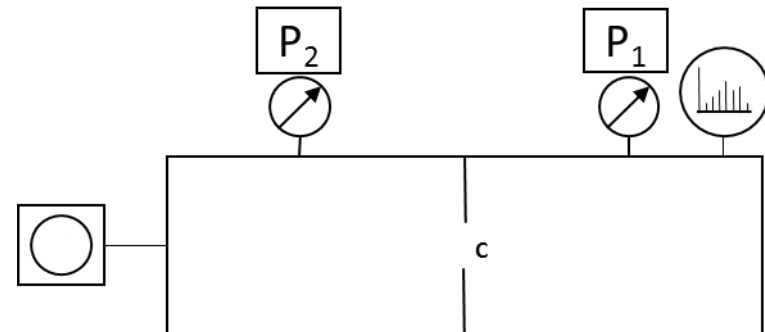
- Introduction: the LHC and the UHV
- Outgassing of collimator materials:
 - Graphite, CFC and MoGr
 - MoGr investigation – bulk material
 - MoGr investigation – coating
 - CuCD
- Conclusions and outlook

The UHV requirements

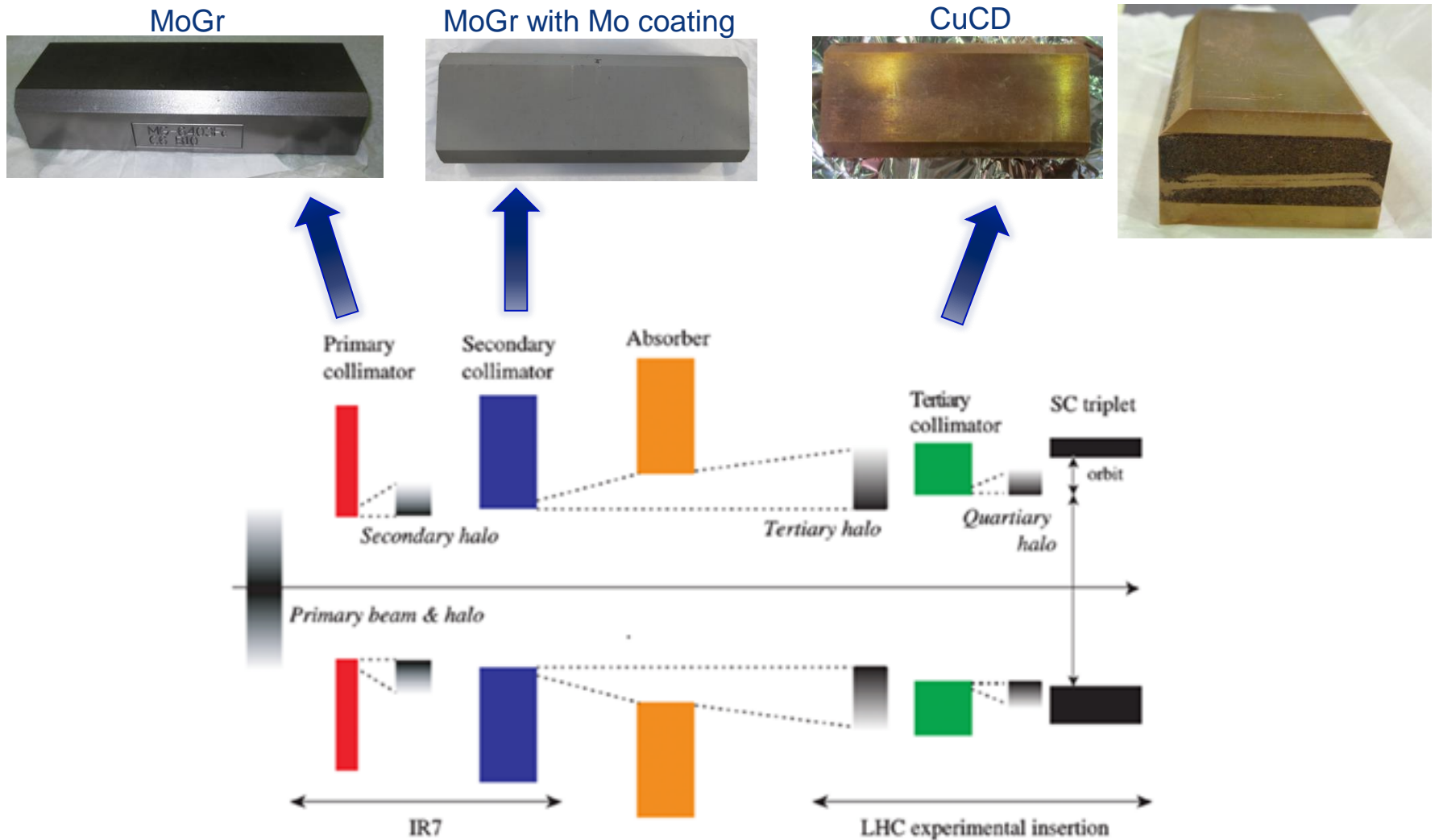
- In all the particle accelerators an high or ultra-high vacuum is required: beam stability and lifetime (beam-gas scattering)
- LHC vacuum acceptance limits for collimators:
 - Low outgassing rate ($1 \cdot 10^{-7}$ mbar·l/s)
 - No NEG saturation (N_2 , CO, CO_2 ,...)
 - Low SEY (ESD, electron cloud)



$$Q = (P_1 - P_2) \cdot C$$

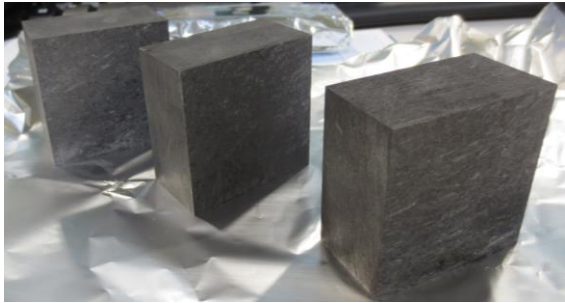


Collimation system upgrade

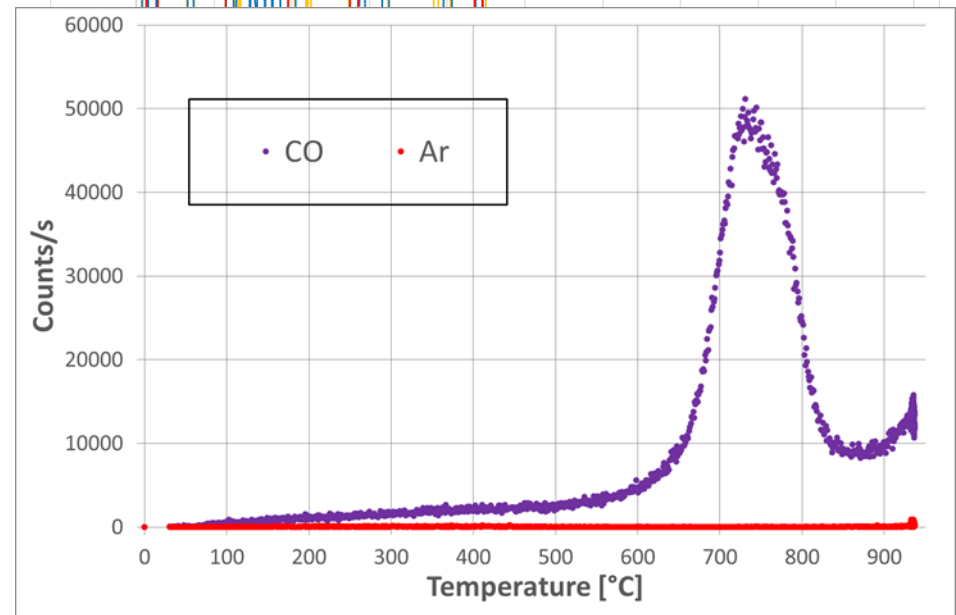
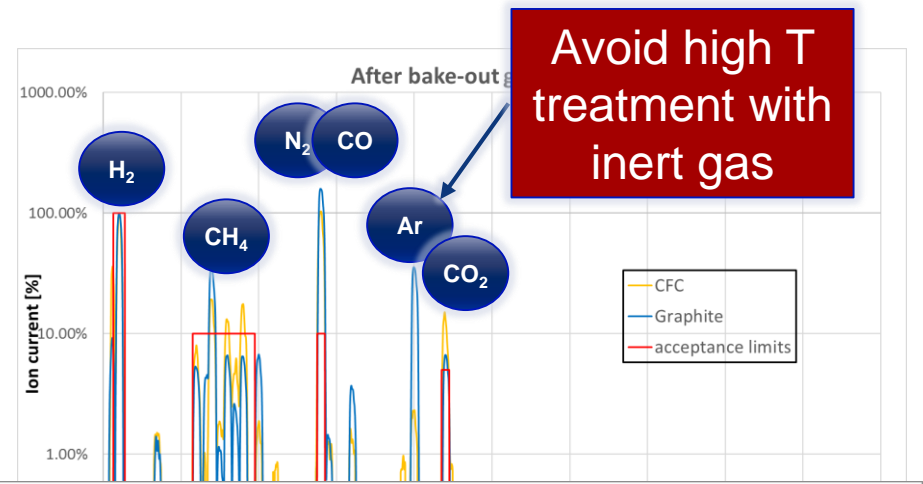
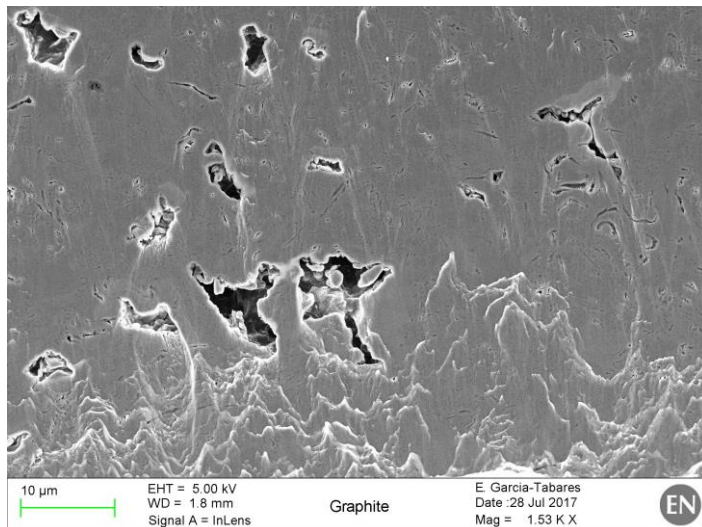


Graphite outgassing – Air content

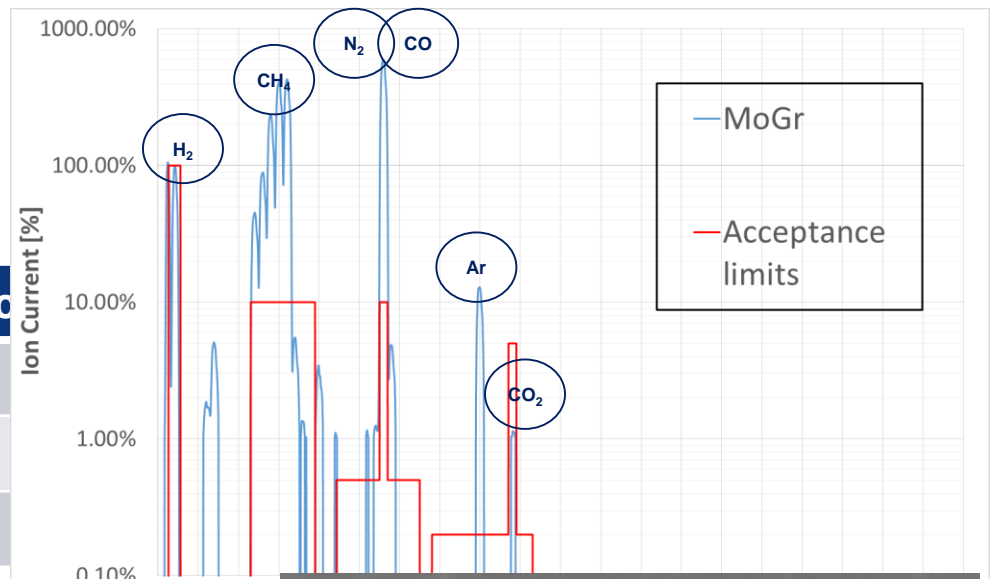
2D Carbon-Fibre-reinforced Carbon (CFC)



Graphite



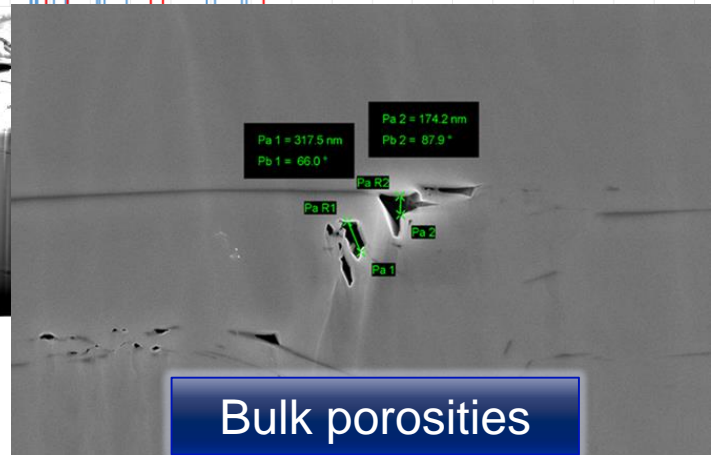
Molybdenum-Carbide Graphite



Material	Q_s [mbar-l/ s-cm ²]
MoGr	$1.9 \cdot 10^{-10}$
Graphite	$1.3 \cdot 10^{-11}$
CFC	$1.9 \cdot 10^{-11}$



Surface damage

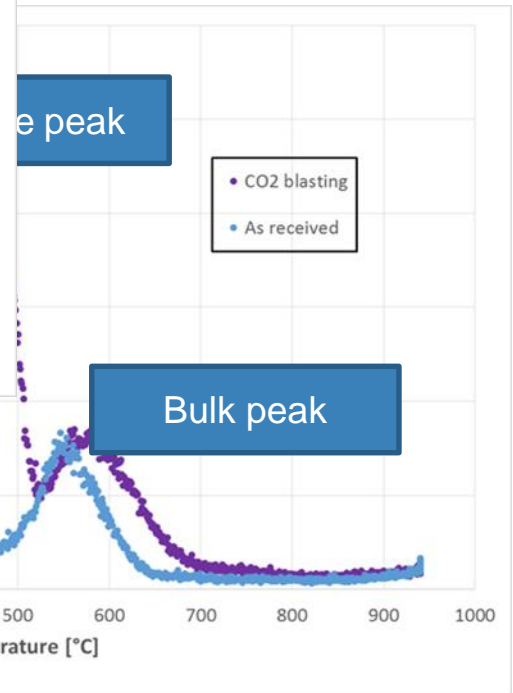
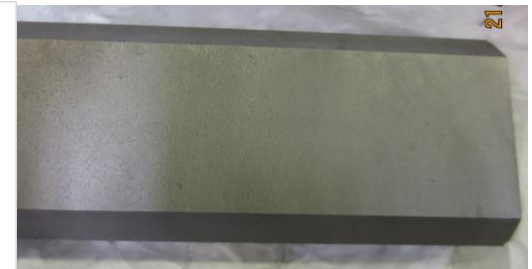
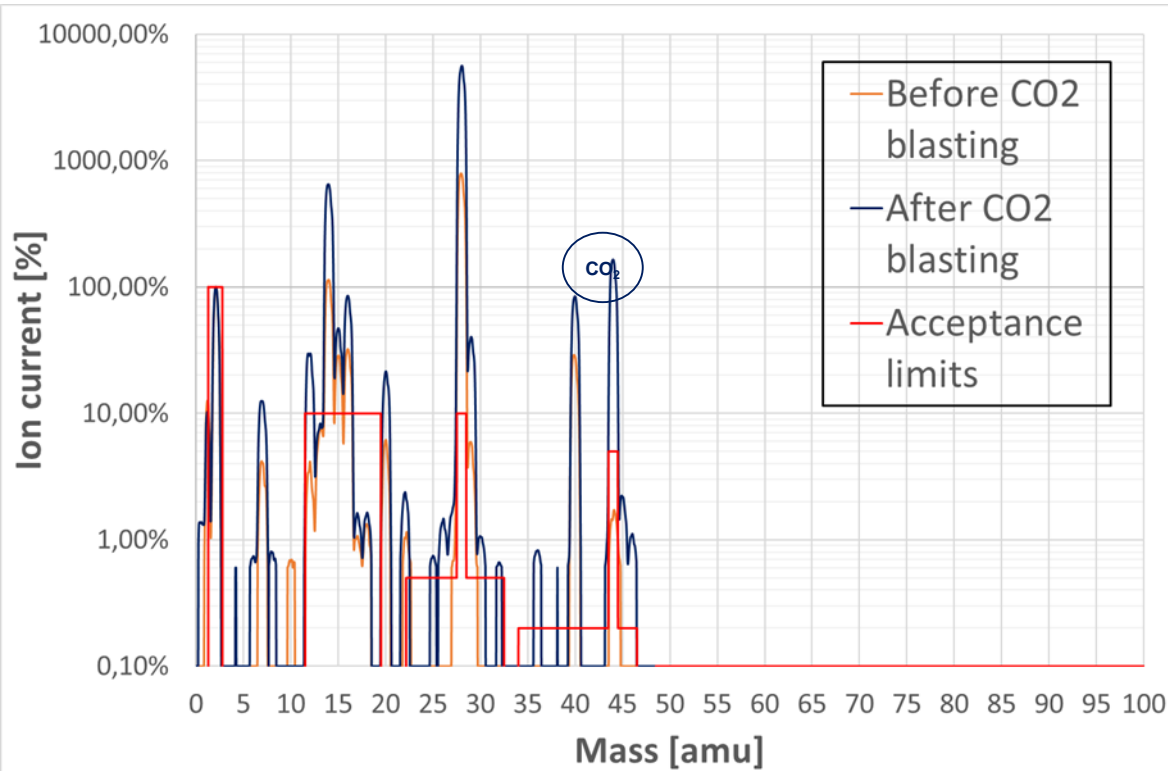


Bulk porosities

10 μ m ESB Grid = 0 V I Probe = 3.9 nA WD = 5.2 mm Detector = SE-TOPO 31 Mar 2017 Alexander
 EHT = 5.00 kV Mag = 2.13 K X 15:54:22 Lunt

1 μ m EHT = 5.00 kV WD = 2.1 mm Signal A = InLens C6 E. Garcia-Tabares Date :28 Jul 2017 Mag = 17.32 K X

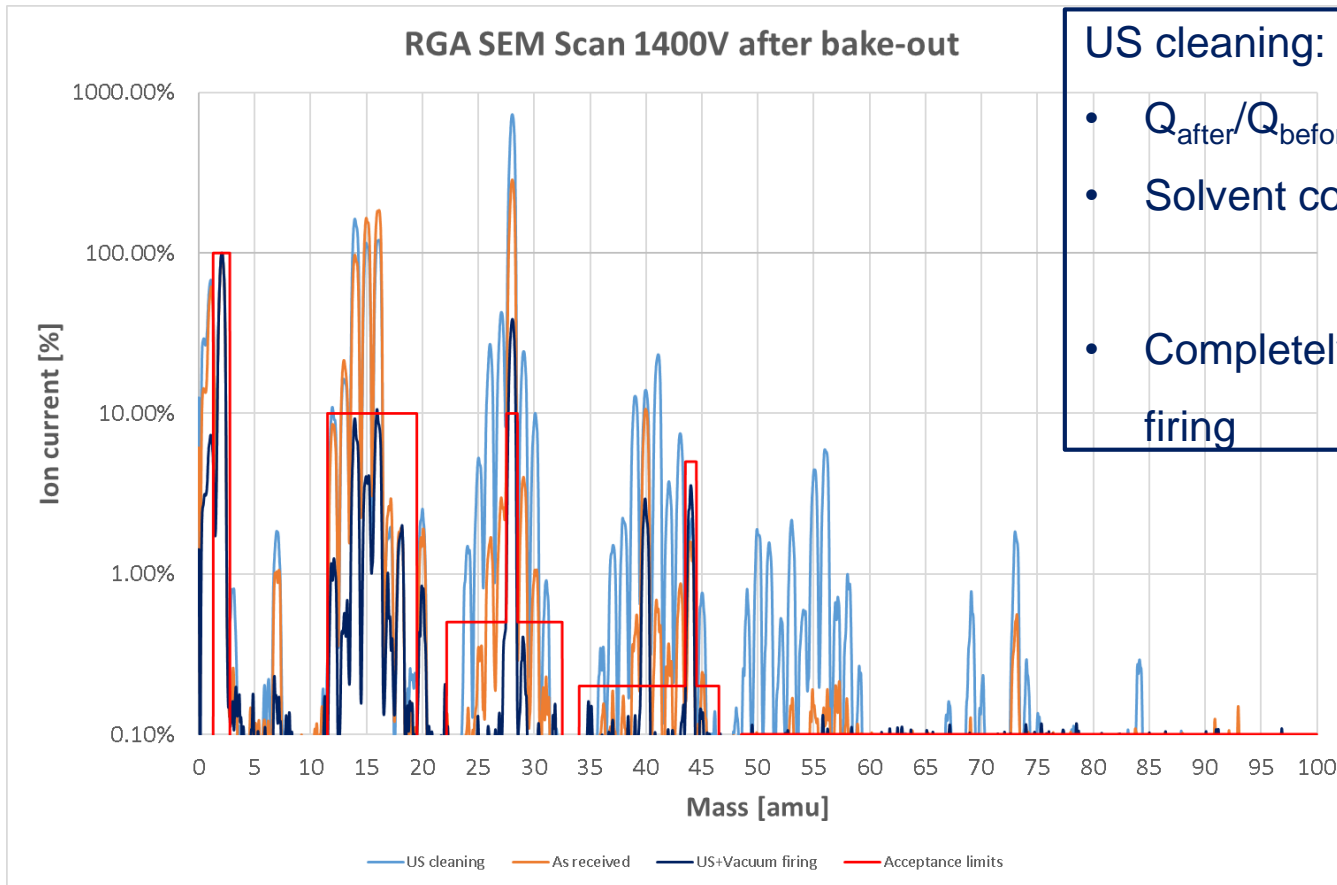
MoGr treatment



CO₂ blasting:

- $Q_{\text{after}}/Q_{\text{before}} = 50$
- CO₂ adsorption
- Air content (N₂, Ar) increased

US cleaning-last grade




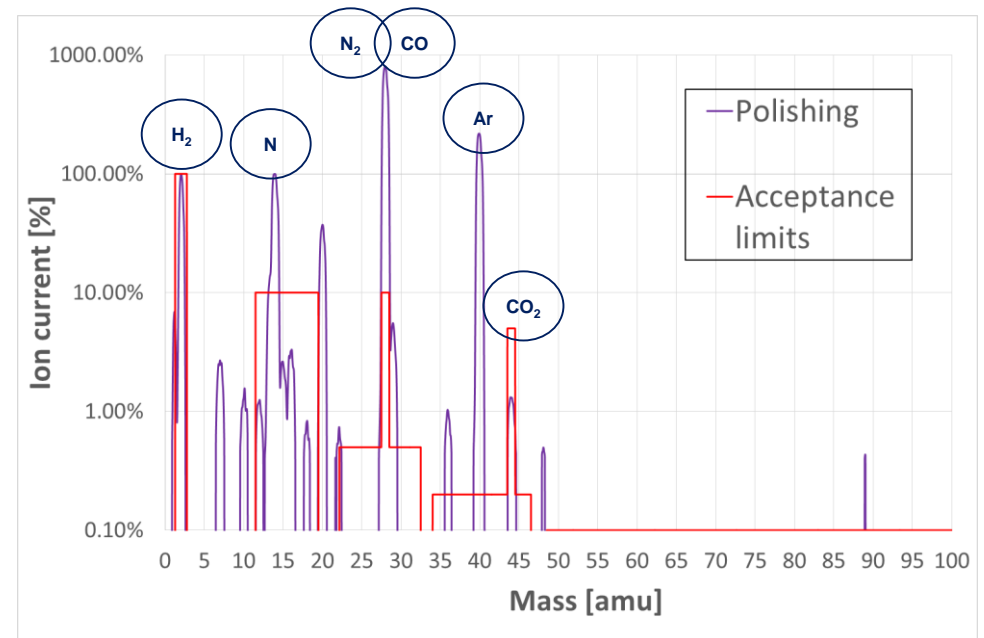
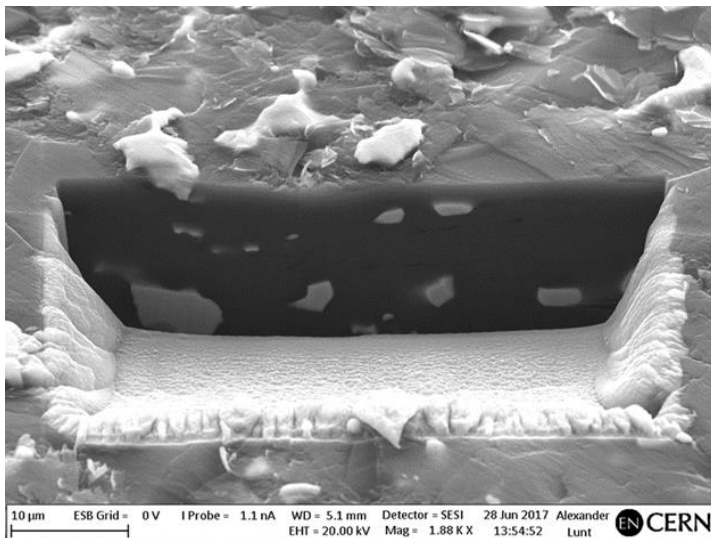
US cleaning:

- $Q_{\text{after}}/Q_{\text{before}} = 3$
 - Solvent contamination
- ↓
- Completely recovered after 48h firing

MoGr treatment

Diamond paste polishing (particle size $1\mu\text{m}$):

- $Q_{\text{jaws}} = 5.4 \cdot 10^{-7} \text{ mbar}\cdot\text{l/s}$ 
- Air still dominant
- Surface damage seems removed

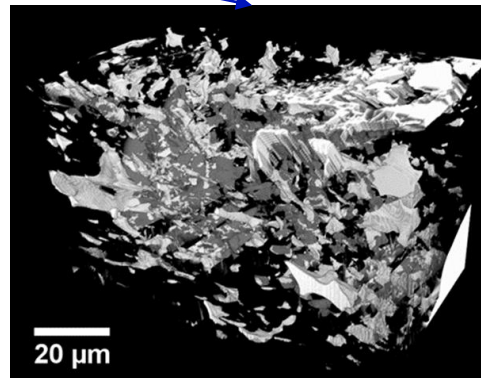
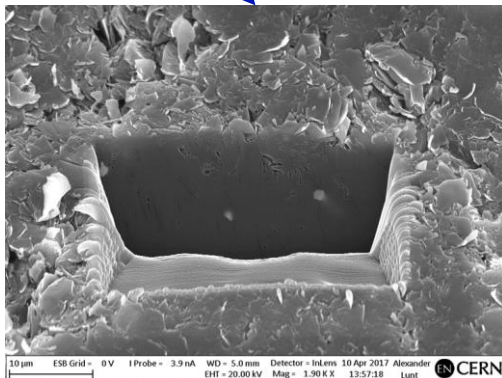
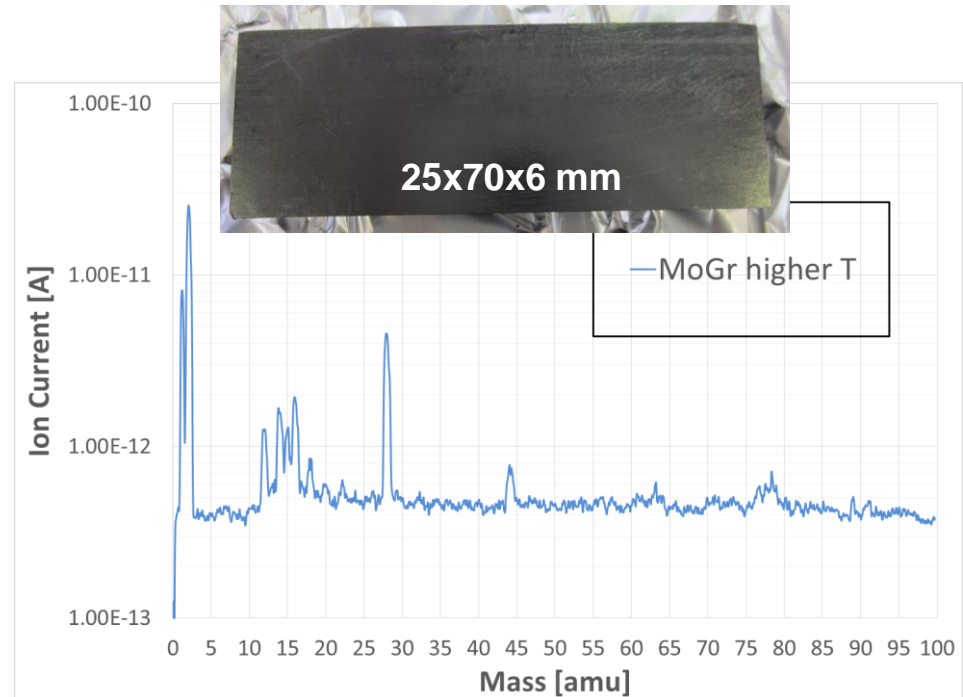


The **surface** plays a role (CO_2 blasting), but there should be also a **bulk contribution** to air trapping

Solution 1: Higher T process

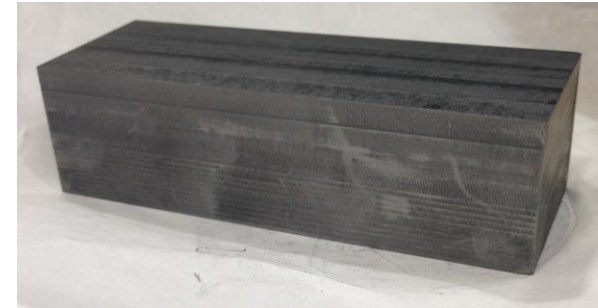
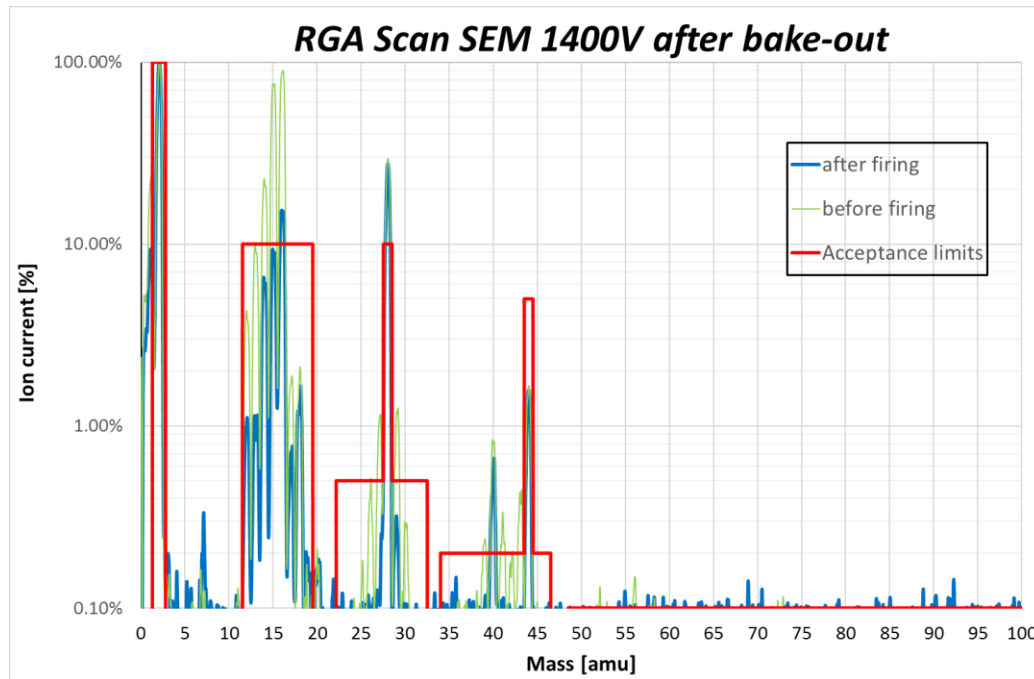
Higher temperature during production process:

- $Q_{\text{jaws}} = 3.1 \cdot 10^{-8}$ mbar·l/s
- H₂ dominated
- Similar surface damaged (FIB)
- Lower density: similar void fraction, lower carbide content (3D FIB)

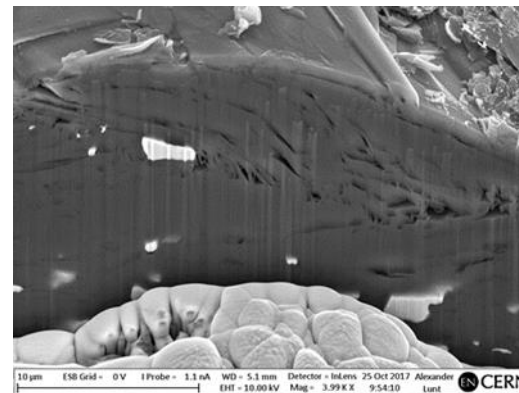
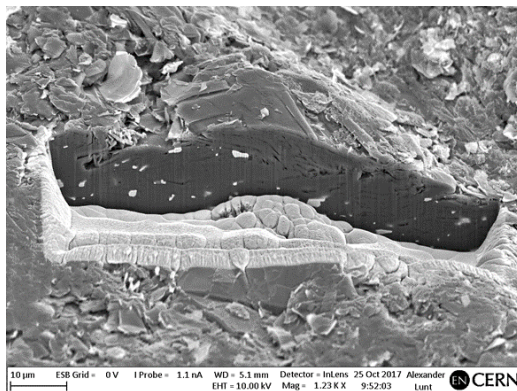


	Compliant sample	Non-compliant sample
%vol carbide	4.5	7.8
%vol void	5.1	5.7

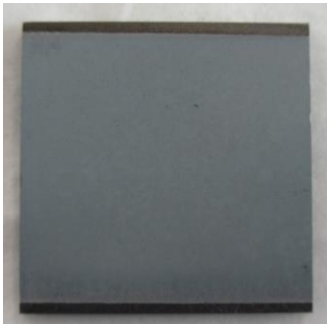
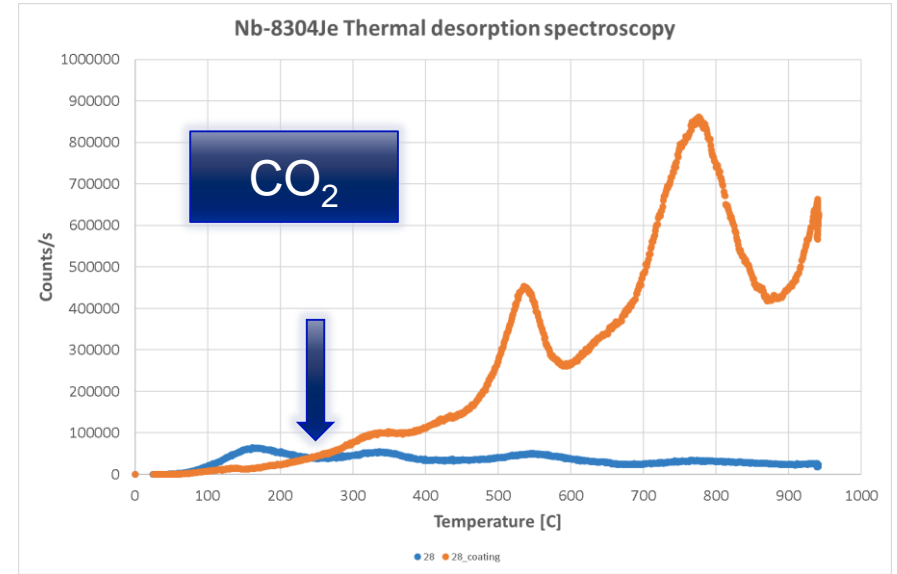
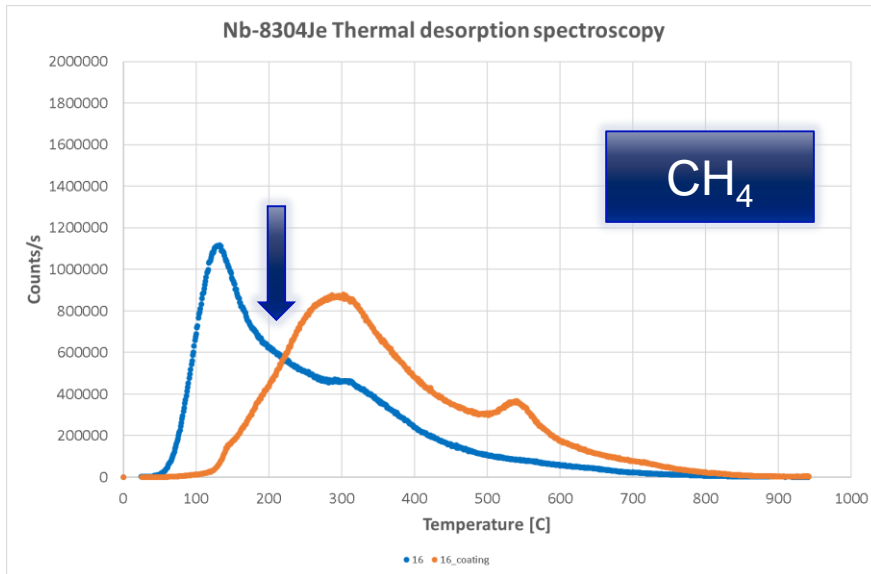
Solution 2: Different compaction



Material	Q_s [mbar·l/ s·cm ²]
As received	$4.7 \cdot 10^{-11}$
48h firing	$3.5 \cdot 10^{-12}$



Mo coating on MoGr – TDS

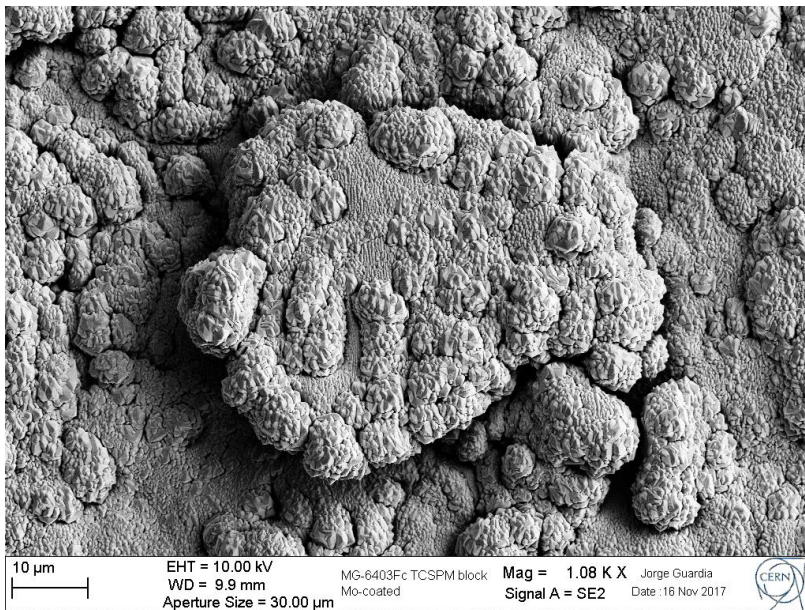


CO₂ blasted MoGr with Mo coating

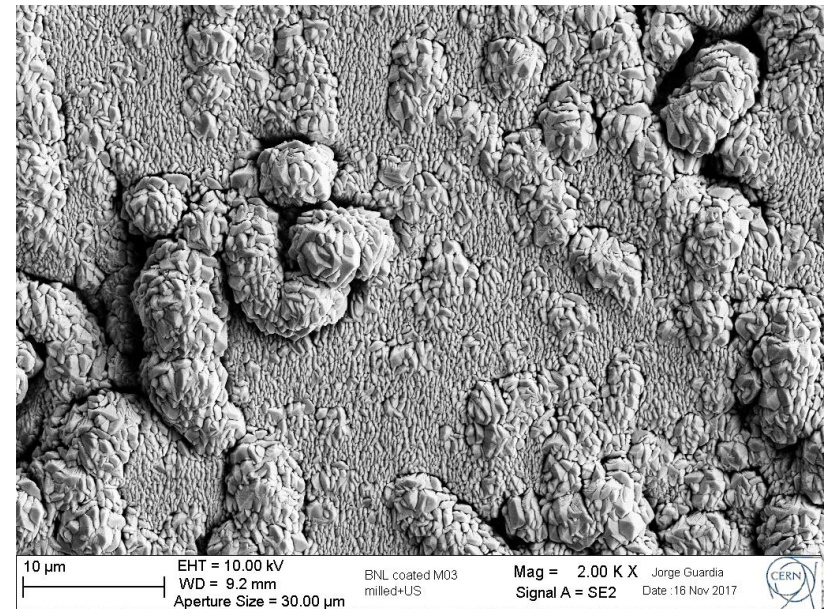
- The coating:
 - reduces the outgassing up to 200-250°C (oxide layer?)
 - increases the outgassing above these T (CO₂ blasting) → with a proper preparation should be compliant

Mo coating on MoGr – SEM

- Need to verify possible air trapping within the Mo layer



CO₂ BLASTING



US CLEANING

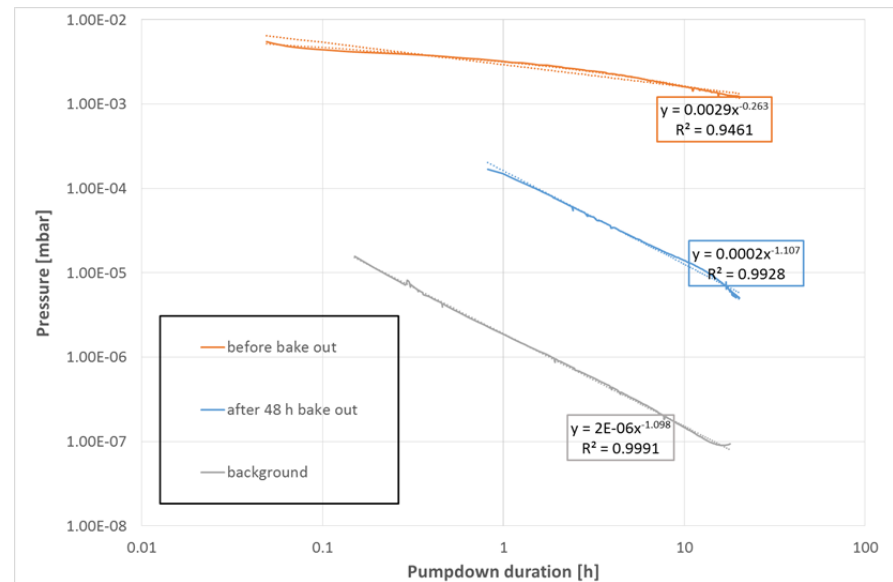
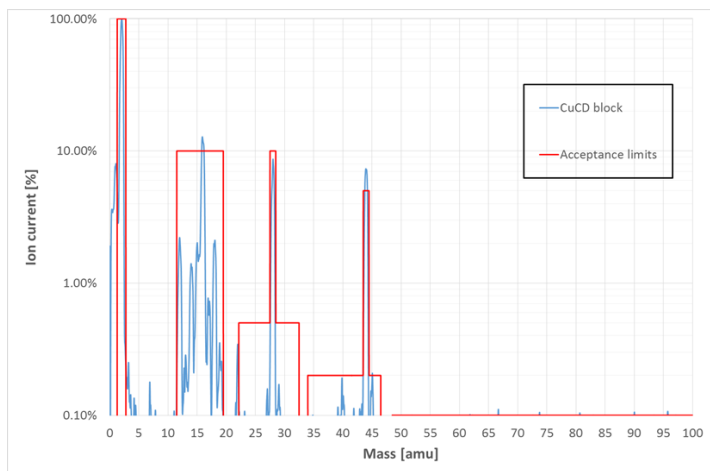
Copper-Diamond

- Robustness against accident situation: W alloy \rightarrow CuCD



- US cleaning before the test \rightarrow impossible to pump-down

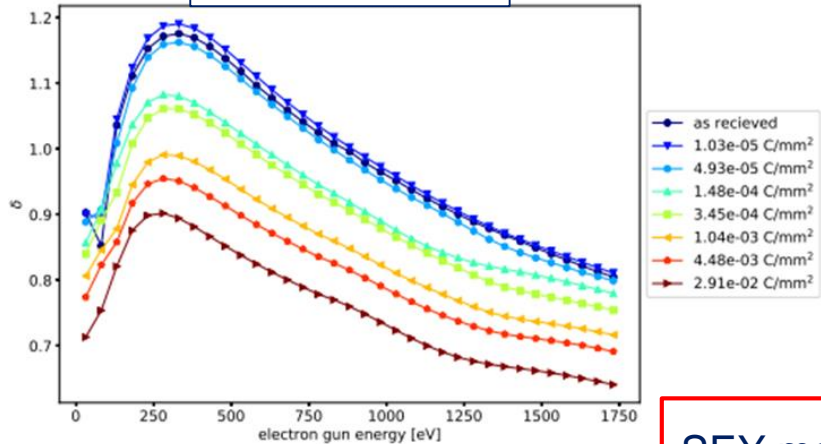
- After 48+24 h of bake-out at 250°C



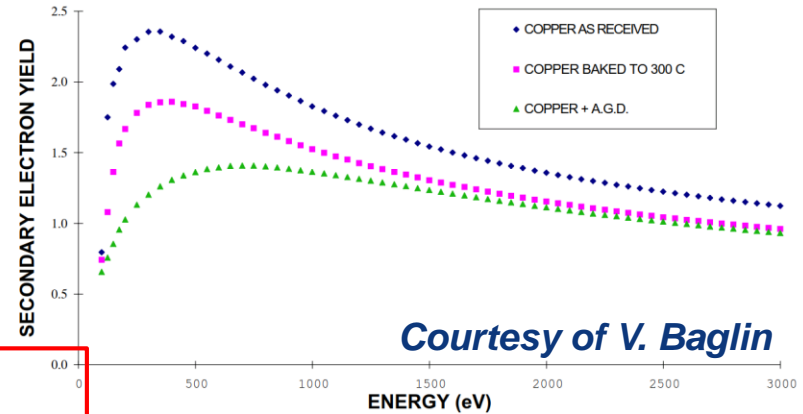
Material	Q_s [mbar·l/ s·cm ²]	Q_{jaws} [mbar·l/ s]
CuCD + cladding	$7.4 \cdot 10^{-12}$	$2.9 \cdot 10^{-8}$ ✓

Secondary Electron Yield

Graphite



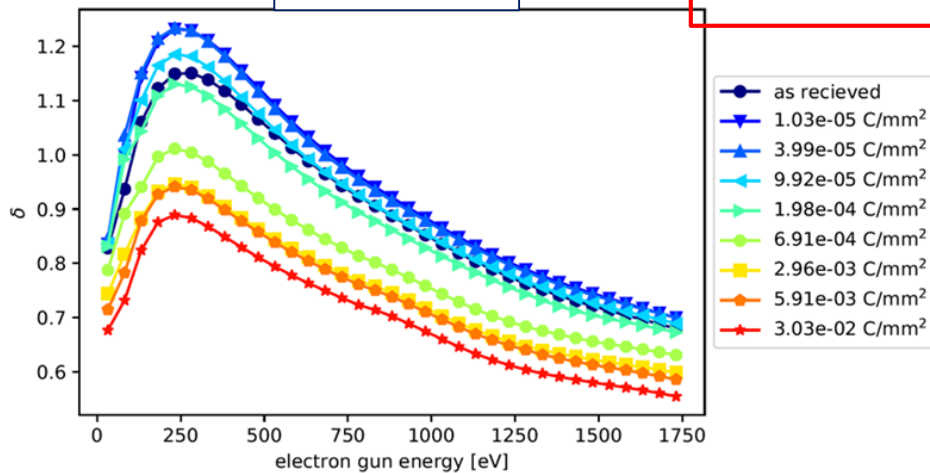
Copper



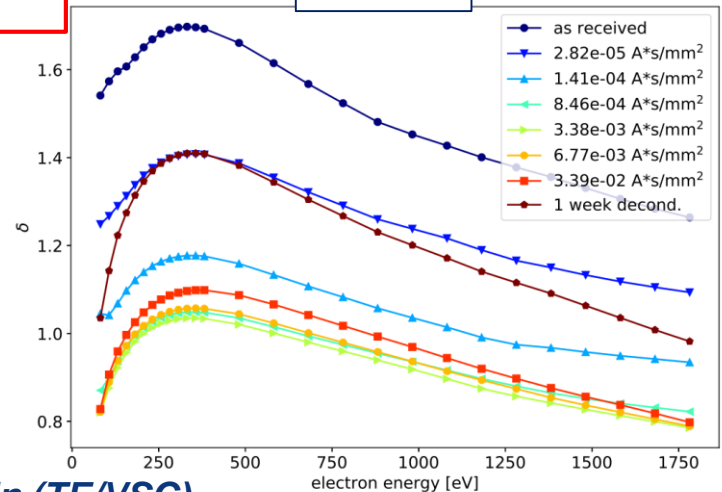
Courtesy of V. Baglin

SEY max
collimator ~ 1.4

MoGr



CuCD



Courtesy of D. Zanin (TE/VSC)

Conclusions and outlook

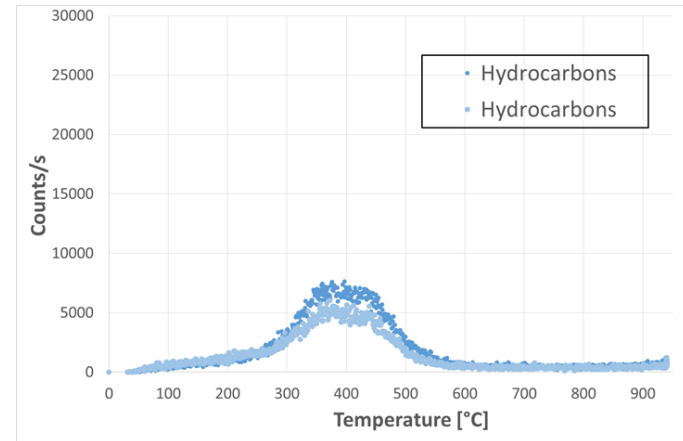
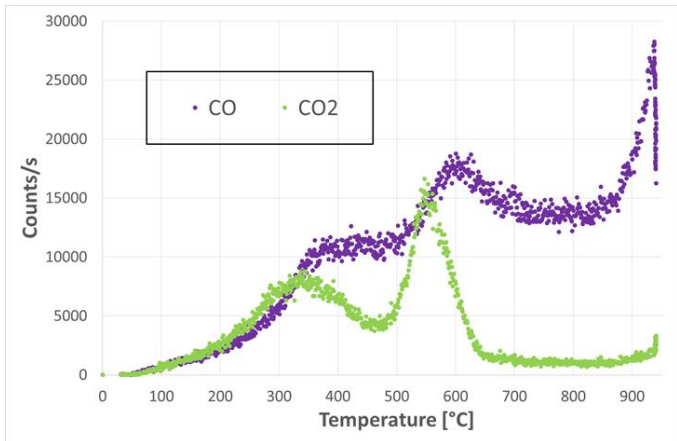
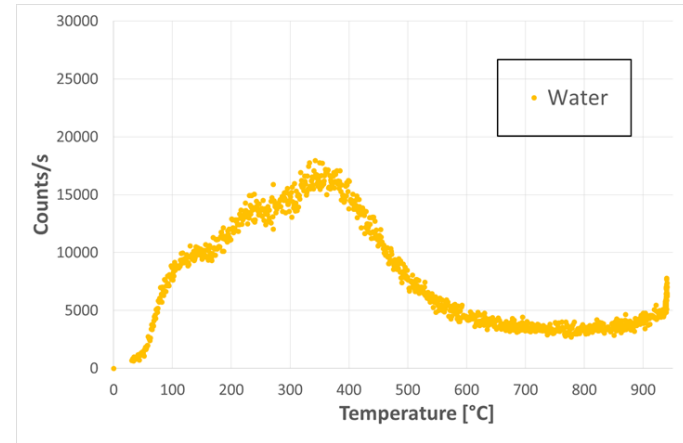
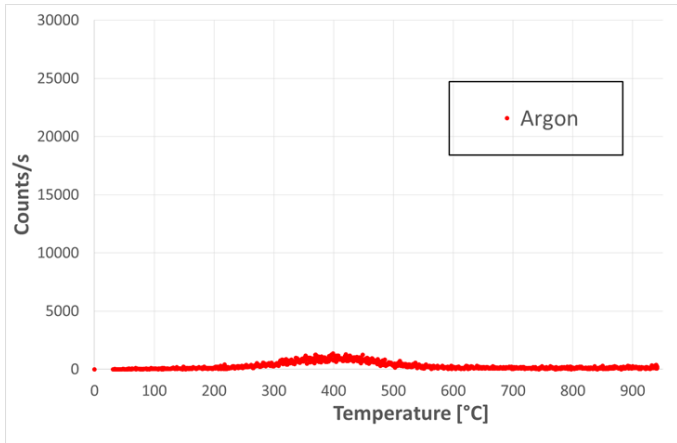
- A **complete** characterization (outgassing, TDS, microscopy, knowledge of the production process,..) is required to understand the phenomena
- Air content in MoGr has to be reduced during the **production**:
 - higher T (Reproducible? Why?)
 - under vacuum compaction
 - longer annealing
- CuCD: promising material, air exposure to be checked
- **Coating** characterization:
 - surface preparations effect on outgassing ✓
 - coating effect on outgassing (ongoing)
 - adhesion



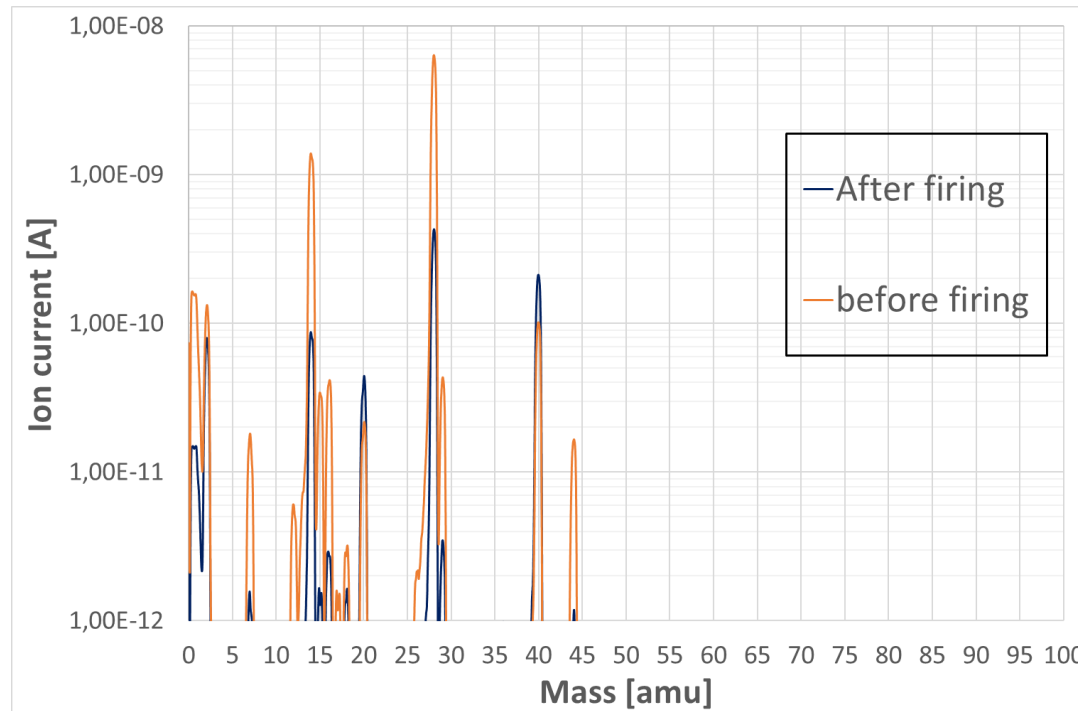
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Thank you for the attention!

TDS-MoGr



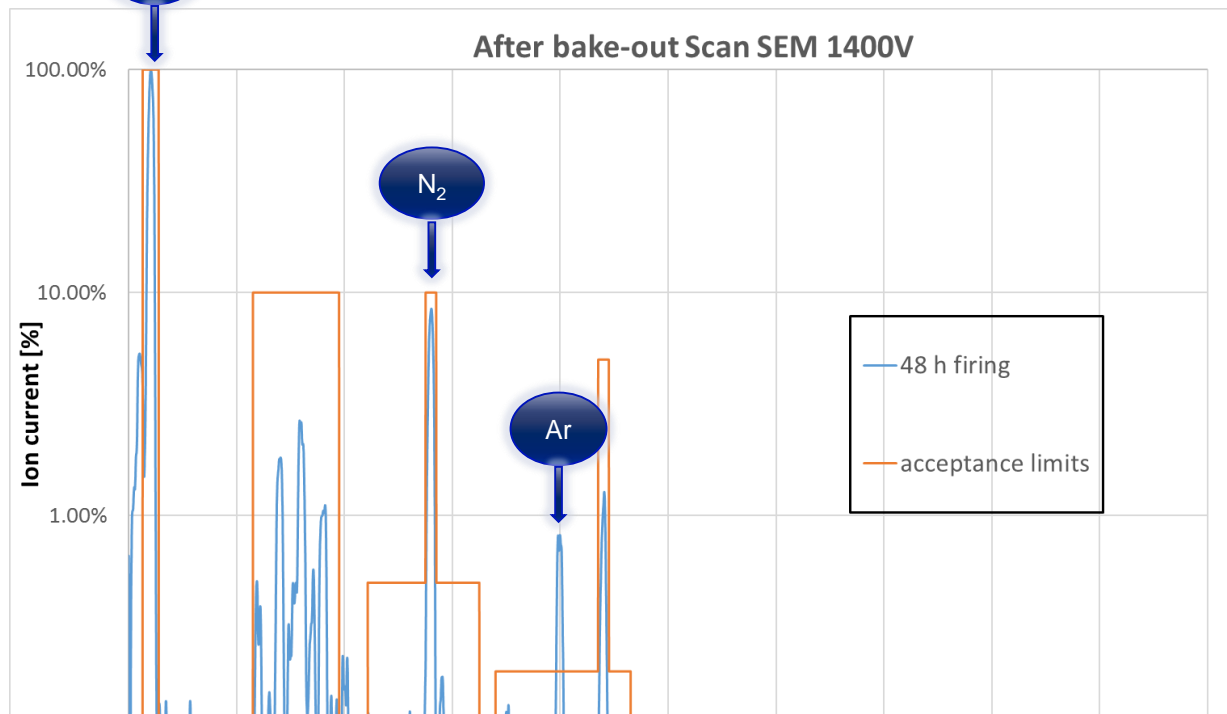
MoGr- 48h firing



48 h, 950°C vacuum firing:

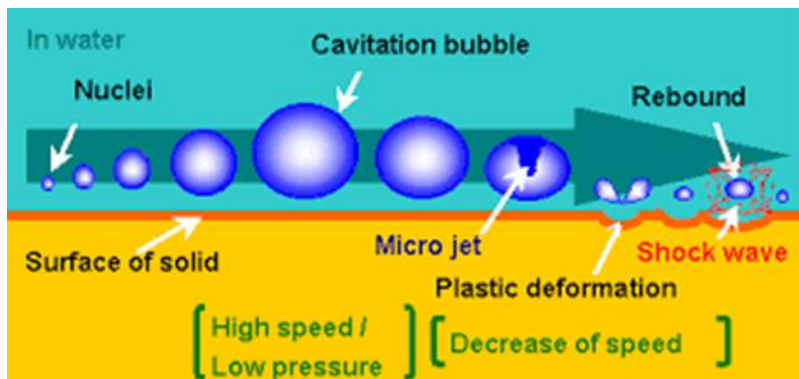
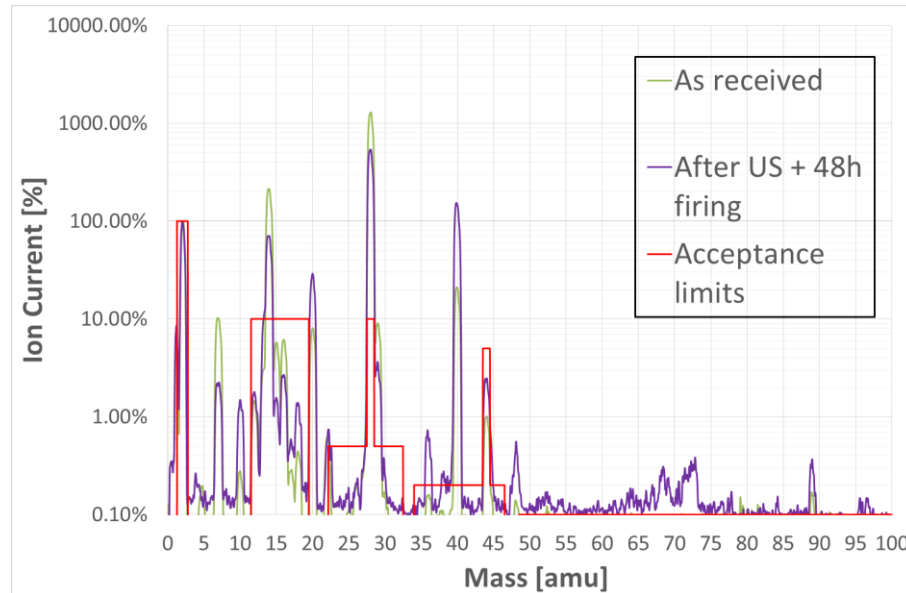
- $Q_{\text{before}}/Q_{\text{after}} = 7$, but still out of the limits (~ 2.5 for 2h firing)
- H_2 decreased
- N_2 decreased, Ar not

CFC- 48h firing



Treatment	Total outgassing [mbar*I/s]	Internal leak [mbar*I/s]
None	$7.5 \cdot 10^{-8}$ ❌	$8.3 \cdot 10^{-9}$ ❌
2h firing, 950°C	$1.1 \cdot 10^{-8}$ ✅	$5.7 \cdot 10^{-9}$ ❌
48h firing, 950°C	$6.9 \cdot 10^{-9}$ ✅	$3.5 \cdot 10^{-10}$ ✅

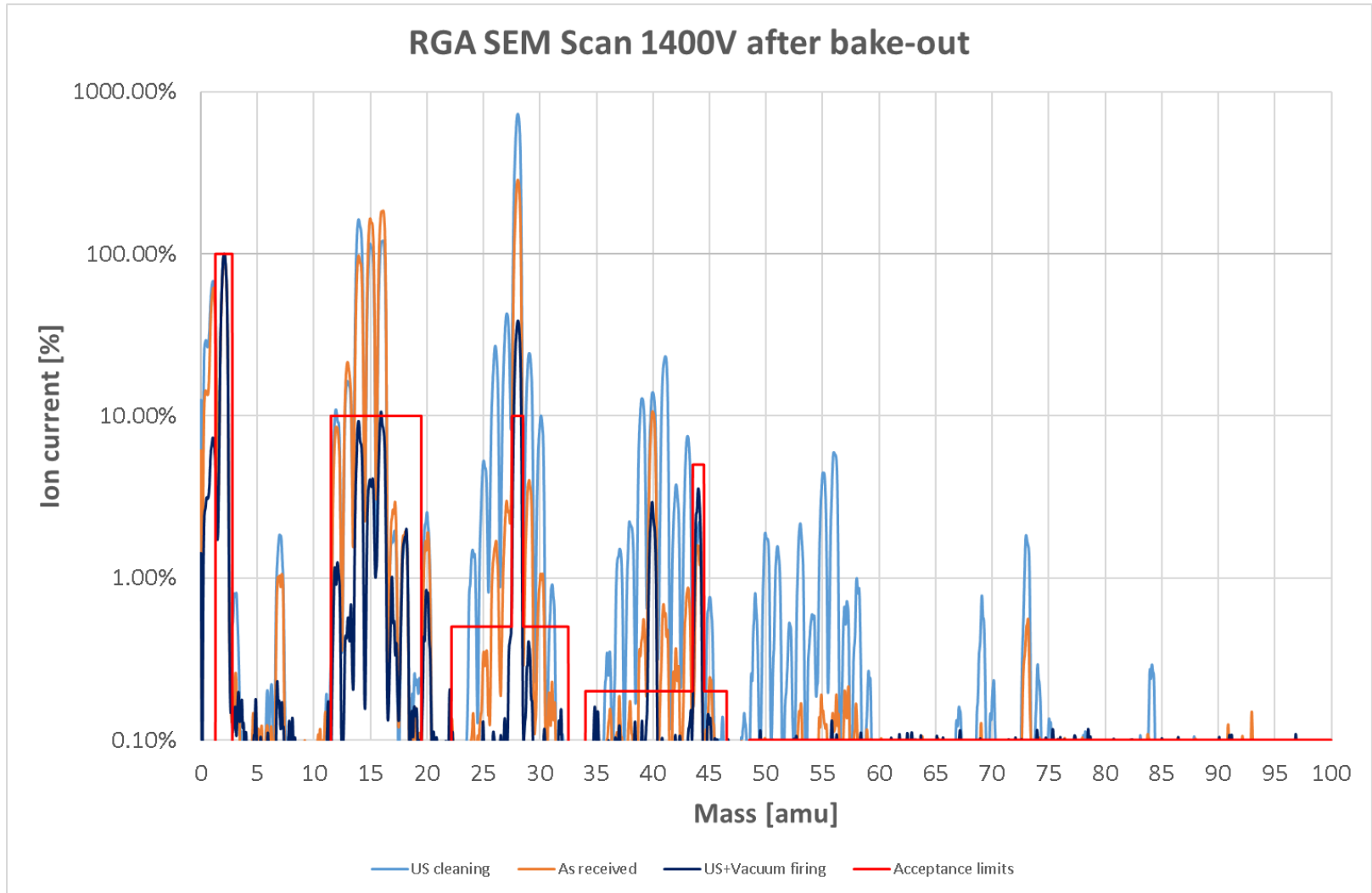
US cleaning-first supplier



US cleaning + 48 h firing:

- $Q_{\text{before}}/Q_{\text{after}} = 16$
 - N_2 decreased, Ar constant (normalized graph)
- result similar to just 48 h vacuum firing

US cleaning-last grade



Outgassing and thermal treatment

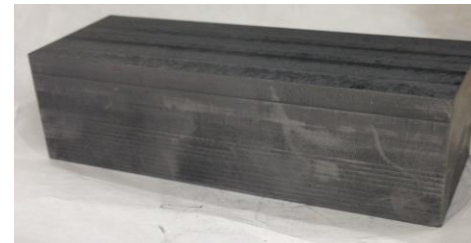
Grade	Thermal treatment	Total outgassing jaws [mbar*l/s]	Internal leak [mbar*l/s]	Gas analysis
<i>Nd-7301Cb</i>	VF 950°C 48h, Ar venting	$1 \cdot 10^{-8}$ ✓		✗
<i>Nd-7301Cb</i>	VF 950°C 48h, Ne venting	$2.5 \cdot 10^{-9}$ ✓	$2.2 \cdot 10^{-9}$ ✓	✓
<i>Nw-8301Ed</i>	None	$1.8 \cdot 10^{-7}$ ✗	$9.3 \cdot 10^{-9}$ ✗	✗
<i>Nw-8301Ed</i>	VF 950°C 48h, air venting	$1.4 \cdot 10^{-8}$ ✓	$5.3 \cdot 10^{-9}$ ✓	✓ ^{1.8}

↻ Reduction ~10 ↻ Reduction

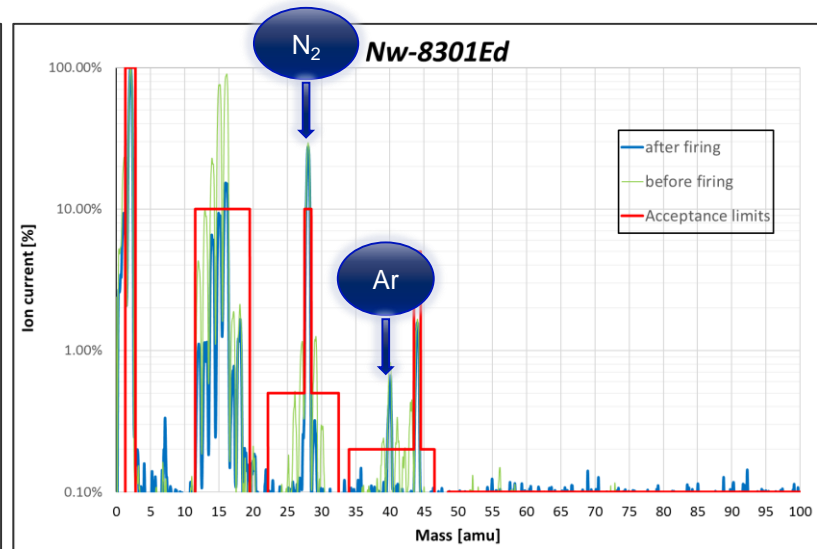
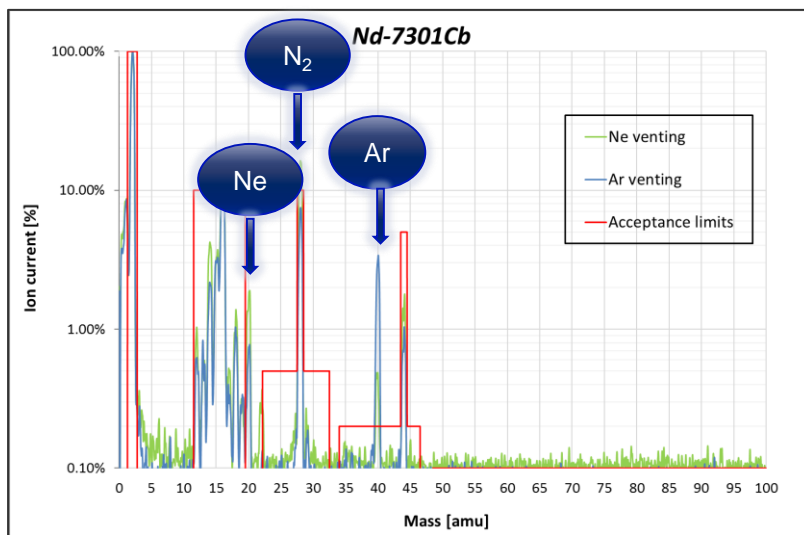
Nd-7301Cb



Nw-8301Ed



Gas venting after firing 48h

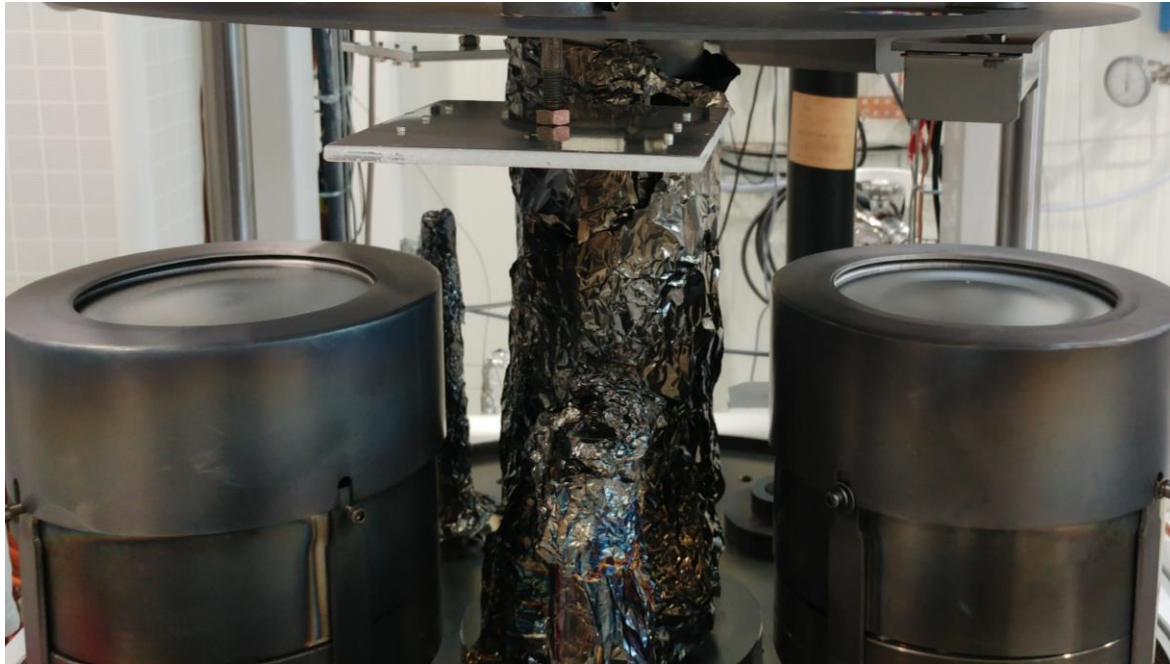


- H₂ dominated
- Adsorption of venting gas

- H₂ dominated
- CH₄ reduction

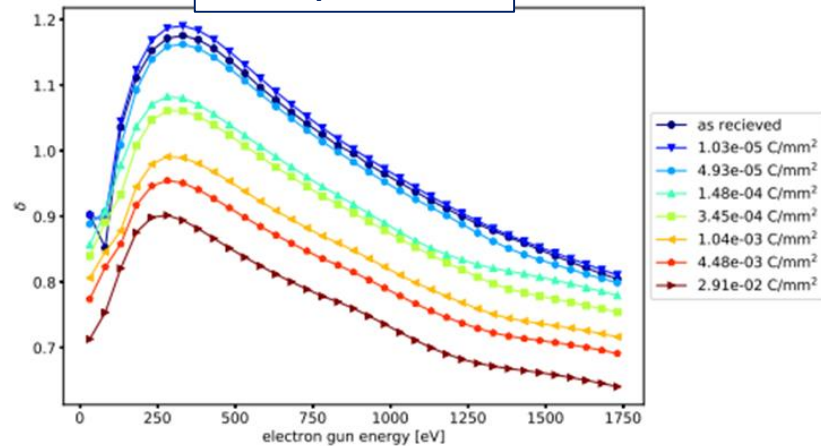


Mo coating machine



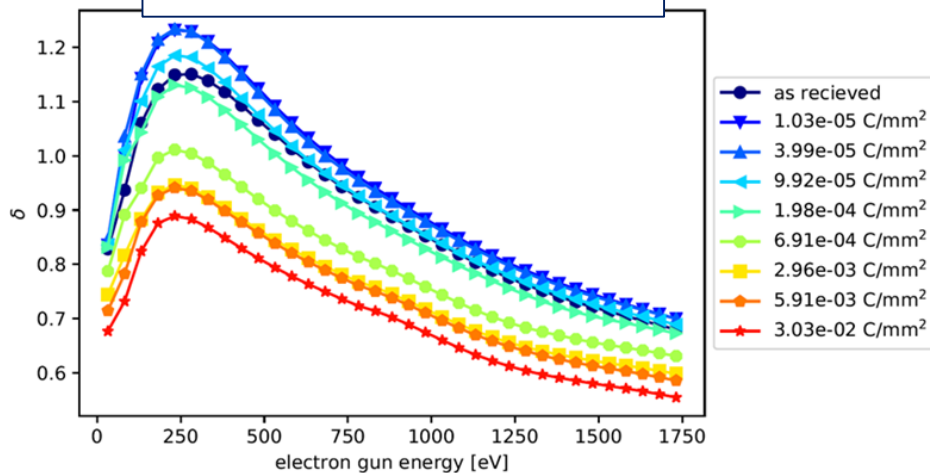
Secondary Electron Yield

Graphite ✓



SEY max
collimator~ 1.4

MoGr as received ✓



MoGr air exposure ✓

