

A detailed wireframe model of a particle accelerator complex, showing various circular and linear sections. The model is rendered in a light gray wireframe style, highlighting the intricate geometry of the facility. A large, prominent circular section is in the foreground, with other smaller sections and structures extending into the background.

# Results from recent investigations and characterizations at GSI

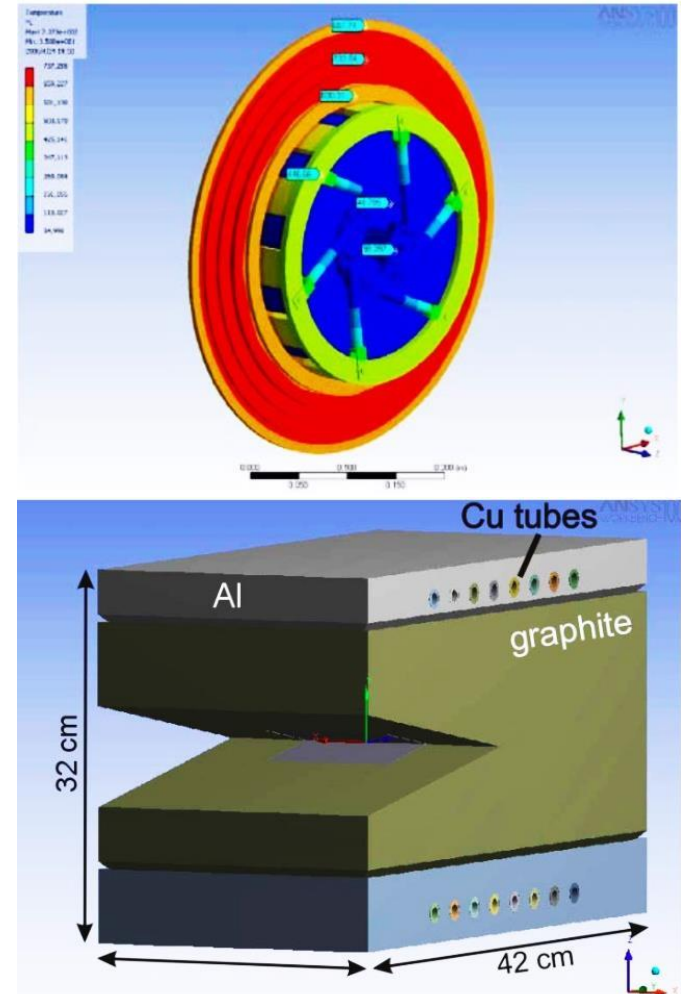
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Pascal Simon, Marilena Tomut

- Motivation
- Materials
- Structural characterization
  - Raman spectroscopy
  - Infrared thermography
- Functional characterization
  - Indentation
  - 3-point bending test
  - Laser flash analysis
- Conclusion and outlook

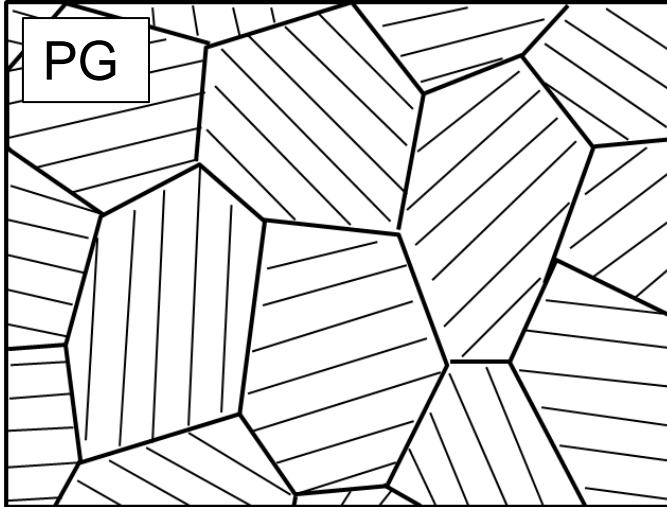
# Motivation

- Properties of graphite:
  - Low density
  - High thermal conductivity
  - Low coefficient of thermal expansion
  - High service temperature
- Graphite materials are used for:
  - Target wheel and beam catchers in Super Fragment Separator
  - Beam dumps in experimental caves
  - Collimators



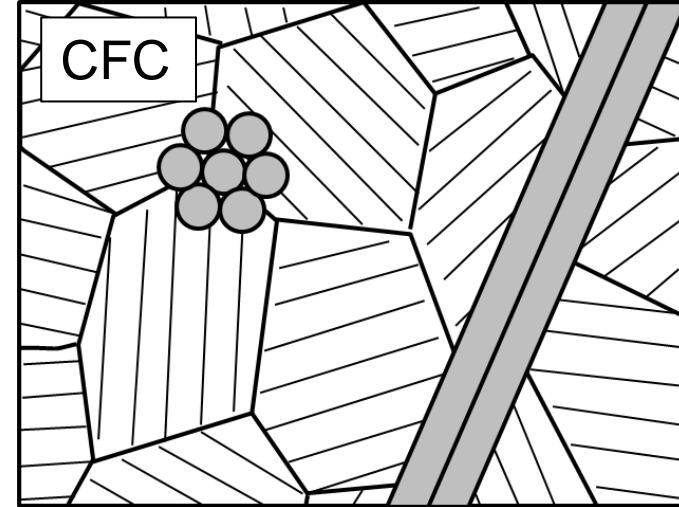
Super-FRS working group, 2008

- Polycrystalline graphite (PG)



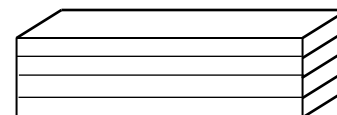
Material	Particle size [ $\mu\text{m}$ ]
R6300	20
R6500	10
R6550	10
R6650	7
POCO ZEE	1

- Carbon fibre reinforced carbon (CFC)



- 2 dimensional fibre orientation
- Fibre plane parallel or perpendicular to surface

In plane  $\parallel$



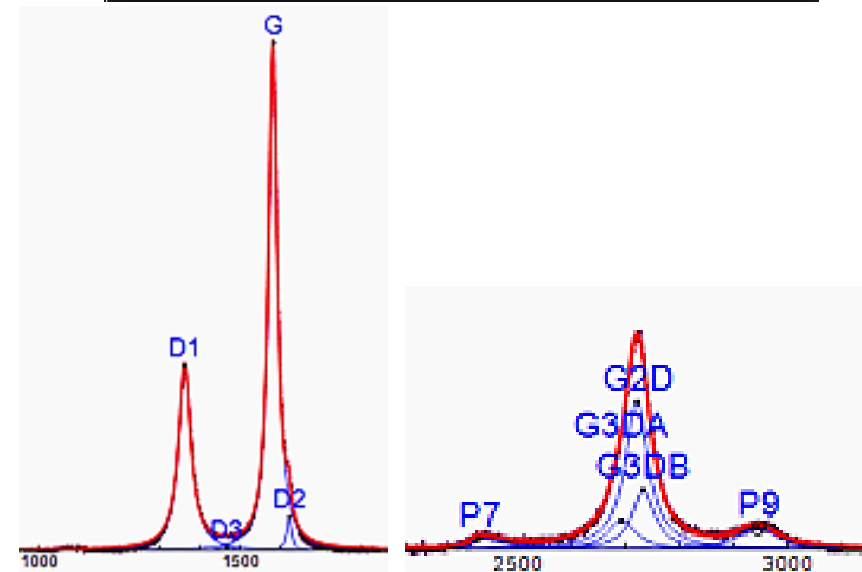
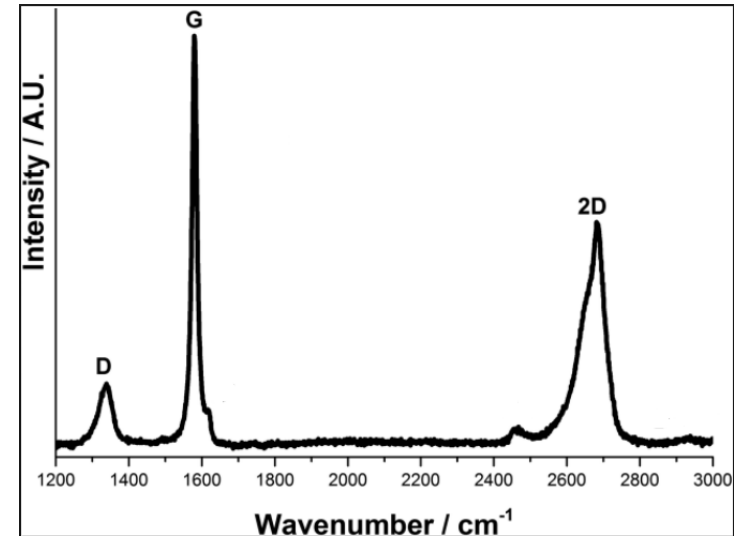
Transversal  $\perp$



# Structural characterization

## Raman spectroscopy

- Main peaks for graphite:
  - D-peak  $\approx 1380 \text{ cm}^{-1}$
  - G-peak  $\approx 1580 \text{ cm}^{-1}$
  - 2<sup>nd</sup> D-peak  $\approx 2700 \text{ cm}^{-1}$
- Ratio of  $I_D/I_G$  allows determination of defect concentration and lattice parameters
- Bands included for Raman spectra deconvolution:
  - D1-D3: Lorentzians
  - D2: Gaussian
  - G: Lorentzian
  - G'2D-G'3DA-G'3DB: Lorentzians
  - P7: Splitlorentzian
  - P9: Lorentzian

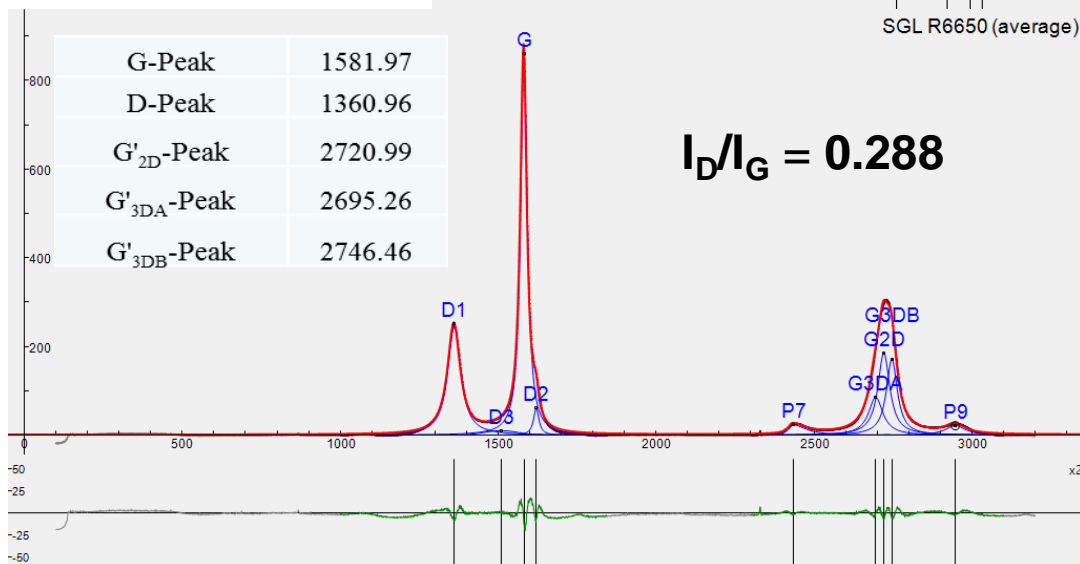
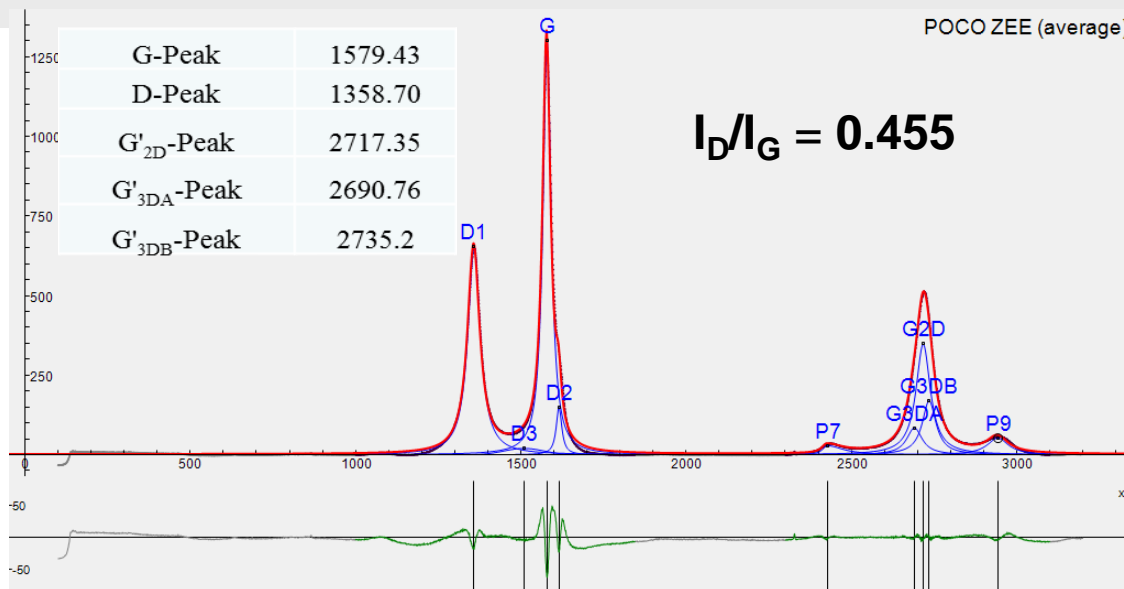


N. Larouche, B.L. Stansfield, Carbon N. Y. 48 pp. 620–629, 2009

# Raman results of isotropic polycrystalline graphite grades

## POCO ZEE

Particle size: 1  $\mu\text{m}$   
 Porosity: 20%  
 Pore size: 0.3  $\mu\text{m}$   
 Density: 1.77  $\text{g/cm}^3$

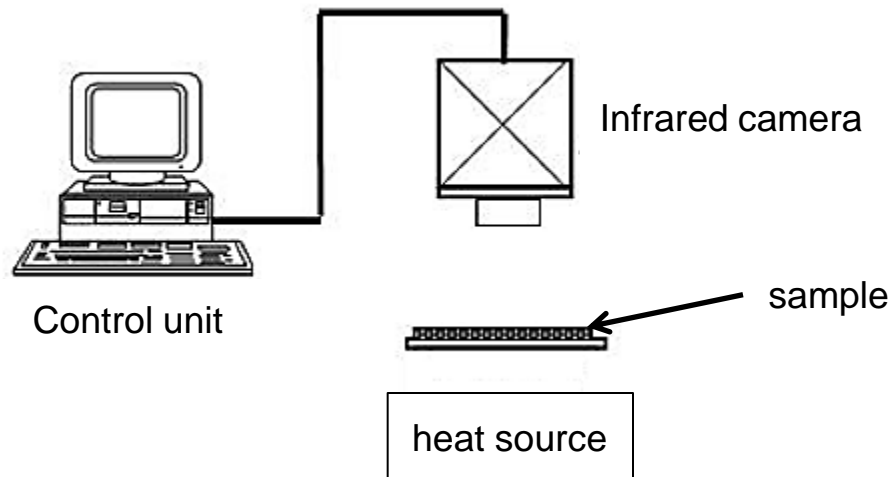


## SGL R6650

Particle size: 7  $\mu\text{m}$   
 Porosity: 10%  
 Pore size: 1.1  $\mu\text{m}$   
 Density: 1.84  $\text{g/cm}^3$

- Infrared thermography acquires and processes thermal information from non-contact measurement devices

## Experimental setup

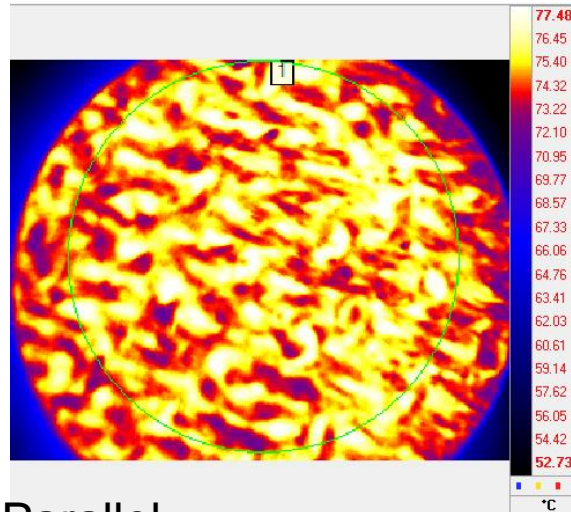


# Infrared thermography

## 2D-CFC

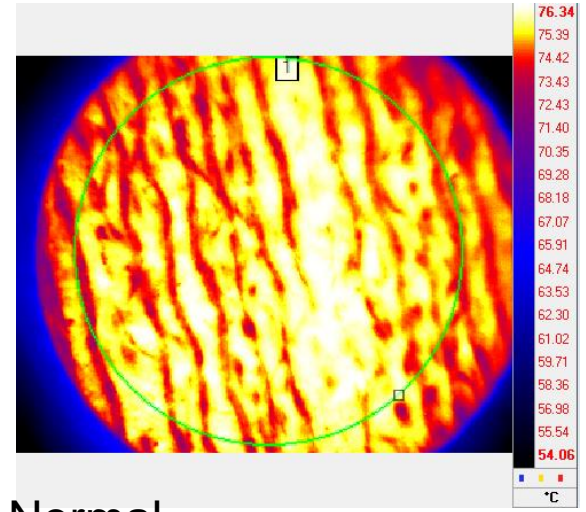
- SGL Mechanical

Fibre plane parallel to surface



Parallel

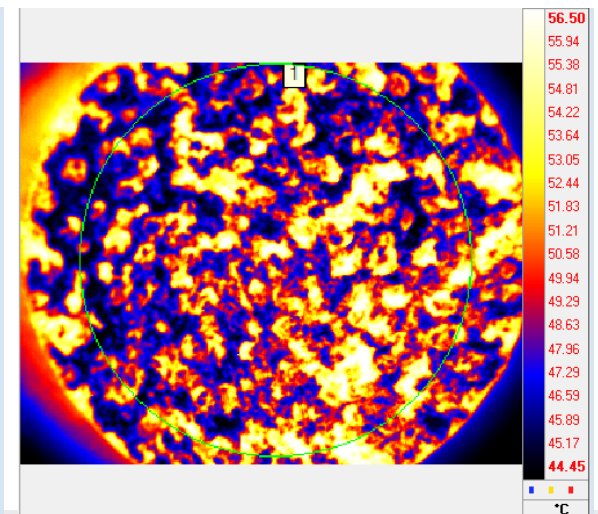
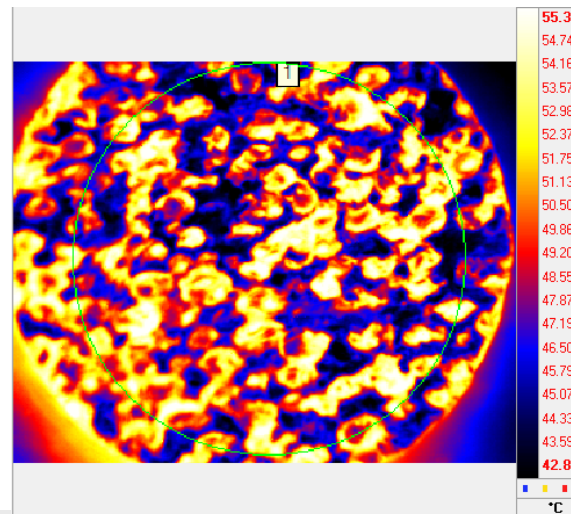
Fibre plane normal to surface



Normal

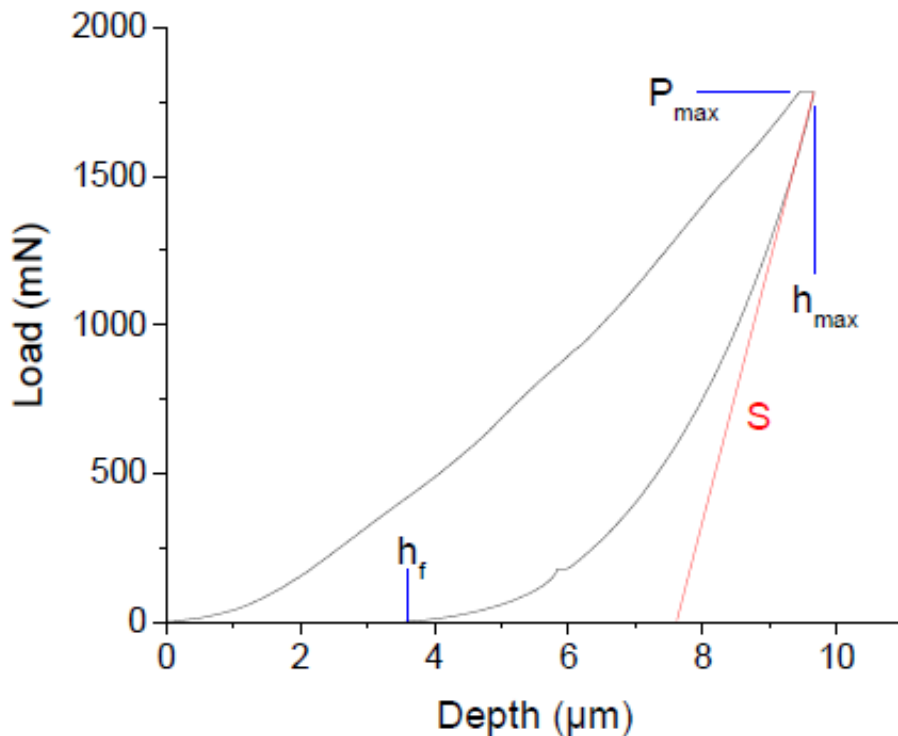
## Graphitic Foam

- POCO FOAM





# Functional characterization Microindentation



$\beta$  = Geometrical correction factor  
 $\vartheta$  = Poisson's ratio

Area function A:

$$A = 24.5 h_f^2$$

Hardness H:

$$H = \frac{P_{max}}{A}$$

Reduced modulus  $E_r$ :

$$E_r = \frac{\sqrt{\pi} \cdot S}{2 \cdot \beta \cdot \sqrt{A}}$$

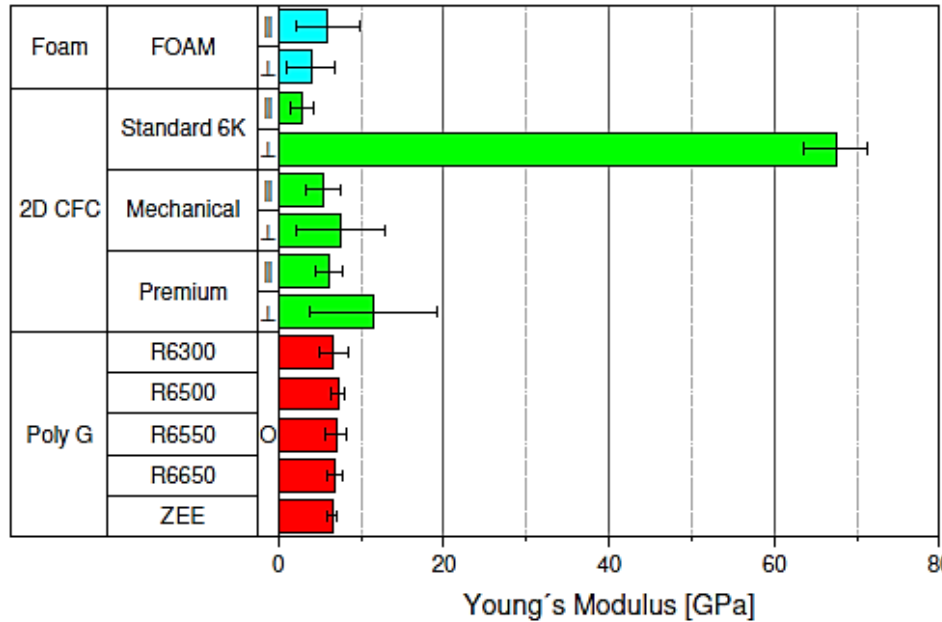
Young's modulus E:

$$\frac{1}{E_r} = \frac{1 - \vartheta^2}{E} + \frac{1 - \vartheta_i^2}{E_i}$$

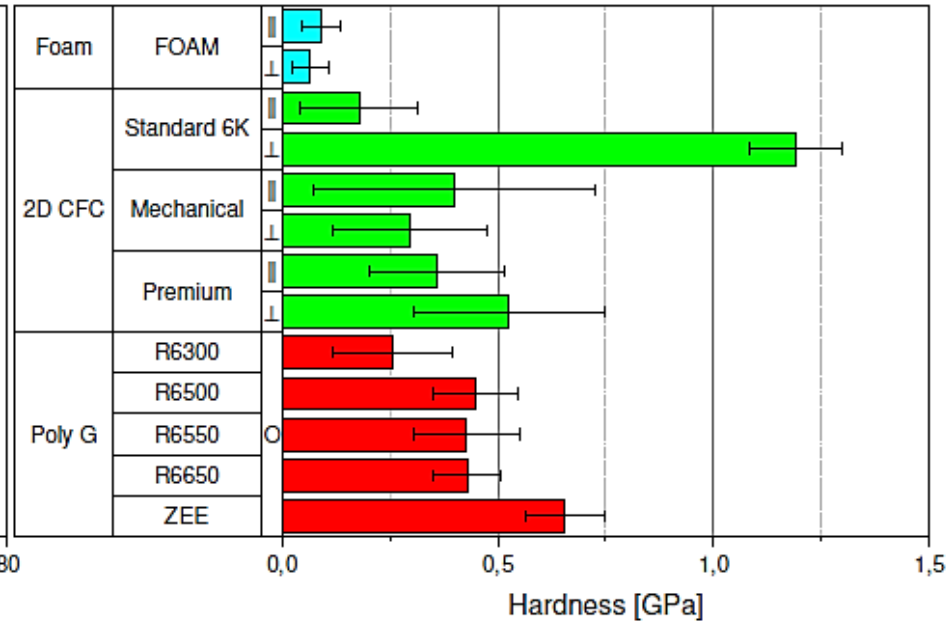
Oliver and Pharr, *J. Mater. Res.*, vol. 7, no. 6, pp. 1564-1583, 1992

# Microindentation of investigated materials

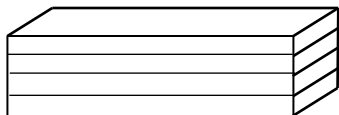
## Young's modulus



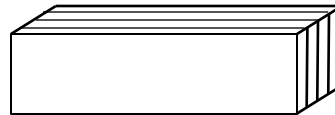
## Hardness



In plane  $\parallel$

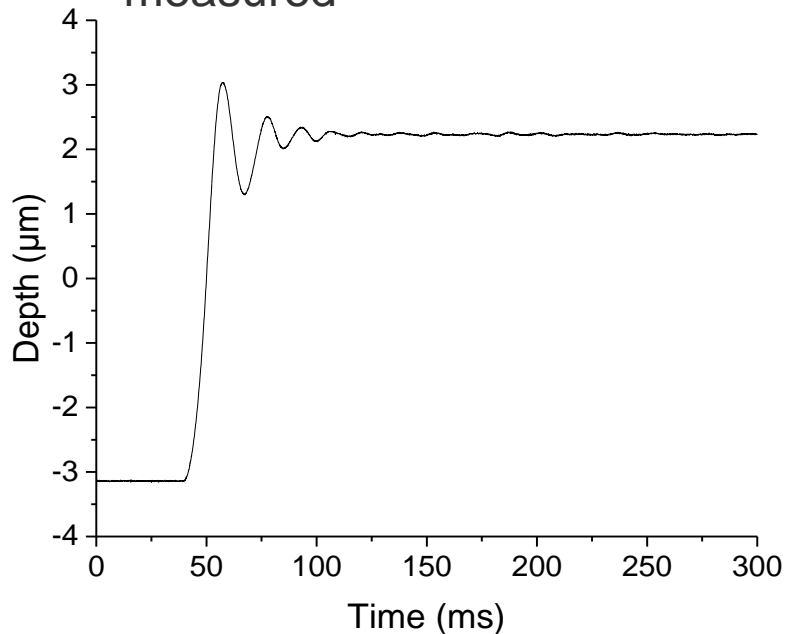


Transversal  $\perp$



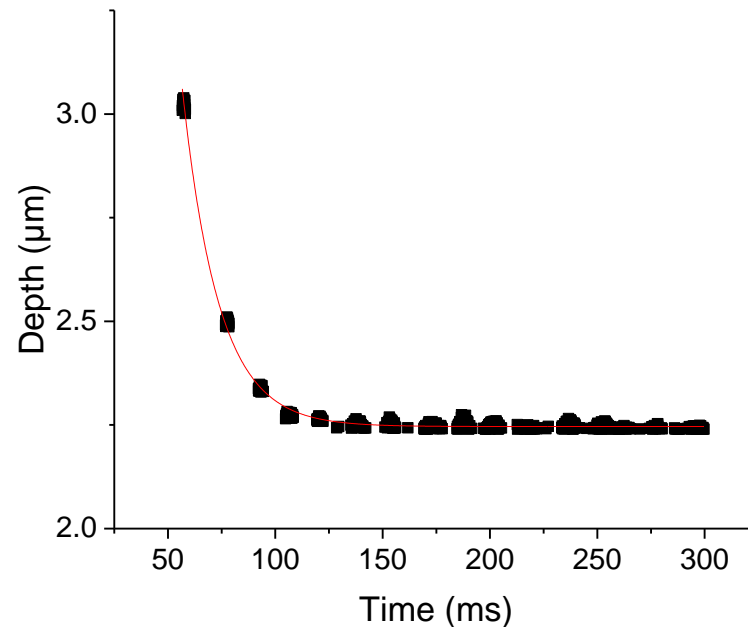
Material	Particle size [ $\mu\text{m}$ ]
R6300	20
R6500	10
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R6650	7
POCO ZEE	1

- Indenter is accelerated with constant force towards the sample
- Resulting bouncing of the indenter on the surface of the sample is measured



Dynamic hardness DH:

$$DH \propto \frac{v_{out}}{v_{in}}$$

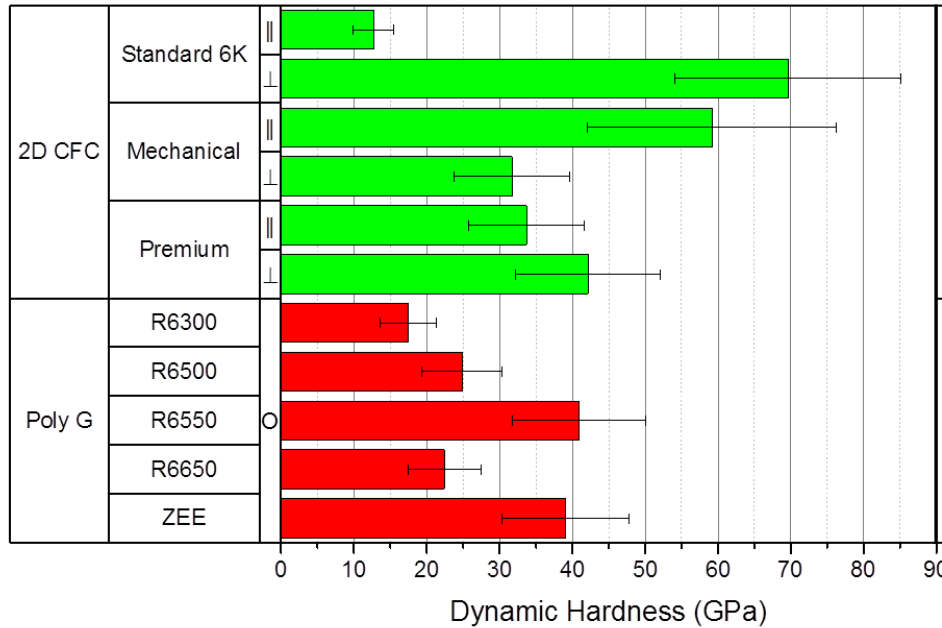


Damping constant k:

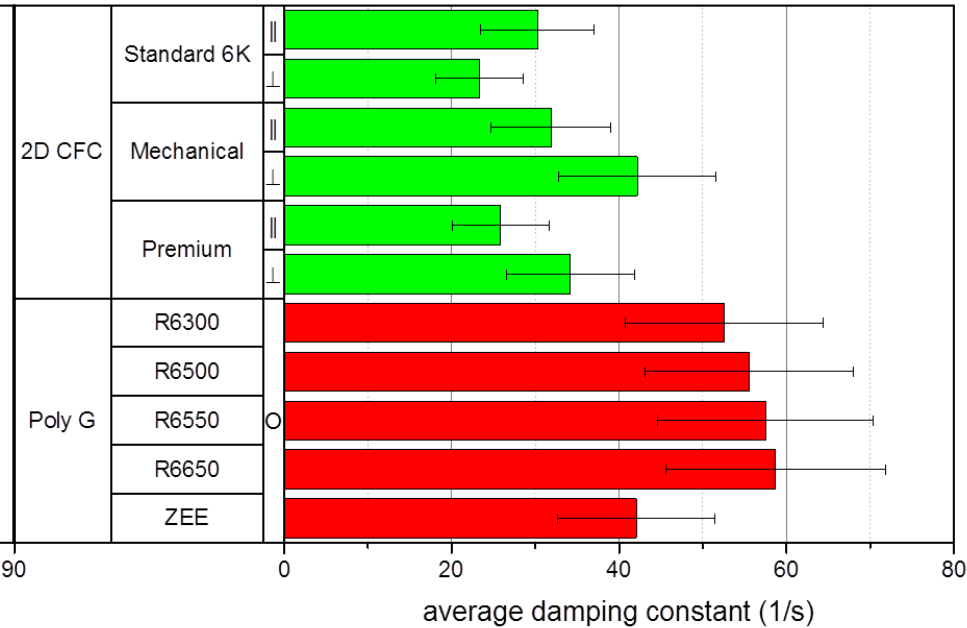
$$d = Ae^{-kt} + d_0$$

# Dynamic indentation results of polycrystalline graphite and carbon fibre reinforced carbon grades

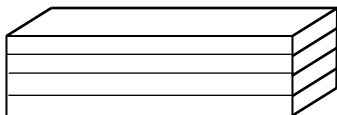
## Dynamic hardness



## Damping constant



In plane  $\parallel$



Transversal  $\perp$

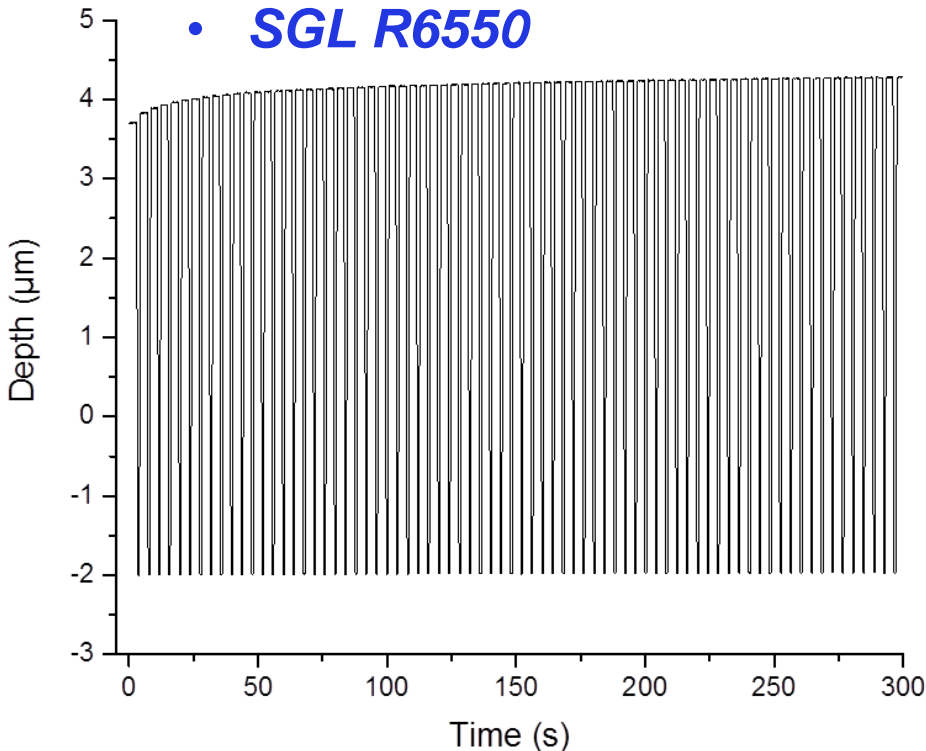


# Multiple Impulse indentation

- Indenter is accelerated with constant force towards the sample
- Indenter is moved back to the initial position and accelerated again
- Allows measurement of fatigue

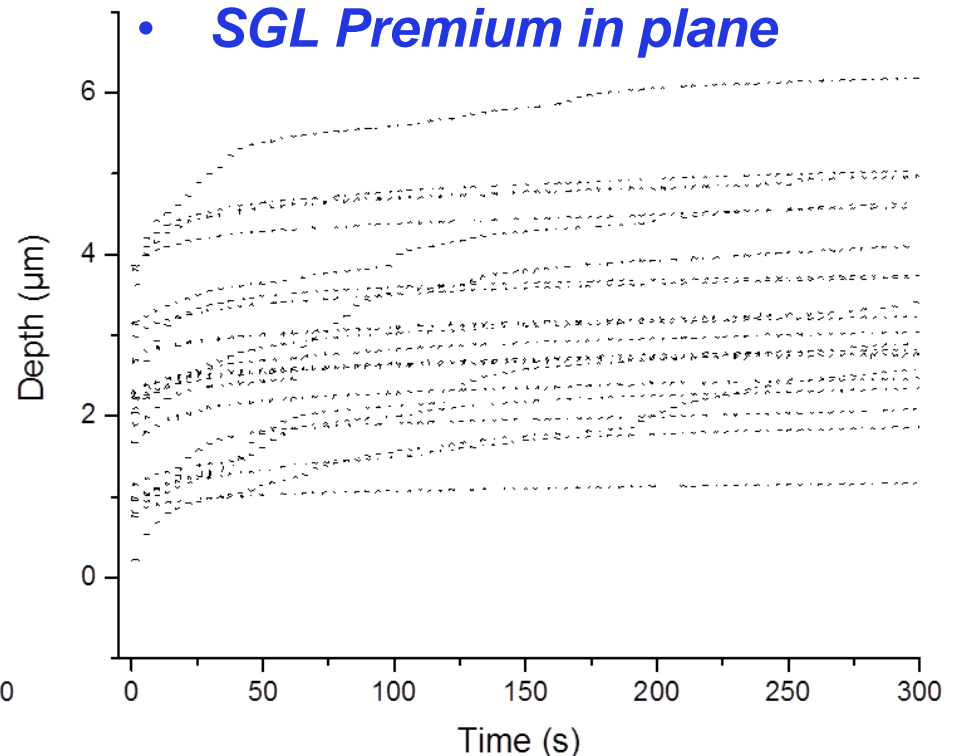
## **Polycrystalline graphite:**

- **SGL R6550**

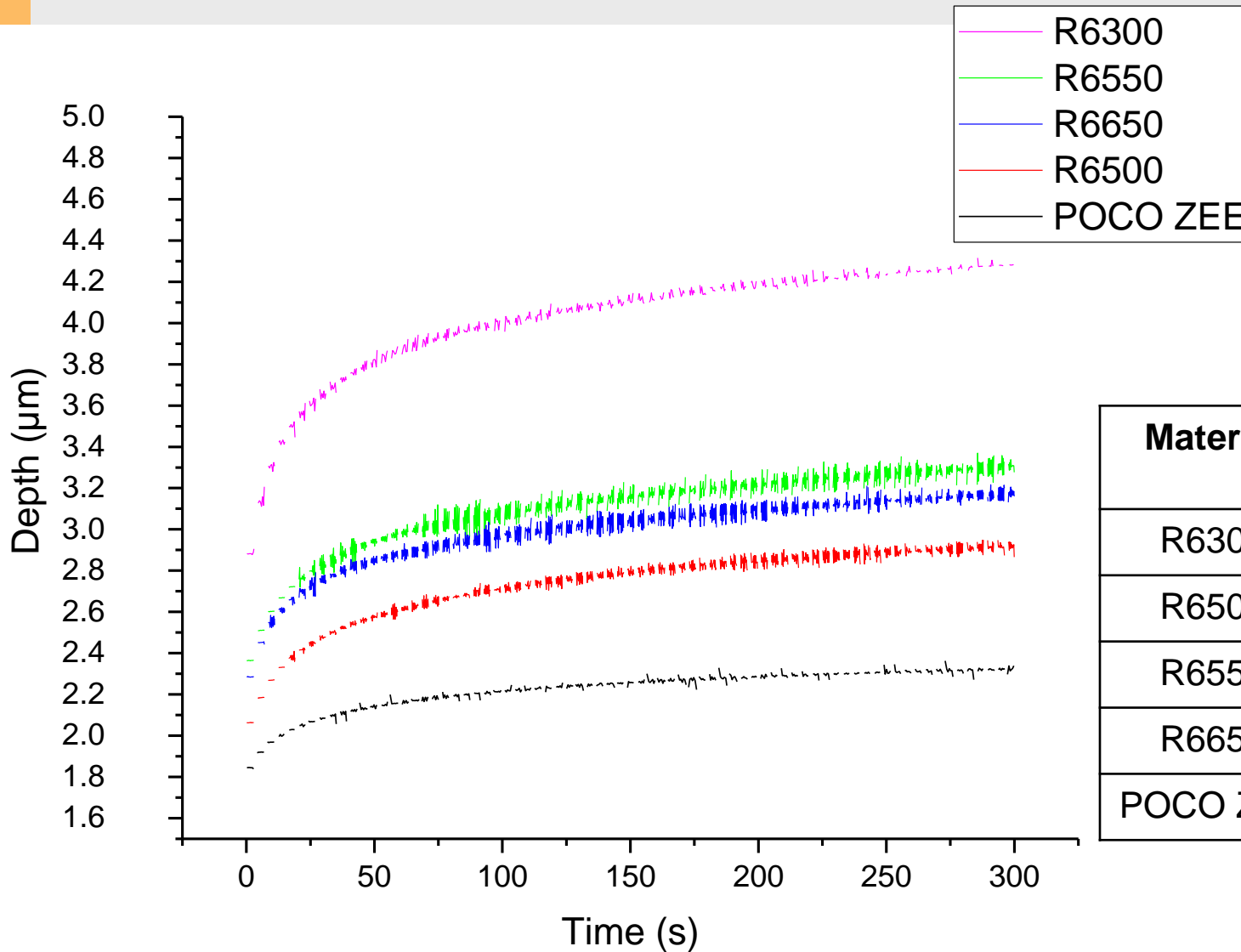


## **Carbon fibre reinforced carbon:**

- **SGL Premium in plane**

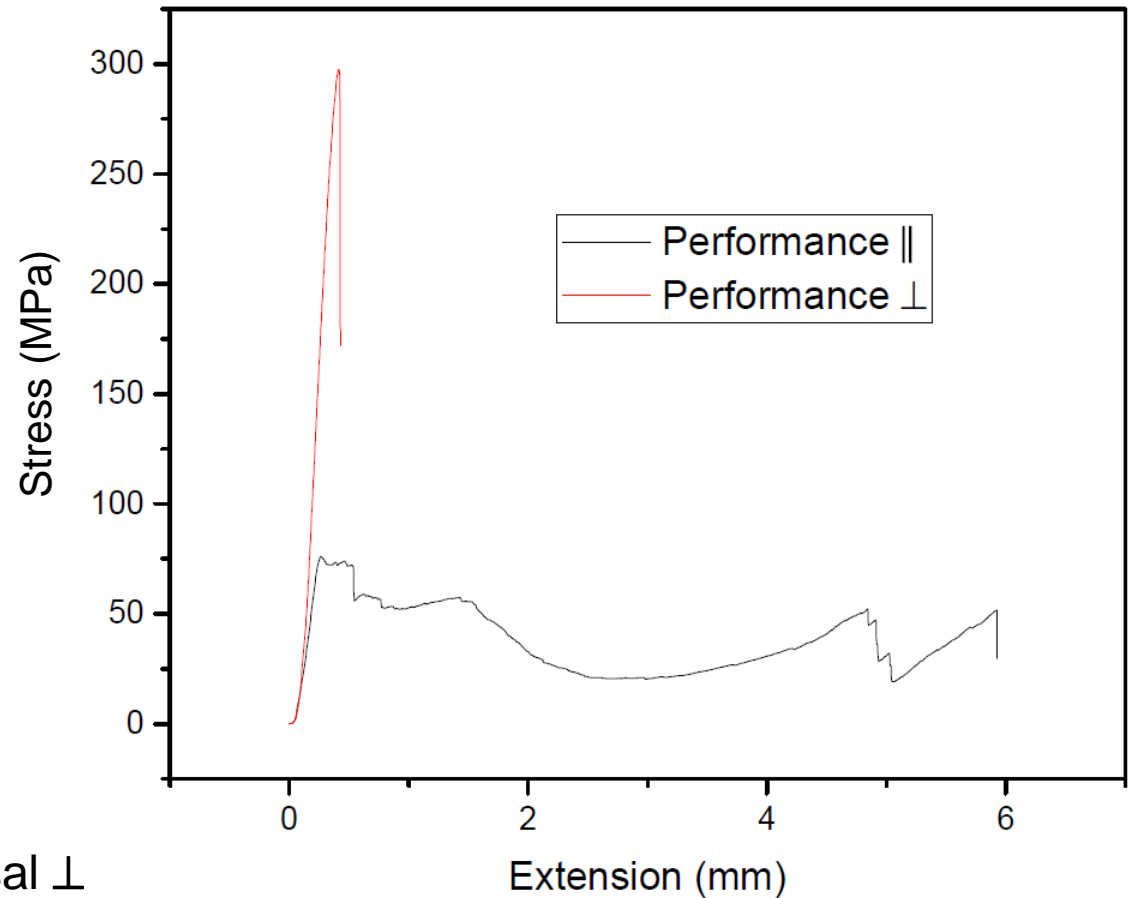
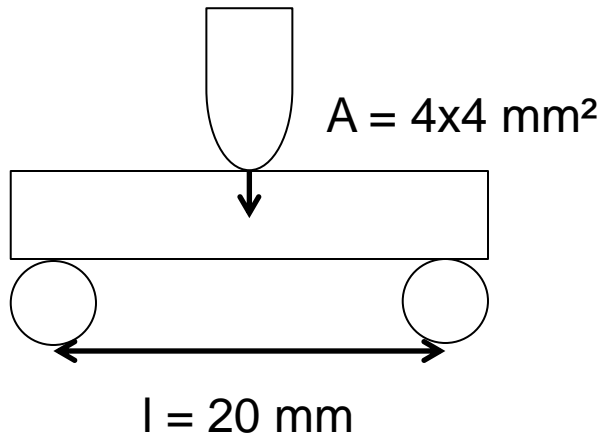


# Multiple impulse results of polycrystalline graphite grades



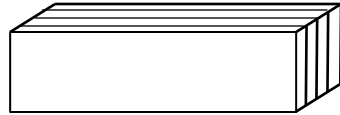
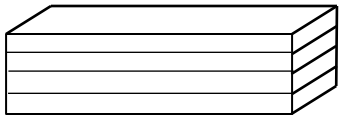
Material	Particle size [µm]
R6300	20
R6500	10
R6550	10
R6650	7
POCO ZEE	1

# 3-point bending test

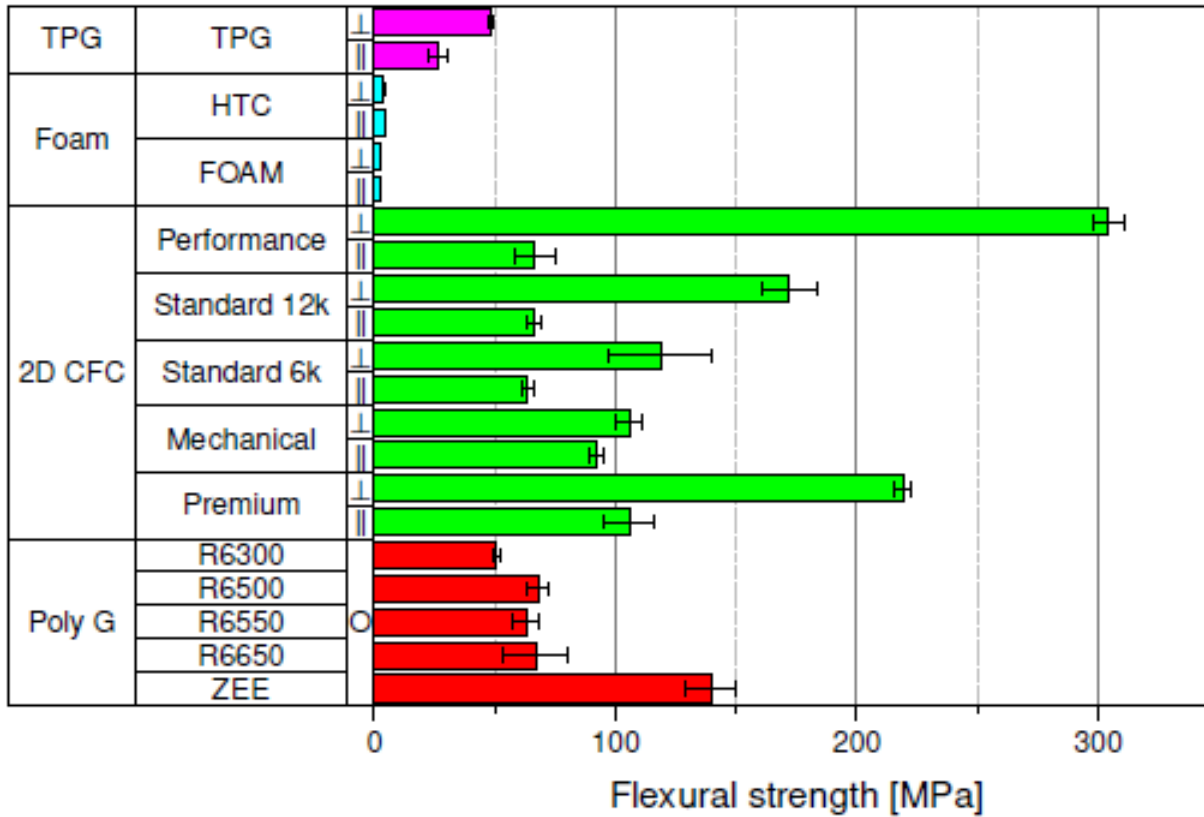


In plane ||

Transversal ⊥

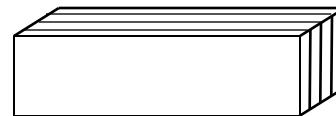
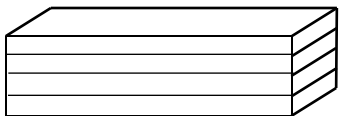


# Flexural strength



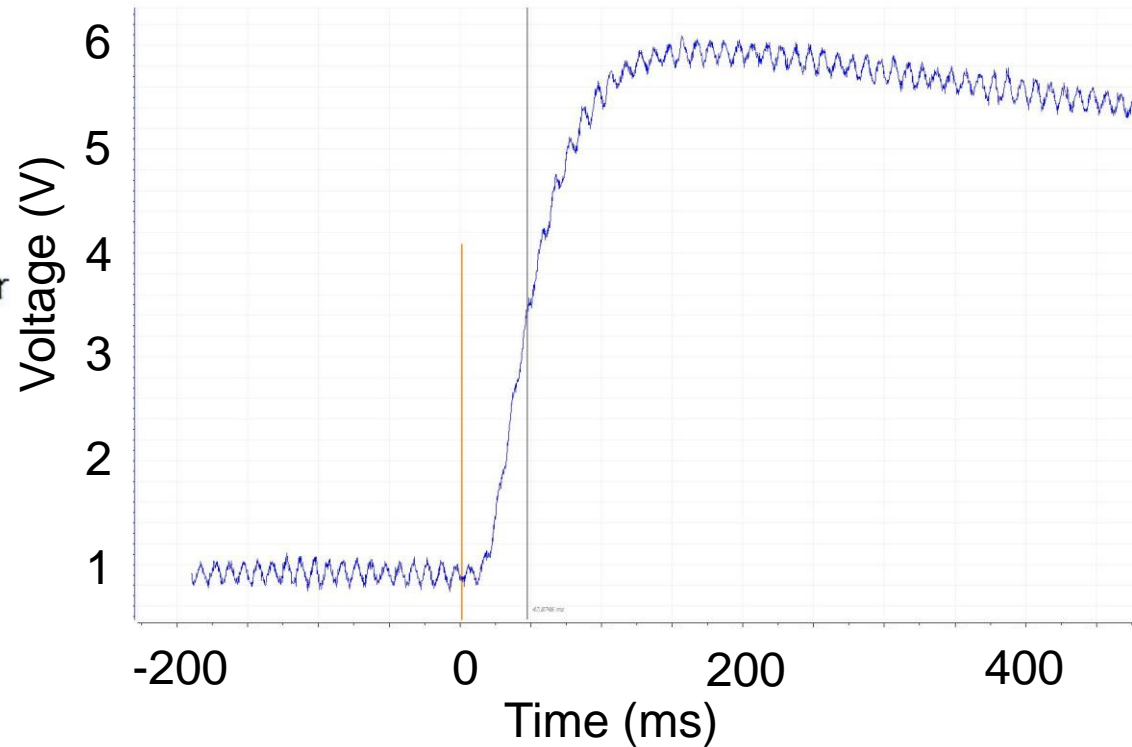
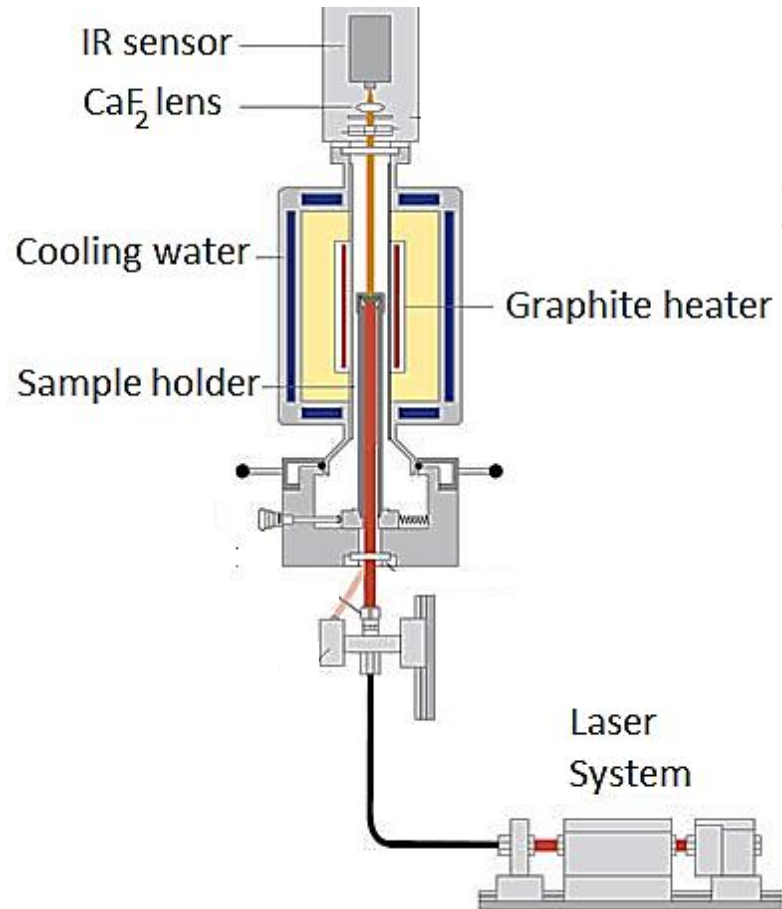
In plane  $\parallel$

Transversal  $\perp$



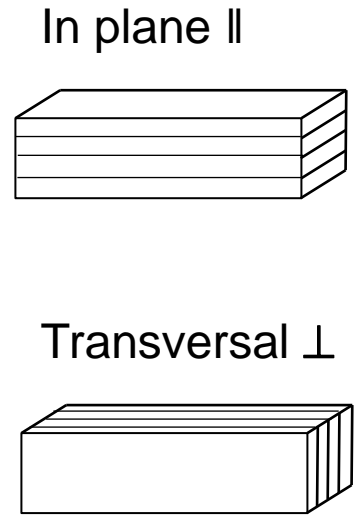
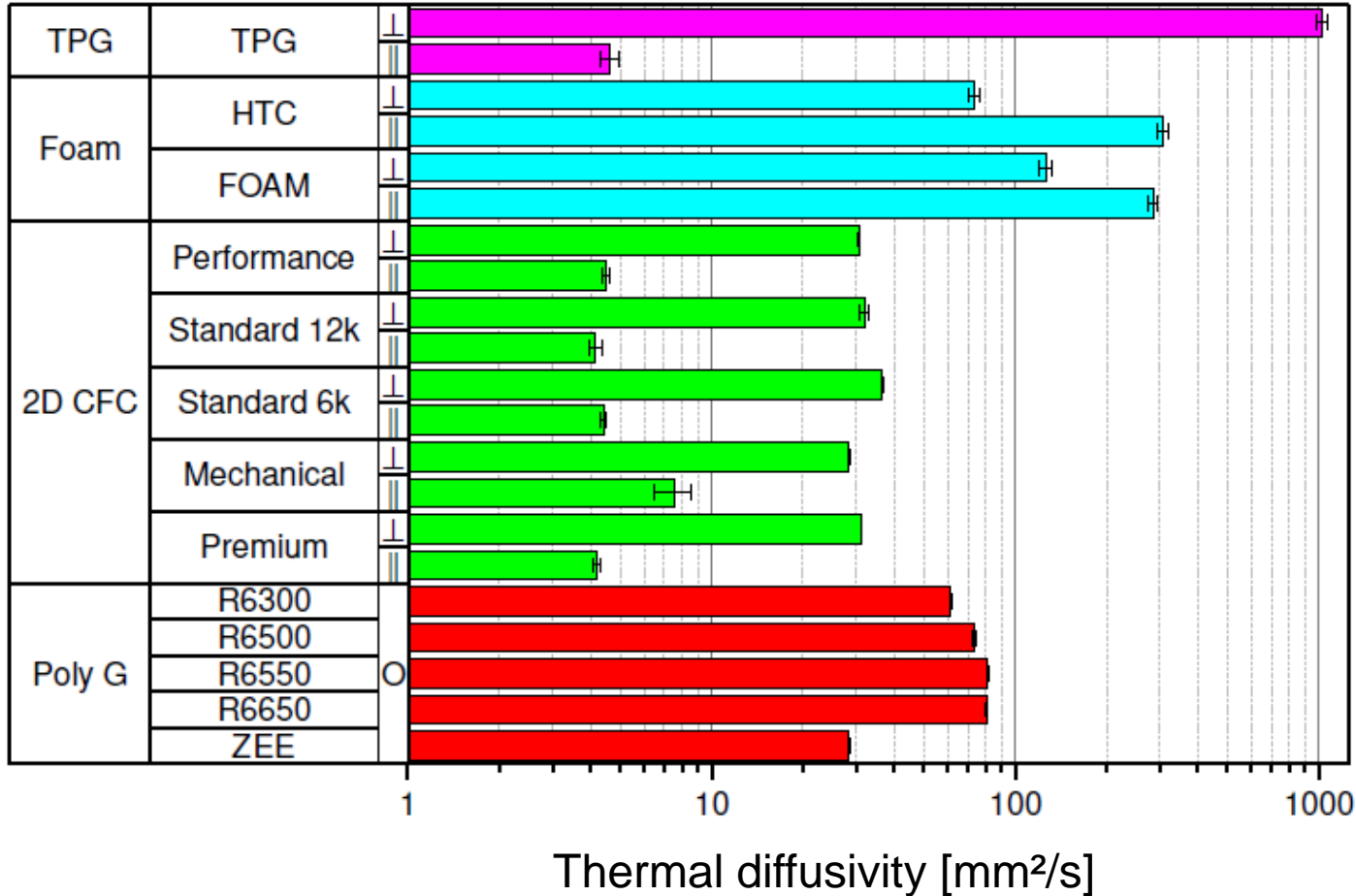


# Laser flash analysis

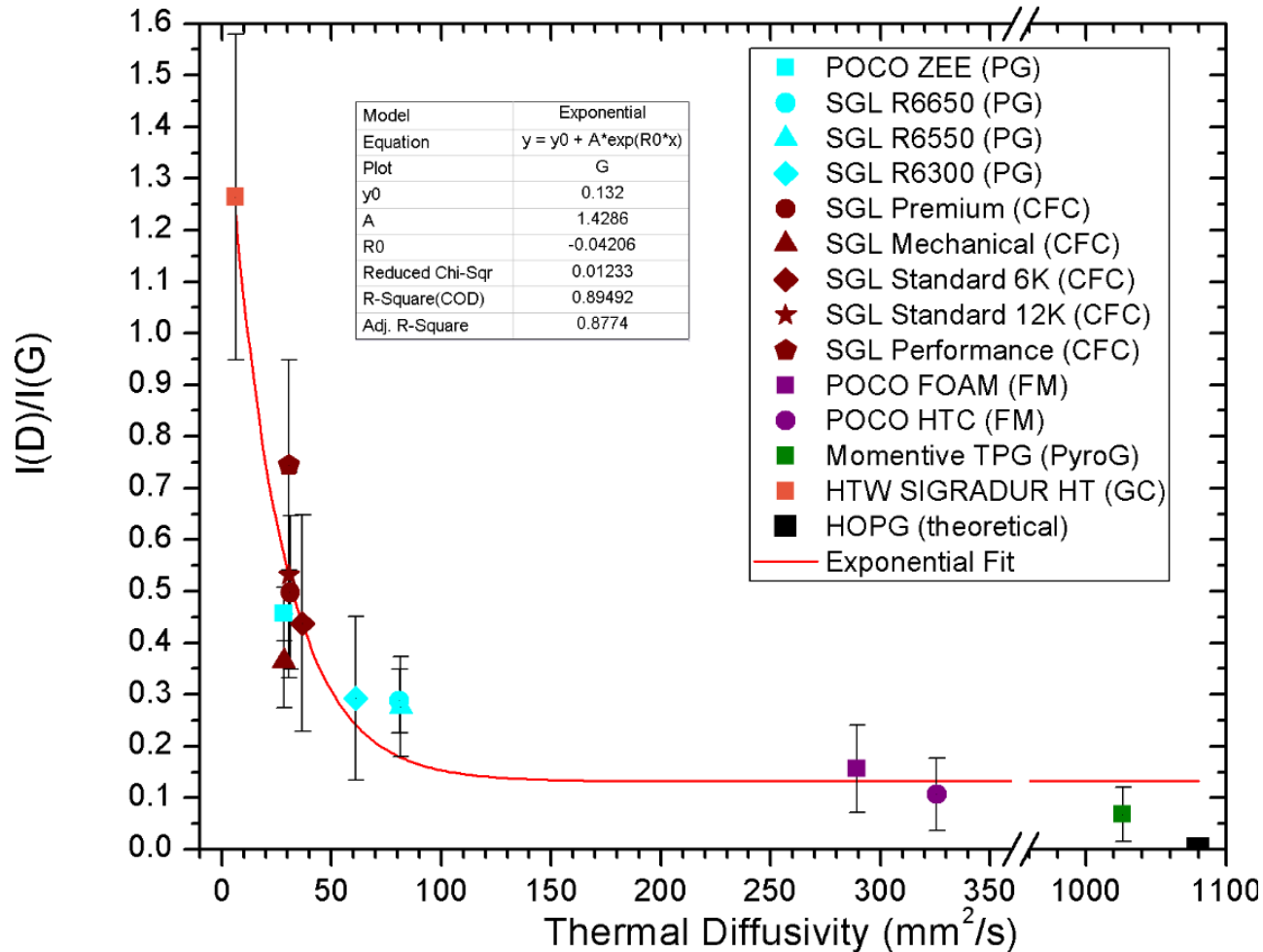


<https://www.netzsch-thermal-analysis.com/de/produkte-loesungen/waerme-und-temperatur-leitfaehigkeitsbestimmung/lfa-427/> (23.11.2017)

# Laser flash analysis results



# Empirical relation between $I_D/I_G$ and thermal diffusivity



- HOPG was used as reference (Ideal case has  $I_D$  zero)
- The relation shows an exponential behavior
- Lower  $I_D/I_G$  implies larger thermal diffusivity

- Properties of polycrystalline graphite depend on the grain size
- Carbon fibre reinforced carbon and graphite foams properties depend on orientation with a strong and a weak direction
- The thermal diffusivity is decaying exponentially with increasing defect concentration
- Results allow calculation of figures of merit and improved simulations to predict the behaviour during irradiation
- Experiments at HiRadMat and at GSI will allow evaluation of beam induced effects and property changes of the different irradiated graphitic materials

Thank you for your attention

Thanks to Roberto Colina-Ruiz, Fabian Jäger, Daniel Schmitt, Pascal Simon and Marilena Tomut for providing data

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