

# CLIC Module

## Heat load calculations, modelling and experimental program

M. Aicheler

On behalf of A. Vamvakas, A. Moilainen and E. Lam

CLIC workshop 2018

23.01.2018

# Outline

- A bit of history
- Experiment
- Numerical approaches
- Conclusion and Outlook

In the frame of the CLIC implementation process we had to provide heat to air/water numbers for all three machines  
 -> work based on CDR effort with updates and some revisions

Drive Beam Machine 3 TeV						Drive Beam Machine 380 GeV						Klystron machine 380 GeV						
Description	total water	unit	total air	unit	local air	Description	total water	unit	total air	unit	local air	Description	total water	unit	total air	unit	local air	unit
<b>Alignment systems:</b>						<b>Alignment systems:</b>						<b>Alignment systems:</b>						
Main beam	0 W		22,259 W		1.0 W/m	Main beam	0 W		3,701 W		1.0 W/m	Main beam	0 W		2,621 W		0.8 W/m	
Drive beam	0 W		18,666 W		0.9 W/m	Drive beam	0 W		2,671 W		0.8 W/m	Drive beam	0 W		0 W		0.0 W/m	
MBQs	0 W		0 W		0.0 W/m	MBQs	0 W		0 W		0.0 W/m	MBQs	0 W		0 W		0.0 W/m	
Sum:	0 W		40,925 W		1.9 W/m	Sum:	0 W		6,372 W		1.8 W/m	Sum:	0 W		2,621 W		0.8 W/m	
<b>BPM@Quads:</b>						<b>BPM@Quads:</b>						<b>BPM@Quads:</b>						
Main Beam	0 W		25,948 W		1.2 W/m	Main Beam	0 W		7,436 W		2.1 W/m	Main Beam	0 W		7,644 W		2.3 W/m	
Drive Beam	0 W		269,620 W		12.6 W/m	Drive Beam	0 W		38,584 W		10.9 W/m	Drive Beam	0 W		0 W		0.0 W/m	
Sum:	0 W		295,568 W		13.9 W/m	Sum:	0 W		46,020 W		13.0 W/m	Sum:	0 W		7,644 W		2.3 W/m	
<b>Vacuum:</b>						<b>Vacuum:</b>						<b>Vacuum:</b>						
Main Beam	0 W		751,825 W		35.3 W/m	Main Beam	0 W		107,590 W		30.3 W/m	Main Beam	0 W		105,560 W		31.7 W/m	
Drive Beam	0 W		337,025 W		15.8 W/m	Drive Beam	0 W		48,230 W		13.6 W/m	Drive Beam	0 W		0 W		0.0 W/m	
Sum:	0 W		1,088,850 W		51.1 W/m	Sum:	0 W		155,820 W		43.9 W/m	Sum:	0 W		105,560 W		31.7 W/m	
<b>Magnets:</b>						<b>Magnets:</b>						<b>Magnets:</b>						
MBQs	5,040,929 W		265,312 W		12.4 W/m	MBQs	895,379 W		47,125 W		13.3 W/m	MBQs	688,237 W		36,223 W		10.9 W/m	
MBQ cables	0 W		132,000 W		6.2 W/m	MBQ cables	0 W		22,000 W		6.2 W/m	MBQ cables	0 W		22,000 W		6.6 W/m	
DBQs	3,369,213 W		177,327 W		8.3 W/m	DBQs	482,152 W		25,376 W		7.1 W/m	DBQs	0 W		0 W		0.0 W/m	
DBQ cables	0 W		408,000 W		19.1 W/m	DBQ cables	0 W		68,000 W		19.1 W/m	DBQ cables	0 W		0 W		0.0 W/m	
Sum:	8,410,142 W		982,639 W		46.1 W/m	Sum:	1,377,530 W		162,502 W		45.7 W/m	Sum:	688,237 W		58,223 W		17.5 W/m	
<b>MBQ stabilisation systems:</b>						<b>MBQ stabilisation systems:</b>						<b>MBQ stabilisation systems:</b>						
Controller	0 W		159,680 W		7.5 W/m	Controller	0 W		45,760 W		12.9 W/m	Controller	0 W		47,040 W		14.1 W/m	
Seismometer & powersupply	0 W		13,695 W		0.6 W/m	Seismometer & powersupply	0 W		2,258 W		0.6 W/m	Seismometer & powersupply	0 W		2,327 W		0.7 W/m	
Piezo actuators	0 W		11,668 W		0.5 W/m	Piezo actuators	0 W		2,720 W		0.8 W/m	Piezo actuators	0 W		2,804 W		0.8 W/m	
Sum:	0 W		185,043 W		8.7 W/m	Sum:	0 W		50,738 W		14.3 W/m	Sum:	0 W		52,171 W		15.7 W/m	
<b>RF systems (unloaded case!):</b>						<b>RF systems (unloaded case!):</b>						<b>RF systems (unloaded case!):</b>						
AS	27,334,217 W		3,727,393 W		174.8 W/m	AS	3,548,084 W		483,830 W		136.2 W/m	AS	3,963,768 W		540,514 W		162.1 W/m	
RF loads	18,394,186 W					RF loads	2,773,331 W		693,333 W		195.2 W/m	RF loads	2,710,723 W		677,681 W		203.3 W/m	
AS WFM	0 W					AS WFM	0 W		19,292 W		5.4 W/m	AS WFM	0 W		18,928 W		5.7 W/m	
PETS	2,764,840 W					PETS	398,661 W		54,363 W		15.3 W/m	Pulse compression & distribution	5,094,787 W		268,147 W		80.4 W/m	
RF distribution	355,031 W					RF distribution	51,192 W		6,981 W		2.0 W/m	Klystron	8,541,260 W		449,540 W		134.9 W/m	
Sum:	48,848,273 W		8,876,684 W		416.3 W/m	Sum:	6,771,267 W		1,257,798 W		354.1 W/m	Modulator	3,768,203 W		198,326 W		59.5 W/m	
<b>RF systems (loaded case!):</b>						<b>RF systems (loaded case!):</b>						<b>RF systems (loaded case!):</b>						
AS	21,955,346 W		2,993,911 W		140.4 W/m	AS	2,623,009 W		357,683 W		100.7 W/m	AS	2,938,744 W		400,738 W		120.2 W/m	
RF loads	10,962,249 W		2,740,562 W		128.5 W/m	RF loads	1,227,283 W		306,821 W		86.4 W/m	RF loads	1,199,278 W		299,820 W		89.9 W/m	
AS WFM	0 W		125,307 W		5.9 W/m	AS WFM	0 W		19,292 W		5.4 W/m	AS WFM	0 W		18,928 W		5.7 W/m	
PETS	2,764,840 W		377,024 W		17.7 W/m	PETS	398,661 W		54,363 W		15.3 W/m	Pulse compression & distribution	5,094,787 W		268,147 W		80.4 W/m	
RF distribution	355,031 W		48,413 W		2.3 W/m	RF distribution	51,192 W		6,981 W		2.0 W/m	Klystron	8,541,260 W		449,540 W		134.9 W/m	
Sum:	36,037,466 W		6,285,217 W		294.8 W/m	Sum:	4,300,145 W		745,139 W		209.7 W/m	Modulator	3,768,203 W		198,326 W		59.5 W/m	
Total per linac <b>ZERO</b> beams:	8,410,142 W					Total per linac <b>ZERO</b> beams:	1,377,530 W		421,451 W		118.6 W/m	Total per linac <b>RF OFF:</b>	688,237 W		226,219 W		67.9 W/m	
Total per linac <b>ONE</b> beam:	57,258,415 W					Total per linac <b>ONE</b> beam:	8,148,798 W		1,679,249 W		472.7 W/m	Total per linac <b>RF ON &amp; NO</b> beam:	12,457,514 W		1,731,488 W		519.4 W/m	
Total per linac <b>TWO</b> beams:	44,447,608 W					Total per linac <b>TWO</b> beams:	5,677,675 W		1,166,591 W		328.4 W/m	Total per linac <b>RF ON &amp; beam:</b>	9,921,046 W		1,213,851 W		364.1 W/m	

416 W/m

537 W/m

Situation as of July 2017

Looking closer on the accelerating structures and their loads

<b>Main Beam:</b>			
Thermal dissipation of AS	435	W	<b>unloaded!</b>
Thermal dissipation of RF loads	322	W	<b>unloaded!</b>
Thermal dissipation of AS	349	W	<b>loaded!</b>
Thermal dissipation of RF loads	192	W	<b>loaded!</b>
total # AS	71,406	---	
total power AS	31,061,610	W	<b>unloaded!</b>
total power AS	24,949,256	W	<b>loaded!</b>
Power to water AS	0.88	---	
total power RF loads	22,992,732	W	<b>unloaded!</b>
total power RF loads	13,702,811	W	<b>loaded!</b>
Power to water RF loads	0.80		

These numbers varied historically from 1 to 0.8

-> we had to understand those numbers better and get them as high as we can

Two beam module test lab:

Heat to air 'measured'

Assume all heat from heater goes to water or air

$$P_{air} = P_{tot} - P_{water}$$

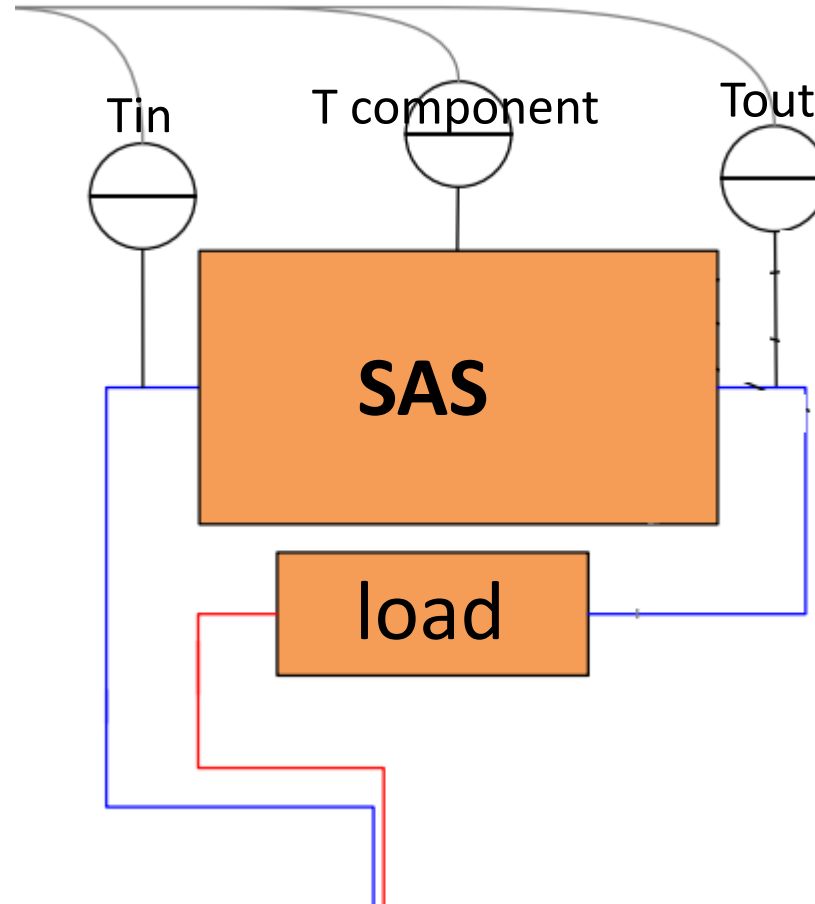
$$P_{water} = \dot{m}_w C_p [T_{out} - T_{in}]$$

$$P_{tot} = V * I$$

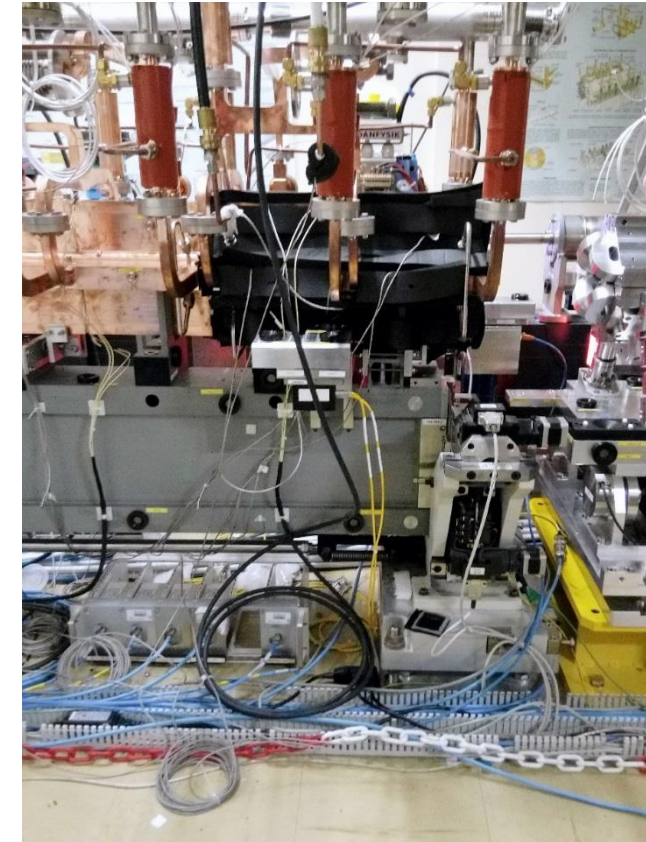
Heat to air theory

$$P_{air} = hA[T_{comp} - T_{ambient}]$$

Cp	4184	J/kg/K
h	11~20	W/m2/K
A	0.7273	M2
m'	0.026~0.039	kg/sec



Naked and insulated SAS



Problem:

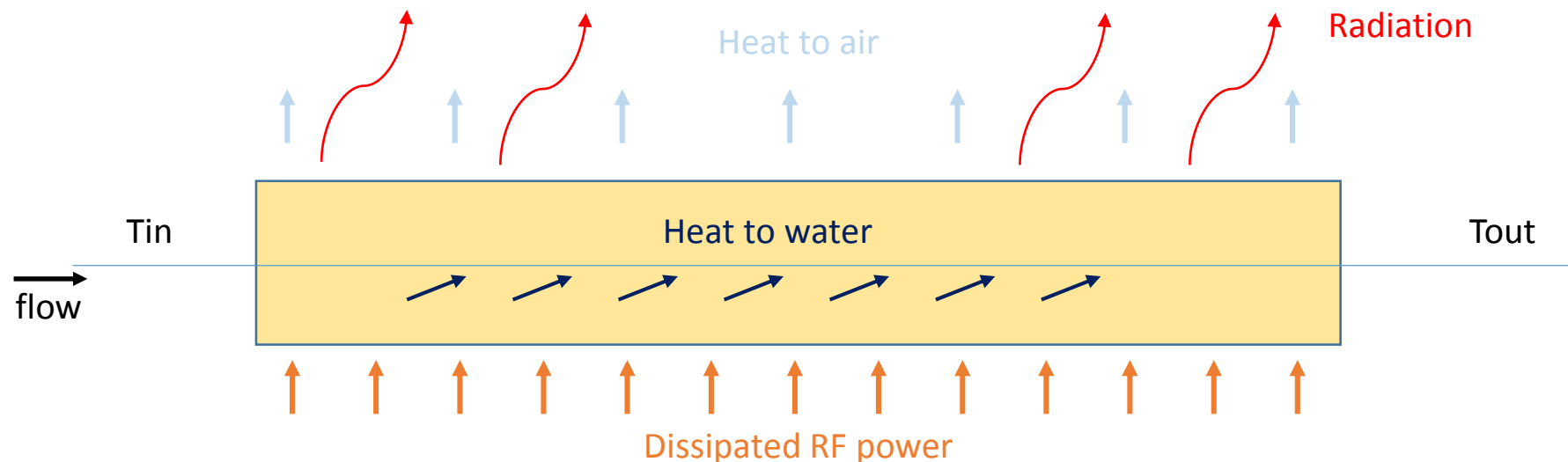
- heat conducted away through girder/waveguides/vacuum system
- Minor errors in temperature accuracy huge errors in power

## Analytical Model

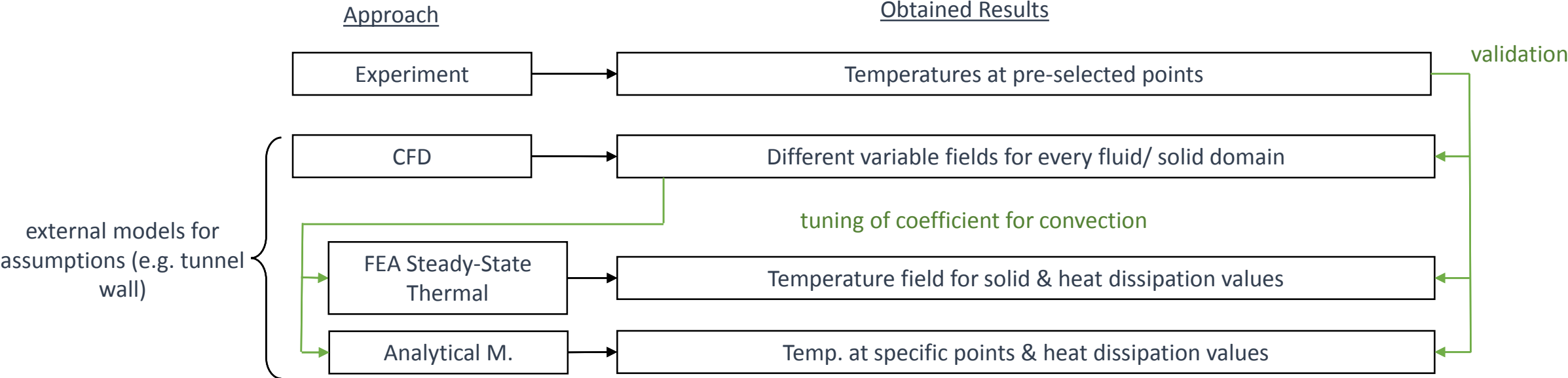
- Simple pipe, heated and cooled all along
- Excludes folding of piping
- Run time for SAS: 1 sec
- Run time for TBM: 3 sec
- Can be used to run many different combinations,

### Downsides:

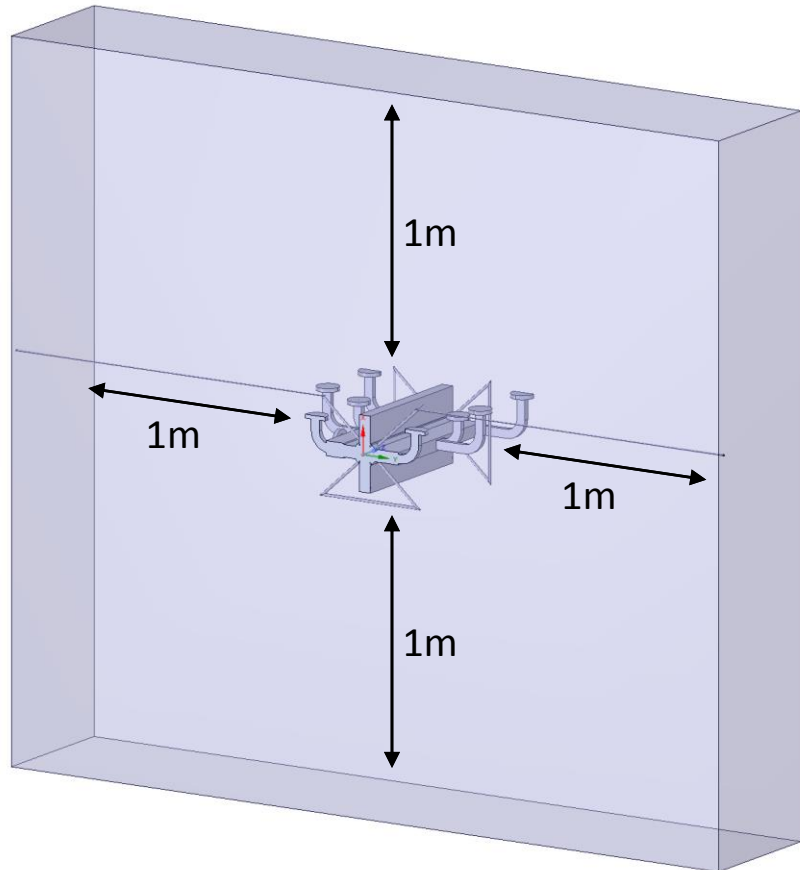
- Heavy assumptions for heat transfer coefficient
- No possibility to simulate real heat channel routing in SAS



# Combined approach



# Problem Definition



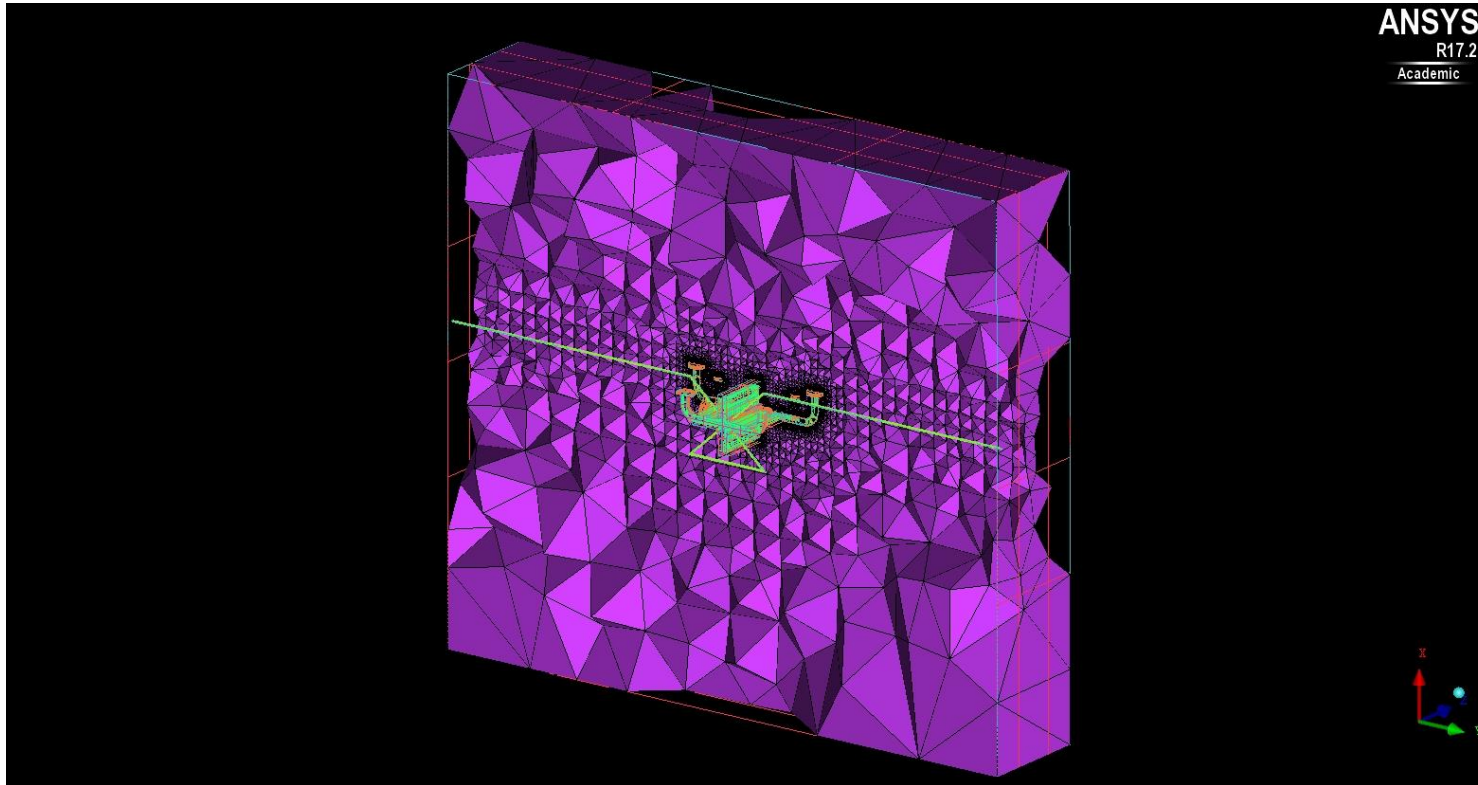
- Only one super-accelerating structure
- In “free” space
- Domain boundary 1 m from the structure
- Artificial pipes

## Materials:

- Copper for the structure and pipes
- Air (variable  $\rho$ , incompressible ideal gas law)
- Water (constant  $\rho$ )



# Meshing



a cross section of the mesh

Mesher: ANSYS ICEM CFD v17.2

Type of elements: tetrahedron

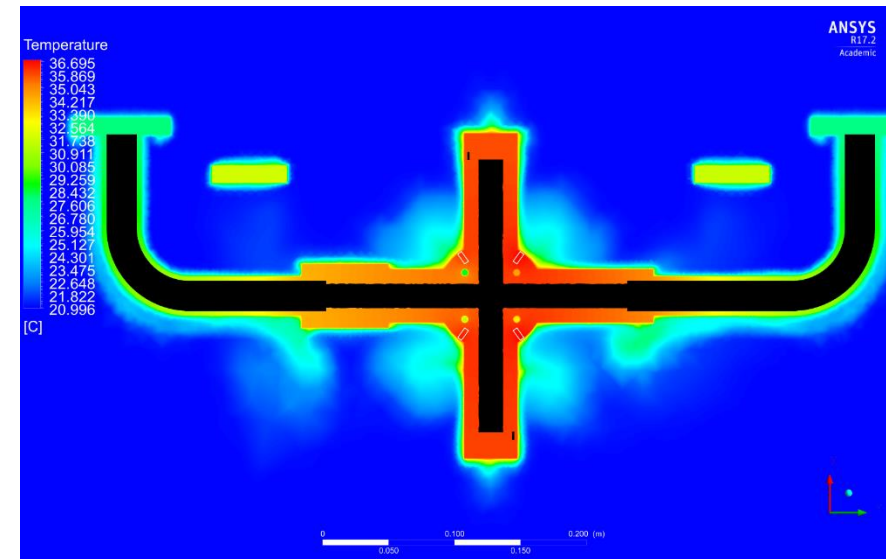
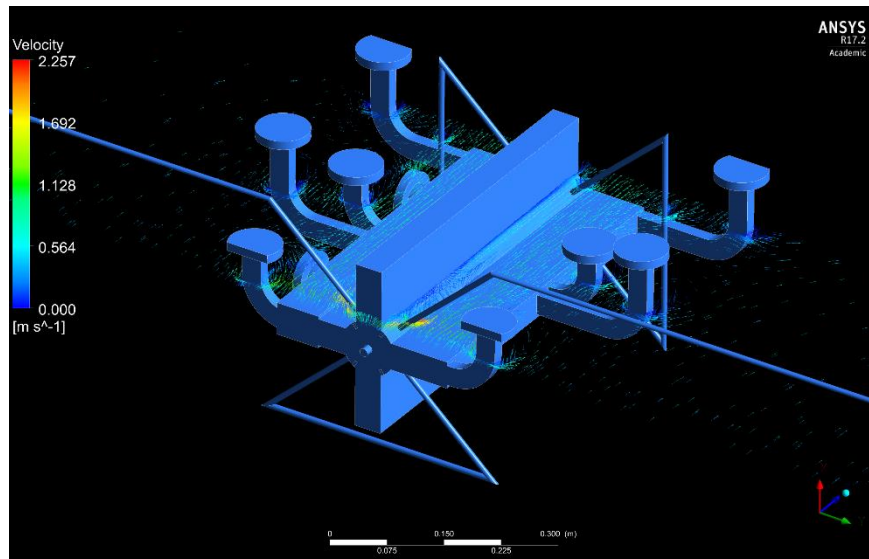
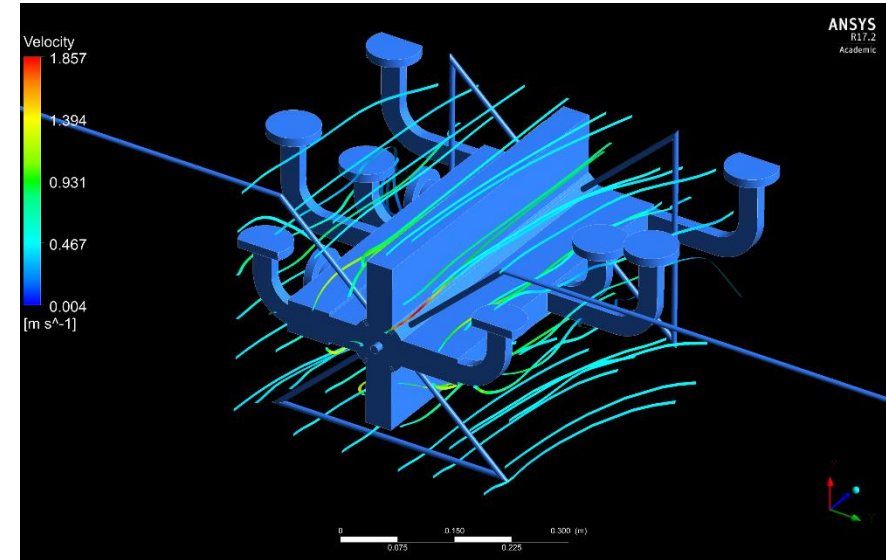
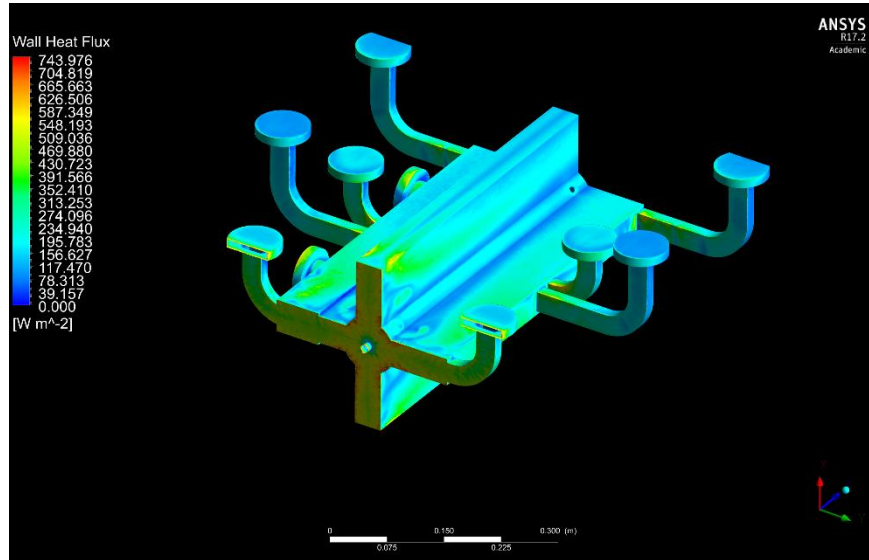
Number of elements:

43 million for the finest mesh

Coarser meshes were generated to determine mesh independence

Minimum size of elements: 1 mm

# Output



# SAS (no compact loads)

SST simulation

CFD simulation (E. Lam)

- horizontal air flow 0.4 m/s

SAS:

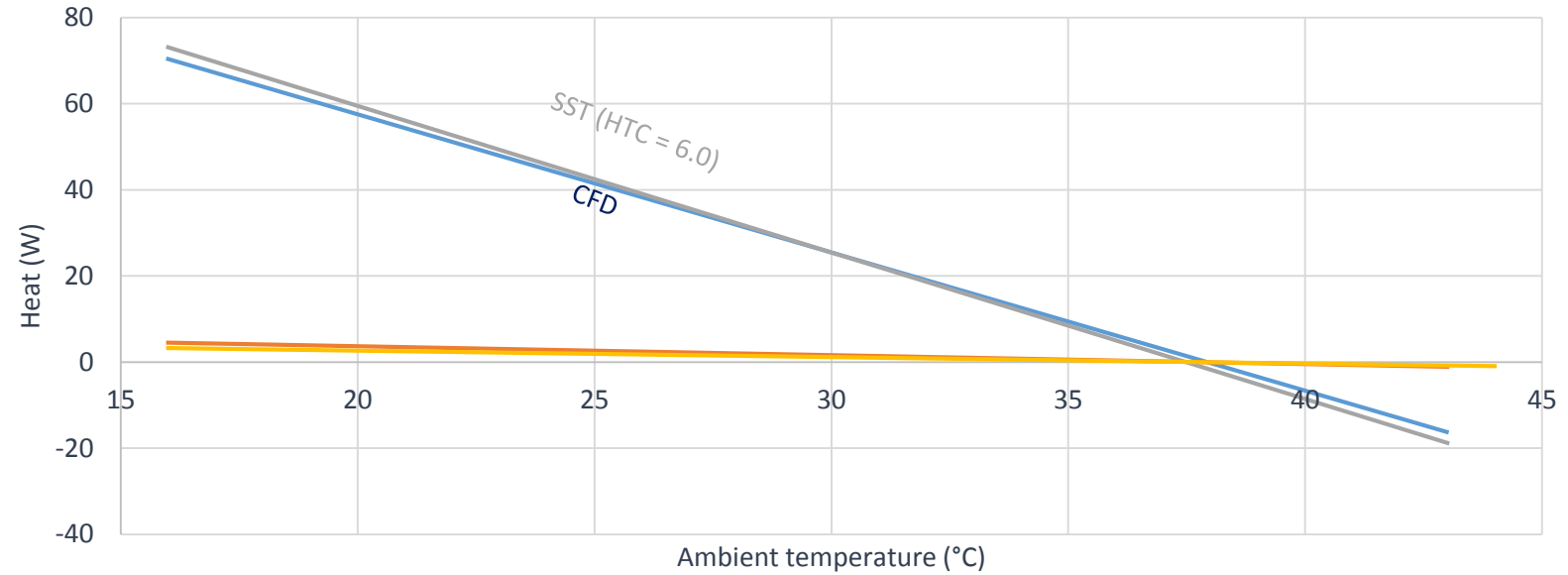
Heat 780 W

Water 27 °C

Flow 1.3 l/min

Heat to air: Convection and radiation

Emissivity  $\epsilon = 0.05$



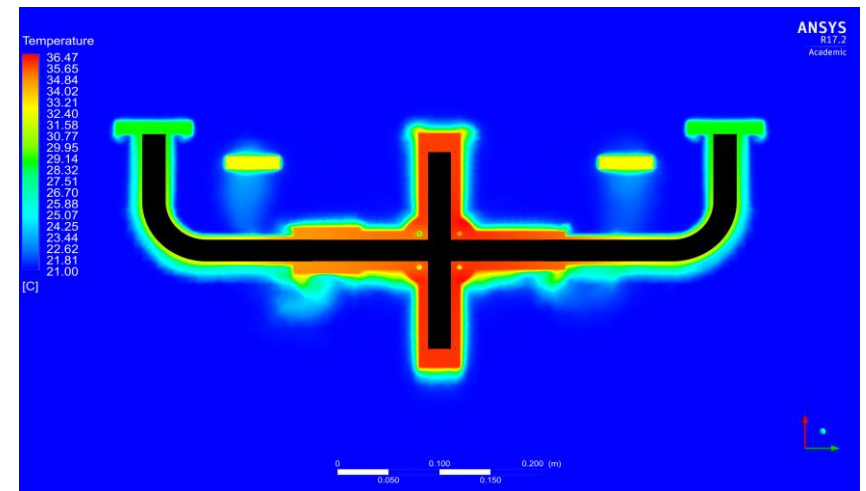
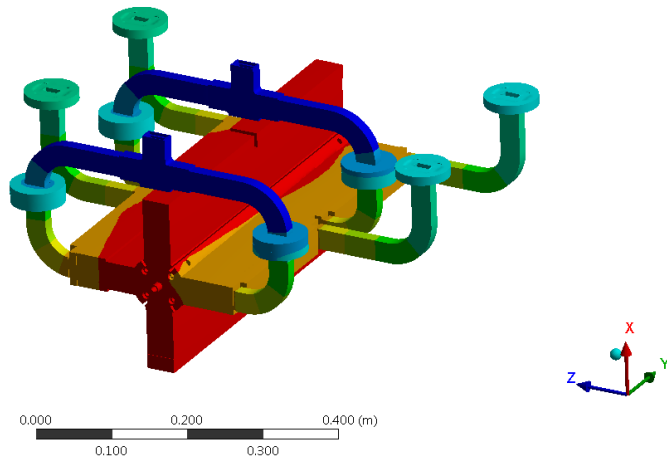
— Linear (CFD, convection) — Linear (CFD, radiation) — Linear (SST, convection) — Linear (SST, radiation)

A. J. Moilanen

E. Lam

A: STEP 0 - SASambient20  
 Temperature  
 Type: Temperature  
 Unit: °C  
 Time: 1  
 07/11/2017 10:24

37.541 Max  
 36.107  
 34.673  
 33.239  
 31.805  
 30.37  
 28.936  
 27.502  
 26.068  
 24.634 Min



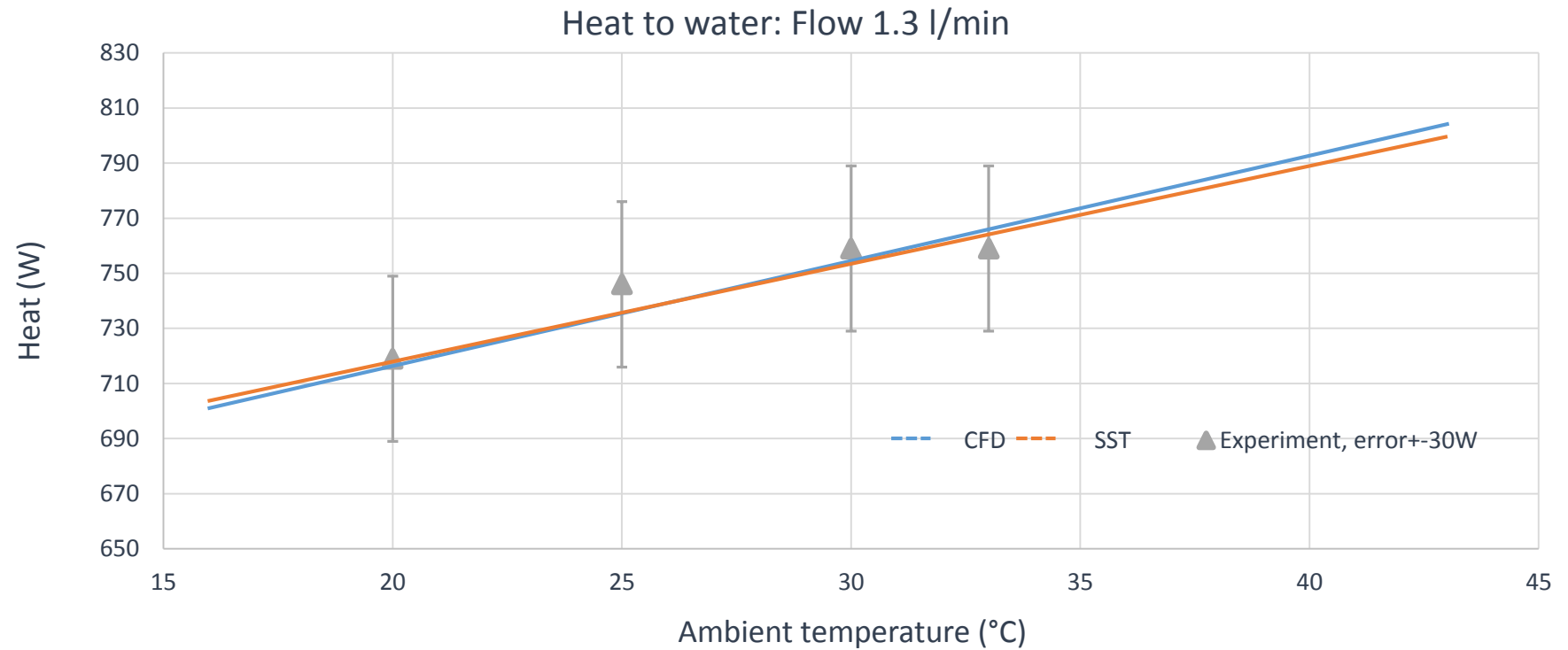
# SAS (no compact loads)

SST simulation

CFD simulation (E. Lam)

Measurement (V. Andavan, A. Vamvakas)

- horizontal air flow 0.4 m/s



## FEM Thermal analysis of the entire CLIC module

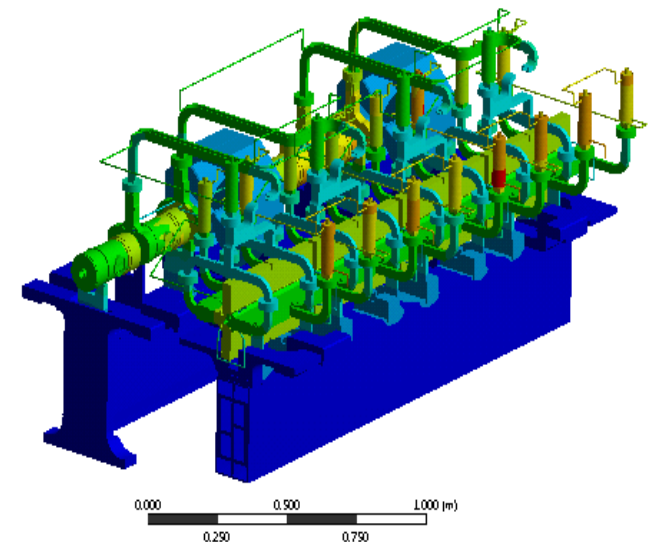
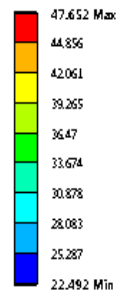
Aim of the Finite Element Method (FEM) simulation is to study heat distribution and dissipation in CLIC module T0#2.

Thermal gradients originate from several sources: RF structures produce heat, components are cooled by water and air flow, ambient temperature varies

The modelling is done using ANSYS 17.2 Workbench. The FEM simulation of includes:

- 3D CAD geometry
- Steady-state thermal analysis (followed by Static structural analysis)
- Isotropic materials: OFE copper, aluminium, stainless steel, SiC
- Thermal loads
- Ambient temperature
- Thermal fluid (water)
- Convection, radiation, conduction

B: MODULE0\_2  
Temperature 3  
Type: Temperature  
Unit: °C  
Time: 1  
12/12/2017 18:34



# FEA thermal simulations for TBM

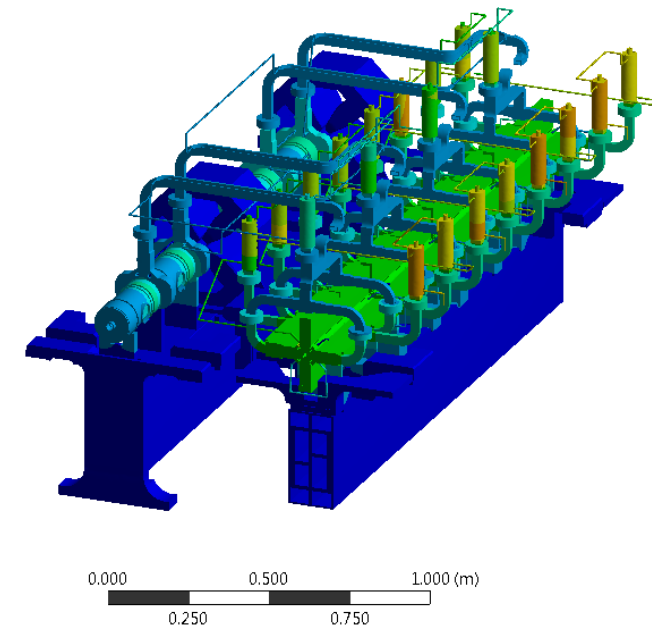
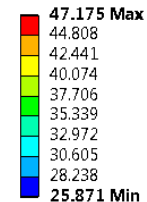
- ANSYS Thermal steady-state analysis
- T0#2 Module
- Run time: ~1hr

		Heating power (W)		
CL	20x	161	3220	
PETS	4x	88	352	
SAS	4x	860	3440	
DBQs	2x	171	342	
<b>Total</b>			<b>7354</b>	<b>W</b>

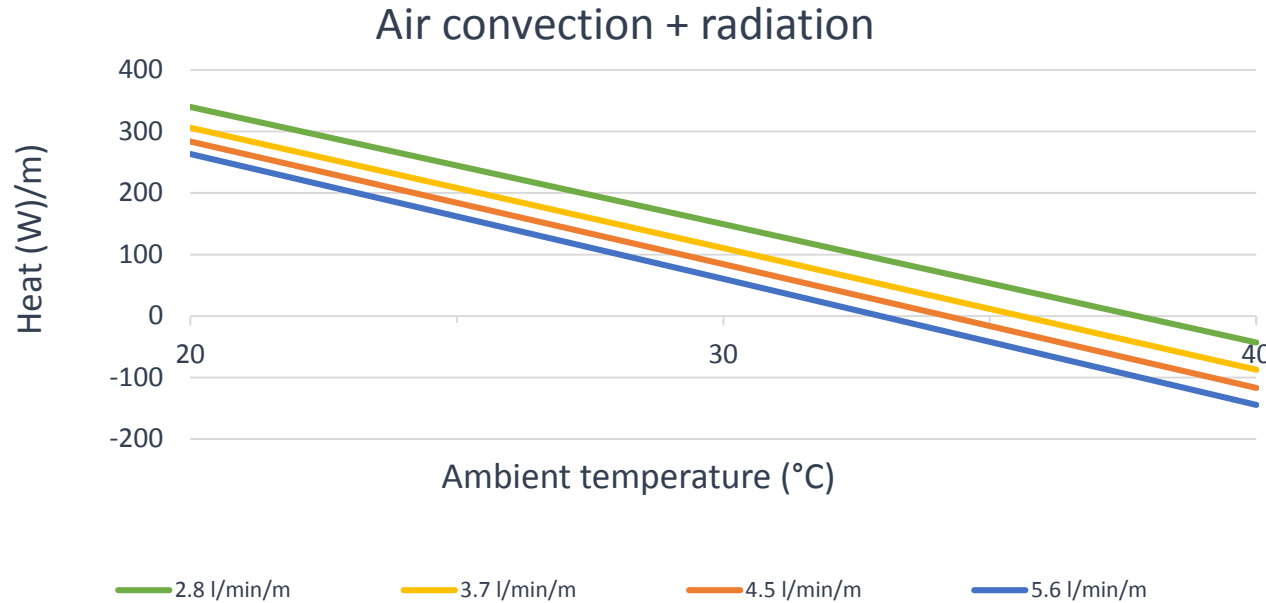
- Total heating power 7354 W
- Cooling water 27 °C, 1.3 l/min
- Ambient T = 20...40 °C
- Convection  $HTC_{air} = 7.5 \text{ W/m}^2\text{K}$
- Radiation to surrounding "space" (T = 18°C)  
(no surface-to-surface effect)

B: STEP 0: MODULE ambient30

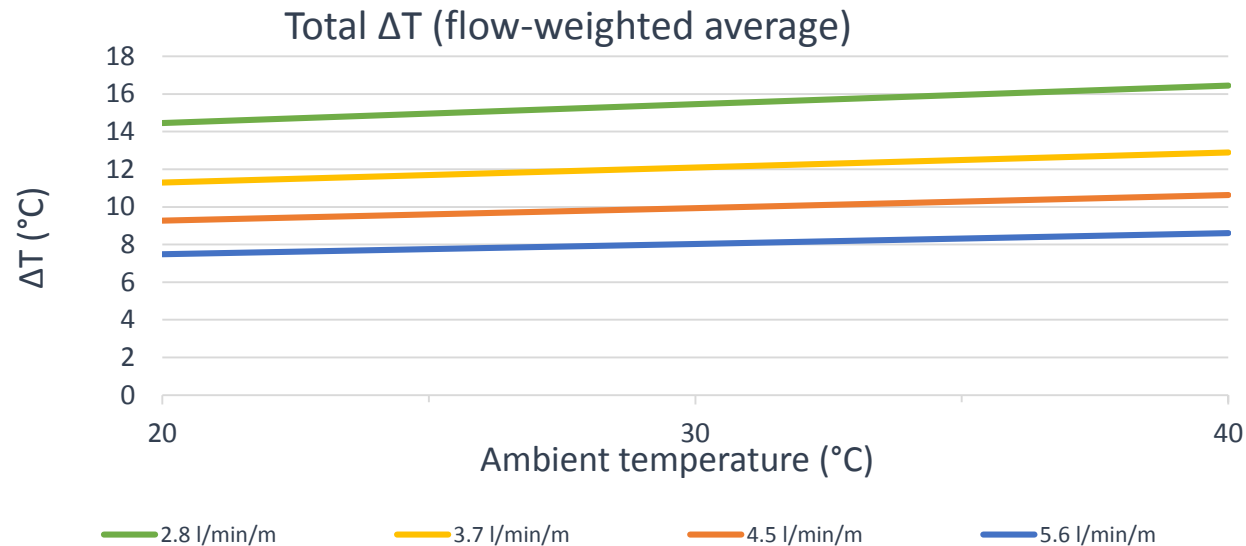
Temperature 3  
Type: Temperature  
Unit: °C  
Time: 1  
07/11/2017 12:02



## Module: Results for different flows: Unloaded case



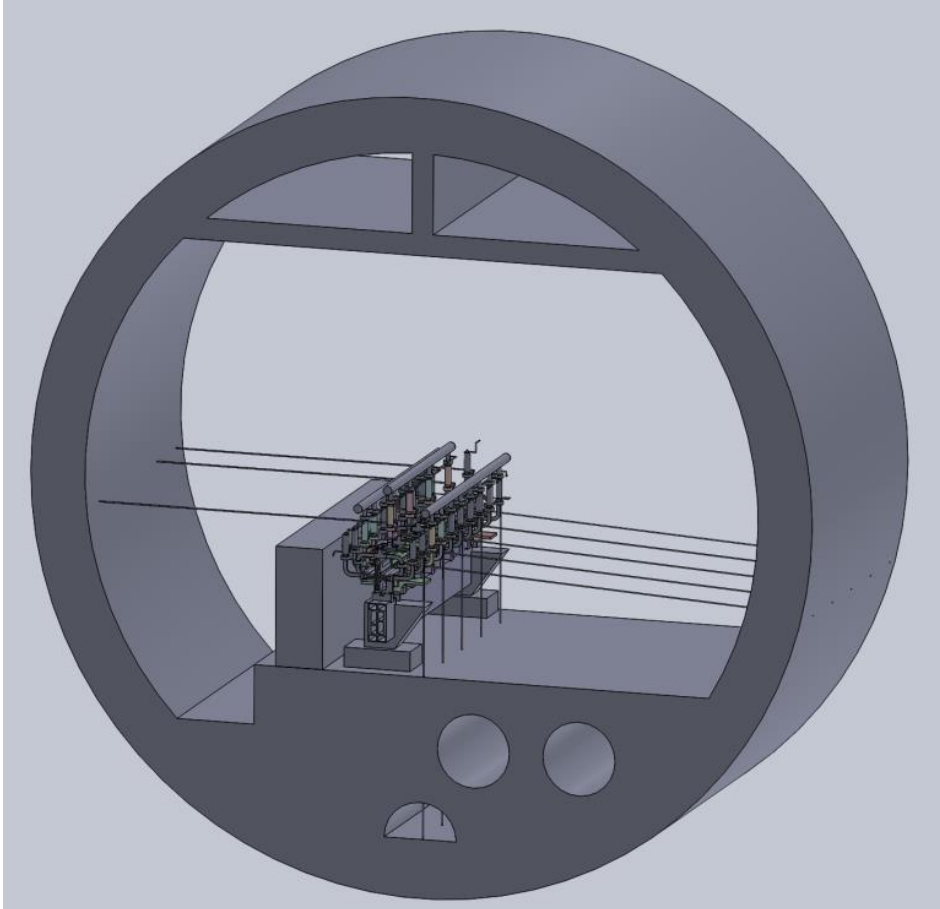
- Higher flow lowers component T (but not below 27°C)
- Higher flow lowers heat to air
- Higher ambient T lowers heat to air
- Zero emission point



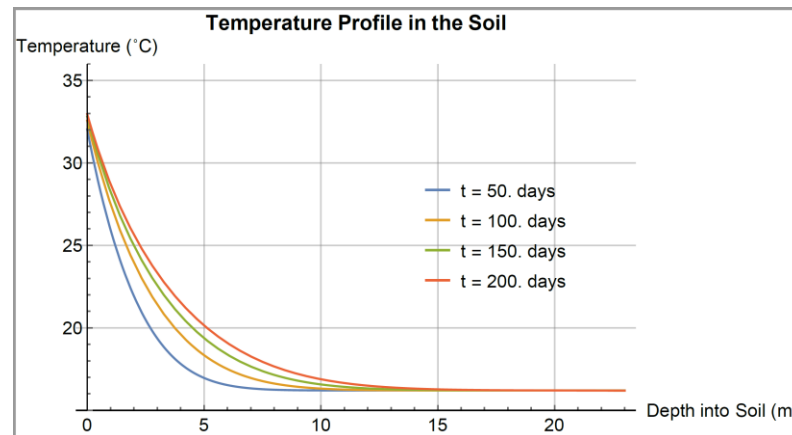
- Higher flow lowers  $\Delta T$  of water!
- Higher ambient T increases  $\Delta T$  of water!

-> to our colleagues from Cooling&Ventilation

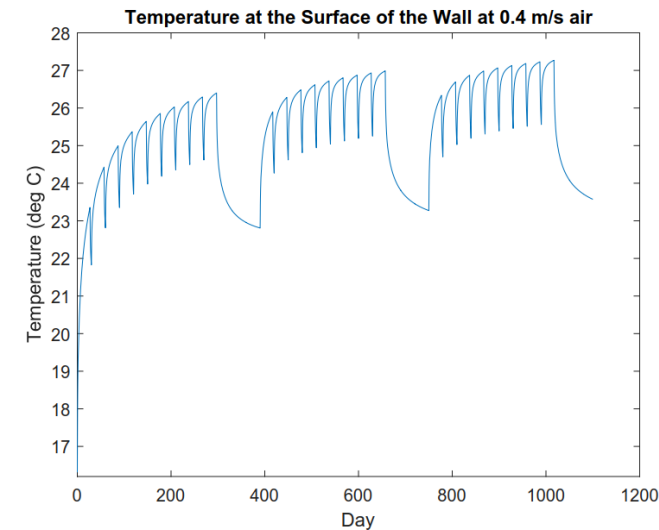
# In the mean time...



- Entire main beam part of the module into CFD for getting a glimpse of longitudinal effects
- Modeling of tunnel wall and soil for evaluation of feasibility of temperature stability requirements
- Machine operation transitioning states



Analytical model in development for assumptions that can be made for the tunnel wall in steady-state CFD or FEA simulations



3 days off per month  
3 months off per year  
Off means 25 °C  
On means 32 °C  
Initial 16.2°C  
Always 0.4 m/s





## Module: Air convection

### Convection to air

- Constant heat transfer coefficient  $6 \text{ W}/(\text{m}^2 \text{ } ^\circ\text{C})$

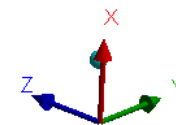
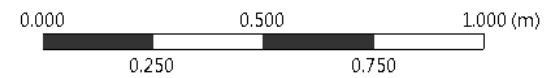
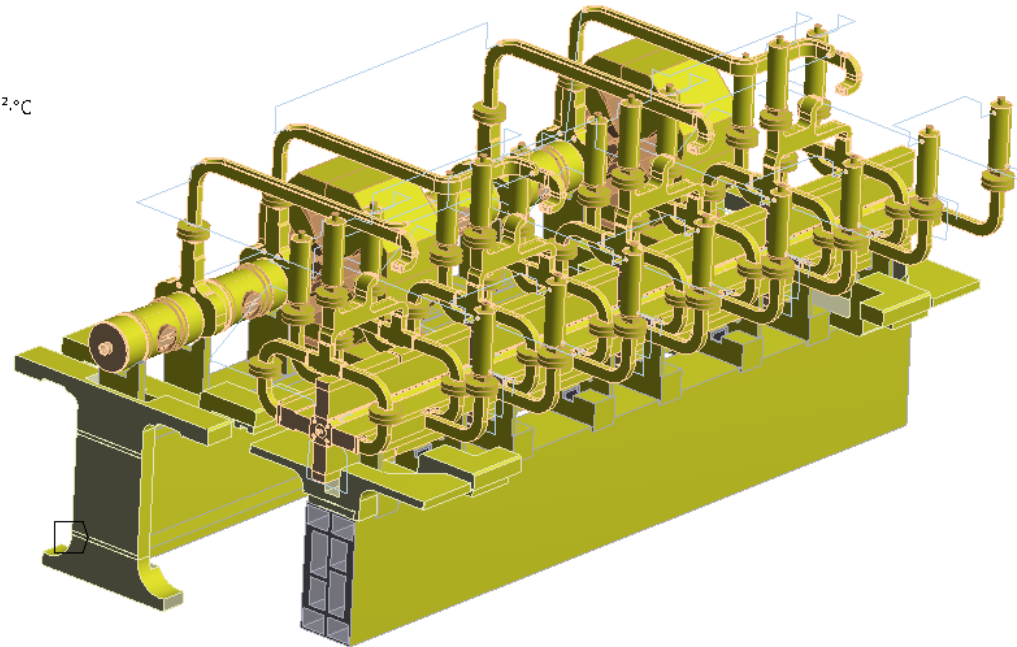
**B: : MODULE0\_2**

Air convection

Time: 1 s

13/12/2017 08:44

■ Air convection: 20. °C, 6. W/m<sup>2</sup>.°C



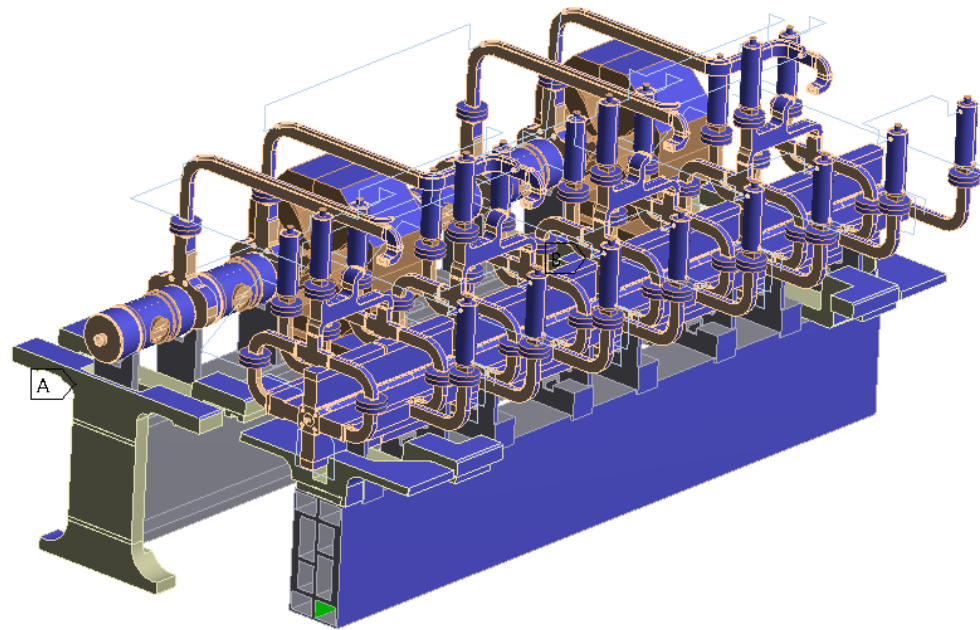
## Module: Thermal radiation

Radiation to surrounding space (ambient temperature):

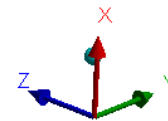
- Emissivity for copper, aluminium and stainless steel (0.05) and SiC (0.83)
- No surface-to-surface effects

**B**: : MODULE T0\_2  
Radiation  
Time: 1. s  
13/12/2017 08:45

**A** Radiation: 20. °C, 5.e-002  
**B** Radiation 7: 20. °C, 0.83



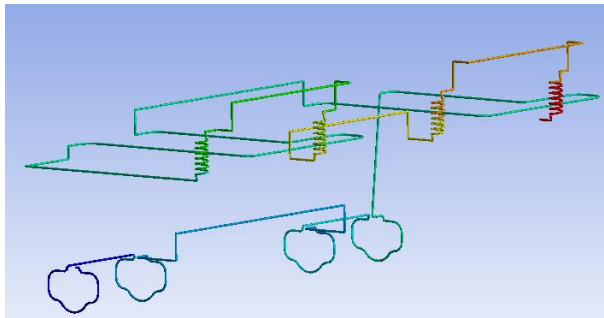
0.000 0.250 0.500 0.750 1.000 (m)



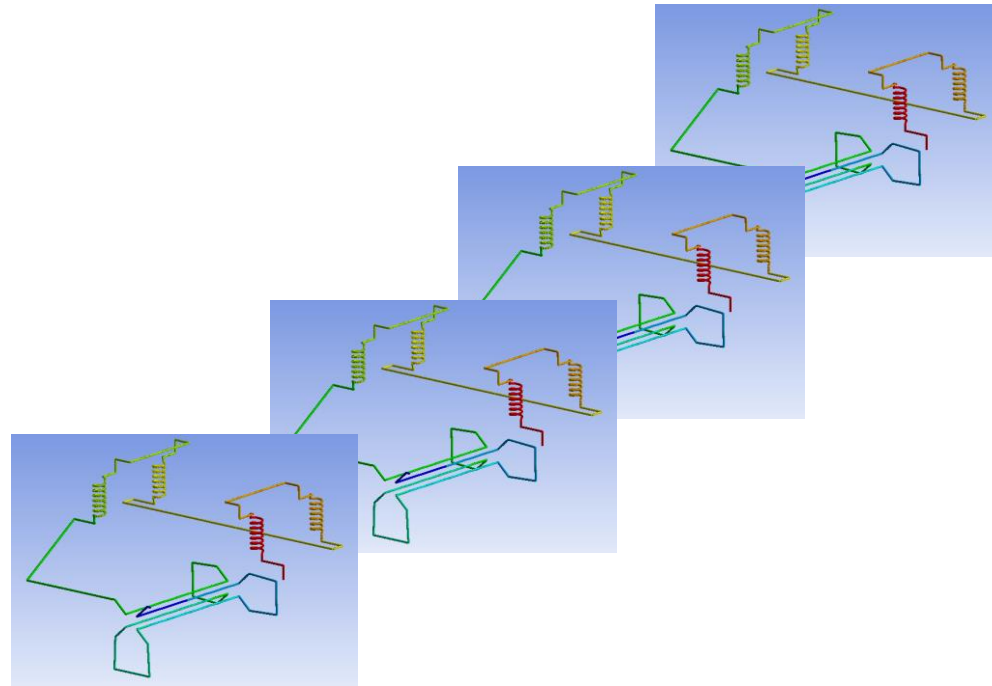
## Module: Water cooling

5 separate cooling circuits

- Water heat transfer coefficient is calculated similarly as in Refs. [1-4]
- Flow can be varied
- Inlet temperature can be varied



2 double PETS and 4 RF loads on series



SAS and 4CLs on series

