



# Progress in NEG Coatings for Particle Accelerators

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CERN, Geneva, Switzerland**



# Outlook

- Introduction
- Pumping properties
- Desorption properties
- Bombardment induced activation and pumping
- Surface resistance
- SEY
- Summary



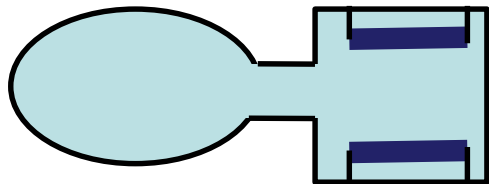
# Two concepts of the ideal vacuum chamber

## Traditional:

- surface which outgasses as little as possible ('nil' ideally)
- surface which **does not pump** otherwise that surface is contaminated over time

## Results in

- Surface cleaning, conditioning, coatings
- Vacuum firing, *ex-situ* baling
- Baking *in-situ* to up to **300°C**
- Separate pumps

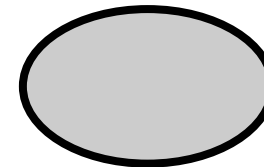


## 'New' (C. Benvenuti, CERN, ~1998):

- surface which outgasses as little as possible ('nil' ideally)
- a surface which **does pump**, however, will not be contaminated due to a very low outgassing rate

## Results in

- NEG coated surface
- There should be no un-coated parts
- Activating (baking) *in-situ* at **150-180°C**
- Small pumps for  $C_xH_y$  and noble gases



# What NEG coating does

## 1) Reduces gas desorption:

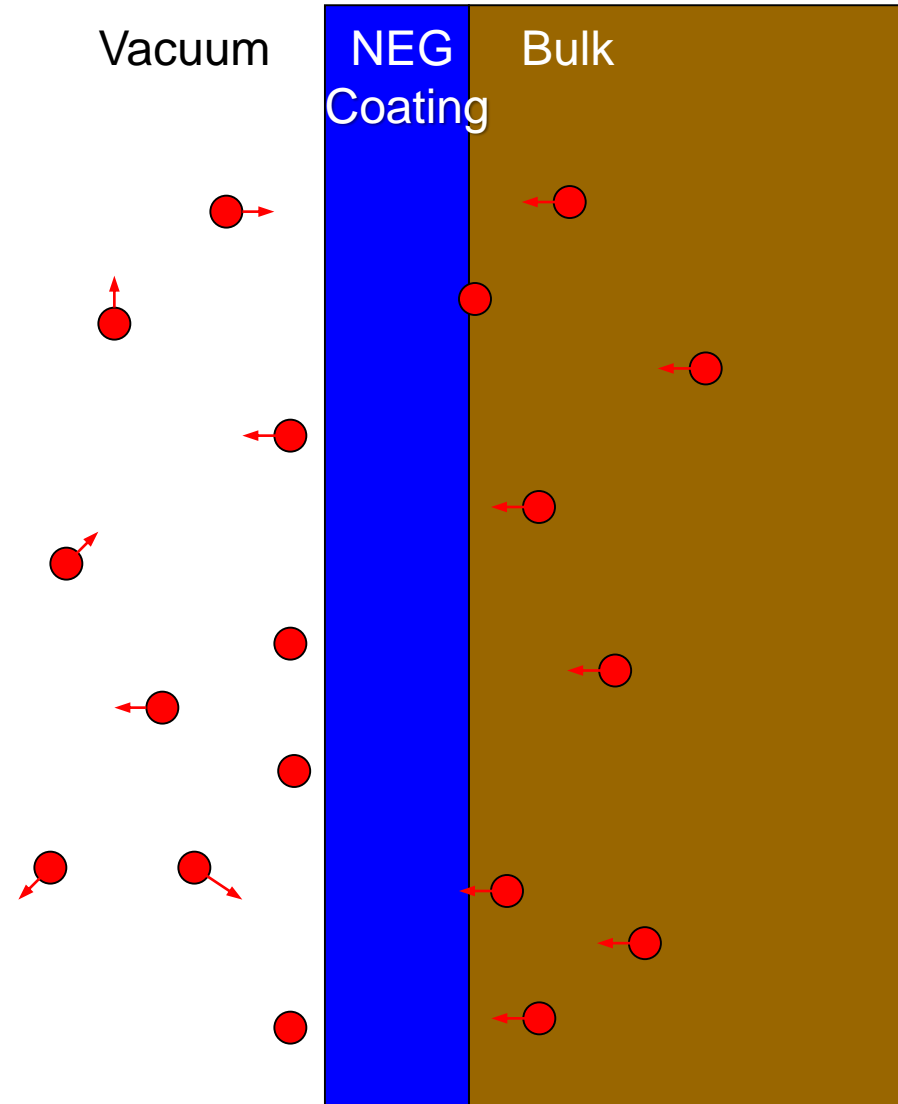
- A pure metal (Ti, Zr, V, Hf, etc.) film ~1- $\mu\text{m}$  thick without contaminants.
- A barrier for molecules from the bulk of vacuum chamber.

## 2) Increases distributed pumping speed, $S$ :

- A sorbing surface on whole vacuum chamber surface

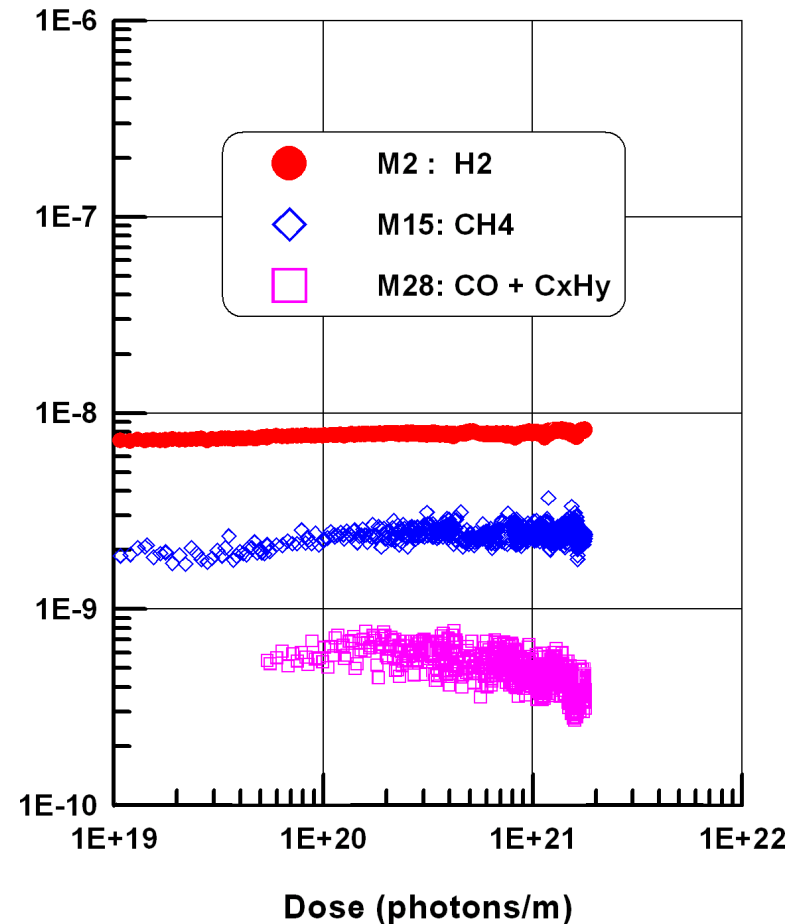
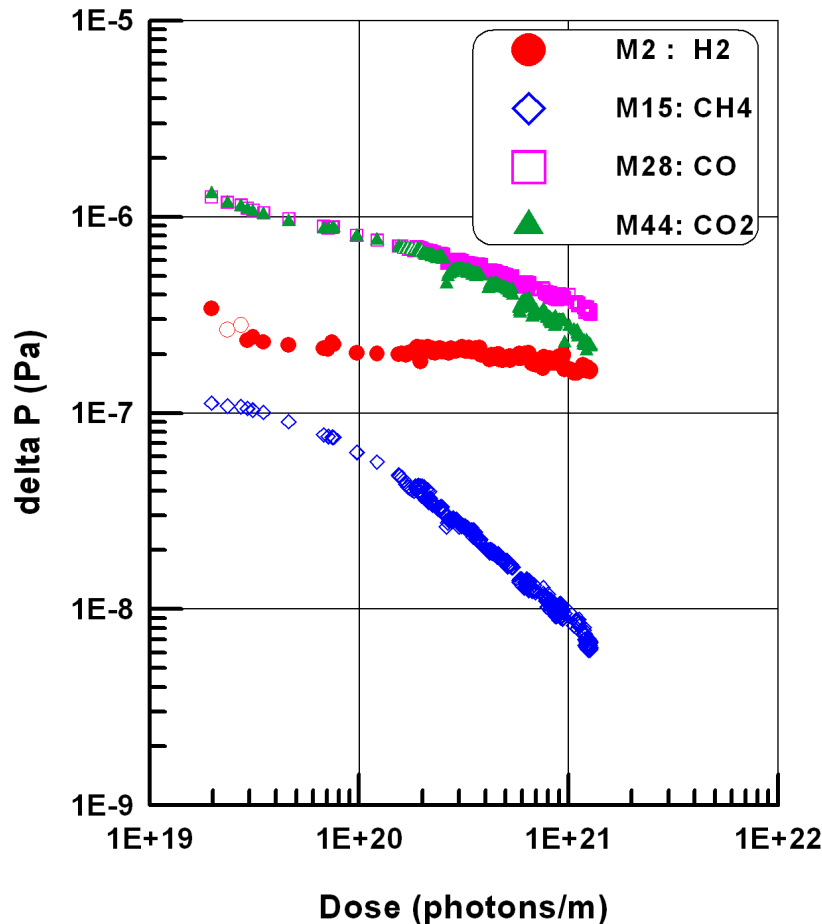
$$S = \alpha \cdot A \cdot v / 4;$$

where  $\alpha$  – sticking probability,  
 $A$  – surface area,  
 $v$  – mean molecular velocity



# Comparison of PSD from 316LN and NEG

Samples coated with Ti-Zr-V at CERN (Switzerland)  
Experiments on the SR beam line at BINP (Russia)



**Stainless Steel (baked at 300°C for 24 hrs)**

V.V. Anashin *et al*, Vacuum 75 (2004) p. 155.

**TiZrV coated vacuum chambers  
(activated at 190°C for 24 hrs)**

# Using these result for the ILC-DR design

Average pressure after 100 Ahr beam conditioning:

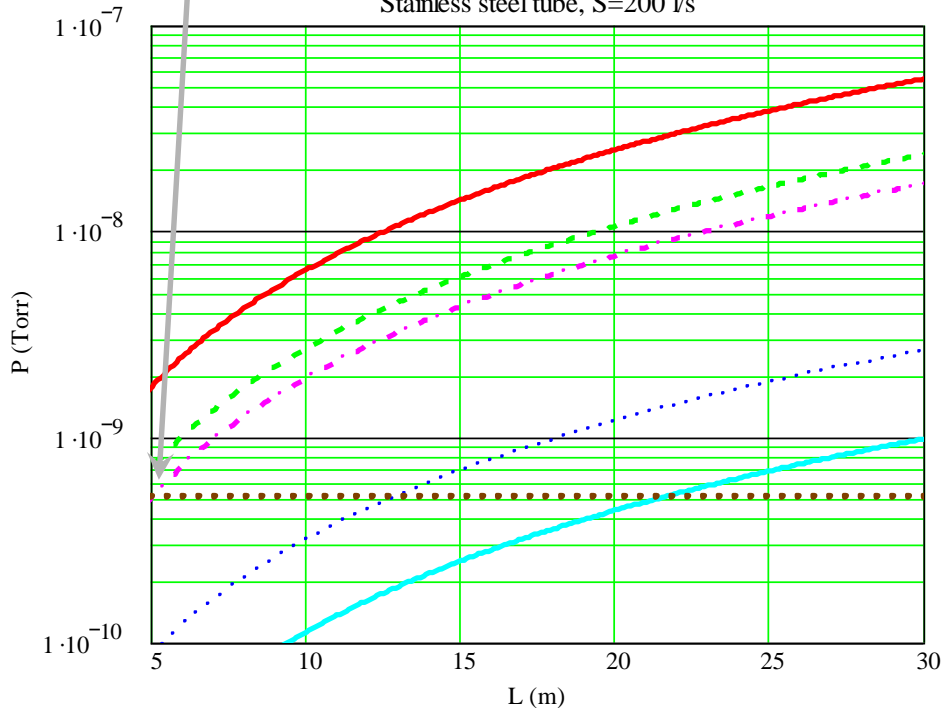
inside a stainless steel tube

$S_{\text{eff}} = 200$  l/s every 5 m

inside a NEG coated tube

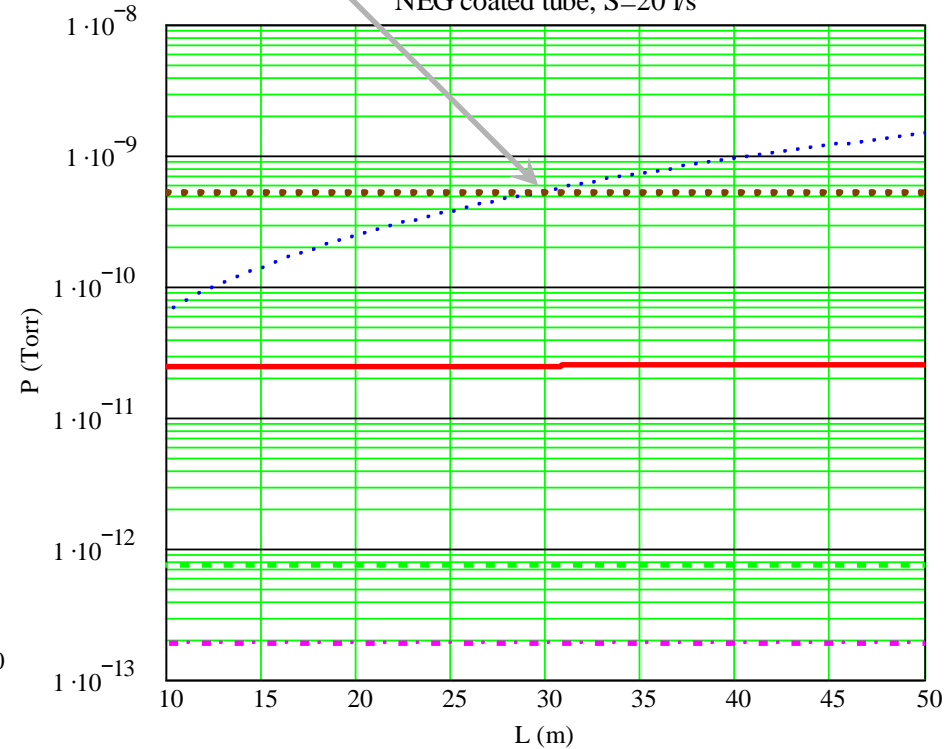
$S_{\text{eff}} = 20$  l/s every 30 m

Stainless steel tube,  $S=200$  l/s



- H2
- CH4
- - - CO
- CO2
- Thermal desorption
- Required CO pressure

NEG coated tube,  $S=20$  l/s



- H2
- CH4
- - - CO
- CO2
- Required CO pressure

# NEG coating for accelerators

- First used in the ESRF (France);
- ELETTRA (Italy);
- Diamond LS (UK);
- Soleil (France) – first fully NEG coated;
- **LHC** (Switzerland) – longest NEG coated vacuum chamber;
- SIS-18 (Germany); MAX-IV (Sweden); Solaris (Poland)
- and many others.

Meanwhile:

- **NEG film capacity for CO and CO<sub>2</sub> is ~1 ML:**
  - If  $P = 10^{-9}$  mbar then 1 ML can be sorbed just in  $\sim 10^3$  s;
  - Lab measurements of different NEG coatings often don't repeat CERN's data on sticking probability and capacity;
  - **However, NEG coated parts of accelerators work well.**

# What else is required?

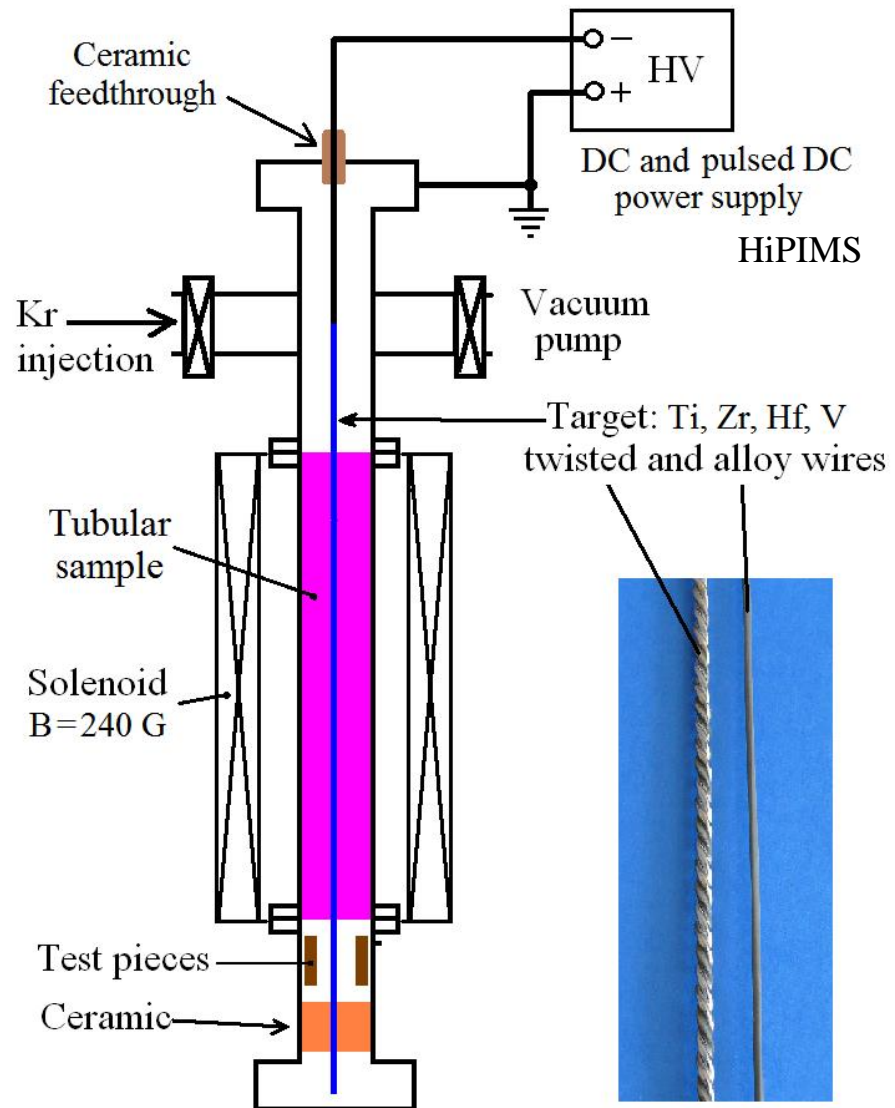
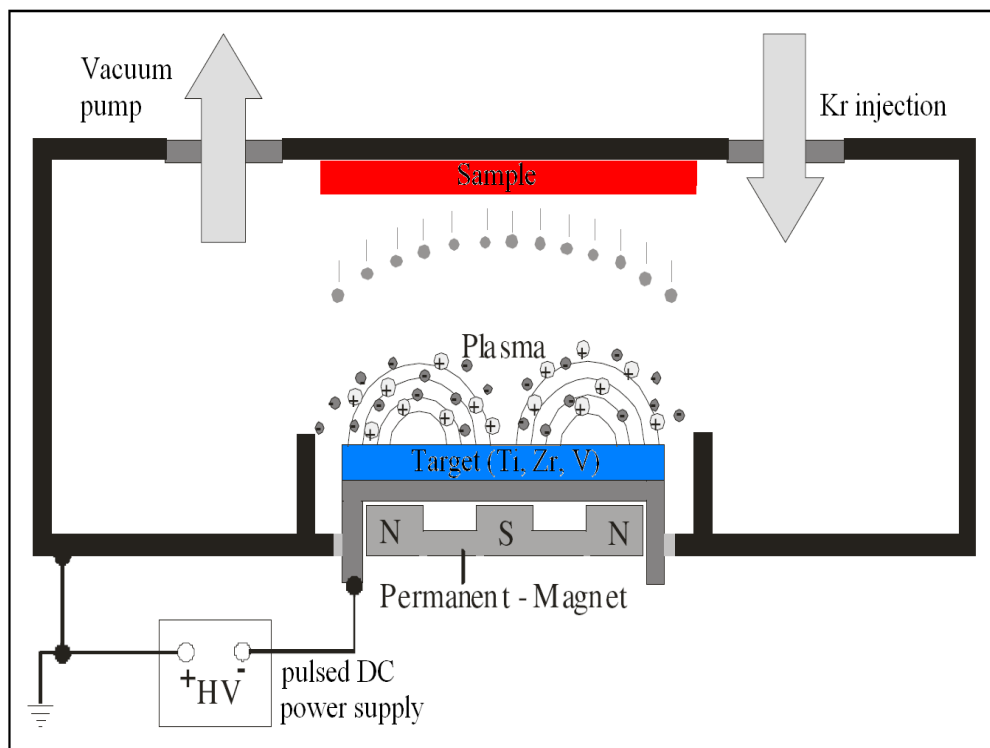
- Input data for accelerator design:
  - $\eta(D, E, T_a)$ ,  $\alpha(M, T_a)$ , pumping capacity;
- Better understanding:
  - what and why;
  - practical 'do's and 'don't's;
- Further development of this coating:
  - lower  $\eta$ ,  $T_a$ , SEY;
  - higher  $\alpha(M)$ , pumping capacity;
  - optimising for an application.



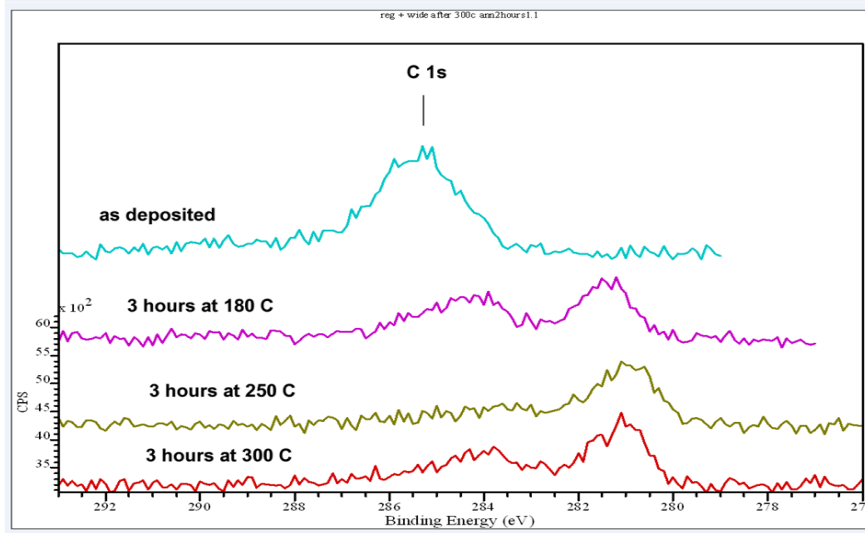
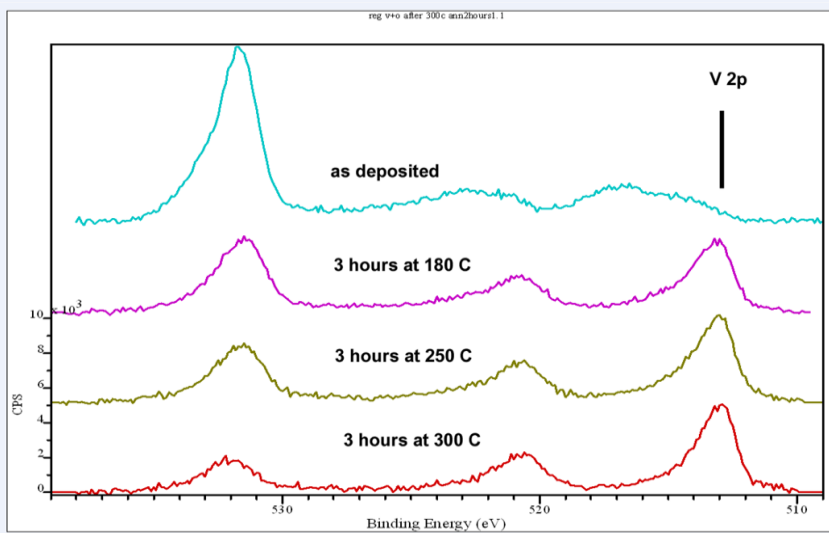
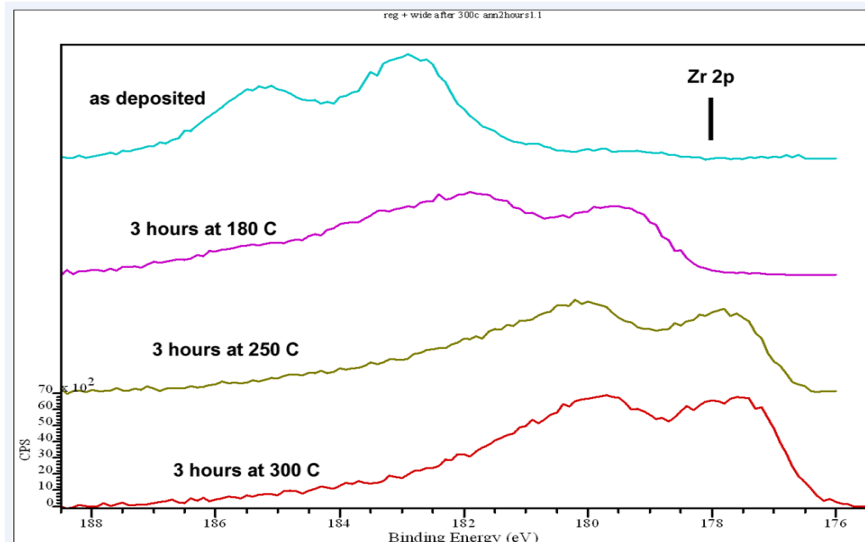
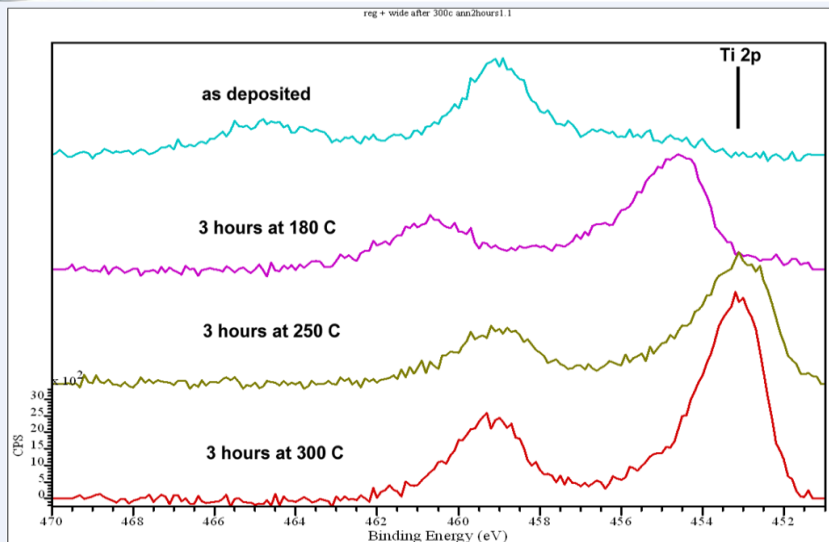
# Deposition method

## Cylindrical magnetron deposition for vacuum chambers

### Commonly used planar magnetron deposition

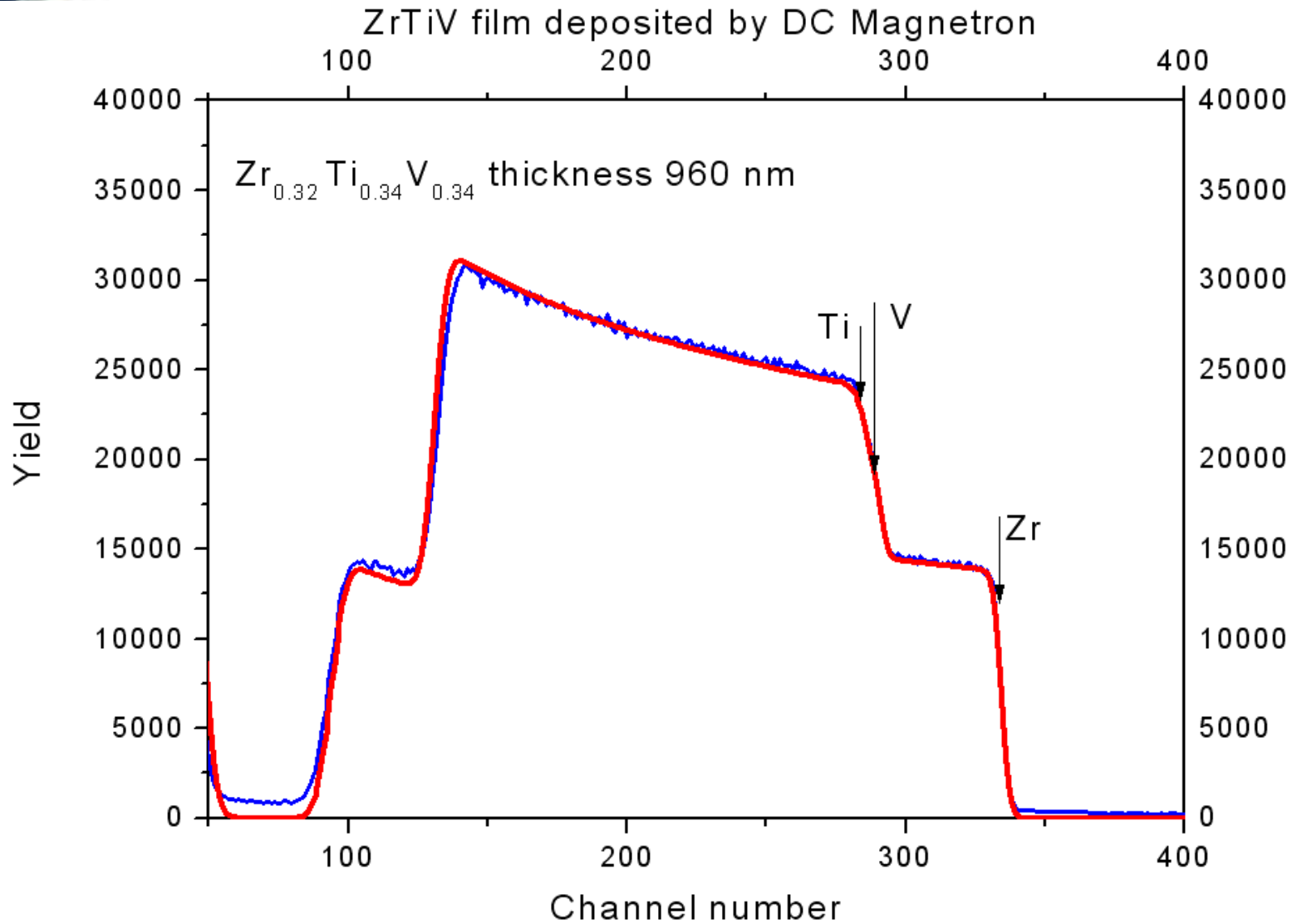


# Region scan of XPS core levels of Ti, Zr, C and V of a Ti-Zr-V film (surface composition and chemical bounding)



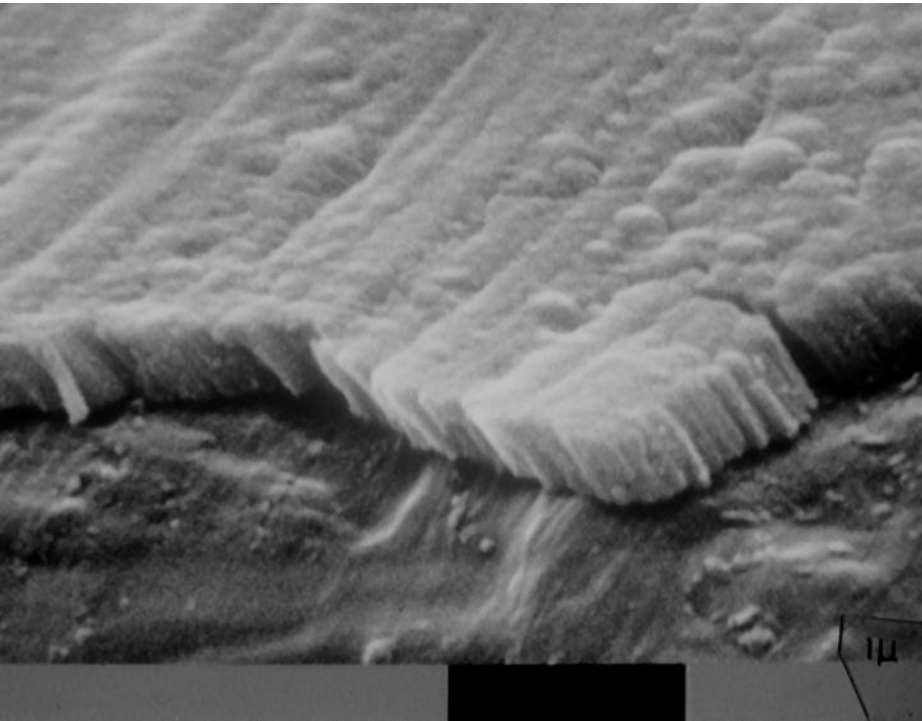


# RBS (film compositions in bulk)

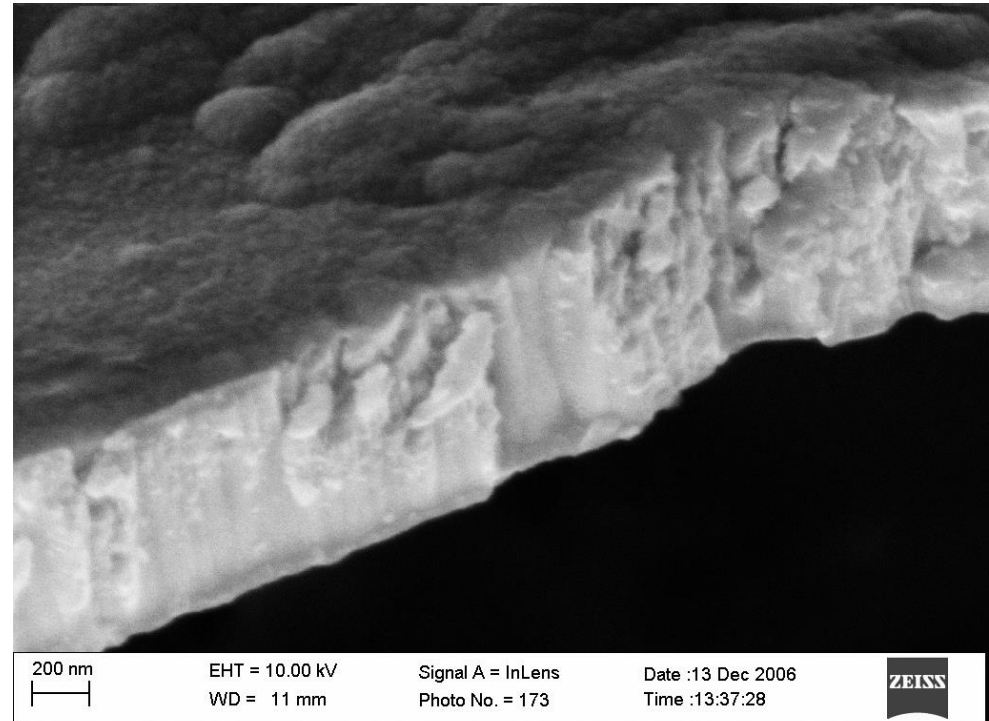


# SEM images of films (film morphology)

columnar



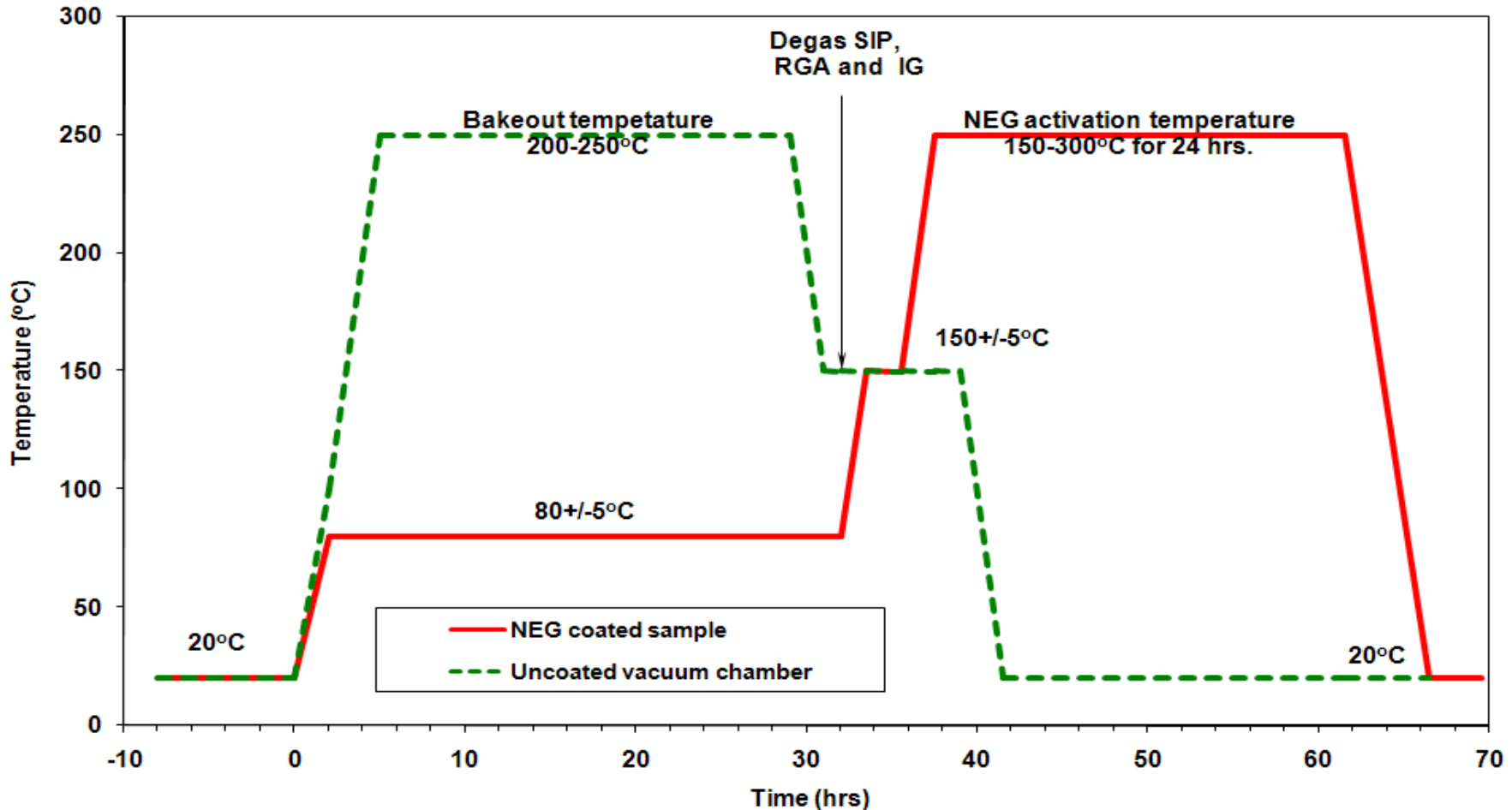
dense



O.B. Malyshev, R. Valizadeh, J.S. Colligon *et al.* J. Vac. Sci. Technol. A 27 (2009), p. 521.



# ASTeC activation procedure

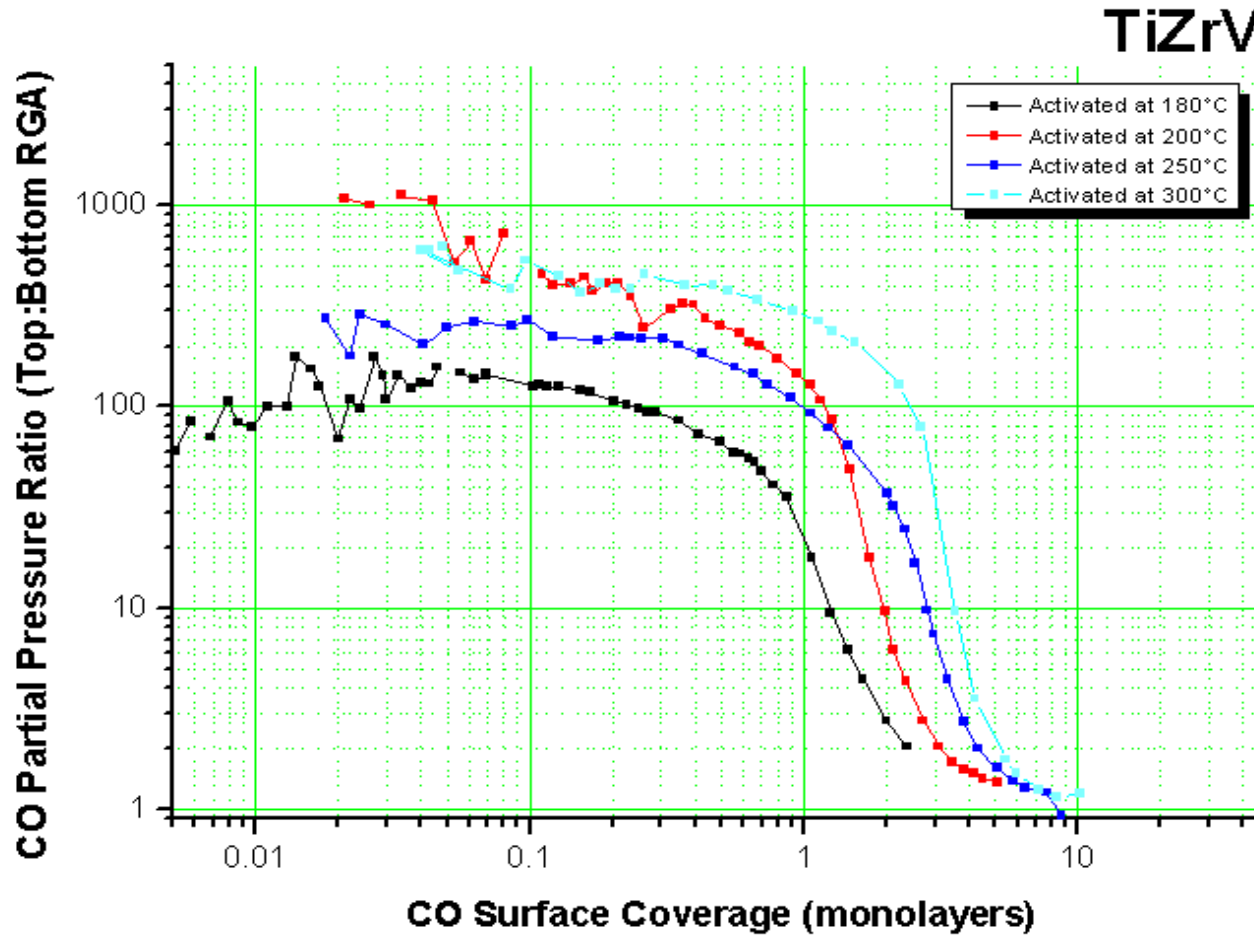


## Advantages of ASTeC activation procedure:

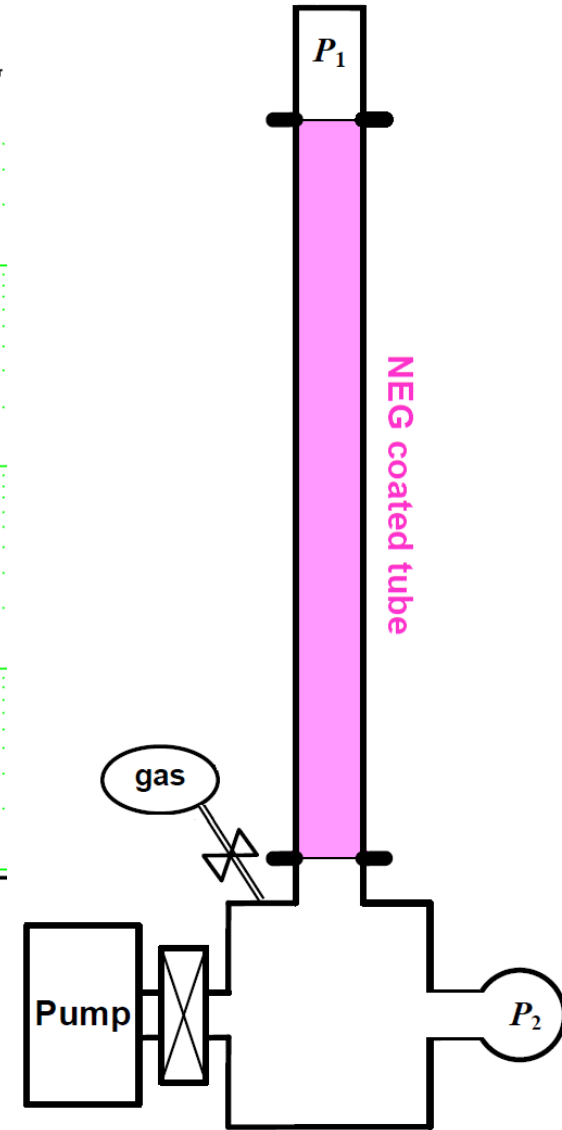
- better activation (less poisoning by das from uncoated parts),
- lower electricity cost,
- lower total thermal expansion.

O.B. Malyshev, K.J. Middleman, J.S. Colligon and R. Valizadeh. *J. Vac. Sci. Technol. A* 27 (2009), p. 321.

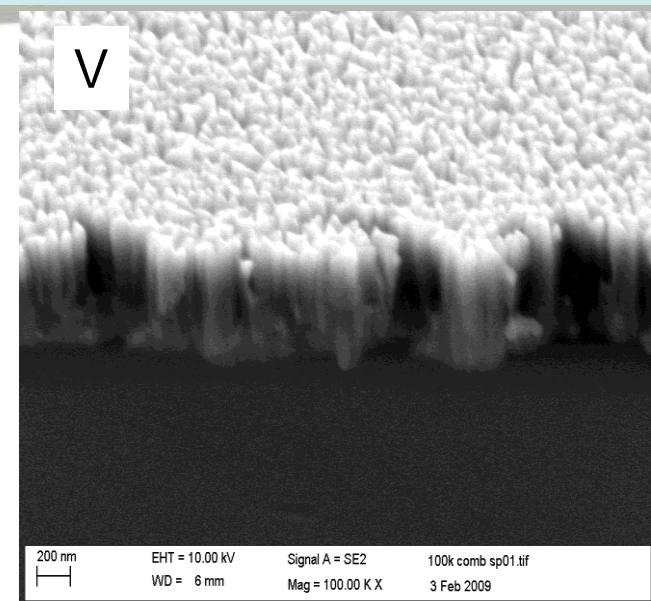
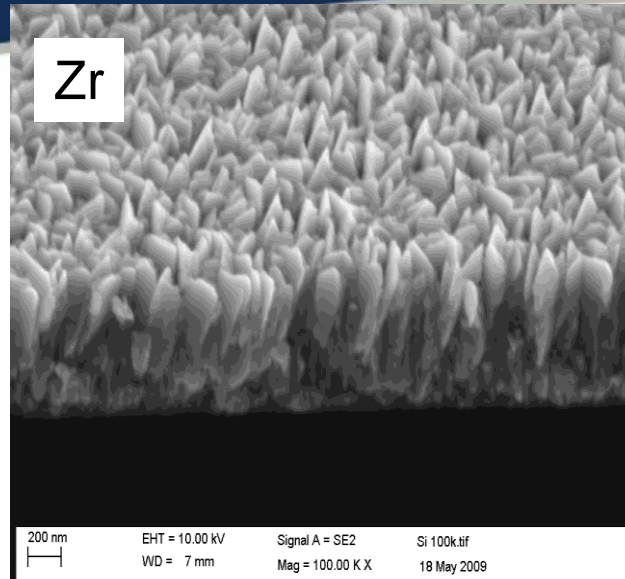
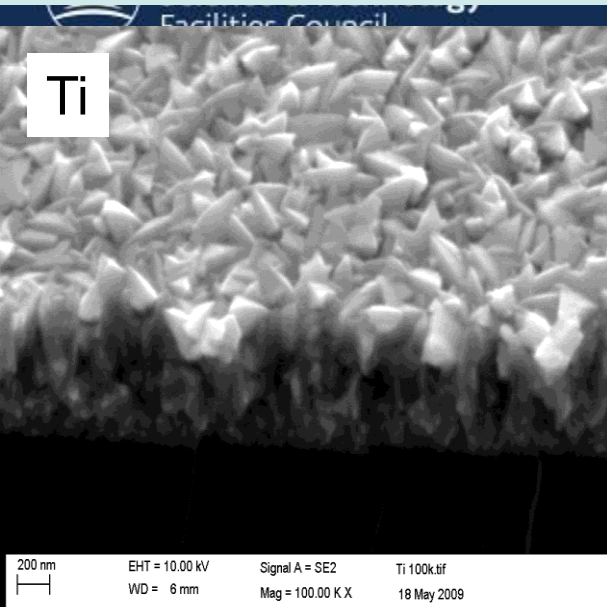
# NEG pumping properties



Pressure ratio  $P_1/P_2$  measured during gas injection is used to estimate:  
 initial sticking probability and sorption capacity



# Thin films deposited on Si sample from a single metal wire



## Cylindrical Magnetron:

Power = 60 W,  $P_{Kr} = 10^{-2}$  mbar,  
Deposition rate = 0.14-0.16 nm/s,  
 $T = 120^{\circ}\text{C}$ .

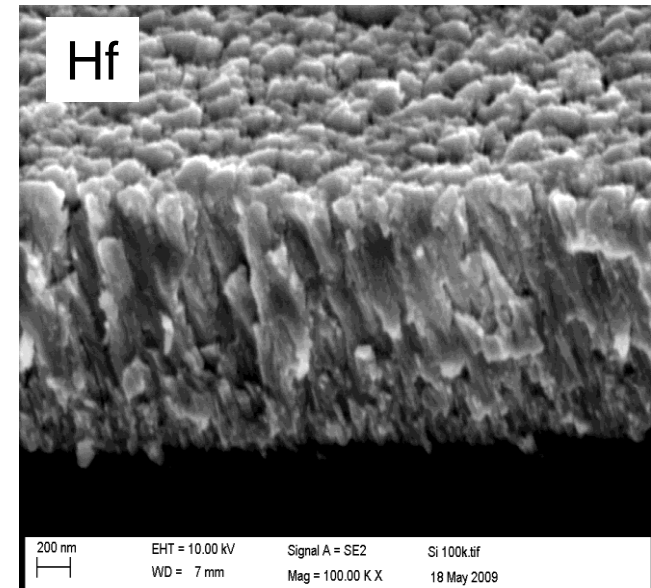
Average grain size: 100 – 150 nm.

Ti:

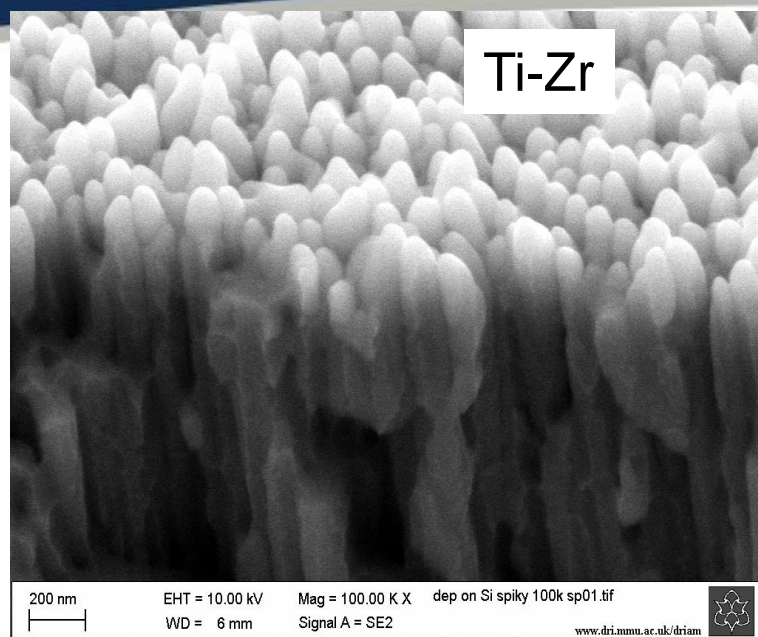
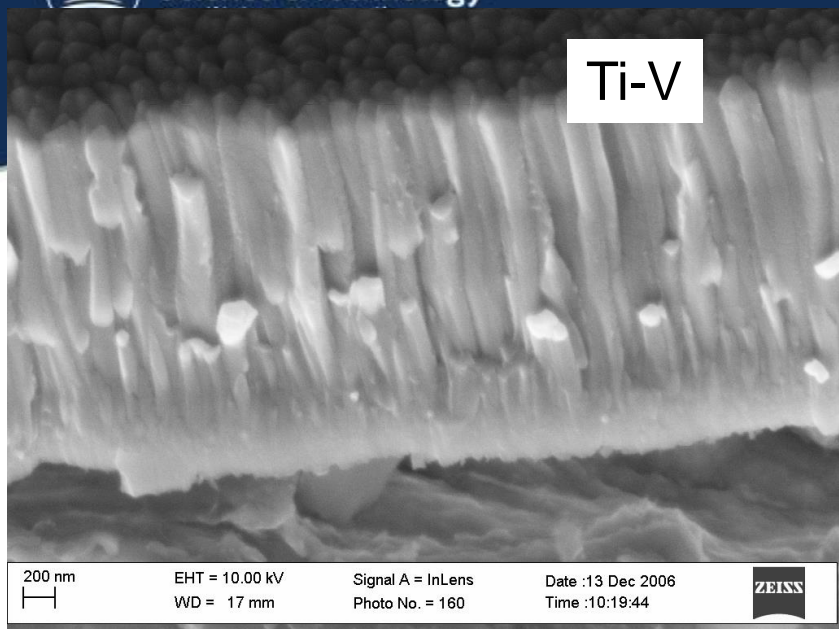
Zr: Hexagonal lattice structure

V: Rhombohedral lattice structure

Hf: Hexagonal lattice structure



# Thin film deposited on Si sample from two twisted wires



## Cylindrical Magnetron:

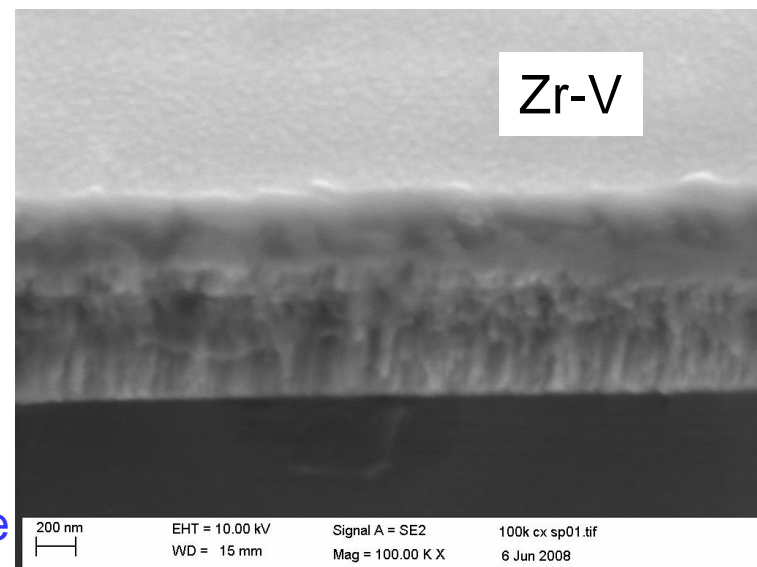
Power = 60 W,  $P_{Kr} = 10^{-2}$  mbar,  
Deposition rate = 0.13-0.16 nm/s,  
 $T = 120^{\circ}\text{C}$ .

## Average grain size:

Ti-V: 50 – 100 nm, Hexagonal lattice structure

Ti-Zr: 50 – 100 nm, Hexagonal lattice structure

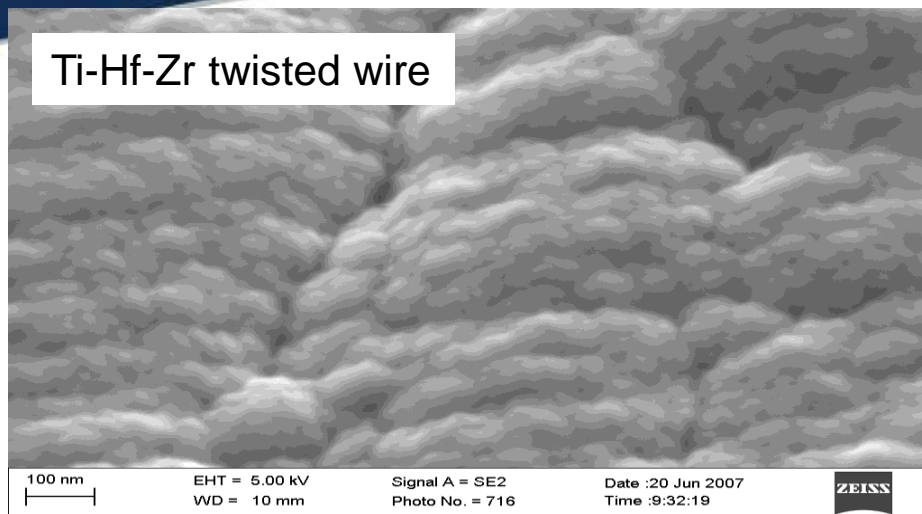
Zr-V: **10 – 20 nm**, Rhombohedral lattice structure



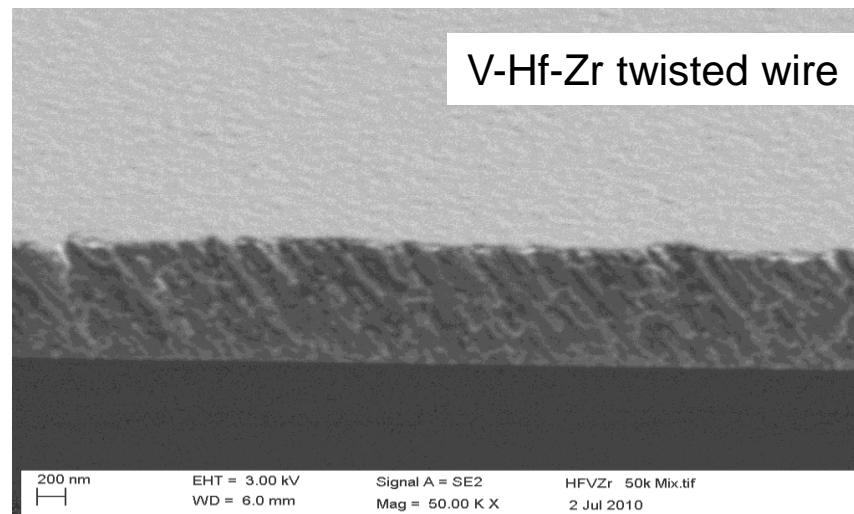


# Ternary NEG film deposited on Si test sample from twisted Ti, V, Zr, and Hf wires and TiZrV alloy wire

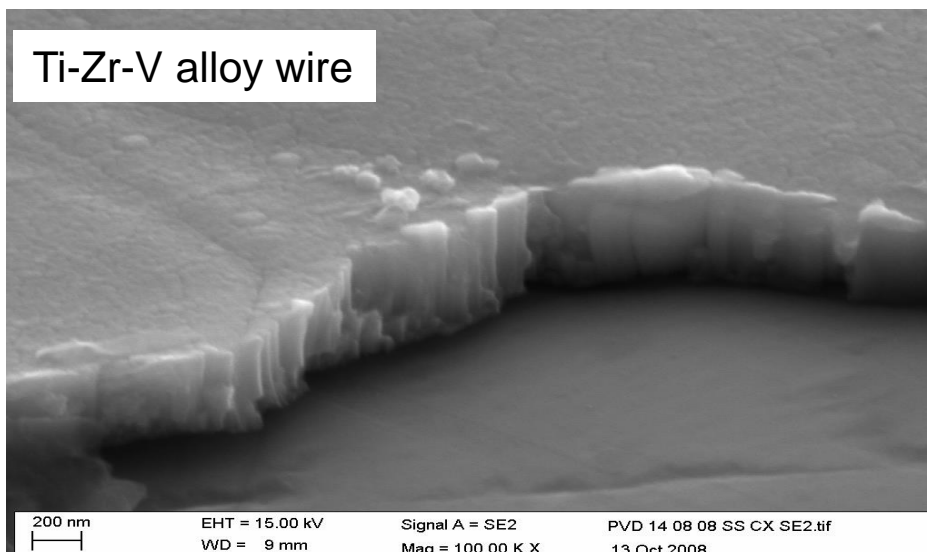
Ti-Hf-Zr twisted wire



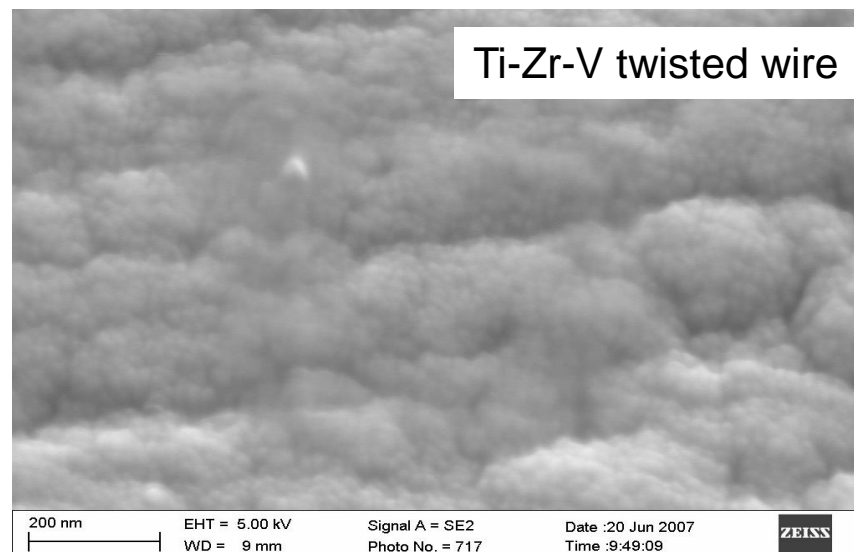
V-Hf-Zr twisted wire



Ti-Zr-V alloy wire

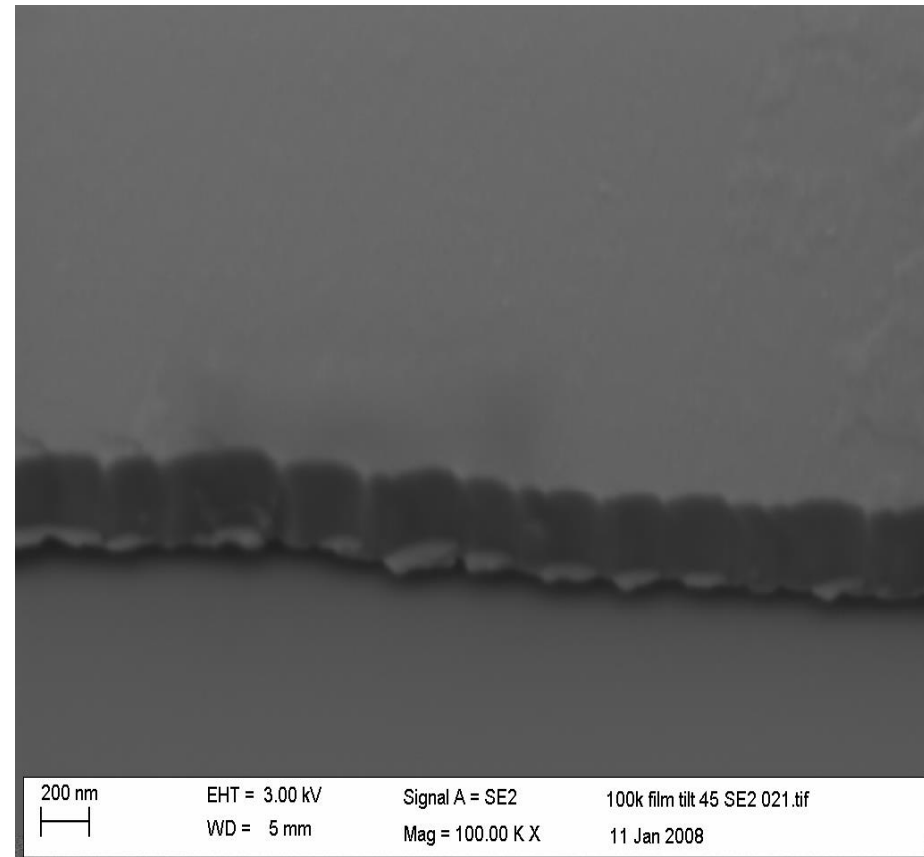
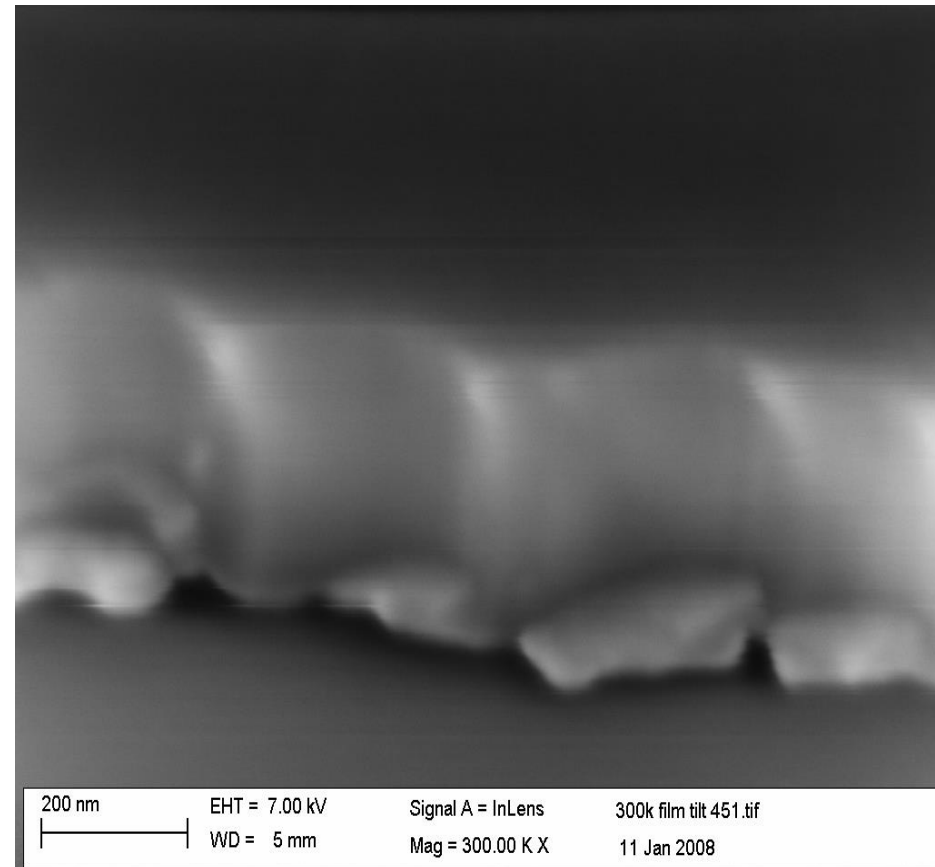


Ti-Zr-V twisted wire



Cylindrical Magnetron: Power = 60 W,  $P_{Kr} = 10^{-2}$  mbar, deposition rate = 0.12 nm/s,  $T = 120^\circ\text{C}$ .  
Average grain size 5 nm. Hexagonal lattice structure.

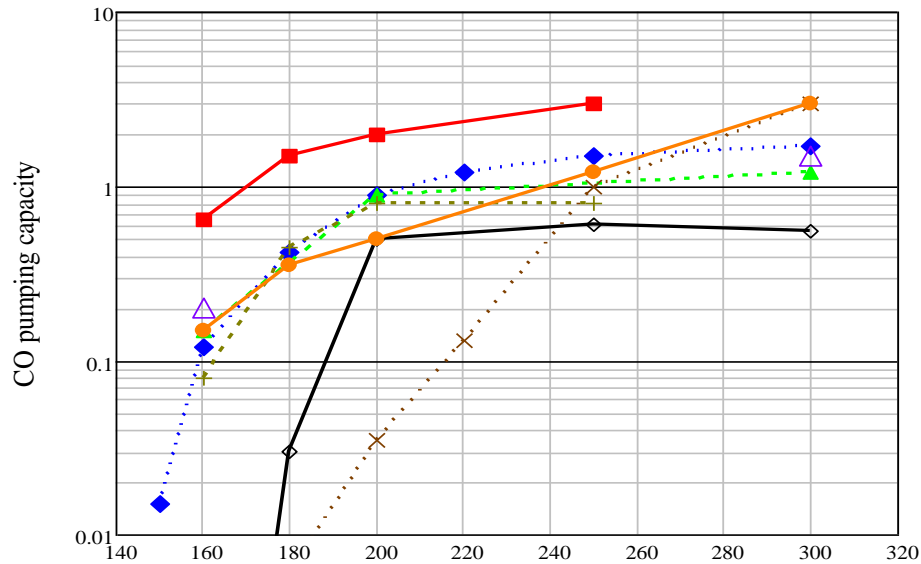
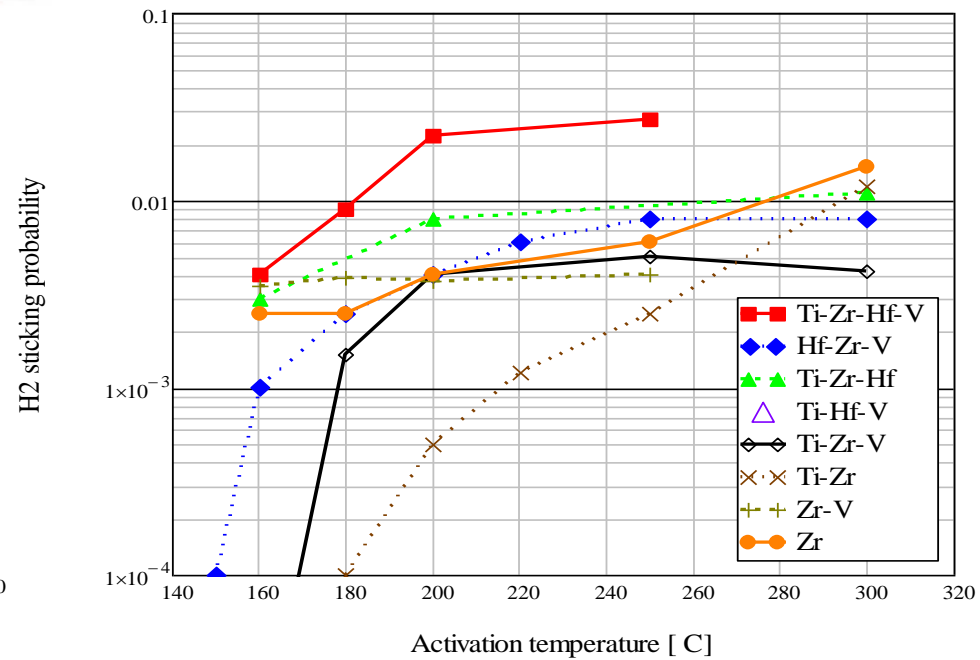
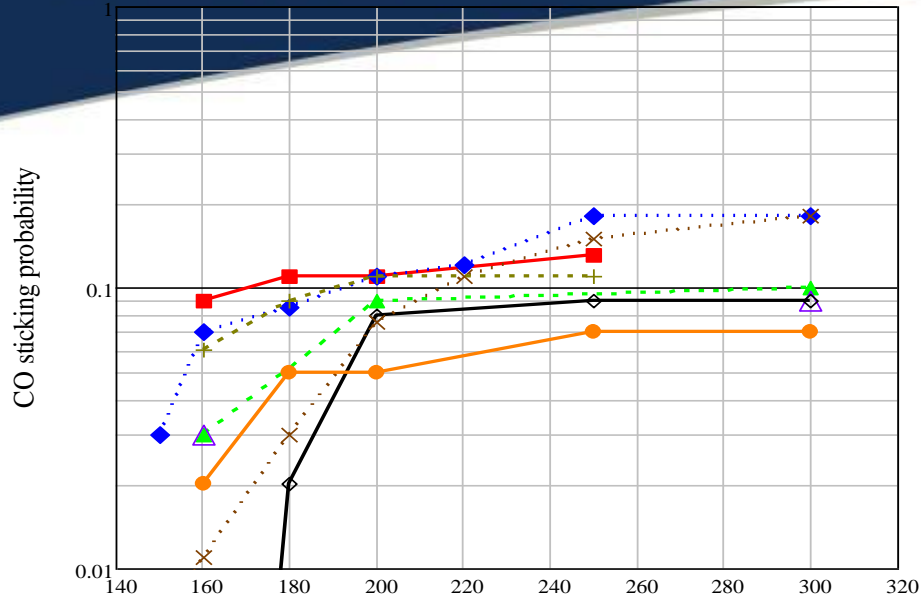
# Quaternary NEG alloy film deposited on Si test sample from twisted Ti, V, Zr, and Hf wires



Cylindrical Magnetron: Power = 60 W,  $P_{Kr} = 10^{-2}$  mbar, deposition rate = 0.12 nm/s,  $T = 120^{\circ}\text{C}$ .  
Very glassy structure.



# Pumping properties of some NEG films



**Ti-Zr-Hf-V** is the best  
**Hf-Zr-V**, **Ti-Zr-Hf**, **Ti-Hf-V** and **Zr** are comparable  
**Ti-Zr-V** is lower  
**Zr-V** (best binary alloy) has the lowest activation temperature



# Pressure in the accelerator vacuum chamber

$$P \propto \frac{\eta}{\alpha}$$

where

$\eta$  - desorption yield (photon, electron or ion stimulated desorption)

$\alpha$  - sticking probability

- Improving pumping properties is limited:

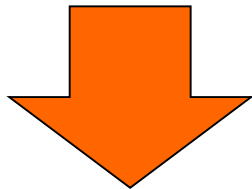
$$\alpha \leq 1$$

- $0.005 < \alpha_{H_2} < 0.02$
- $0.1 < \alpha_{CO} < 0.5$
- $0.4 < \alpha_{CO_2} < 0.6$

- Reducing the desorption yields  $\eta$  in orders of magnitude was our aim

# Reducing the gas desorption from the NEG coatings

- Main gases in the NEG coated vacuum chamber are  $H_2$  and  $CH_4$ 
  - Only  $H_2$  can diffuse through the NEG film under bombardment or heat
  - $CH_4$  is most likely created on the NEG surface from diffused  $H_2$  and C (originally from sorbed CO and  $CO_2$ )
  - Therefore the  $H_2$  diffusion must be suppressed



- Where  $H_2$  come from?



# Reducing the gas desorption from the NEG coatings

Gas molecules are contained  
on the NEG coating surface

after exposure to air

minimise exposure to air

inside the NEG coating

trapped during deposition

purity of discharge gas

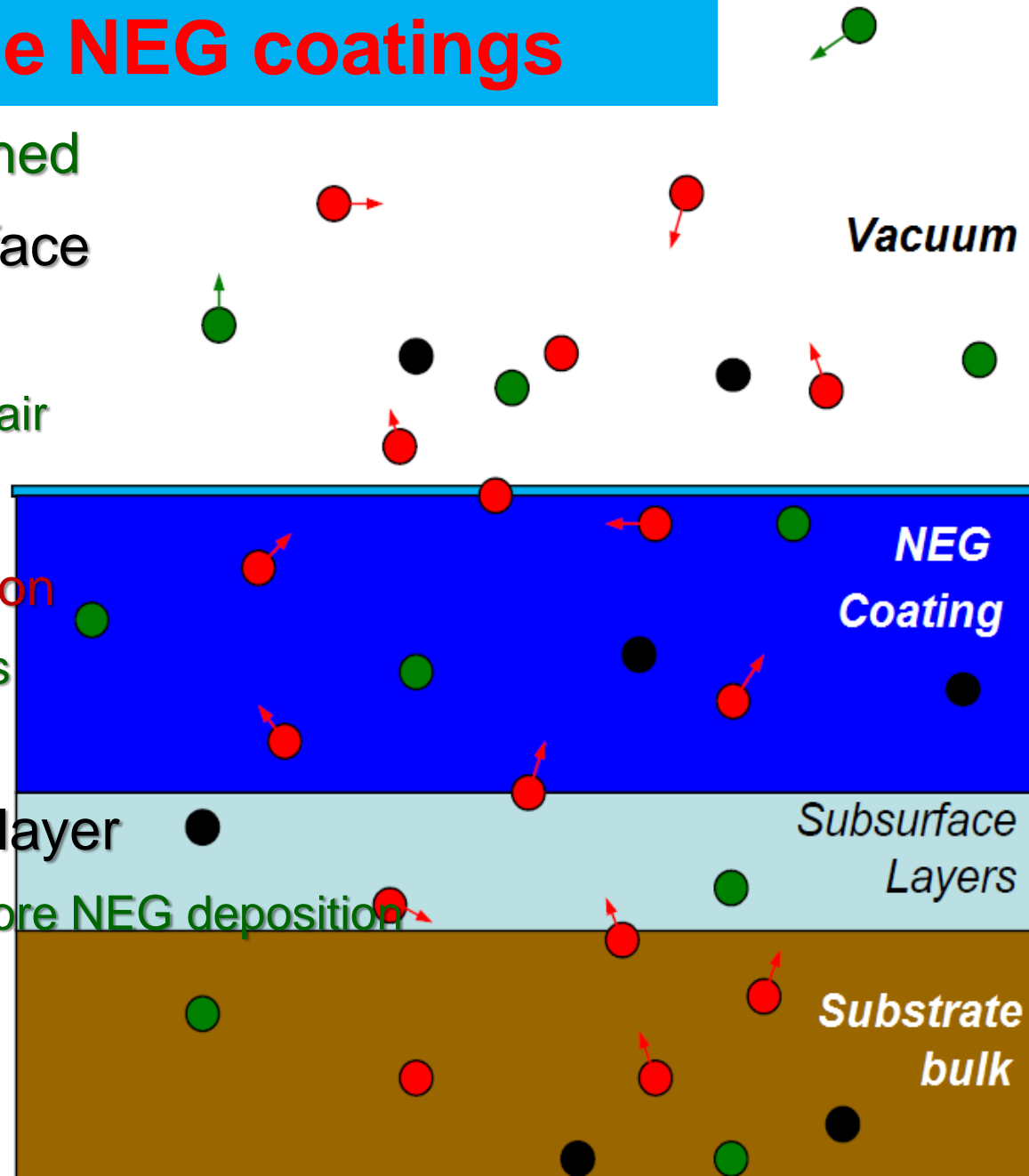
background pressure

in subsurface substrate layer

substrate bakeout before NEG deposition

in the substrate bulk

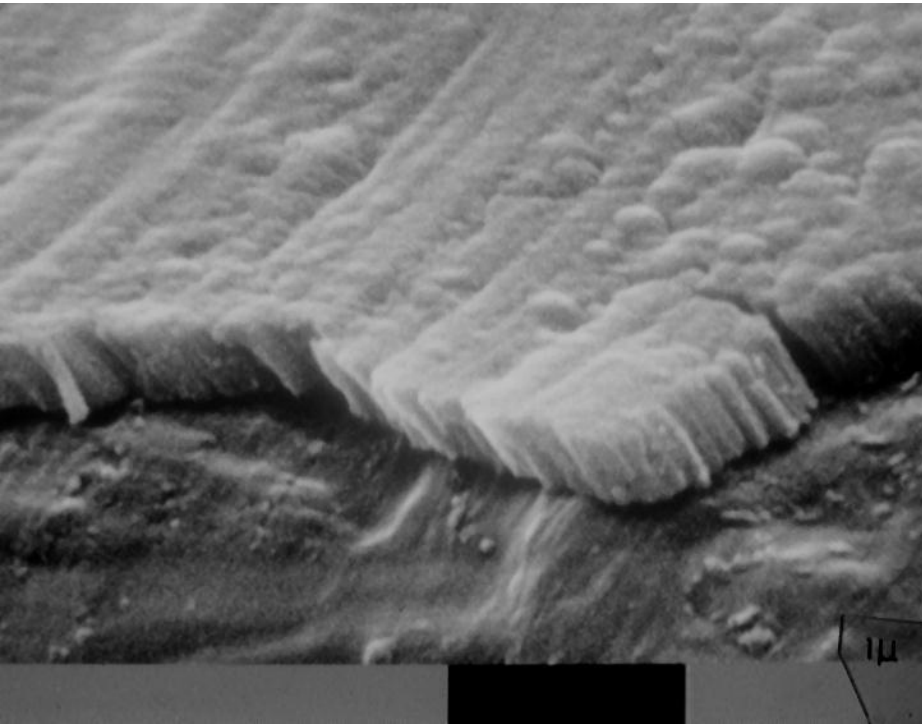
vacuum firing



# SEM images of films (film morphology)

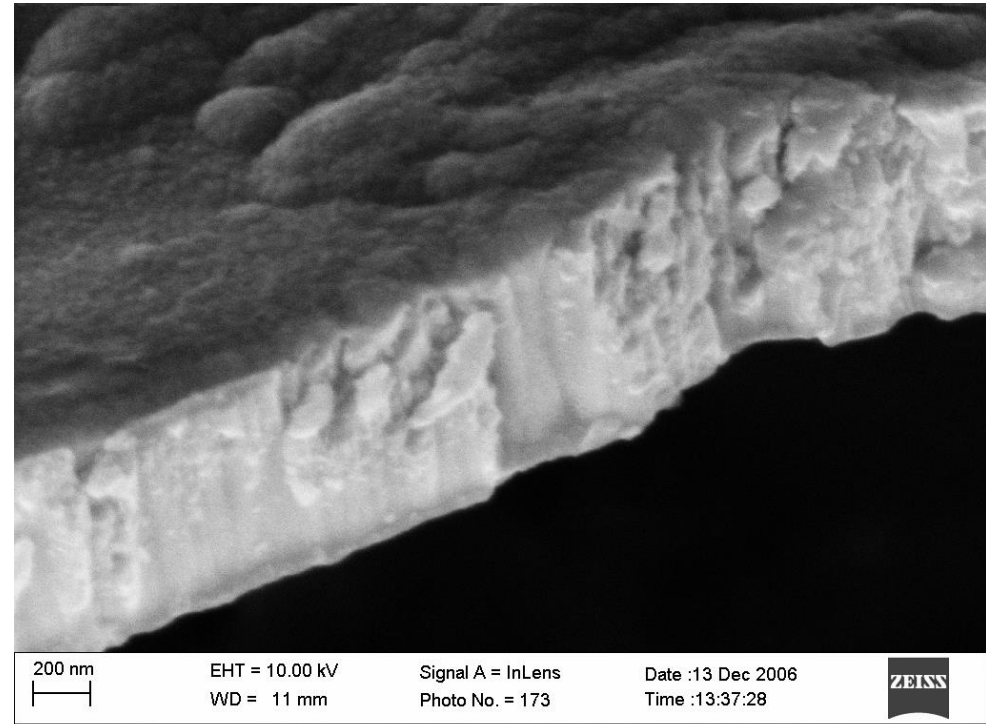
columnar

Best for pumping



dense

A first candidate for a barrier



O.B. Malyshev, R. Valizadeh, J.S. Colligon *et al.* J. Vac. Sci. Technol. A 27 (2009), p. 521.



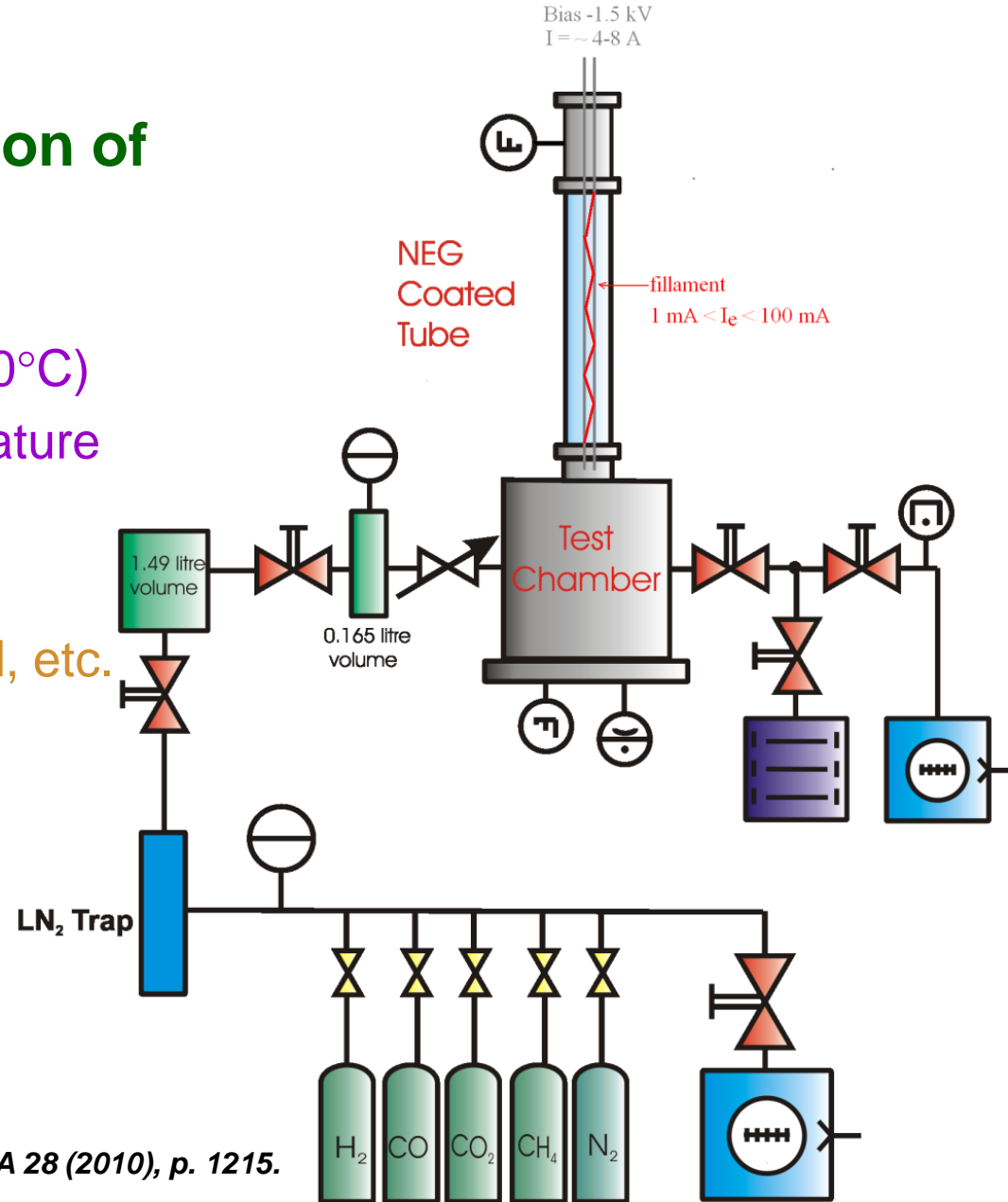
# Electron stimulated desorption facility

## ESD is studied as a function of

- Electron energy
- Dose
- Wall temperature (-5 to +70°C)
- Activation/bakeout temperature

## Can be used for samples with:

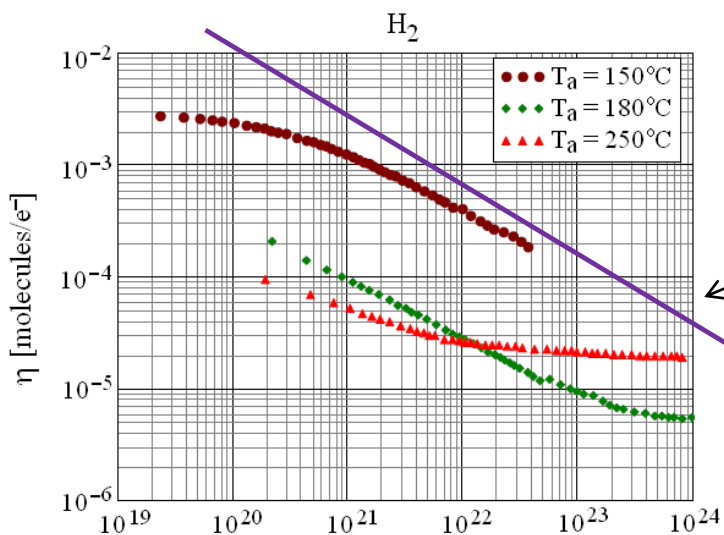
- Specially treated samples
  - Vacuum fired, polished, etc.
- Low desorption coating
- No coatings
- NEG coating
  - ESD measurements
  - Sticking probability measurements



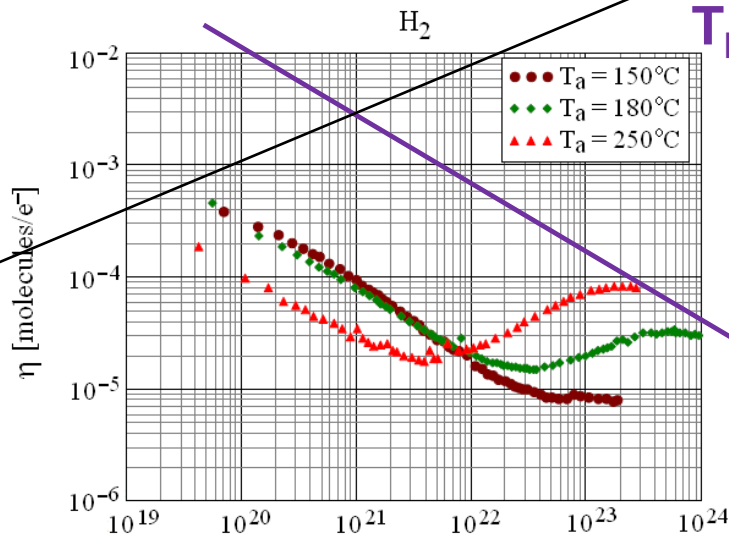


# ESD yield from NEG coated samples

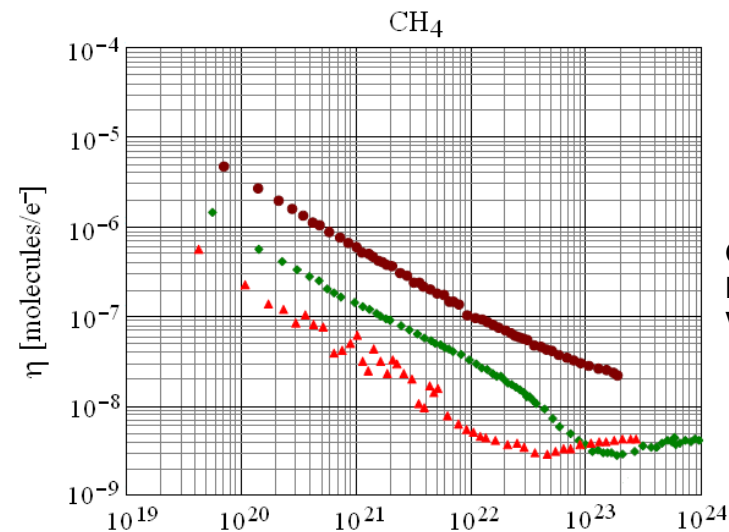
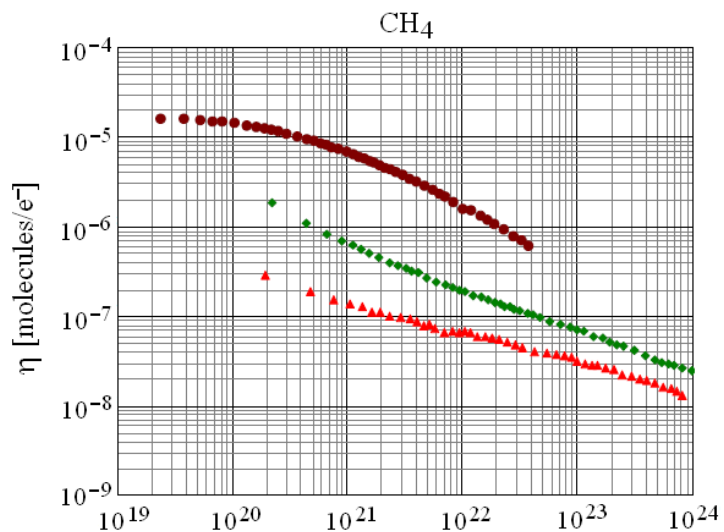
(a) Dense film



(b) Columnar film



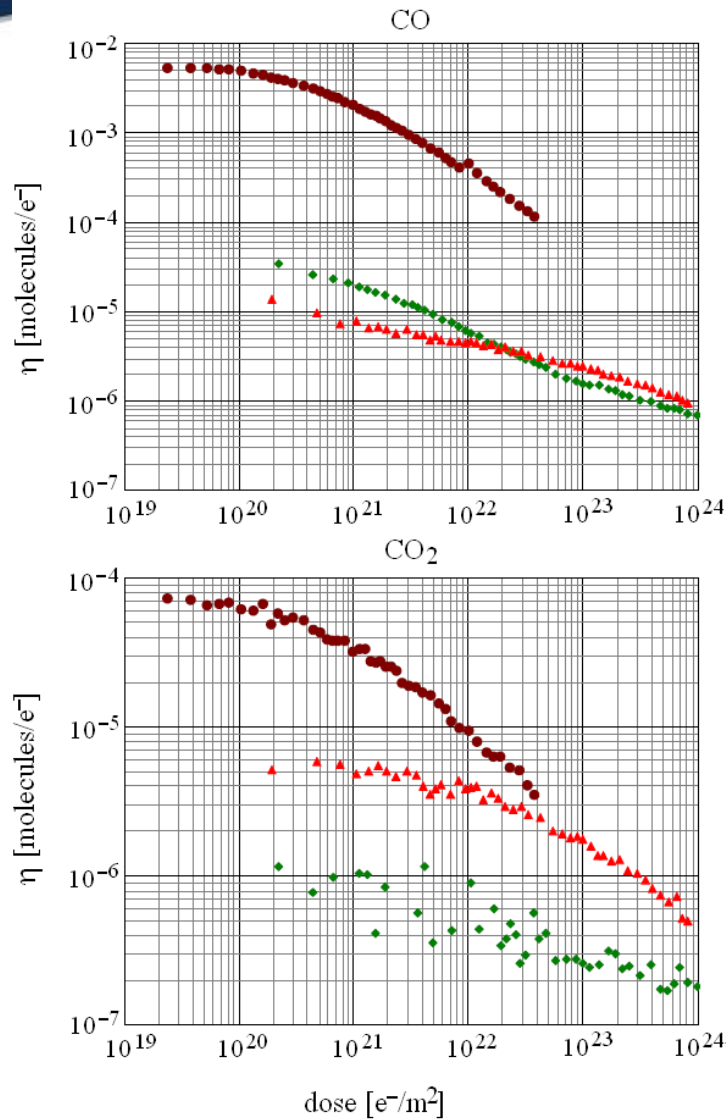
316LN  
 $T_b = 250^\circ C$



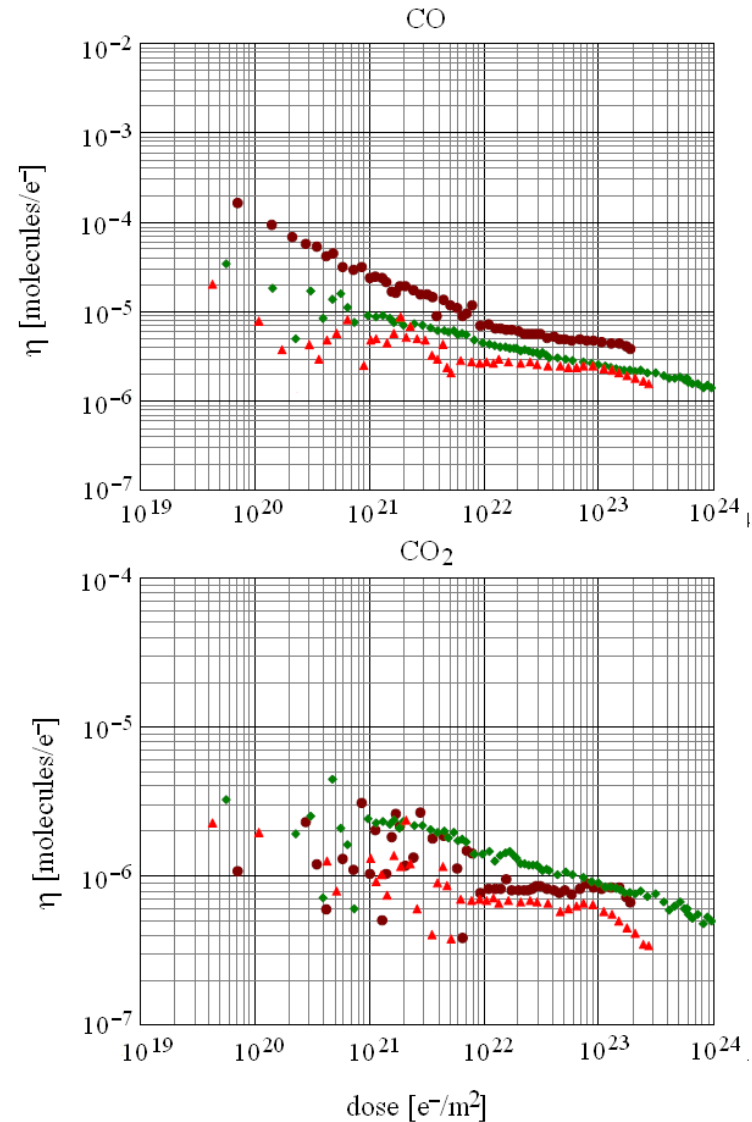
O.B. Malyshev,  
 R. Valizadeh, et al.  
 Vacuum 86, 2035 (2012).

# ESD yield from NEG coated samples

(a) Dense film

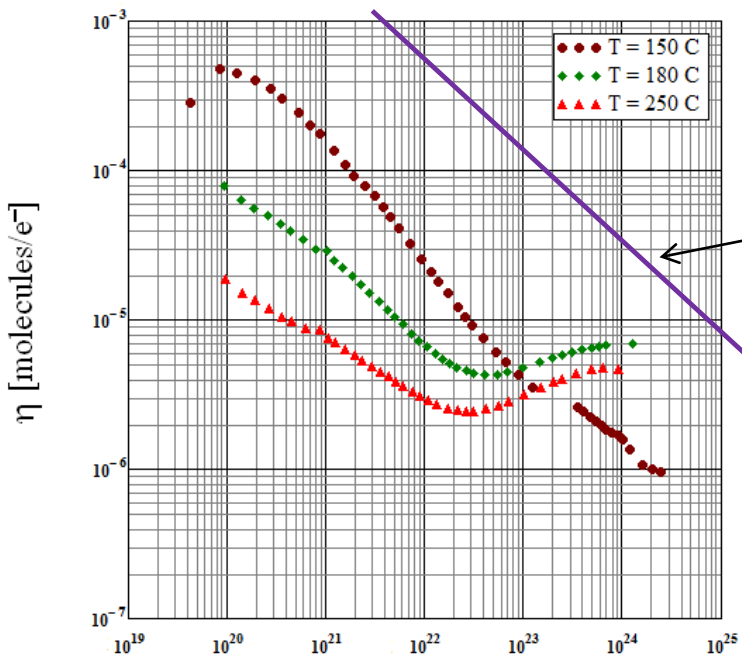


(b) Columnar film

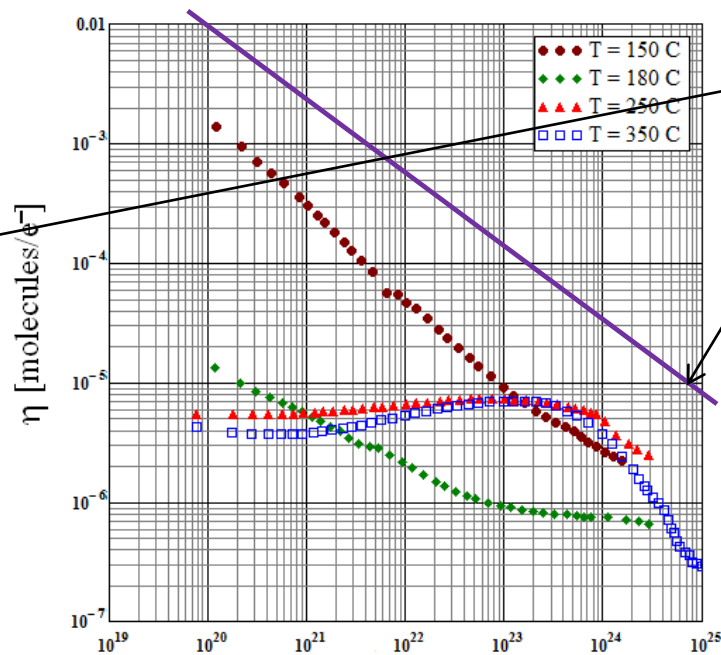


# H<sub>2</sub> ESD from NEG coated vacuum fired 316LN

(a) Columnar film



(b) Dense film

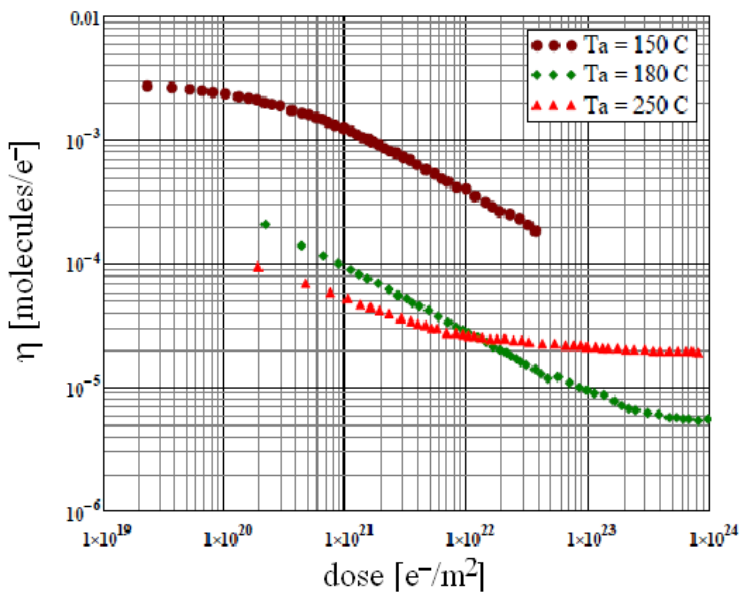
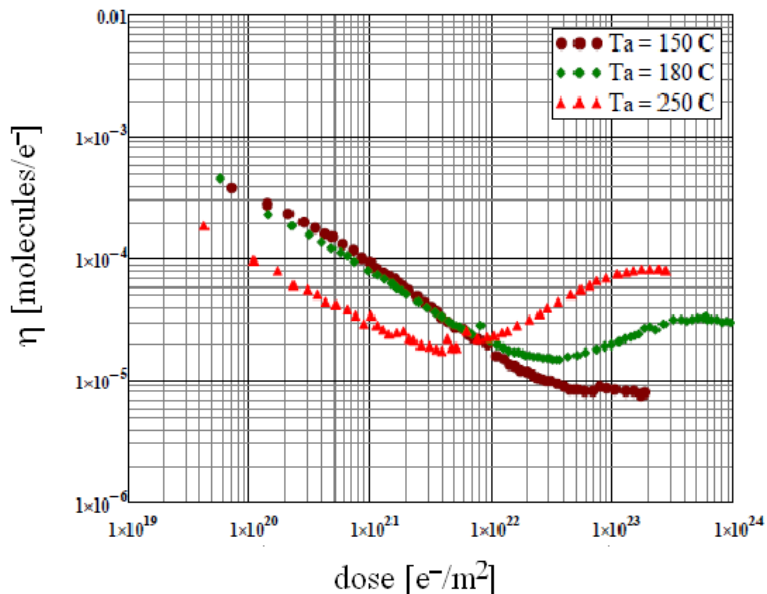


316LN  
T<sub>b</sub>=250°C

O.B. Malyshev,  
R. Valizadeh, et al.  
JVST A 32, 061601  
(2014)

Vacuum fired

No vacuum firing



O.B. Malyshev,  
R. Valizadeh, et al.  
Vacuum 86, 2035  
(2012).

# Dual layer

*Vacuum*

- **Columnar layer:**
  - Activated at lower temperature
  - Provides higher sticking probability and pumping capacity
- **Dense layer:**
  - Provides lower ESD
- **Dual Layer:**
  - Combines benefit of both
  - For more details: see A. Hannah's poster EM286 on Thursday

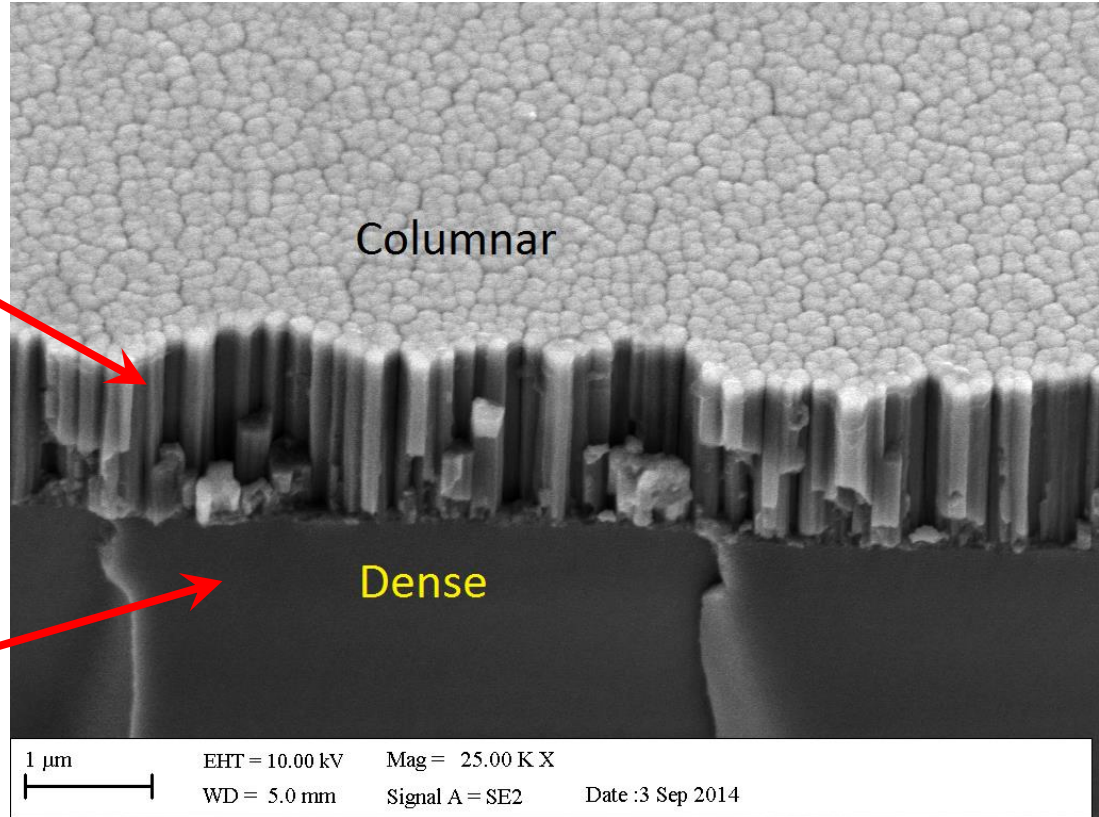
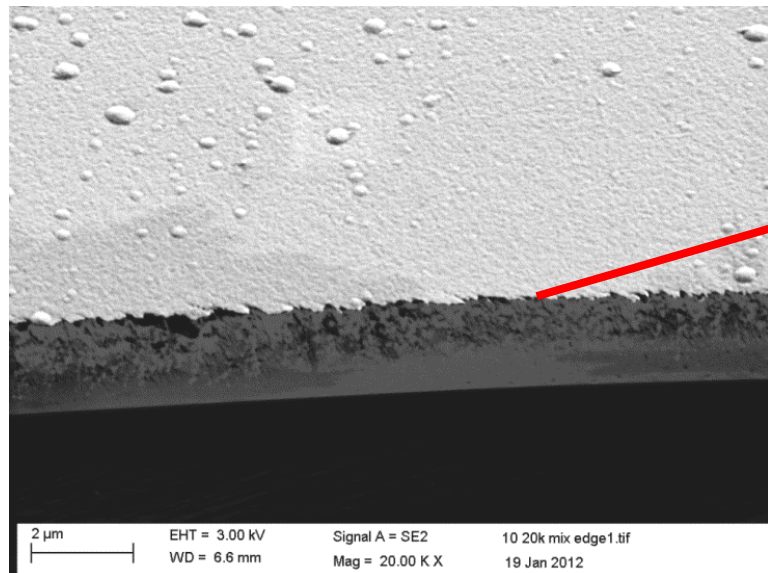
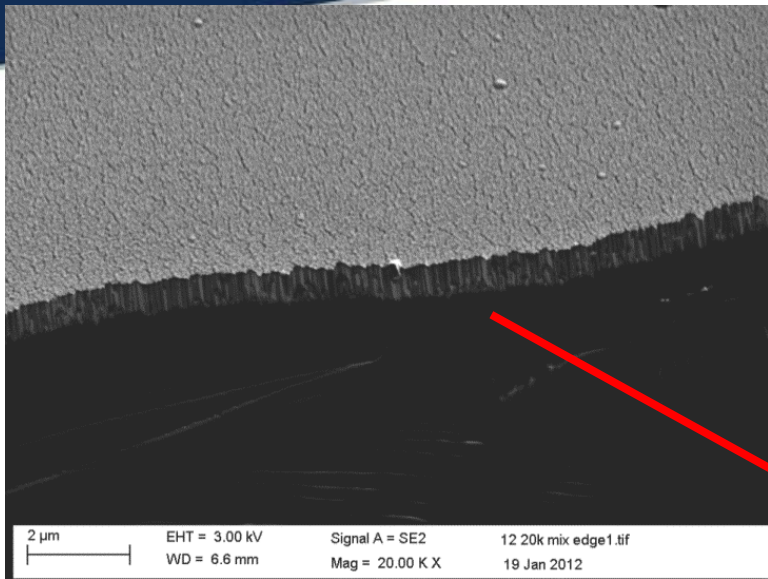
*Columnar NEG Coating*

*Dense NEG Coating*

*Bulk metal*



# Dual layer



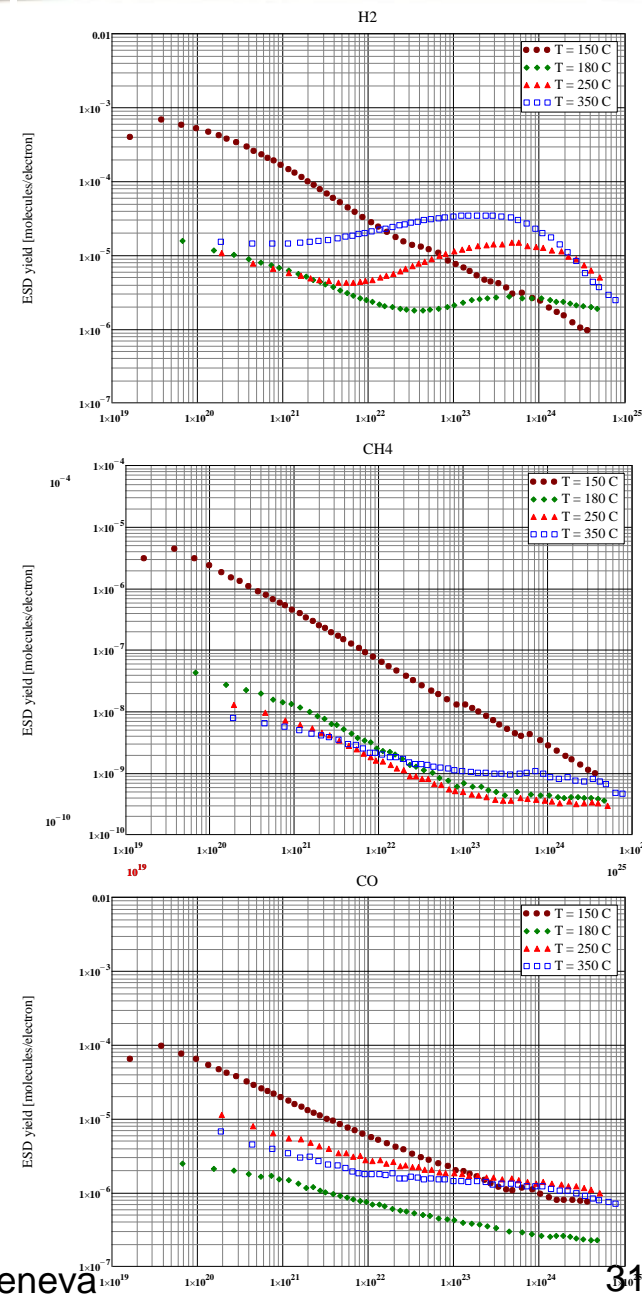
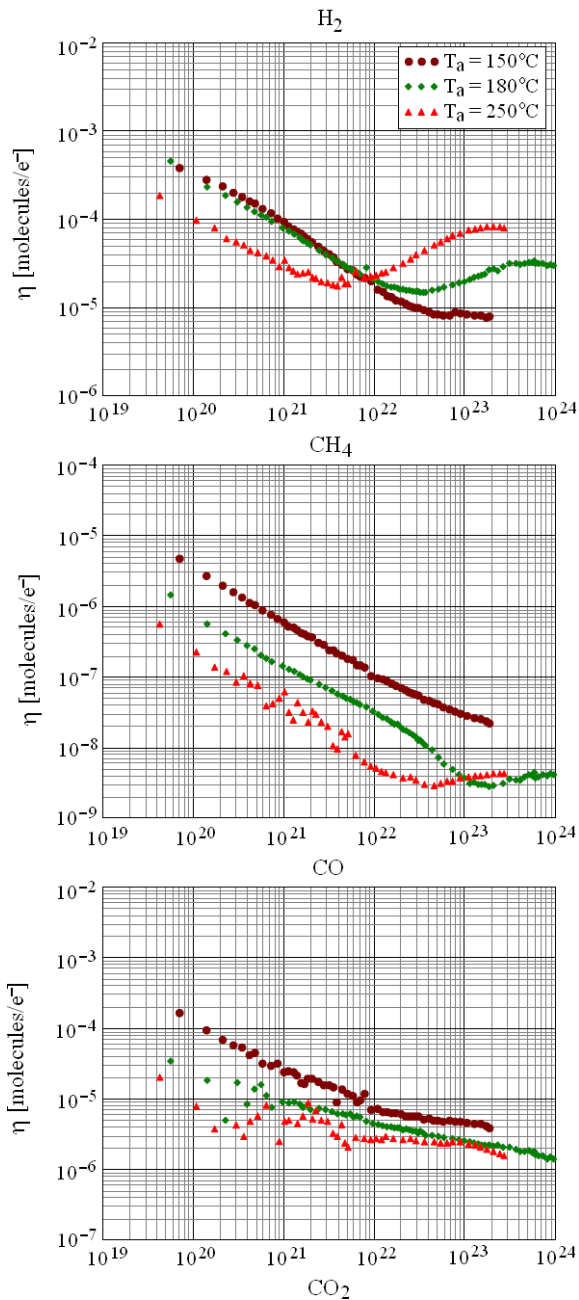
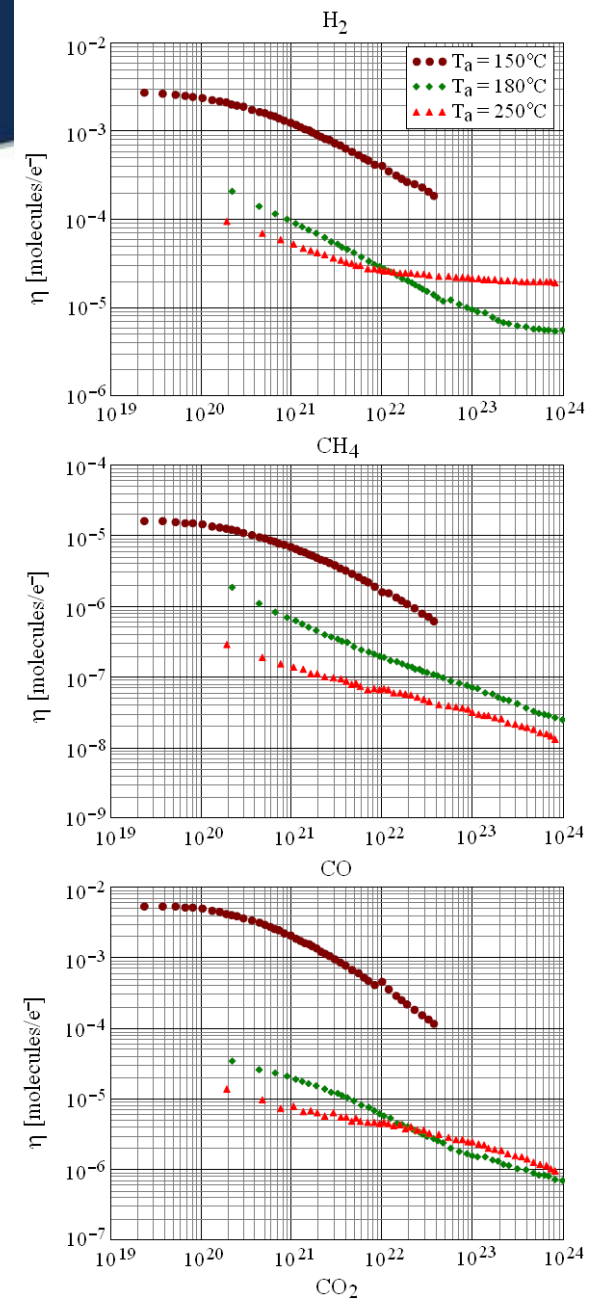
O.B. Malyshev, R. Valizadeh and A.N. Hannah. *JVST A* 34, 061302 (2016)

# ESD for dense, columnar and dual layer NEG

(a) Dense film

(b) Columnar film

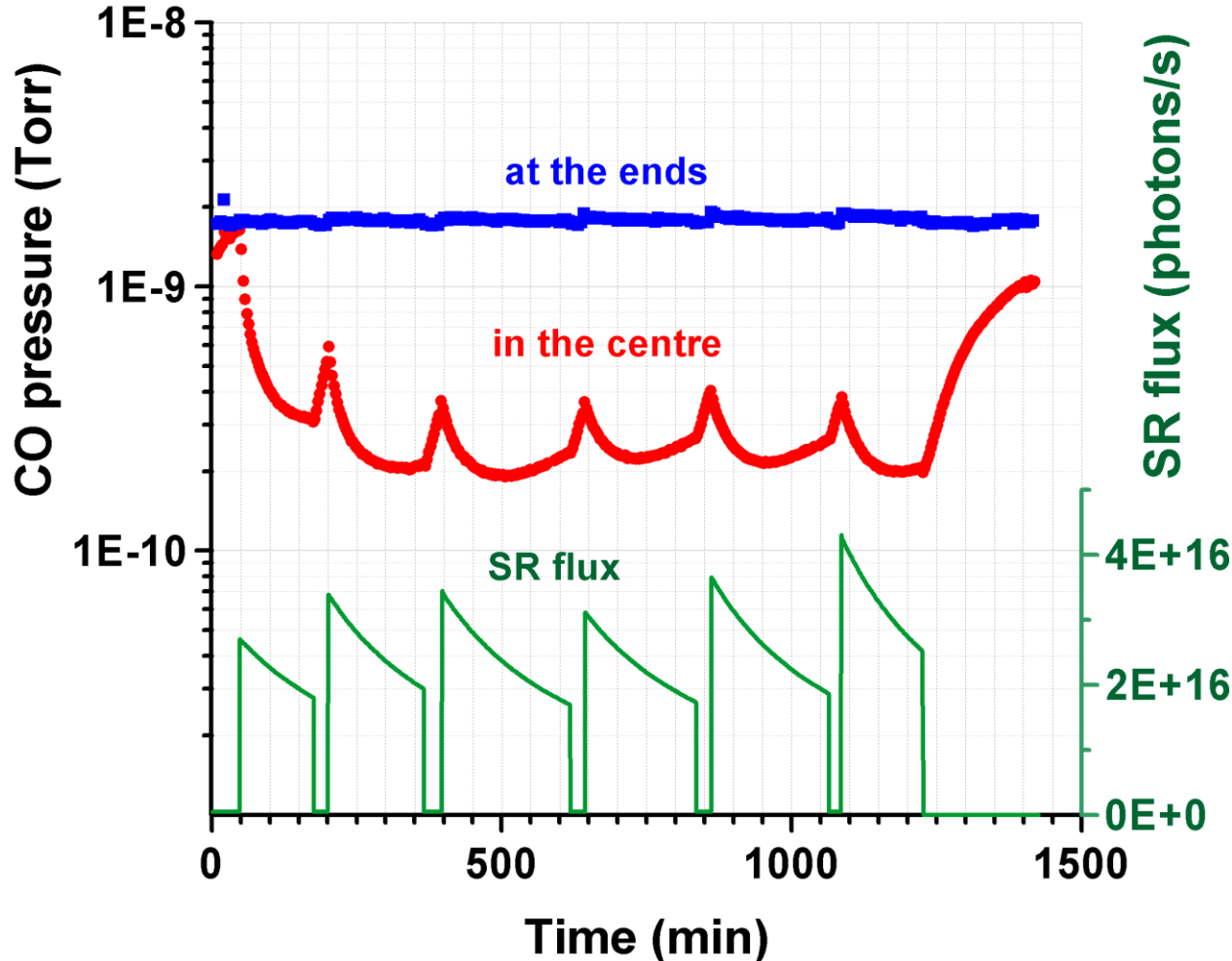
(c) Dual Layer





# NEG Coated Vacuum Chamber: SR Induced Pumping

NEG TiZrV coated surface saturated with CO (i.e. no pumping speed) exposed to SR



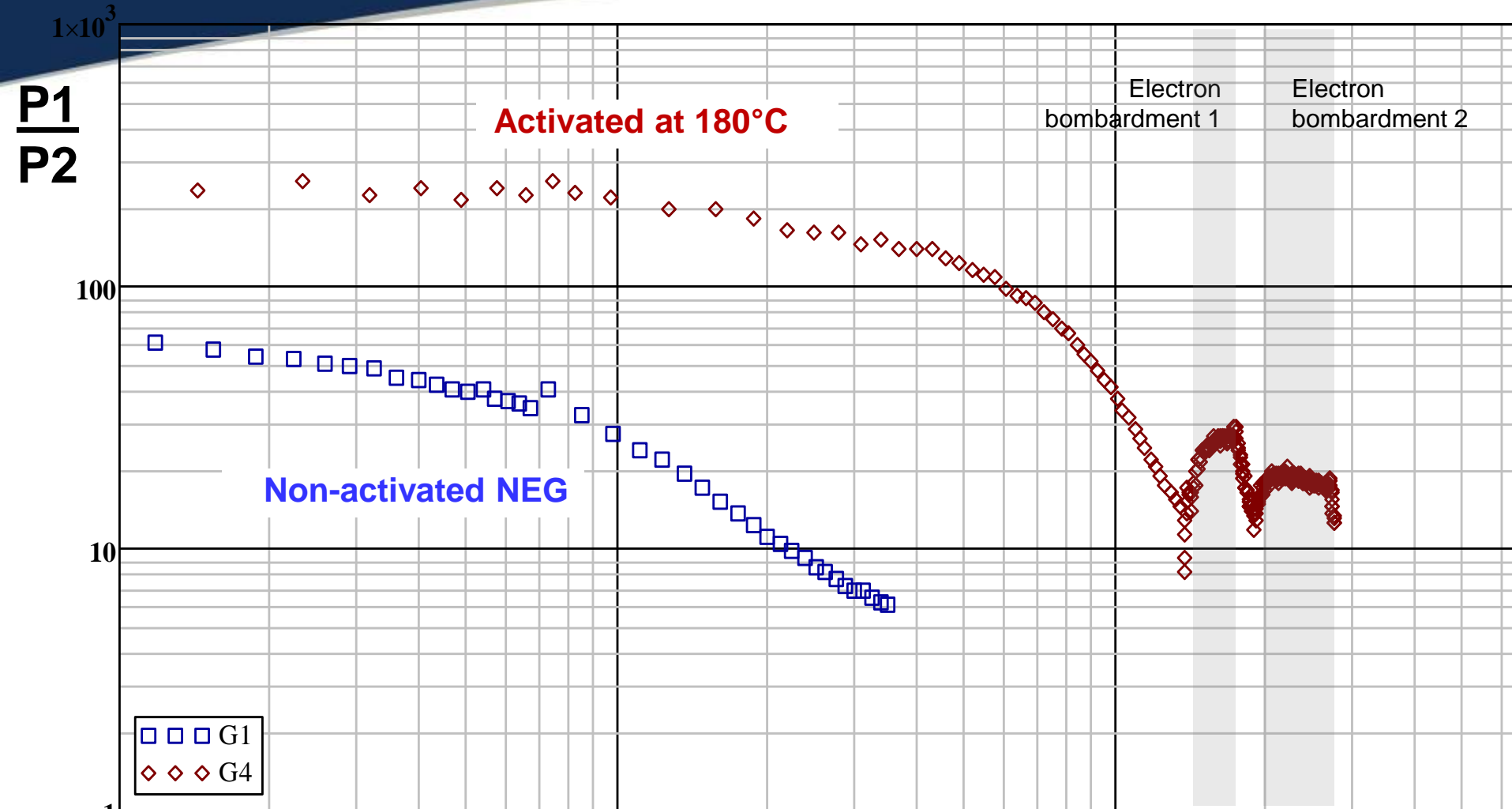
The photon stimulated NEG activation efficiency estimated as

$$\sigma_{\gamma} = 2 \times 10^{-5} [\text{CO}/\gamma]$$

V.V. Anashin et al. *Vacuum* 75 (2004), p. 155.



# Electron stimulated NEG activation



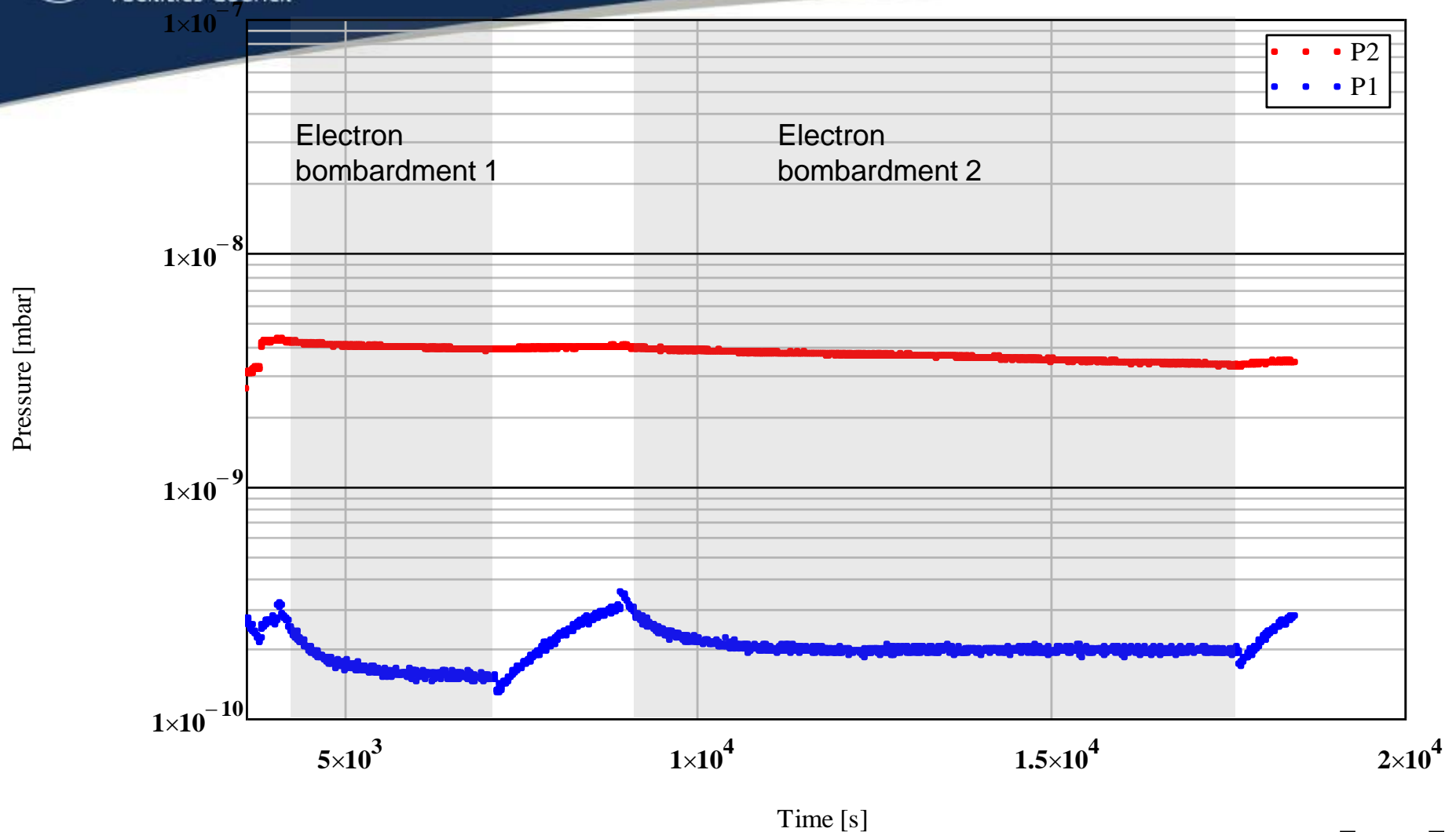
The electron stimulated NEG activation efficiency estimated as  $7.9 \times 10^{-4} < \sigma_1 < 2.4 \times 10^{-3} \text{ [CO/e}^-]$

$$\sigma_1 \left[ \frac{\text{CO}}{e^-} \right] = \frac{\Omega_{\text{CO}}}{D}$$





# Electron stimulated NEG activation



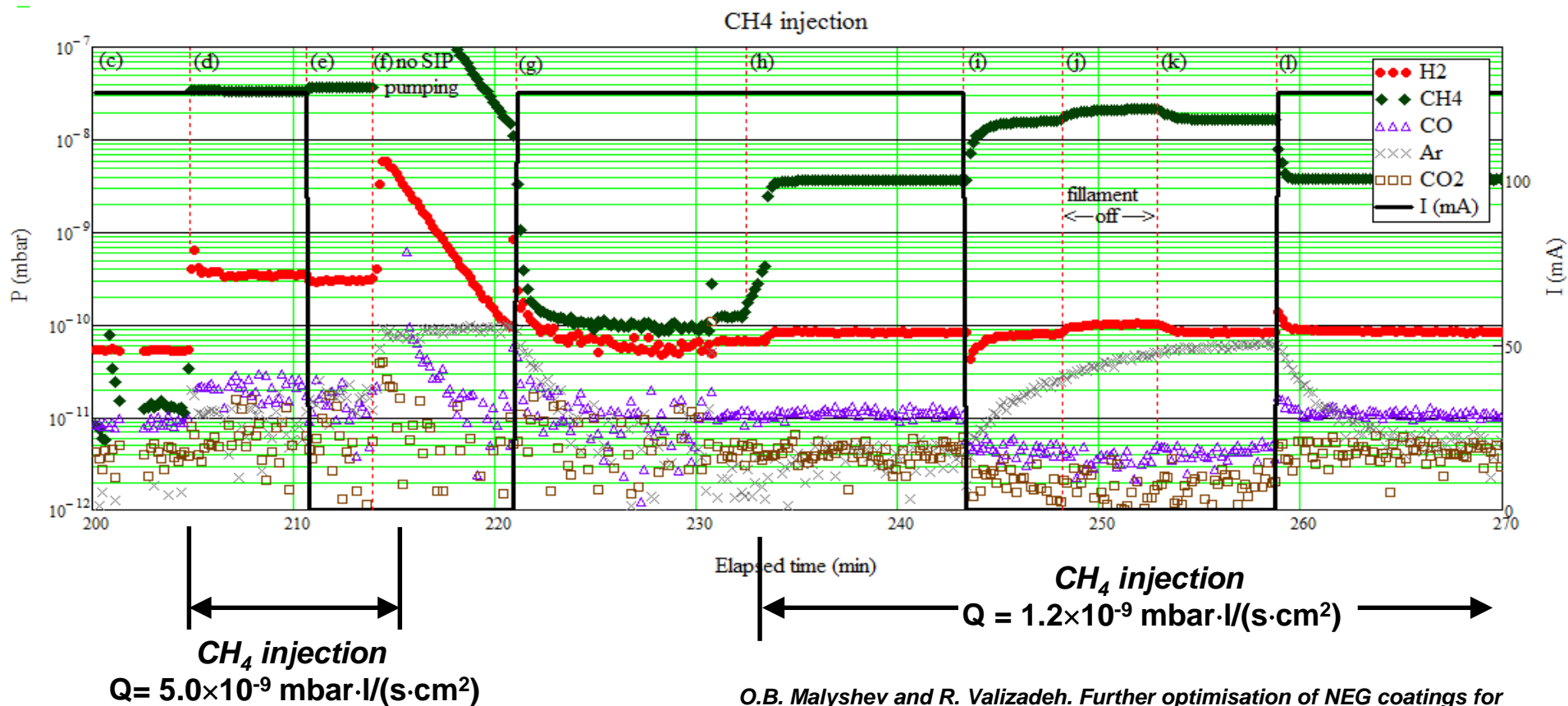
The electron stimulated NEG activation efficiency estimated as

$$\sigma_2 = \frac{Q_{CO}}{k_B T} \frac{q_e}{I} = 2.2 \times 10^{-3} \left[ \frac{CO}{e^-} \right]$$



# CH<sub>4</sub> problem

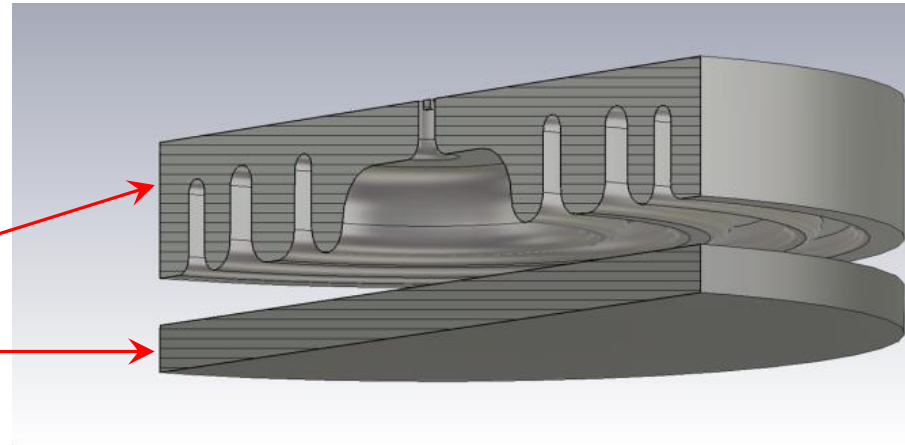
- NEG does not pump CH<sub>4</sub> and other hydrocarbons
- However, CH<sub>4</sub> can be pumped in a presence of SR or electron bombardment:  $\chi = 2.3 \times 10^{-5} \text{ CH}_4/\text{e}^-$ .



O.B. Malyshev and R. Valizadeh. Further optimisation of NEG coatings for accelerator beam chamber. Proc. IPAC-5 (2014) p. 2399.

# Surface resistance: method

- The cavity geometry consists of two parts:
  - a body of the cavity
  - a planar sample,
  - separated by an air gap.
- Contactless
- RF chokes in order to keep the RF power within the cavity

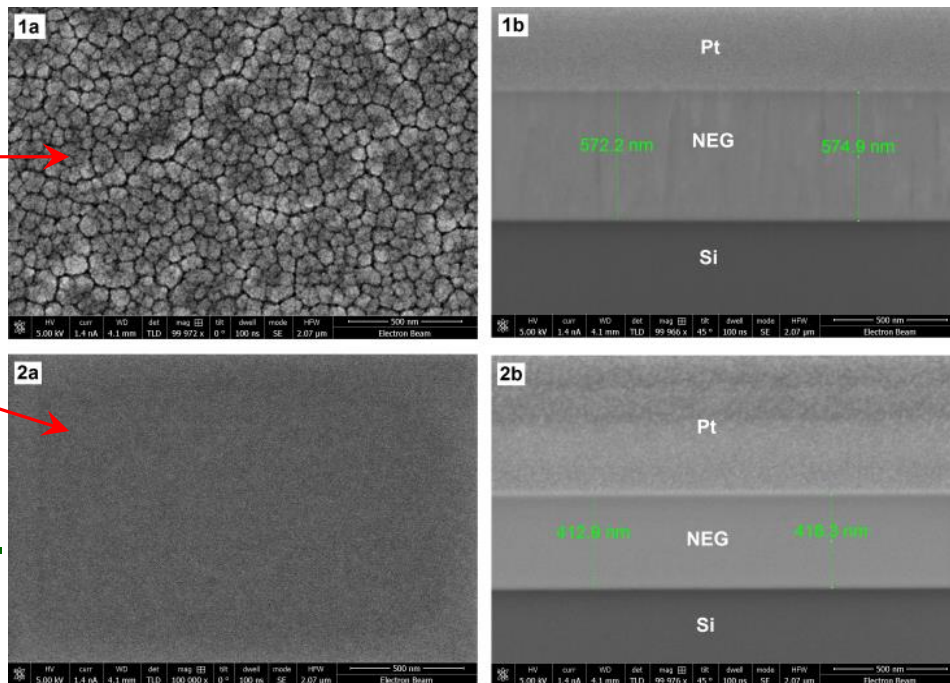


$$R_S^{sam} = \frac{G Q_0^{-1} - R_S^{cav} p_c}{p_s}$$

- Modelled with CST Microwave Studio.
- $G = 235 \Omega$ .
- The field ratios  $p_c = 0.625$  and  $p_s = 0.375$  for perfect electric conductor boundary conditions.

# NEG coatings

- NEG films
  - columnar
  - dense
- Deposited on:
  - polycrystalline copper
  - silicon Si(100) substrates.
- The substrate size was 100 mm × 100 mm × 2 mm
- Sample thickness:
  - from 0.7 to 18 μm



O.B. Malyshev, L. Gurrán, P. Goudket, K. Marinov, S. Wilde, R. Valizadeh and G. Burt.. Nucl. Instrum. Methods Phys. Res., A 844, 99-107 (2017)



## Analytical model

- The expressions for the surface impedance of a planar metallic film deposited on a substrate (dielectric or metallic) are derived by following the standard approach employed in calculating the transmission and reflection coefficients in layered media

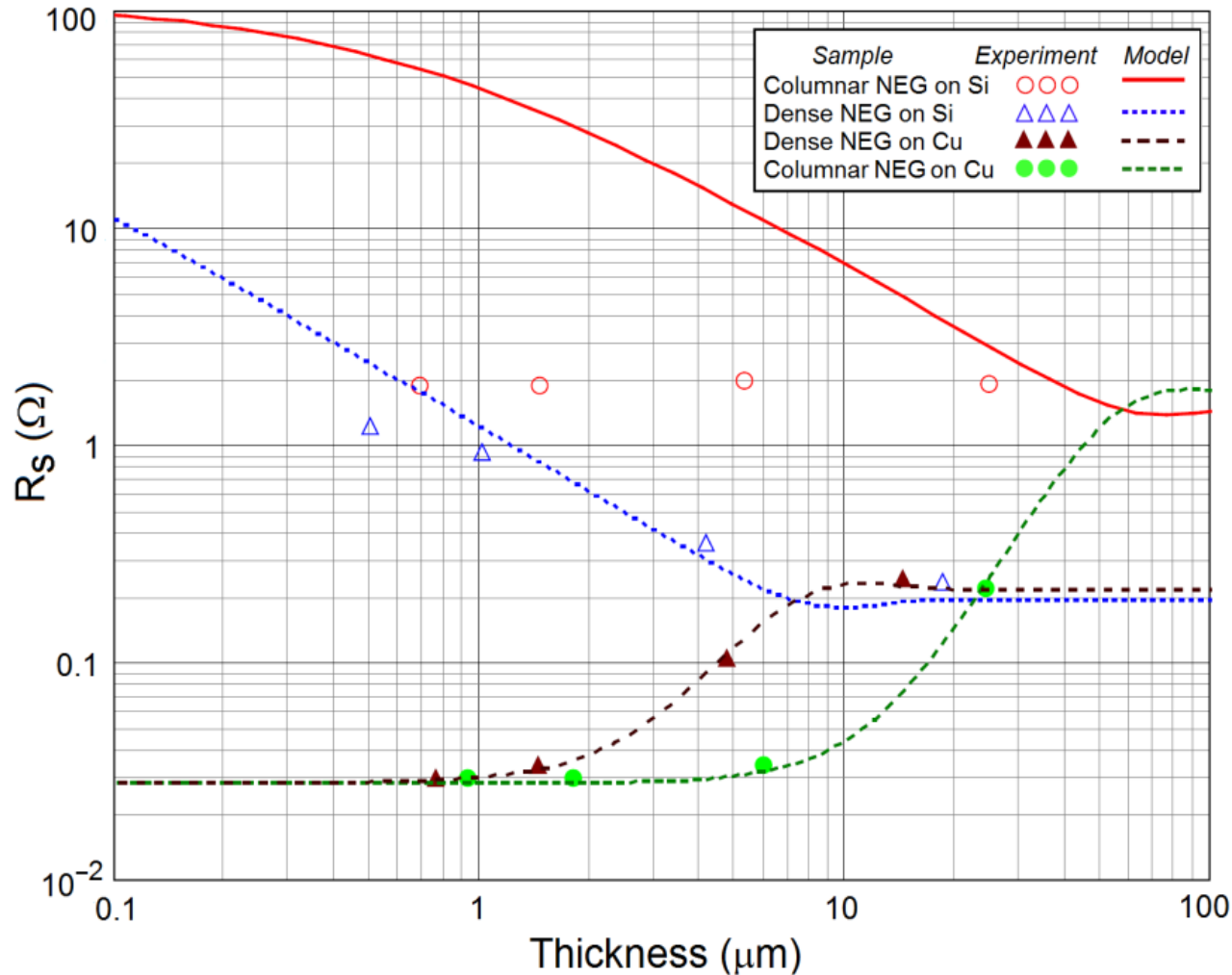
$$R_s = R_1 \frac{1 - \delta^2 \exp(-4\kappa_1 d_1) - 2\delta \sin(2\kappa_1 d_1) \exp(-2\kappa_1 d_1)}{1 + \delta^2 \exp(-4\kappa_1 d_1) + 2\delta \cos(2\kappa_1 d_1) \exp(-2\kappa_1 d_1)} \quad \text{for NEG on metal substrate;}$$

$$R_s = R_1 \frac{1 - \exp(-4\kappa_1 d_1) + 2 \sin(2\kappa_1 d_1) \exp(-2\kappa_1 d_1)}{1 + \exp(-4\kappa_1 d_1) - 2 \cos(2\kappa_1 d_1) \exp(-2\kappa_1 d_1)} \quad \text{for NEG on Si substrate.}$$

O.B. Malyshev, L. Gurrán, P. Goudket, K. Marinov, S. Wilde, R. Valizadeh  
and G. Burt.. Nucl. Instrum. Methods Phys. Res., A 844, 99-107 (2017)



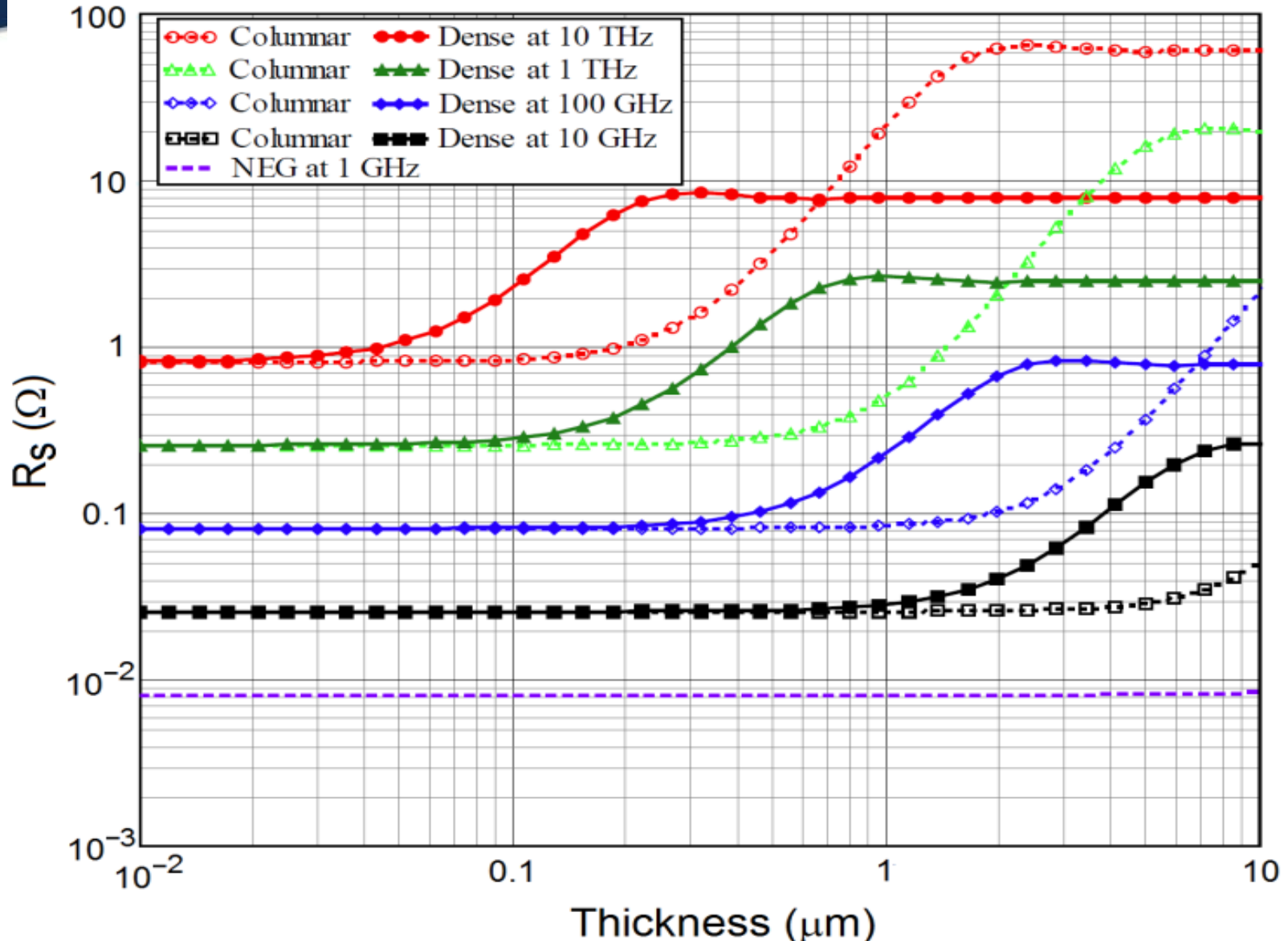
## The surface resistance $R_S$ of dense and columnar NEG coatings on copper and silicon substrates as a function of film thickness



The bulk conductivity was obtained with the analytical model:

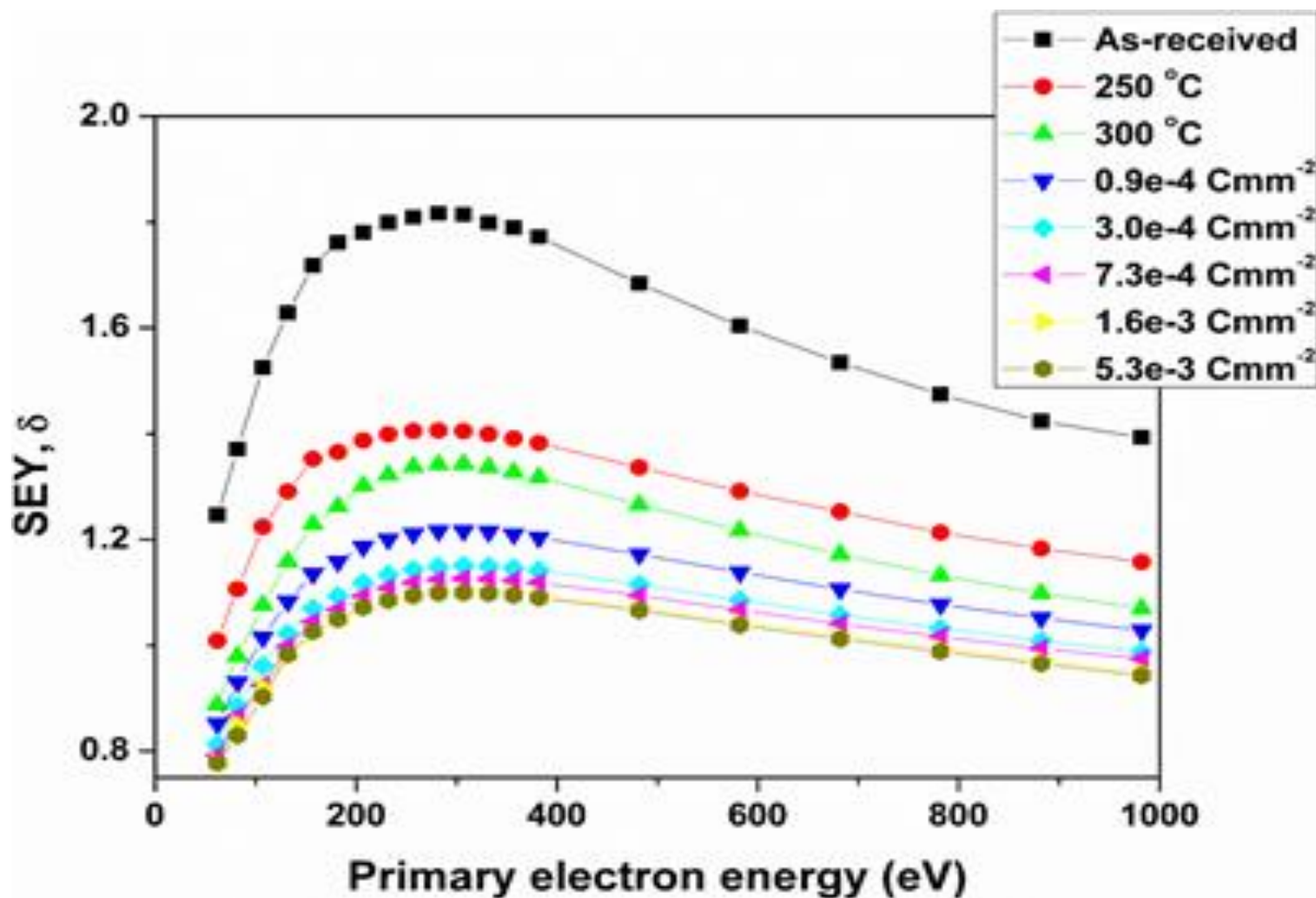
- $\sigma_d = 1.4 \times 10^4 \text{ S/m}$  for the columnar NEG coating
- $\sigma_d = 8 \times 10^5 \text{ S/m}$  for the dense NEG coating

# The surface resistance $R_s$ as a function of NEG film thickness on copper at various frequencies





# SEY from columnar NEG







## Ongoing studies

- NEG coating of narrow tubes  $< 10$  mm diameter
  - See presentations at IPAC'2018
- Higher electric conductivity NEG coatings
  - i.e. better than for Ti,Zr,Hf and V alloys
  - See presentations at IPAC'2018



# Conclusions

- NEG coating is a technology that allows to meet **UHV/XHV** vacuum specification in long narrow vacuum chambers.
  - PSD and ESD After NEG activation at 180°C the initial  $\eta(316LN)/\eta(\text{Ti-Zr-V}) =$ 
    - =20 for H<sub>2</sub>, =1000 for CH<sub>4</sub> and =200 for CO.
    - Vacuum firing => an order of magnitude lower ESD
    - $\eta(\text{Ti-Zr-Hf-V}) < \eta(\text{Ti-Zr-V})$ .
    - **Best results is for the dense and dual layer NEG activated at 180 °C**
  - Often the only vacuum solution
  - Lower cost of pumping system
- NEG film requires *activation* at 150-180 °C instead of 250-300 °C usual bakeout:
  - Shorter bellows or less number of bellows
  - Wider choice of material for vacuum chamber and components
- SR (or electron bombardment) induced activation/pumping:
  - NEG can be (re-)activated by irradiation/bombardment
  - NEG can pump CH<sub>4</sub> molecules *during* irradiation/bombardment
- The bulk conductivity:
  - $\sigma d = 1.4 \times 10^4 \text{ S/m}$  for the columnar NEG coating
  - $\sigma d = 8 \times 10^5 \text{ S/m}$  for the dense NEG coating
- SEY < 1.1 can be obtained after activation or by conditioning

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