



CMS Upgrade Workshop –  **Fermilab** , 30th of October, 2009

DC-DC Converter Development at RWTH Aachen University

Lutz Feld, Rüdiger Jussen, Waclaw Karpinski,
Katja Klein, Jennifer Merz, Jan Sammet

I. Physikalisches Institut B – RWTH Aachen University



Federal Ministry
of Education
and Research



RWTHAACHEN
UNIVERSITY

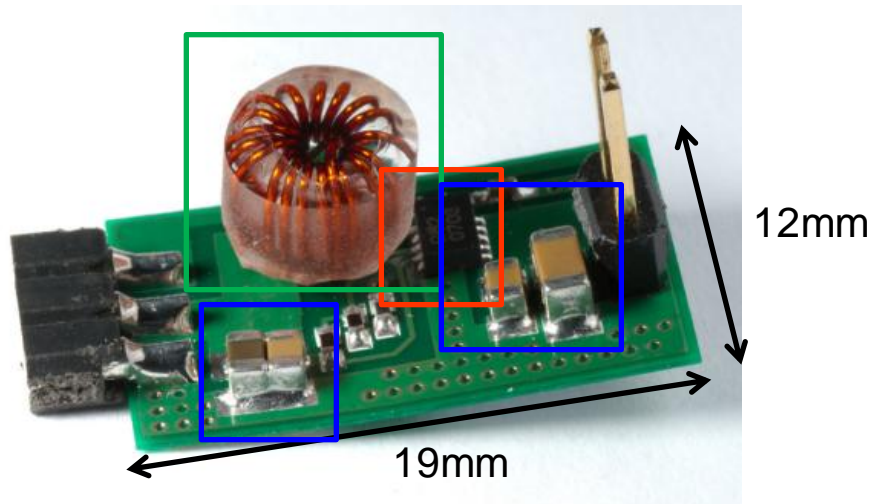
→ This talk only covers the R&D with commercial converter ASICs

- Aachen Buck Converters with commercial ASICs
- Efficiency Measurements
- System Test Measurements with Strip Tracker Modules
- Converter Noise Measurements (EMC)

- Summary



Idea of Aachen R&D: develop Converters based on **commercial non-radiation-hard** buck converter ASICs; optimize for low mass, low space, low noise; and study in system test



PCB:

2 copper layers a 35 μ m
FR4 200 μ m
 $V = 12 \times 19 \text{mm}^2 \times 10 \text{mm}$
 $m = 1.0 \text{g}$

Chip: Enpirion **EQ5382D**

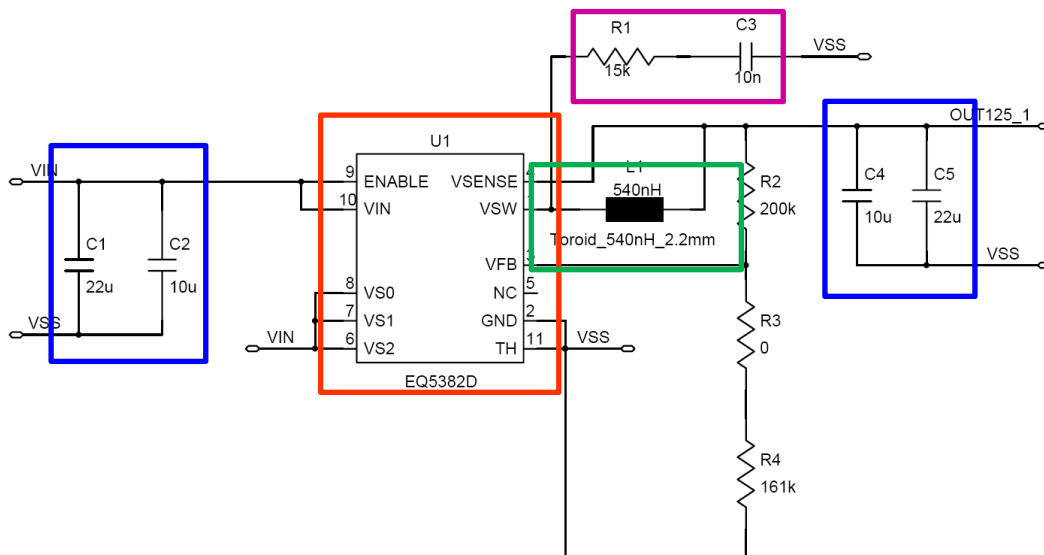
$V_{IN} = 2.4\text{-}5.5\text{V}(\text{rec.}) / 7.0\text{V}(\text{max.})$
 $I_{OUT} \leq 0.8\text{A}$
 $V_{OUT} = 1.30\text{V} / 2.55\text{V}$
 $f_S \approx 4\text{MHz}$

External air-core inductor:

Custom-made toroid, $\varnothing \approx 6\text{mm}$
 $L = 600\text{nH} (200\text{nH})$
 $R = 80\text{m}\Omega (40\text{m}\Omega)$

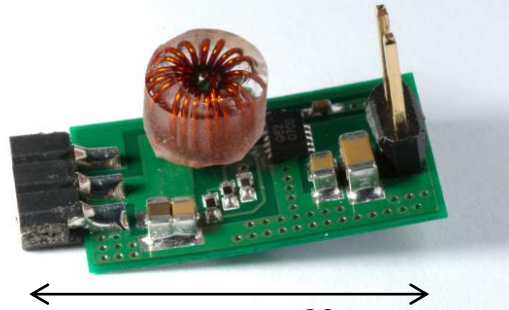
Input / output filter capacitors

Snubber to reduce ringing



Three different converter PCBs → different geometry and filter-capacitor assembly:

AC2-StandardC

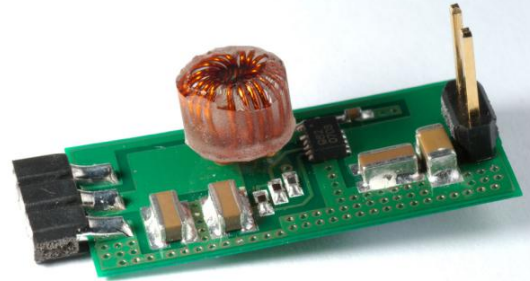


AC2-StandardC

23mm

- Standard capacitors

AC2-ReverseC

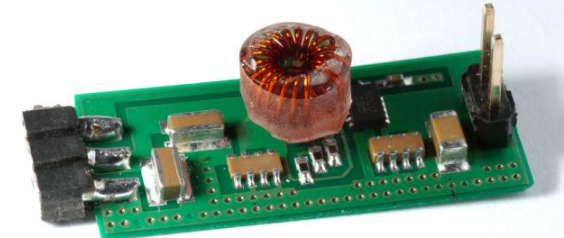


AC2-ReverseC

28mm

- Reverse geometry caps

AC2-IDC

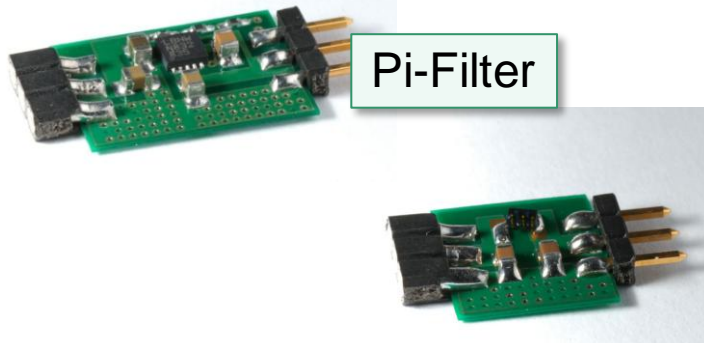


AC2-IDC

30mm

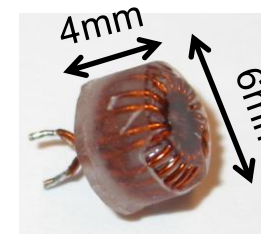
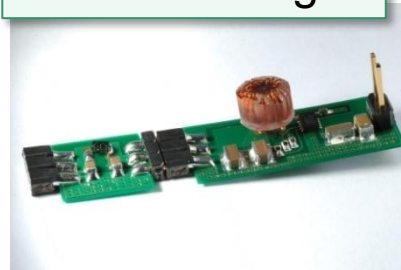
- 2 Inter-Digitated Capacitors (IDC) with eight terminals

Low Drop-Out (LDO)

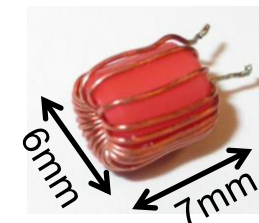


Pi-Filter

Modular design:

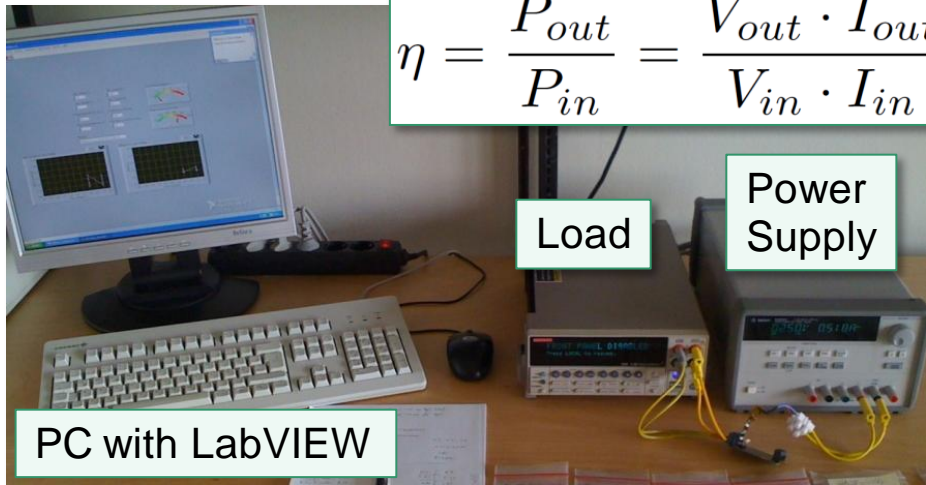


“Tiny Toroid“
 $L = 200\text{nH}$
 $R_{DC} = 40\text{-}50\text{m}\Omega$
 $m = 0.2\text{g}$

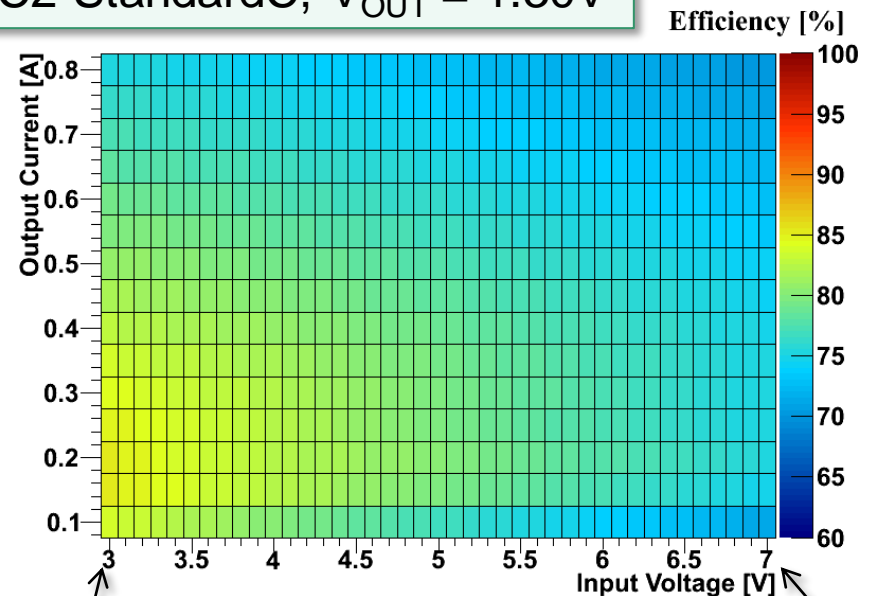


“Mini Toroid“
 $L = 600\text{nH}$
 $R_{DC} = 80\text{-}100\text{m}\Omega$
 $m = 0.3\text{g}$

$$\eta = \frac{P_{out}}{P_{in}} = \frac{V_{out} \cdot I_{out}}{V_{in} \cdot I_{in}}$$



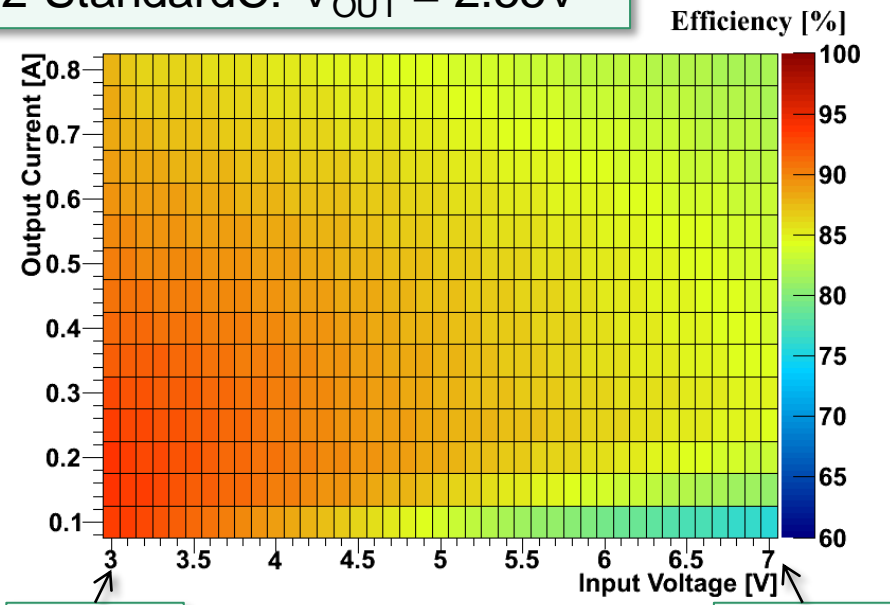
AC2-StandardC, $V_{OUT} = 1.30V$



$r = 2.3$

$r = 5.4$

AC2-StandardC: $V_{OUT} = 2.55V$



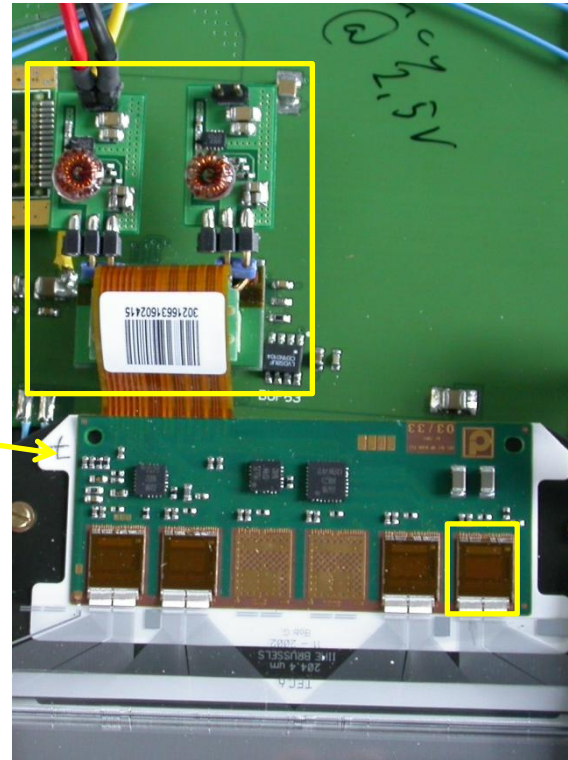
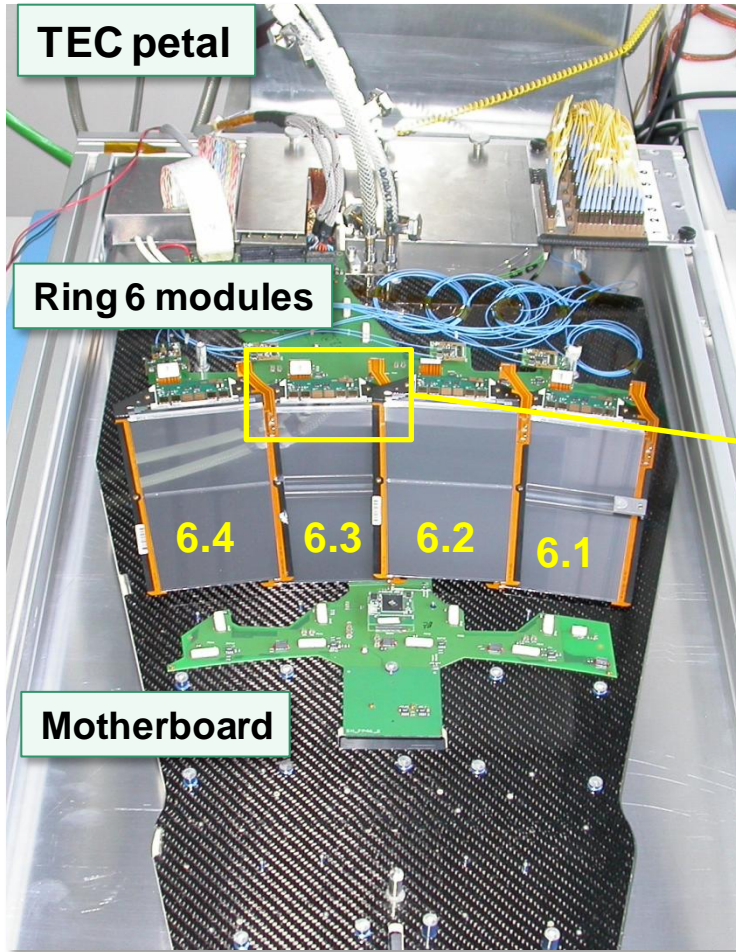
$r = 1.2$

$r = 2.7$

- Inductor: Mini Toroid ($L = 600nH$)
- Efficiency is 75-85% for $V_{OUT} = 1.30V$
- For smaller conversion ratio, η is up to 10% higher ($V_{OUT} = 2.55V$; $\eta = 85-95\%$)

SLHC readout chips and module prototypes not available before 2010/11

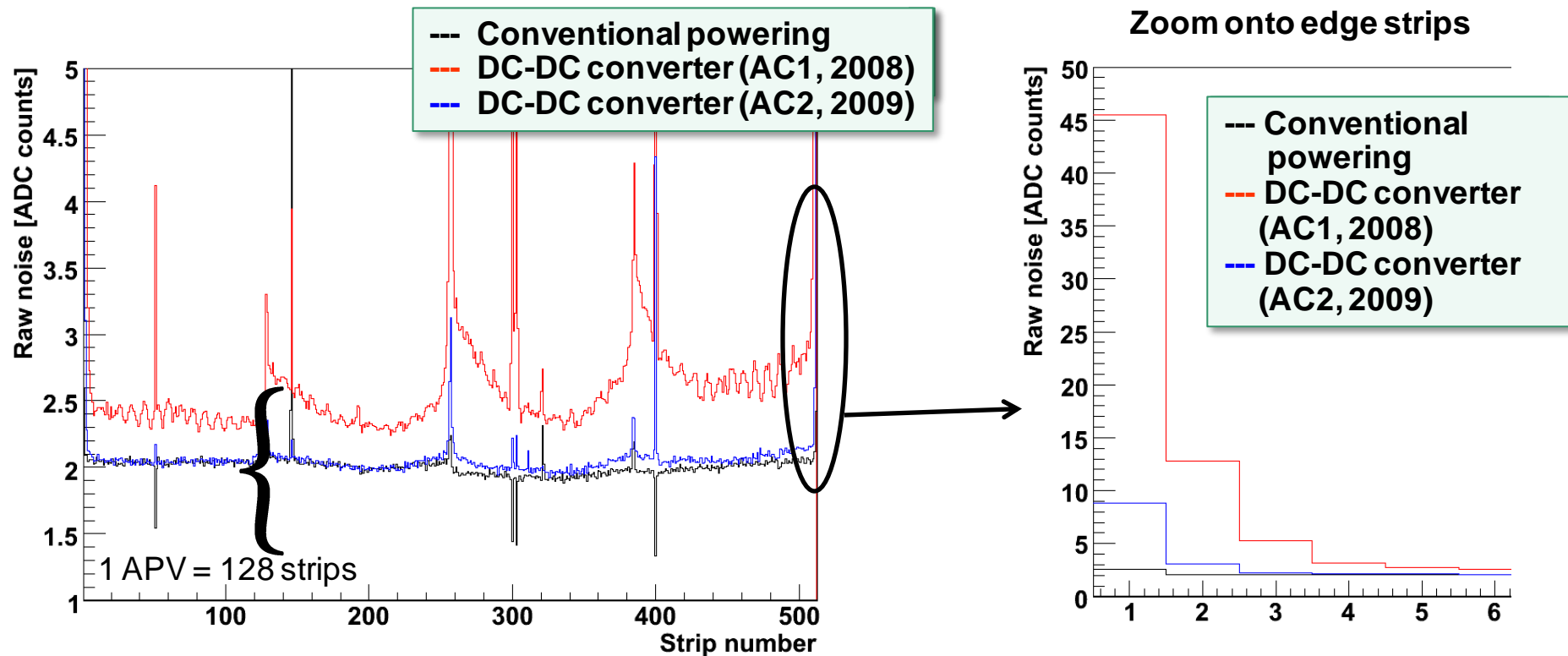
→ We believe a lot can be learned from current CMS strip tracker hardware



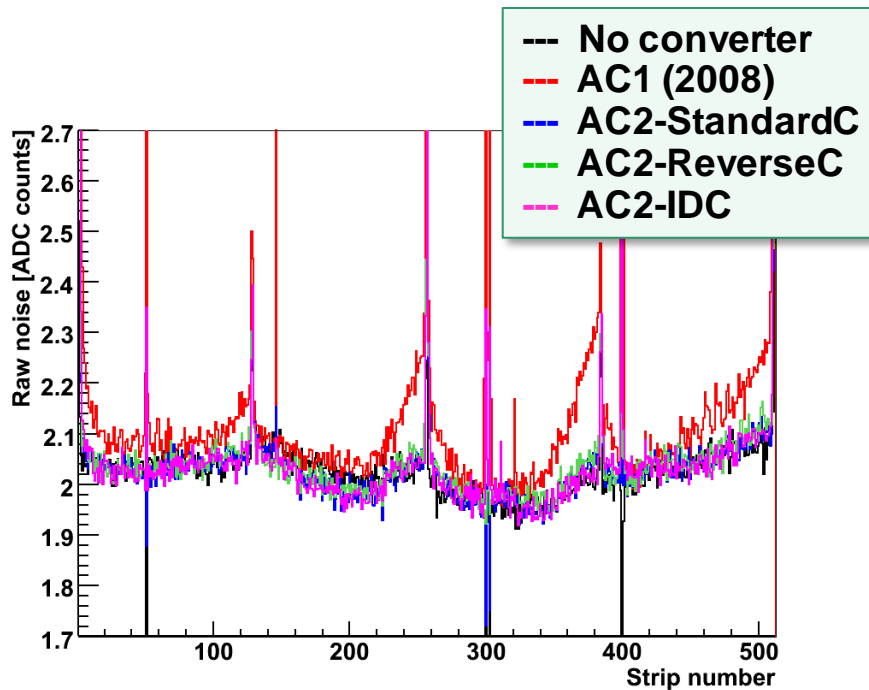
APV25 readout chip:

- 0.25 μ m CMOS
- 128 channels
- **analogue readout**
- per channel: pre-amp., CR-RC shaper, pipeline
- $\tau = 50$ ns
- 1.25V & 2.50V supply
- $I_{2.50V} = 120$ mA
- $I_{1.25V} = 60$ mA

- Two DC-DC converters per module
- Integrated via additional adapter
- V_{IN} from external power supply



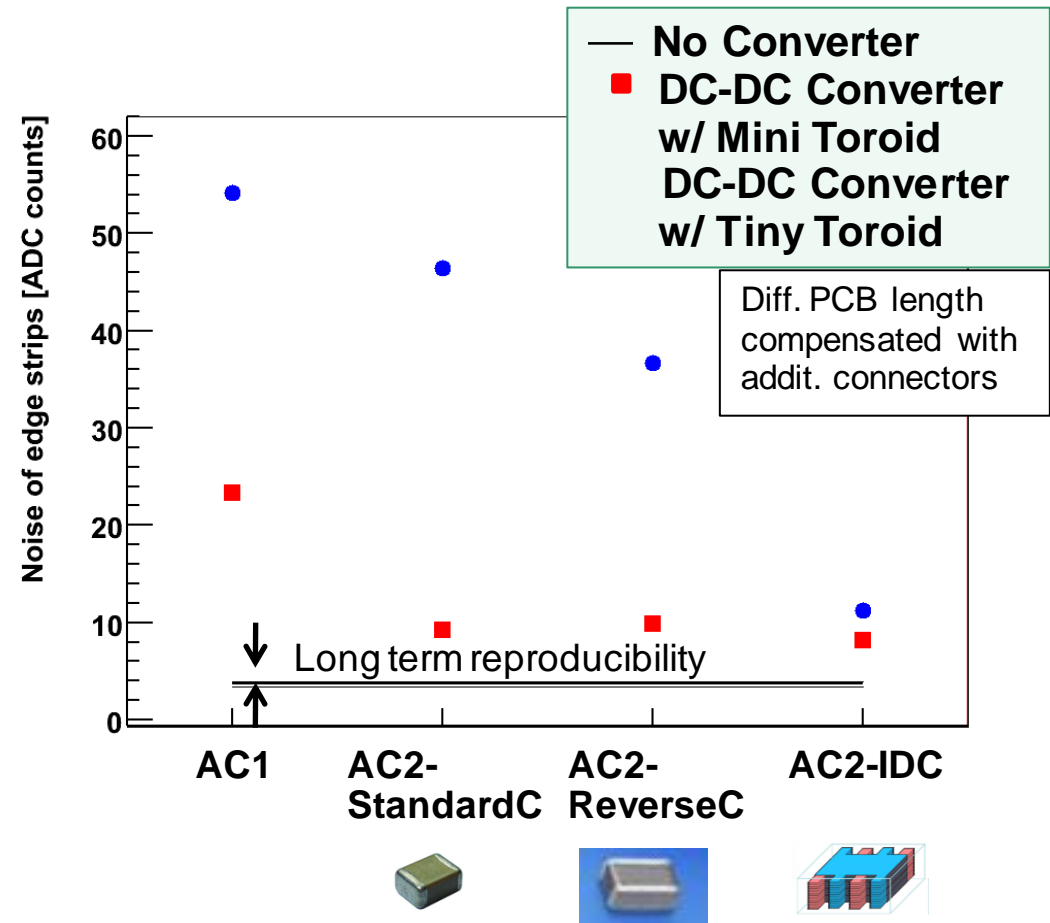
- Raw noise: RMS of fluctuation around pedestal value
- Edge channels are particularly sensitive (explanation in back-up slides)
- Large increase with previous generation of boards (**AC1, 2008**), in particular on edge strips; both conductive (ripple) and radiative (inductor) contributions

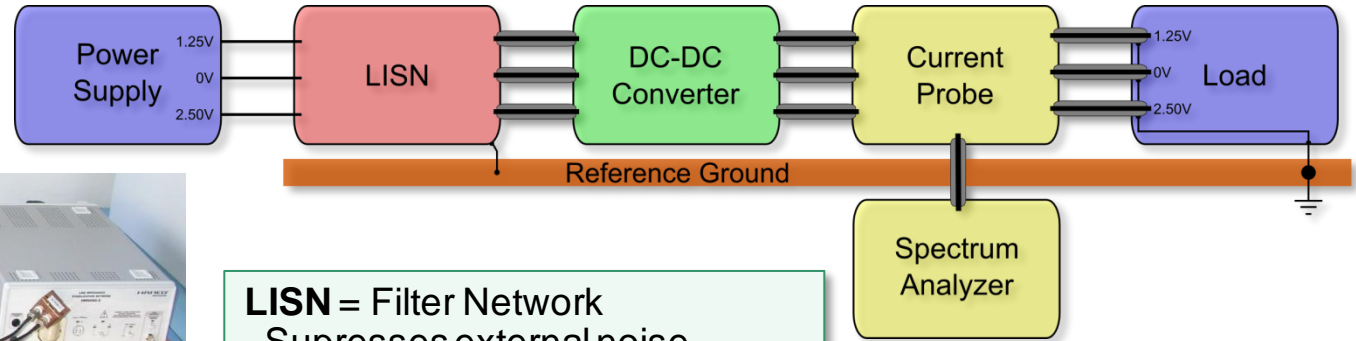
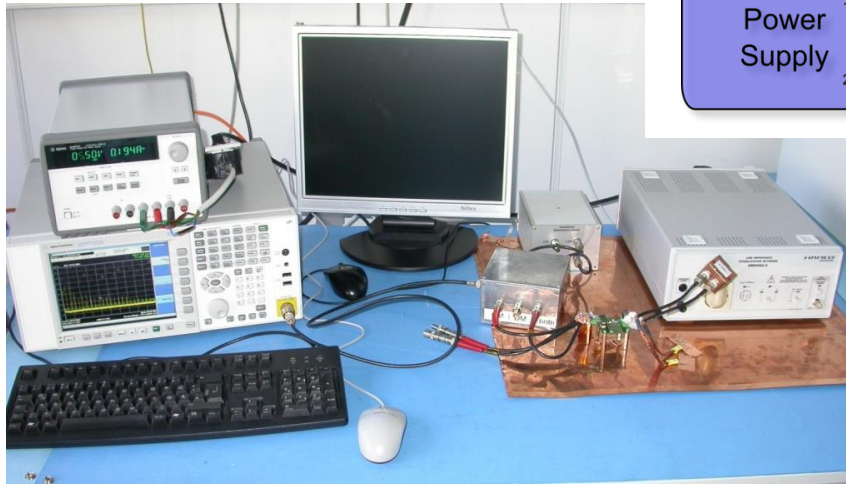


Sensitive variable chosen for all following comparisons:

$$N = \sqrt{N_1^2 + N_{512}^2}$$

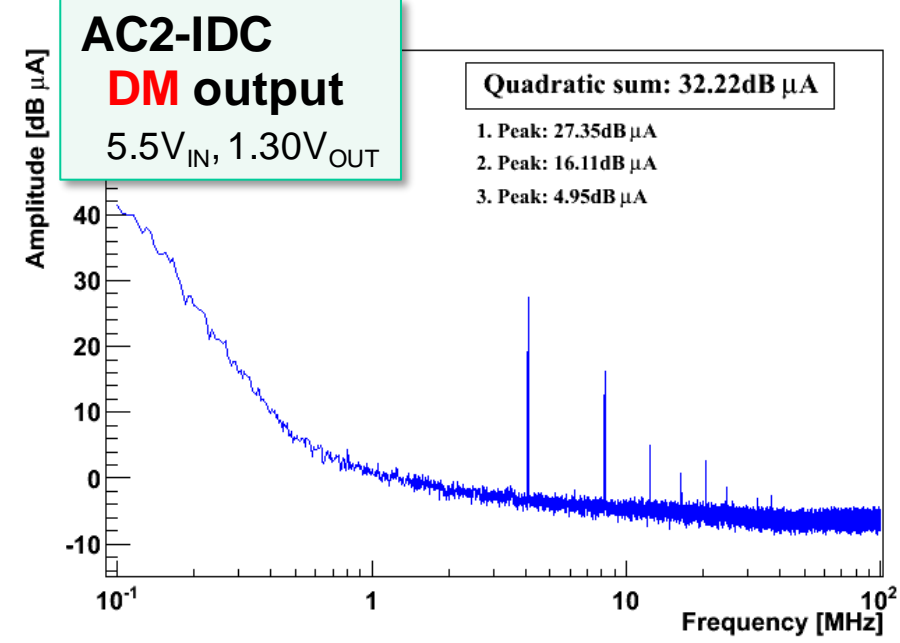
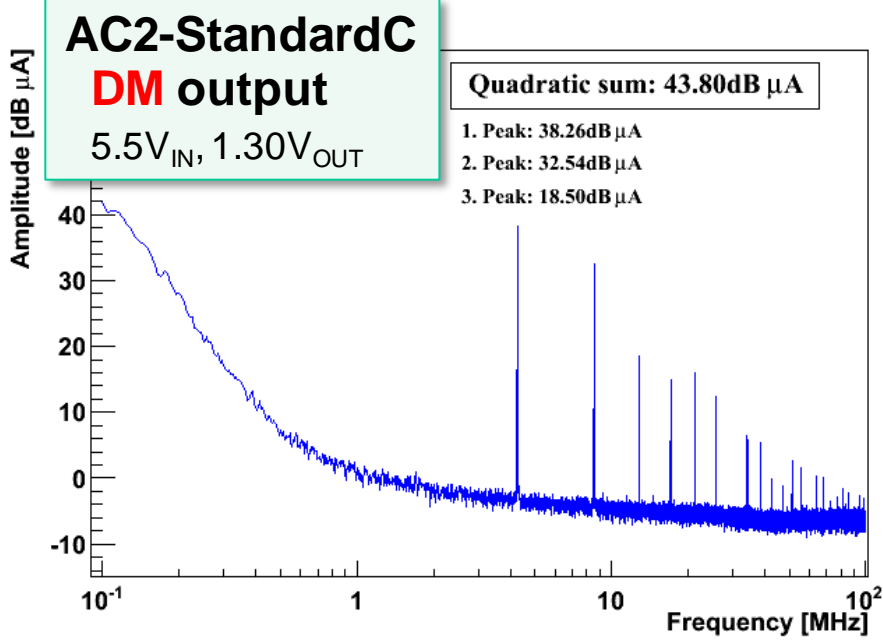
- Lower noise than with 2008 boards
- Mini Toroid shows lower noise and 5-30% higher efficiency ($\Delta I_L = V_L \cdot t_{ON} / L$)
- Boards with IDCs perform best

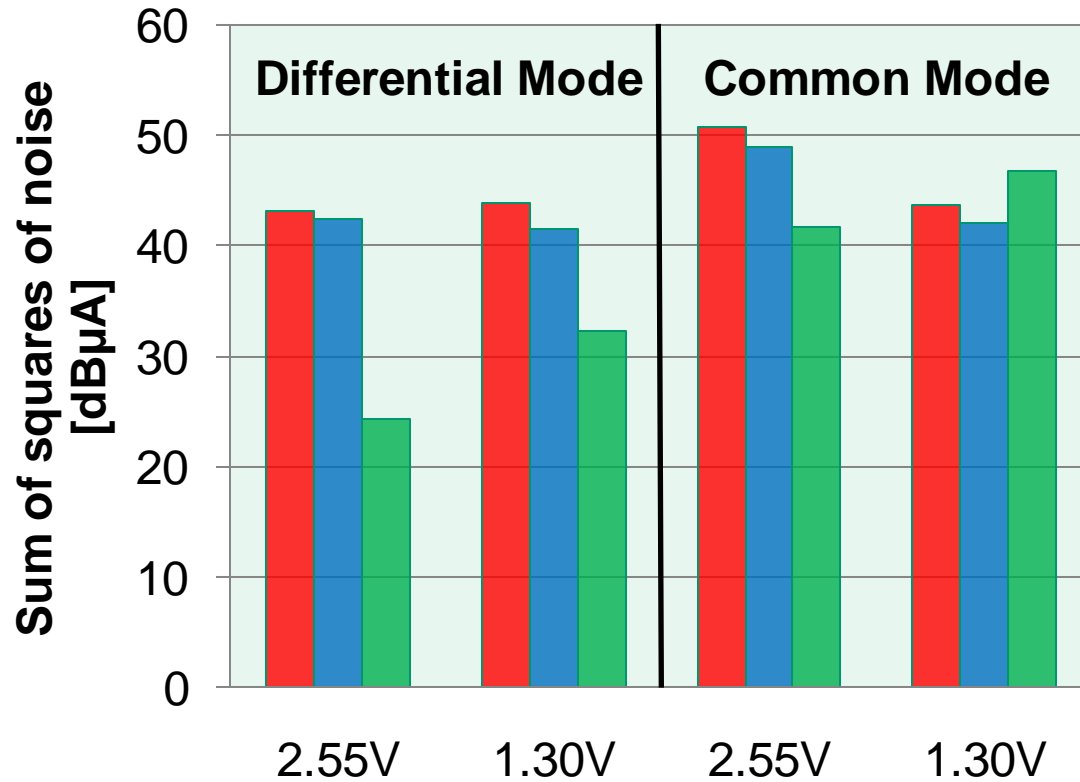




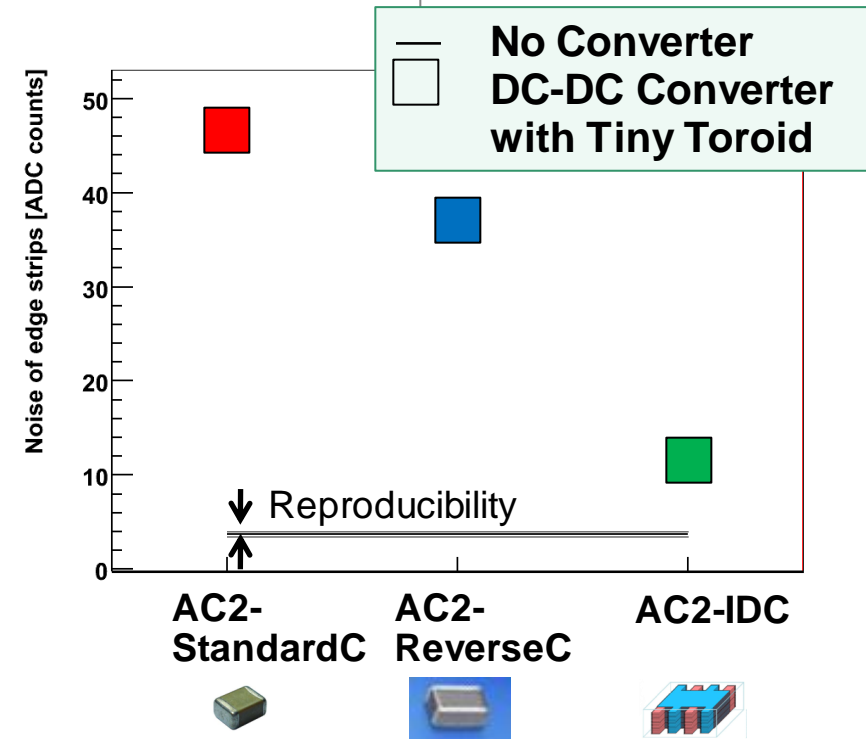
LISN = Filter Network

- Suppresses external noise
- Avoids reflection of the noise currents inside the test system



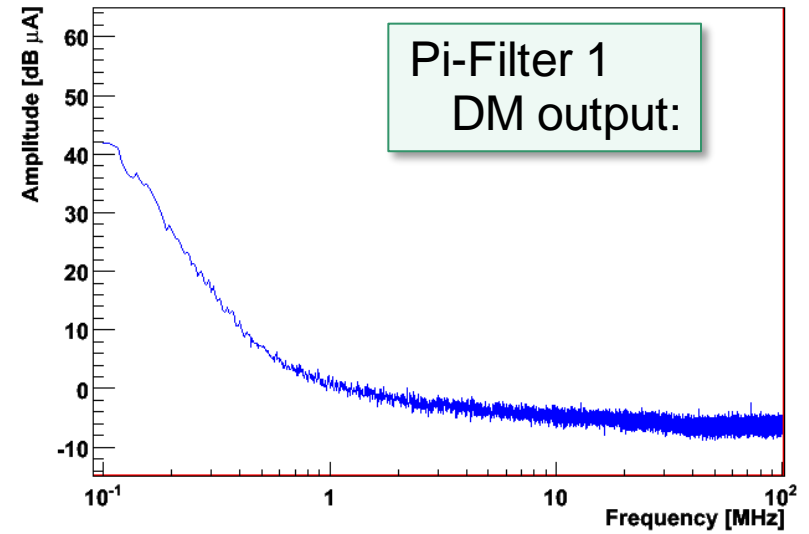
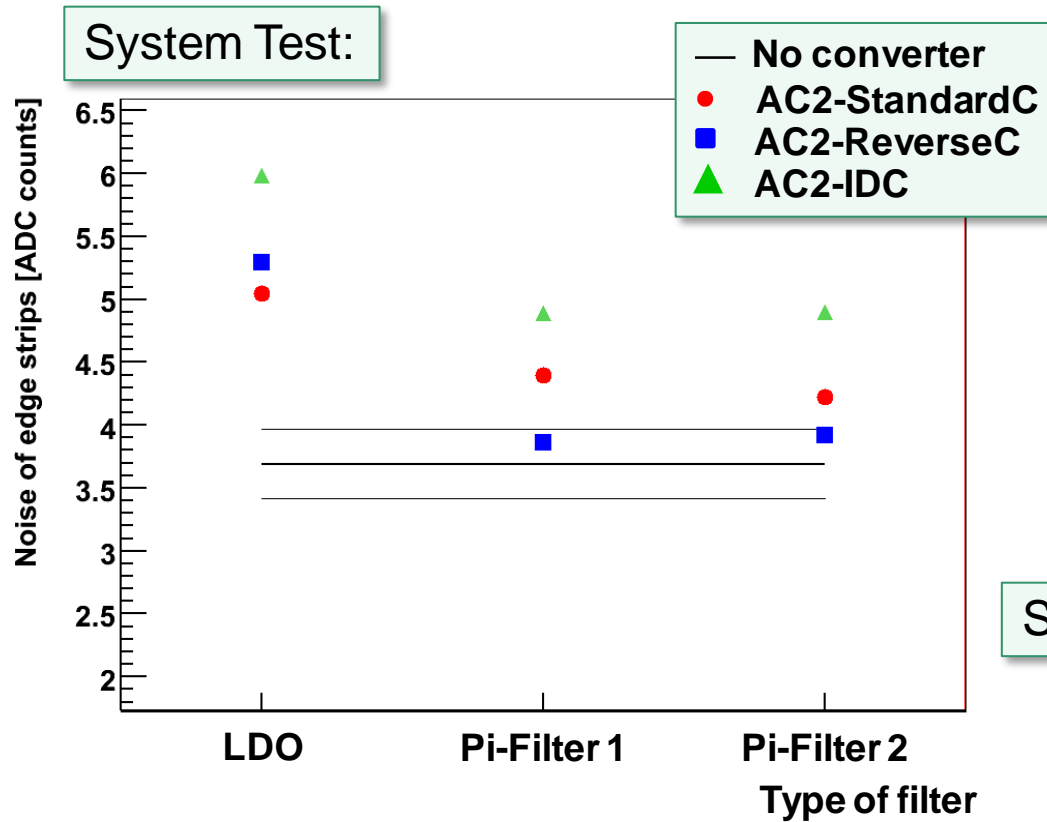


- AC2-StandardC
- AC2-ReverseC
- AC2-IDC

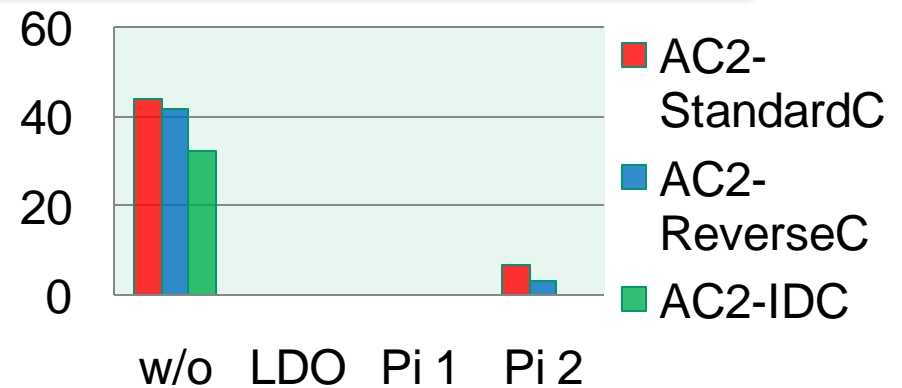


→ Lowest Differential Mode noise from AC2-IDC board

→ But higher Common Mode noise with AC2-IDC for 1.30V?



Sum of squares of DM noise [dB μ A]



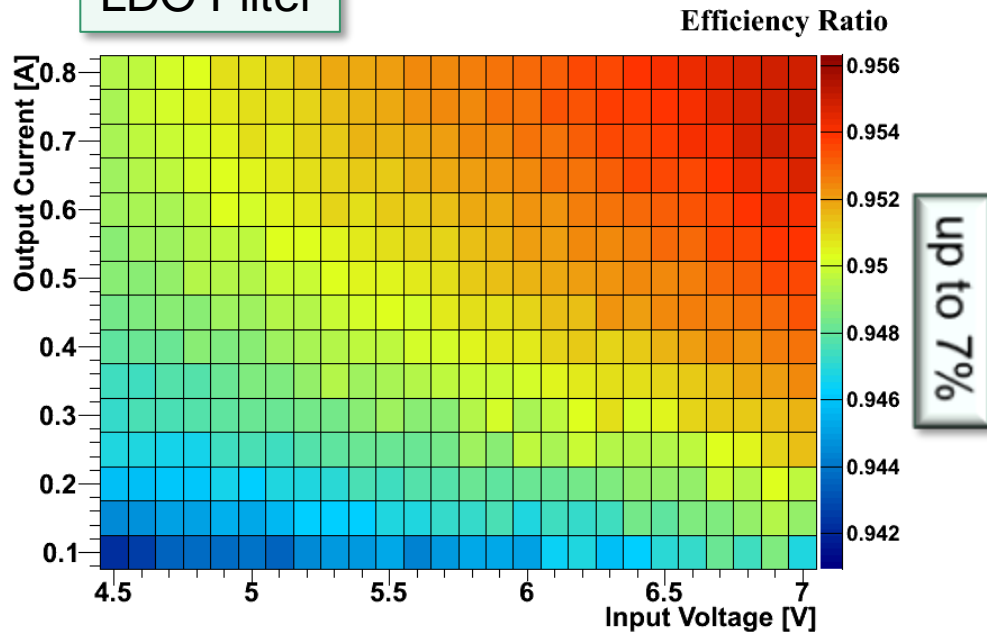
- π -filters are as effective as LDO regulator!
- AC2-IDC performs “worst” with filters/LDO; likely reason: higher CM

π -Filters vs. LDO: What about Efficiency?

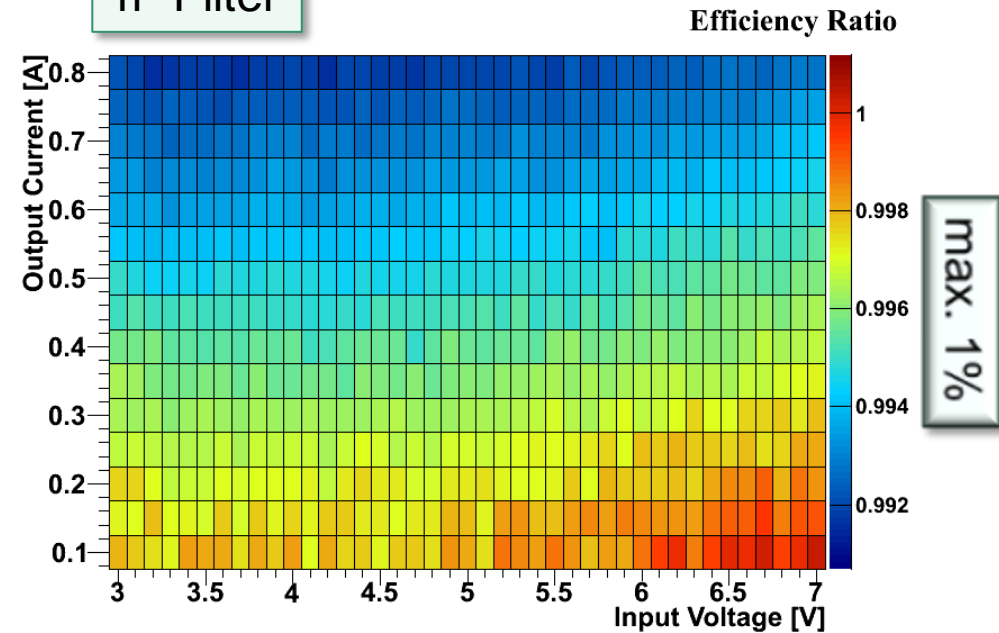
Efficiency with LDO (π -Filter) / efficiency without LDO (π -Filter)

was measured for all board types, filters and $V_{OUT} = 1.25V$ and $2.50V$;
e.g. standard capacitors, $1.25V$:

LDO Filter



π -Filter



- Losses of up to 7% observed with LDO regulator (50mV drop out voltage)
- Losses with our π -Filters stay below 1%
- π -filter clearly preferred

- Buck Converters with commercial non-radiation-hard chips have been developed that add very little noise into the current tracker system
- Small, low-mass 600nH air-core toroids with low R_L have been fabricated
- π -Filters reduce the noise to the level of conventional powering with $< 1\%$ efficiency loss, and are preferred over LDOs
- We are now studying the integration of custom rad-hard converters developed by the CERN PH-ESE Group (F. Faccio, S. Michelis, ...)
- Measurements of the Converters with the ASICs from CERN are ongoing, results will be presented in the next Power WG Meeting at CERN in November



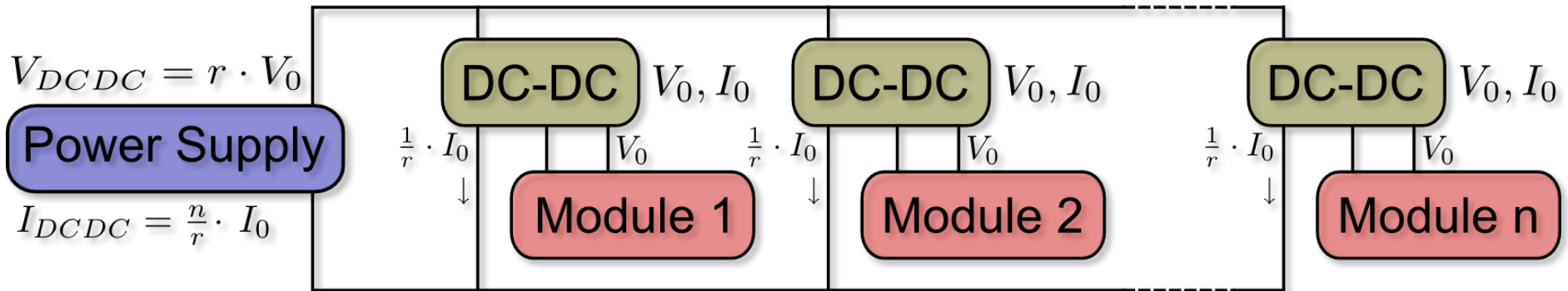
BACKUP – SLIDES

The total power consumption of the new CMS Tracker will increase:

- Power cables to the tracker have to be reused, no space for add. ones
- Lower voltage (ASIC technology)
 - Current in the cables to the Tracker will increase, even if the power consumption would stay the same

→ A new powering scheme is mandatory: **DC-DC conversion:**

Conversion ratio:
 $r = V_{IN} / V_{OUT} \ (r > 1)$



- n modules are powered in parallel
- DC-DC Buck Converters:

Cable losses: (r = 4, Efficiency $\eta = 80\%$)

- without converter: $P_{Cable} = 30.0 \text{ kW}$
- with converter: $P_{Cable} = 2.3 \text{ kW}$

- Convert higher input voltage to a lower output voltage
“Step-down Converter” $U_{in} > U_{out} \rightarrow I_{in} < I_{out}$
- Losses without DC-DC: $P_{cab} = R \cdot I^2$
- Losses with DC-DC Conversion: $P_{cab,DCDC} = R \cdot (n \cdot I_0)^2 \cdot (1/r)^2 = R \cdot I^2 \cdot (1/r)^2$

DC-DC Converters: **Buck Converters**

- **High-voltage tolerant (up to 12V) and radiation-hard ASICs needed:**

- Up to $\sim 10^{15}$ n/cm² (1MeV neutron equivalent) and ~ 100 Mrd (TID)
→ **CERN AMIS2: Prototype** for radiation hard Converter [F. Faccio et al.]

- **Efficiency:**

- $$\eta = \frac{P_{out}}{P_{in}} = \frac{V_{out} \cdot I_{out}}{V_{in} \cdot I_{in}}$$

→ **Efficiency Measurements**

- **Inductors:**

- CMS Tracker: B=3.8T
→ Converters have to be magnetic field resistant
- Ferrite material saturates in a strong magnetic field
→ Use of air-core coils inevitable
- Air-core coils are bulky and radiate noise

→ **Magnetic Field Tests**

- **Converter switching noise:**

- Switching device ($f_{SWITCH} \sim$ MHz)
- Additional source of noise in the system

→ **Spectrum Analysis (Converter Noise)**

→ **System Test Measurements**

(With current CMS Tracker Hardware)

→ **Susceptibility Measurements**

- **Material budget:**

- Material budget of the new CMS Tracker should decrease, even with converters

→ **Simulation of the MB**

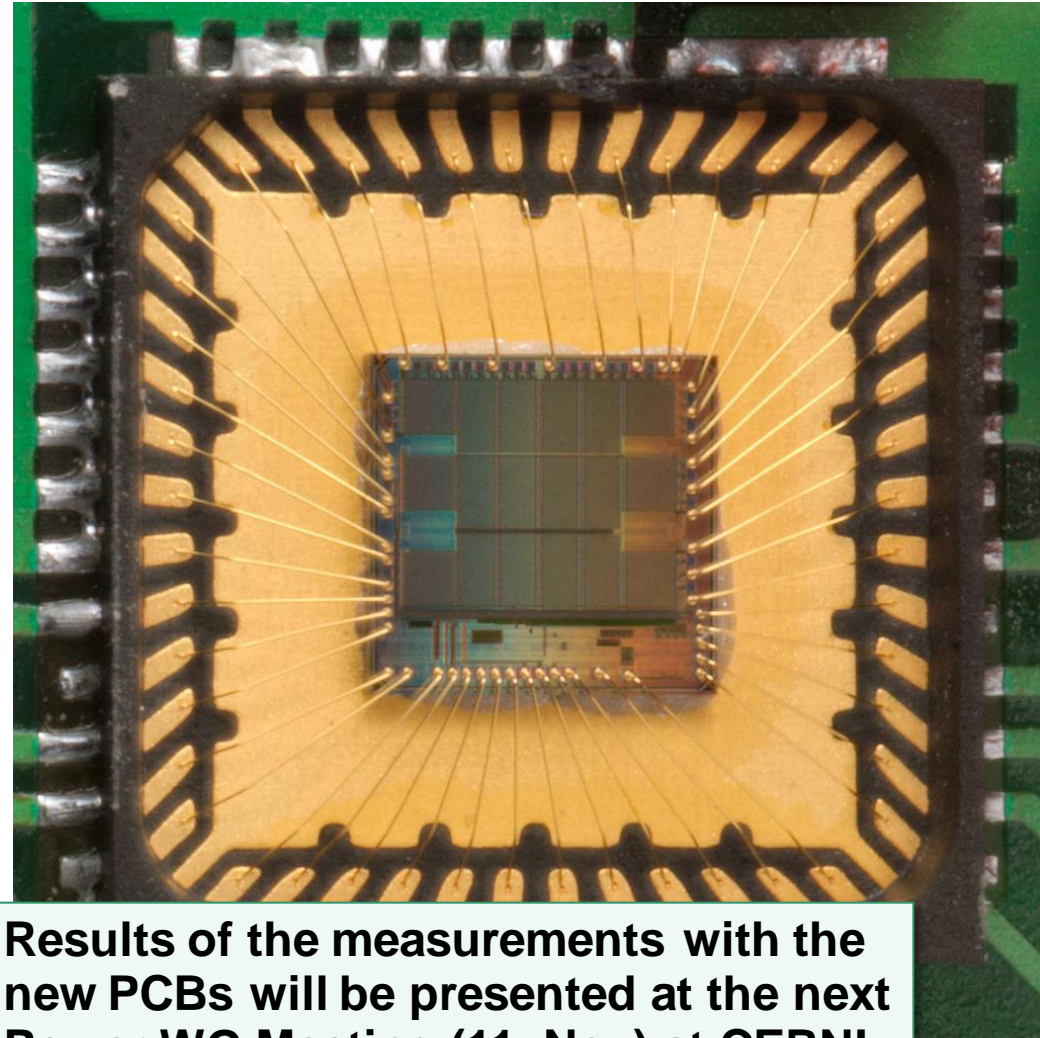
→ **R&D: CO₂-Cooling Test System**

- **Space constraints:**

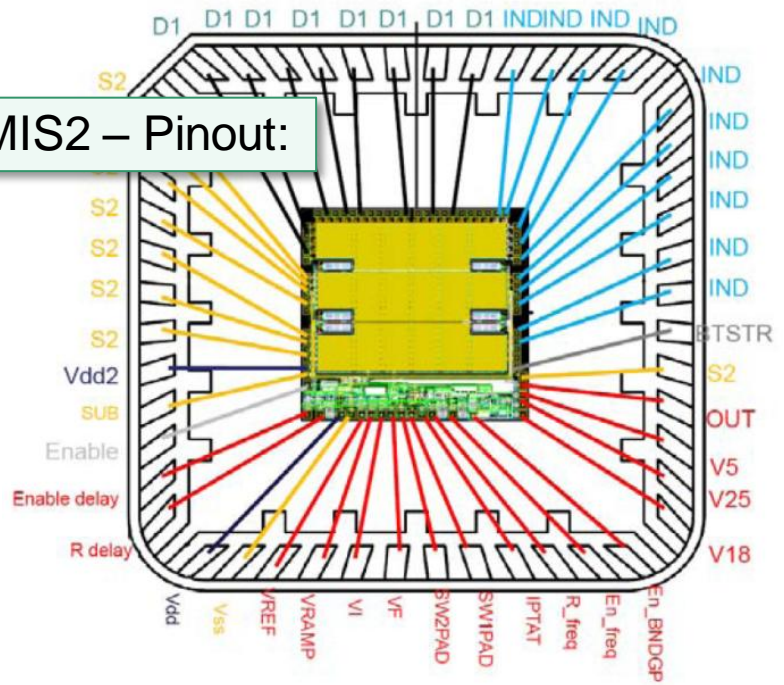
- Where can the Converters be placed? Maximum dimensions?

- Package: QFN32
- $V_{OUT} = 1.2..5V$; $I_{OUT} < 2.8A$; $f_{SW} = 0.6..3MHz$
- Tested up to 300 Mrad = 3000 kGy with only 2% efficiency loss (after annealing)
- Integrated feedback loop with bandwidth of 20KHz
- Internal voltage reference
- Lateral HV transistors are used as power switches
- Noise and efficiency on upcoming slides

AMIS2 – Picture:

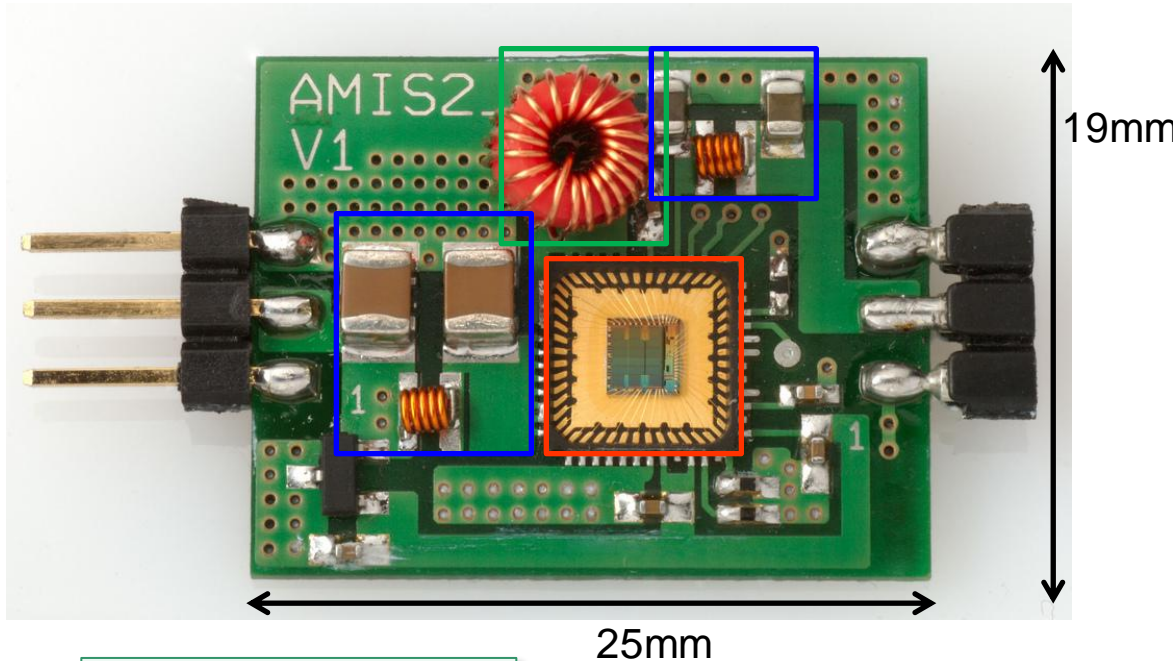


AMIS2 – Pinout:



Results of the measurements with the new PCBs will be presented at the next Power WG Meeting (11. Nov) at CERN!

Aachen R&D: develop Converters based on (not yet) radiation-hard buck converter ASICs; optimize for low mass, low space, low noise; and study in system test



PCB:

2 copper layers a $35\mu\text{m}$
FR4 1mm
 $V = 19 \times 25 \text{mm}^2 \times 10 \text{mm}$
 $m = 2.5 \text{g}$

Chip: AMIS2 by CERN

$V_{\text{IN}} = 6\text{-}11\text{V}(\text{rec.}) / 12\text{V}(\text{max.})$
 $I_{\text{OUT}} < 3\text{A}$
 $V_{\text{OUT}} = 1.2\text{V}$ and 2.50V
 $f_{\text{S}} \approx 1\text{MHz}$

External air-core inductor:

Custom-made toroid, $\varnothing \approx 6\text{mm}$,
height = 7mm, $L = 600\text{nH}$, $R = 80\text{m}\Omega$

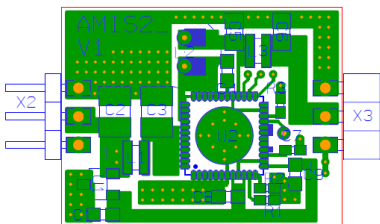
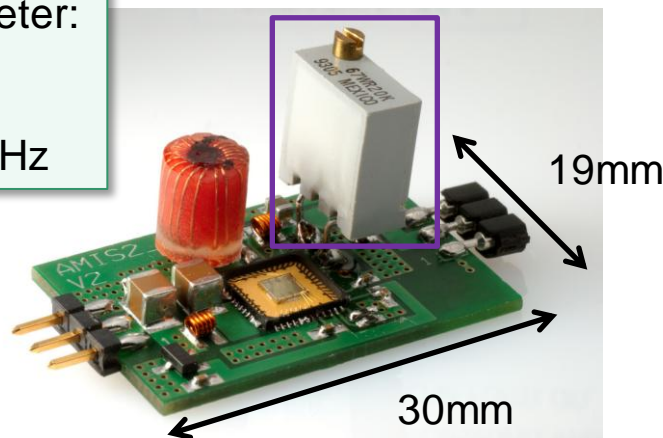
Input and output π -filters

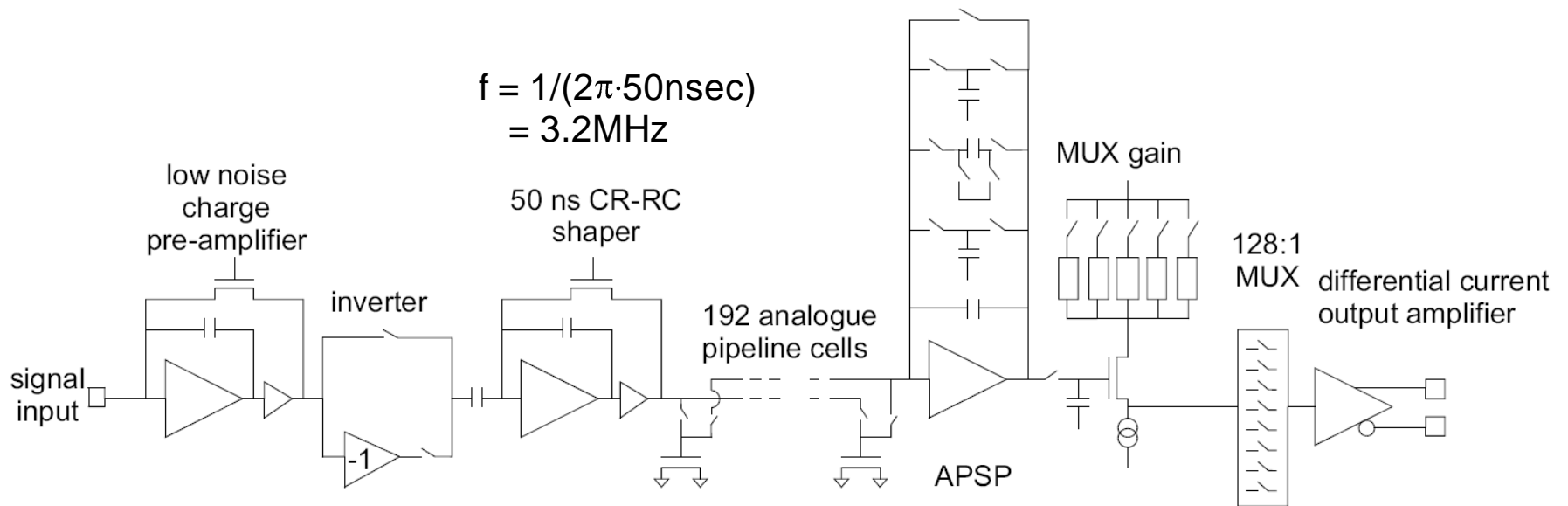
$L = 12.1\text{nH}$, $C = 22\mu\text{F}$

Potentiometer 20k Ω for altering f_{S}

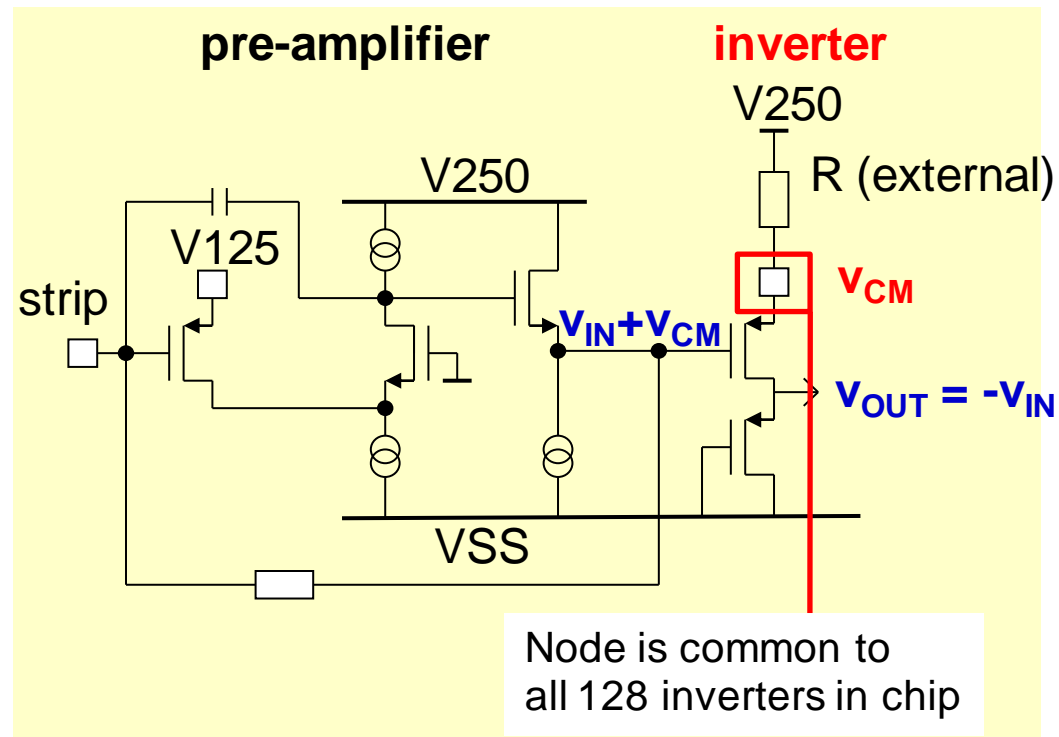
20k Ω Potentiometer:

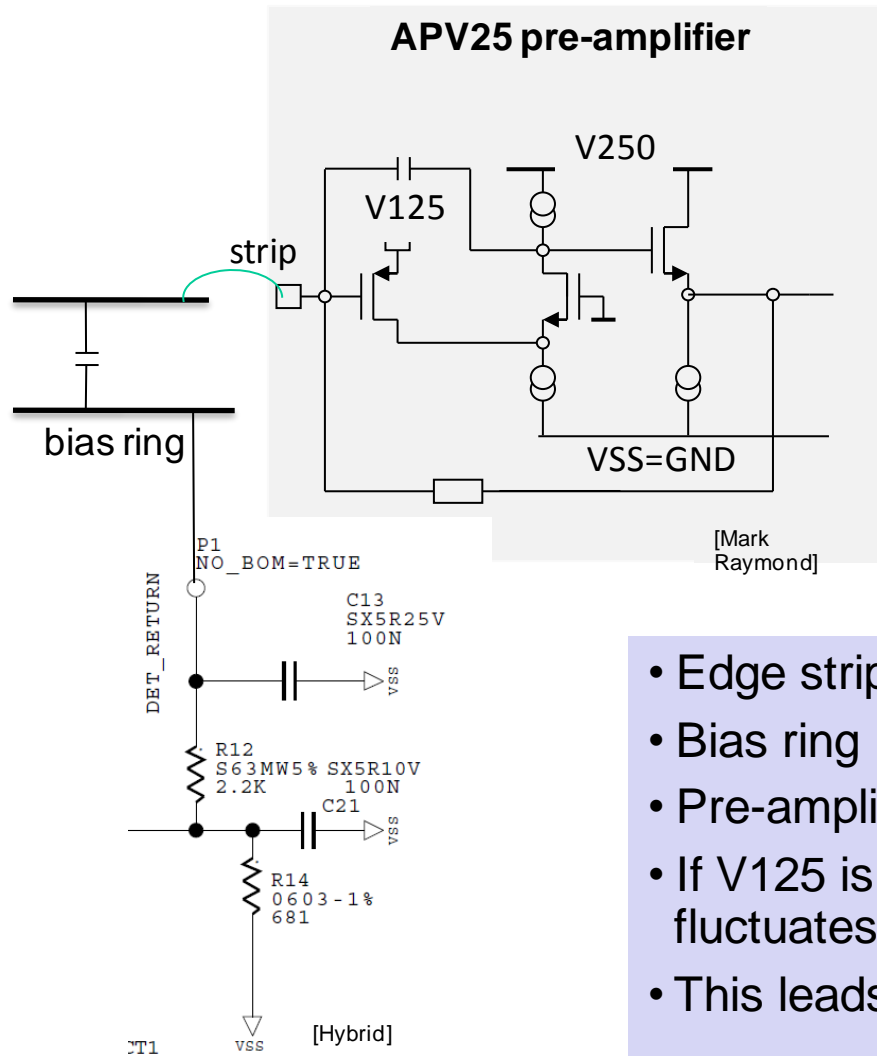
$m = 3,7\text{g}$
 $A = 19 \times 30 \text{mm}^2$
 $f_{\text{S}} = 600\text{kHz}..3\text{MHz}$





- 128 APV inverter stages powered from 2.5V via common resistor (historical reasons)
 \Rightarrow mean common mode (CM) of all 128 channels is effectively subtracted on-chip
- Works fine for regular channels which see mean CM
- CM appears on open channels which see less CM than regular channels
- CM imperfectly subtracted for channels with increased noise, i.e. edge channels





- Edge strips are capacitively coupled to bias ring
- Bias ring is AC coupled to ground
- Pre-amplifier is referenced to 1.25V
- If V125 is noisy, pre-amp reference voltage fluctuates against input
- This leads to increased noise on edge channels