

Light Triggering of Thyristors

Pulse Power for Kicker Systems workshop at CERN

Janusz Rodziewicz *et al.*

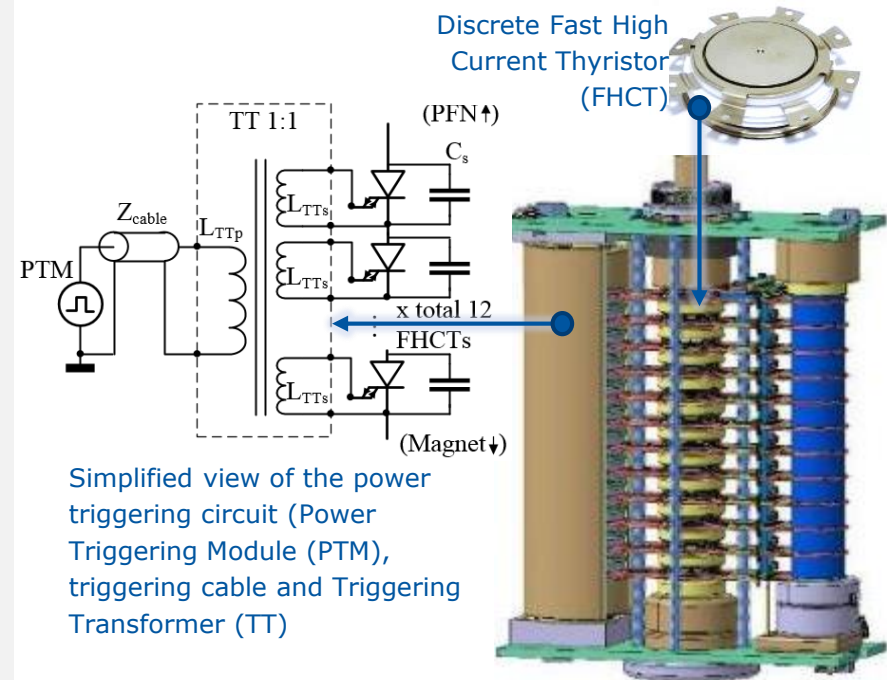
CERN TE-ABT R&D Working group

Outline

- Solid-state devices challenges in segmented extraction kicker systems
- Basics of Optical Absorption
- Few examples of light activated pulsed power devices:
 - Light-Triggered Thyristor (LTTs © Infineon)
 - Laser Pumped Silicon Thyristor (LPST © APP Inc.)
 - Laser Gated and Pumped Thyristor
- About the investigations at CERN

Solid-state switches challenges in segmented extraction kicker systems

- **Low turn-on delay** – The necessity of immediate switch re-triggering and asynchronous beam abort requests from switch a low turn-on delay as during this time the uncontrolled beam energy can damage the accelerator downstream equipment;
- **Easy maintenance/accessibility** aseptically in replacements of thyatron/ ignitron based systems, regular cables can not be used to connect the PTM;
- **Extremely stringent requirements** reliability, availability and fault-tolerance;
- **Gate pulse requirements** most of pulsed power semiconductors (bipolar technologies) follow the trend of increasing request on gate current, FHCT: $2e^3A$ in peak and rise rate of $5e^3 A/\mu s$;
- **Triggering system robustness to EMI- erratic coupling**, the noise of less than 1% of the nominal gate pulse can set the switch into an uncontrolled conduction, possibly destructive. Case aseptically of easy-triggerable devices.
- **Operating voltage de-rating** limited radiation hardness of semiconductor switches implies the necessity of stacking of multiple switches;
- **Sourcing aspect** of selected switch;



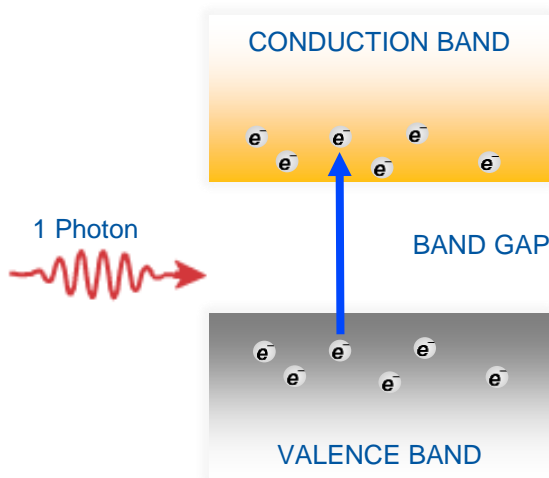
Simplified view of the power triggering circuit (Power Triggering Module (PTM), triggering cable and Triggering Transformer (TT)

Main switch of future SPS Beam Dumping System, 3D Model

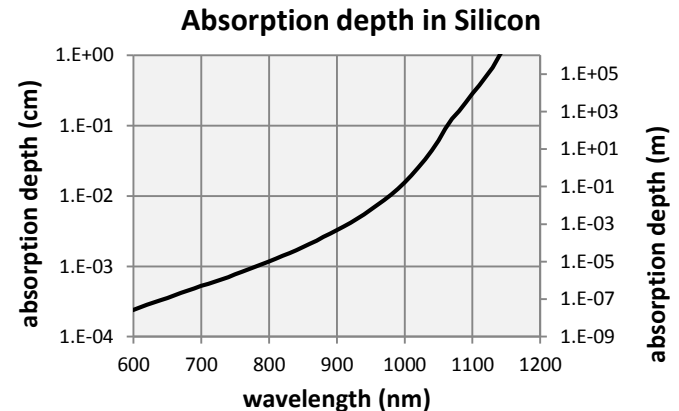
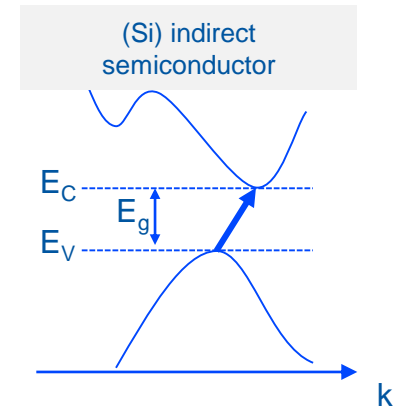
Basics of Optical Absorption

Optical absorption is fundamental process which is exploited when optical energy is converted into electrical energy.

- The energy has to be conserved
- The momentum has to be conserved



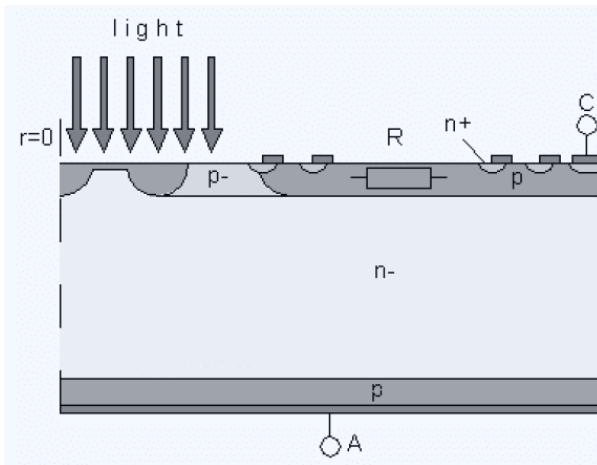
Wavelengths **over 1100nm** are **ineffective** because photon energy is insufficient for the electron-hole pair generation. Light **effectiveness goes down** too, when wave length becomes **less than 1000nm** due to low light penetration into silicon and electron-hole pair recombination close to surface.



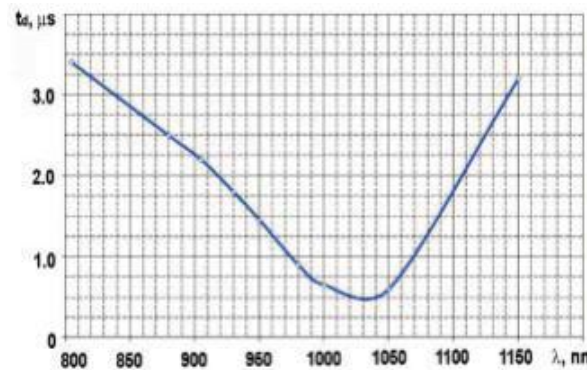
Light-Triggered Thyristor (LTTs)

Light pulse parameters example:
40mW, 10 μ s long, 0.4 μ J,
850nm-1000nm wavelength

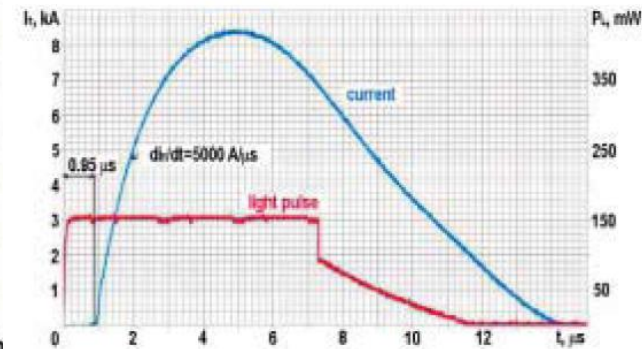
- The central area of the LTT consist of a Break-over Diode (BoD) and a multiple Amplifying Gate structure.
- The BoD is located inside the light sensitive area.



Cross-section of the center of the light-triggered thyristor.

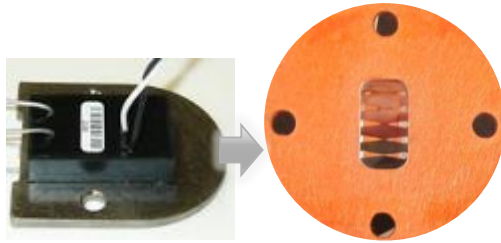


Simulated LTT turn-on delay time versus laser diode wave length ($P_{LM} = 200$ mW, $V_A = 100$ V)

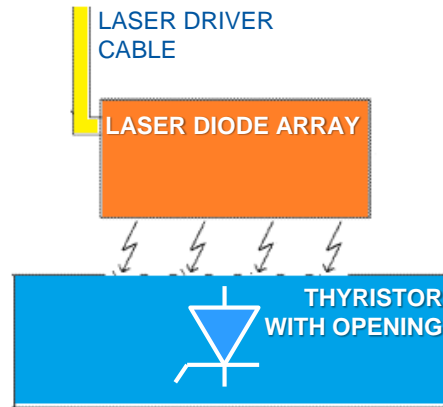


Anode current turn-on example waveforms.

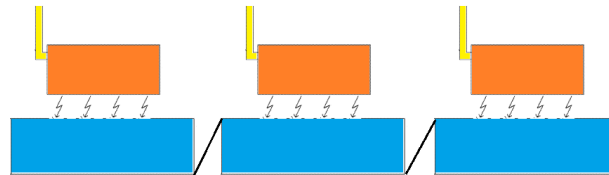
Laser Pumped Silicon Thyristor © APP Inc.



Commercially available APP Inc. switch modified for laser pumping – with openings windows patterned in the anode metallization.



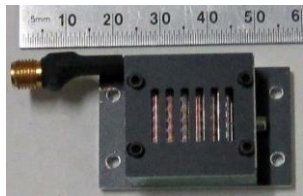
One switch embodiment view.



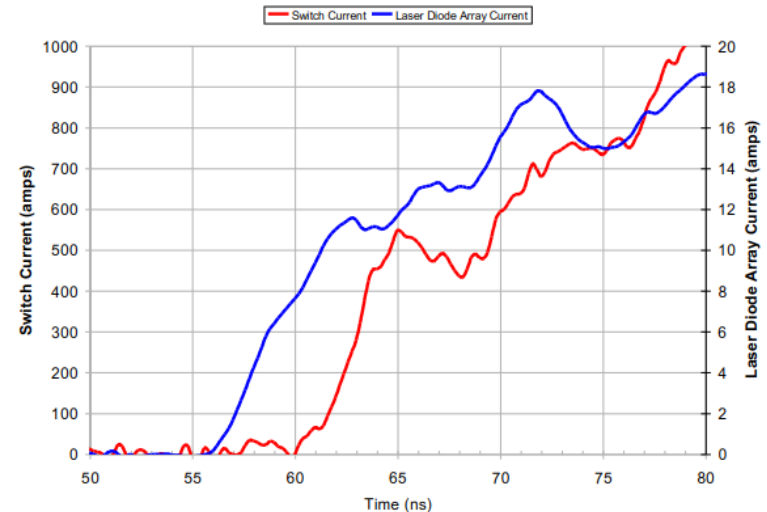
Series connected stacks, each device has it separate photon source. Each of the thyristors are coupled together with stage to stage connection.

Light pulse parameters example:
650W in peak, 170uJ, 400ns FWHM, 1000nm wavelength

Demonstrated performance:
2500A in less than 40ns



1kW Laser diode array

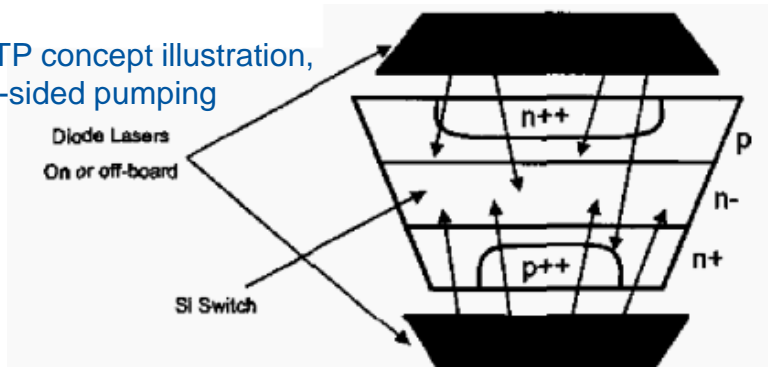


5ns of turn-on delay measured between the switch current and laser driver current.

Laser Gated and Pumped Thyristor

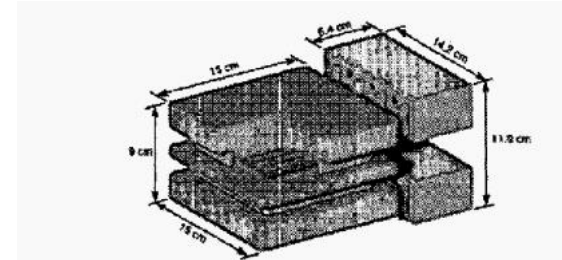
First developed for Electra, a Krypton Fluoride (KrF) laser.
Primary energy transfer time of 800 μ s for a
Marx-charged one-stage magnetic pulse compressor

LGTP concept illustration,
two-sided pumping

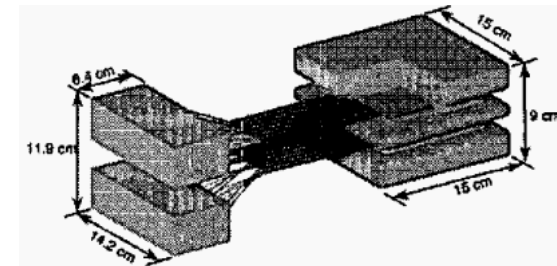


Light pulse parameters example:
5kW/cm² over 50ns followed by continuous illumination
levels 500, 1000, 2000, 5000 W/cm² in order to reduce
forward dissipation.

Demonstrated performance of 16.4kV devices:
Single shot operations at 3kA/cm² , 30kA/ μ s/cm²



On-Board (Direct Illuminating)
Conceptual Embodiment.

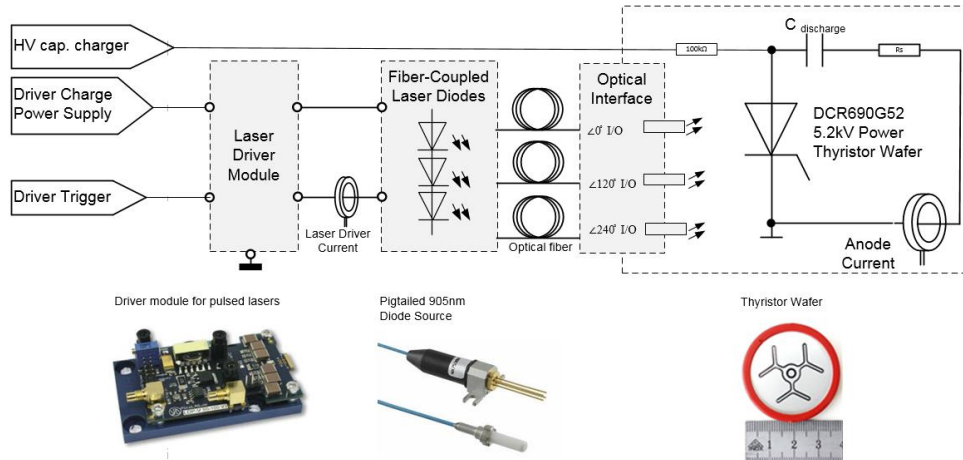
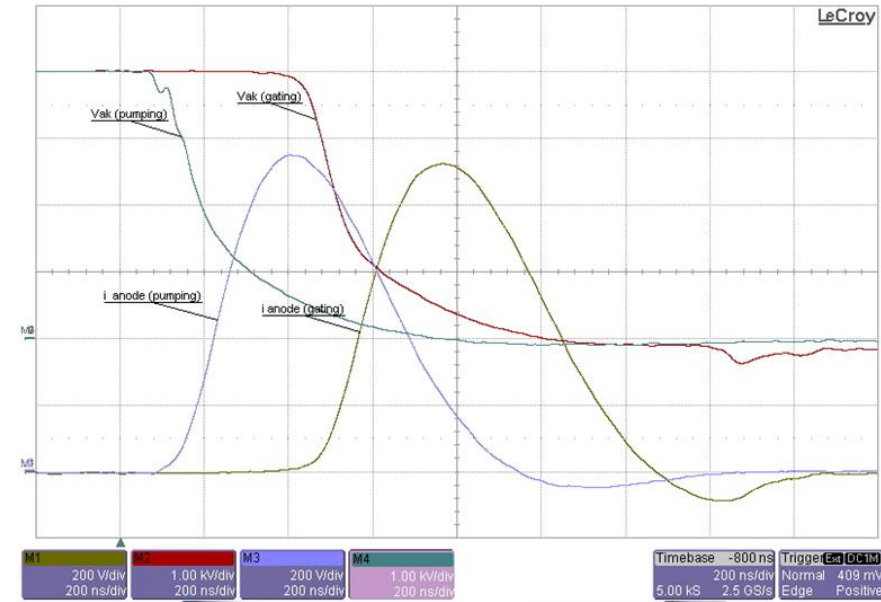


Off-Board (Indirect Illuminating)
Conceptual Embodiment.

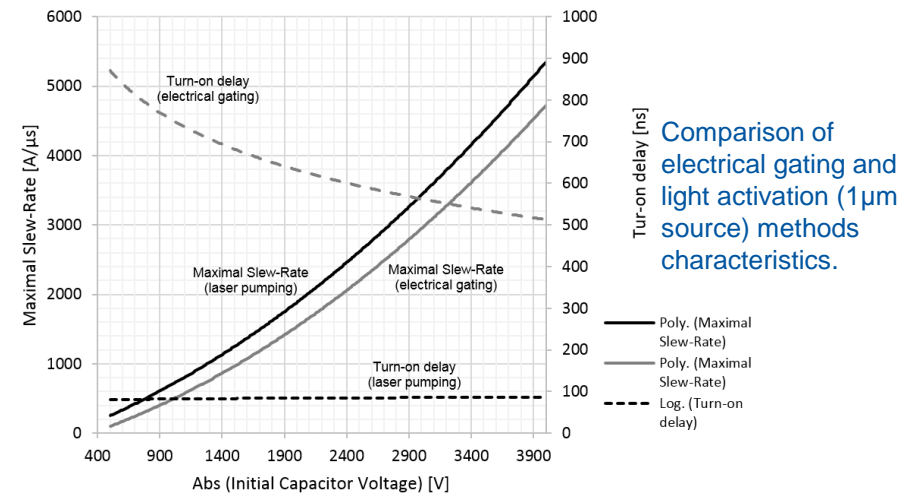
Investigations at CERN



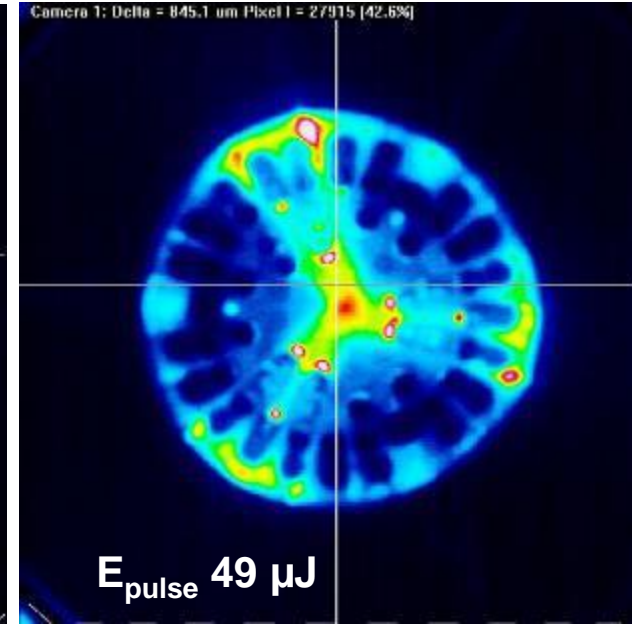
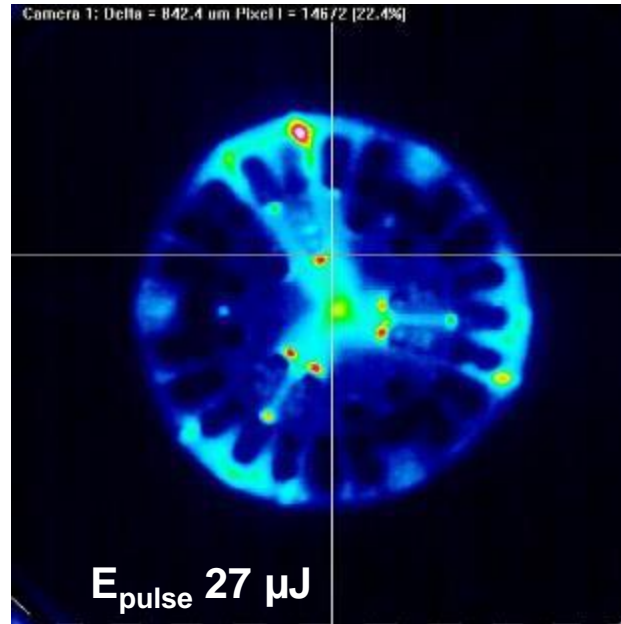
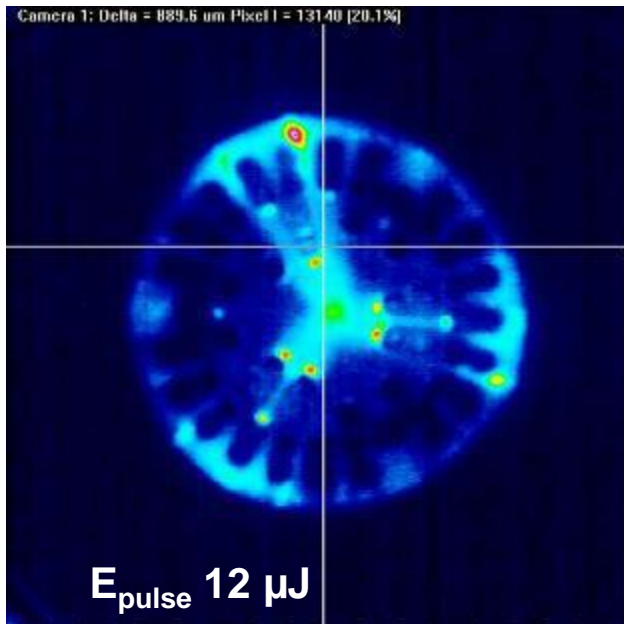
So far in our investigations we use market available Low Cost SCR Phase Control Thyristors. Activation is being achieved through gate distribution illumination with an appropriate light source.



Example view of electrical test setup.



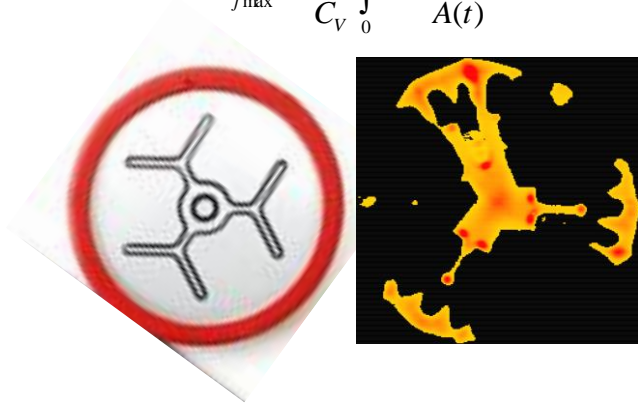
Wafer illumination profile imaging with a CCD camera, 905nm light source



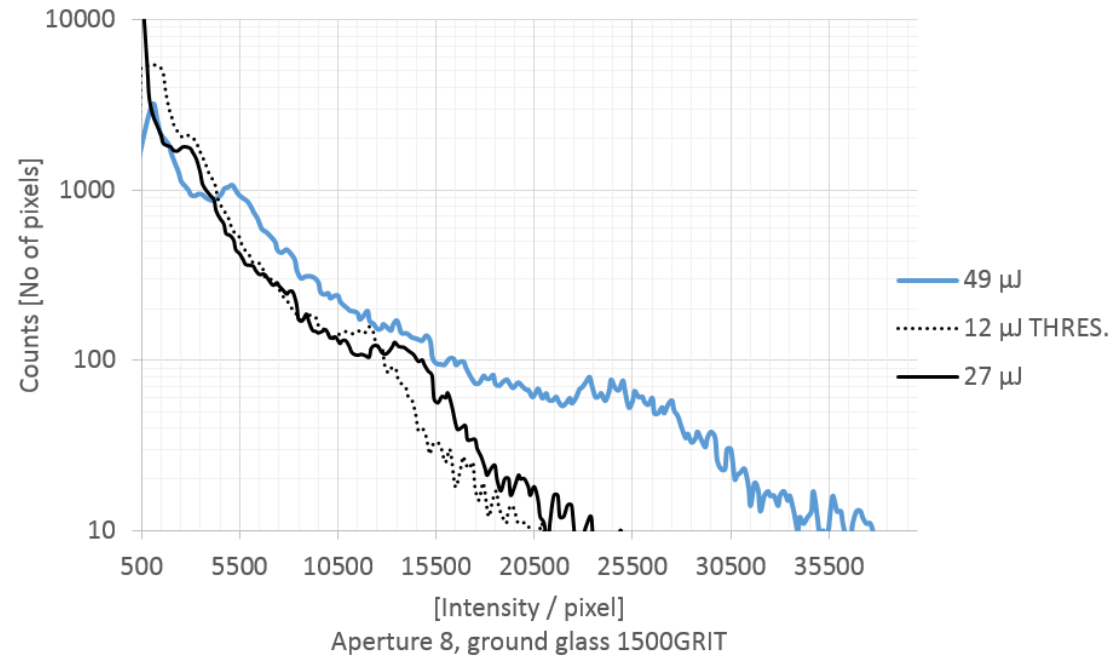
Wafer illumination profile imaging with a CCD camera, 905nm light source

- In electrical test 12μJ pulse energy defines a threshold where the SCR thyristor starts turning-on (very slowly)
- If the threshold intensity is known, one can rad-out the initial conductive area A(t) at the very beginning of the thyristor turn-on. This area is directly linked to maximum allowable di/dt capability of the device. C_v is the specific heat of silicon, t_f is the falling time of the blocking voltage.

$$\Delta T_{j\max} = \frac{1}{C_V} \int_0^{t_f} V_{AK}(t) \frac{di}{dt} \times t \, dt$$



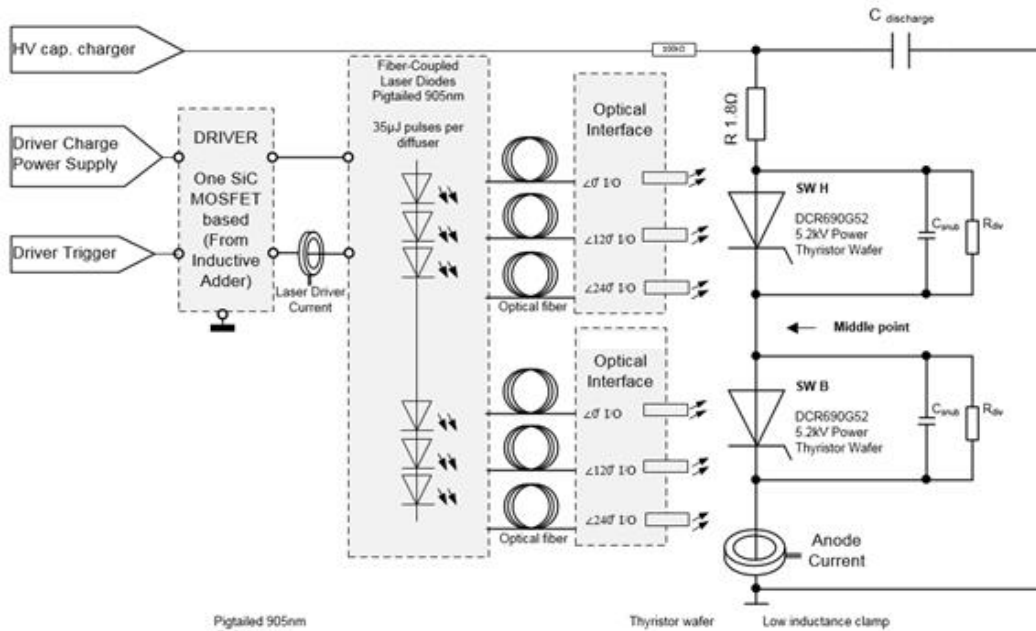
Mapping of the area illuminated above the threshold intensity. 49uJ light pulse.



Tests with a series of two connected SCR thyristor devices



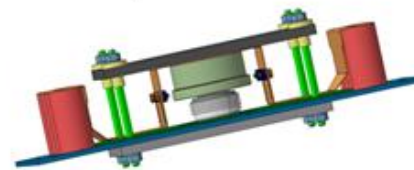
- Fiber-coupled light source limitation;
- A correct balance of the total voltage between series connected switches is curtail for the performance;
- Small differences in commutation characteristics between the switches can be compensated by means of a snubber circuit



Pigtailed 905nm diode source



Thyristor wafer



Low inductance clamp

Thank you for
your attention

Questions ?

REFERENCES

- “Integrated Silicon Optoelectronics”, “Basics of Optical Emission and Absorption”, Zimmermann H., Springer, (2010)
- “Laser Pumping of 5kV Silicon Thyristors for Fast High Current Rise-Times”, Howard D. Sanders, Steven C. Glidden, Daniel M. Warnow, Applied Pulsed Power, Inc., (2011)
- “Direct Light-Triggered Solid-State Switches For Pulsed Power Applications”, J. Przybilla, R. Keller, U. Kellner, H.-J. Schulze, F.-J. Niedernostheide, T. Peppel, PPC-2003. 14th IEEE International, Volume: 1
- “Novel Light Triggering Thyristor for phase control and Pulse Power Applications”, A.V.Grishanin, V.A.Martynenko, A.A.Khapugin, S.A. Tundykov and S.A. Safronenkov, JSC Electrovipryamitel, Saransk, Russia and A.V.Konuchov, All-Russian Electrotechnical Institute, Moscow, Russia, Published in Bodos Power, (June 2012)
- United States Patent ,Glidden et al. “LASER PUMPING OF THYRISTORS FOR FAST HIGH CURRENT RISE-TIMES”, US 8,461,620 B2, Jun. 11, (2013)
- “Technological Breakthroughs in Light-Activated Thyristors for Pulsed Power”, Douglas M. WeidenheimerS, David Giorgi',Titan Pulse Sciences Division, (2004)
- W.C. Nunnally, R.B. Hammond, “Photoconductive Power Switches”, Los Alamos N.L., New Mexico, (1983)
- Yeh, Chai, “Handbook of Fiber Optics: Theory and Applications”, Elsevier Science, Saint Louis, (2013)
- N. Mohan, T. M. Undeland, “Power Electronics and Devices”, Second Edition, John Wiley & Sons, Inc., (1995)