

# Inductive Adder for FCC Injection Kicker Systems

# Requirements for the FCC injection Inductive Adder

| Parameter             | Unit              | Value      |
|-----------------------|-------------------|------------|
| Pulse flat top length | [ $\mu\text{s}$ ] | 2.00       |
| Flat top tolerance    | [%]               | $\pm 0.50$ |
| Field rise time       | [ $\mu\text{s}$ ] | 0.425      |
| Voltage               | [kV]              | 15.70      |
| Current               | [kA]              | 2.50       |
| System impedance      | [ $\Omega$ ]      | 6.25       |
| Pulse frequency       | [Hz]              | 115        |

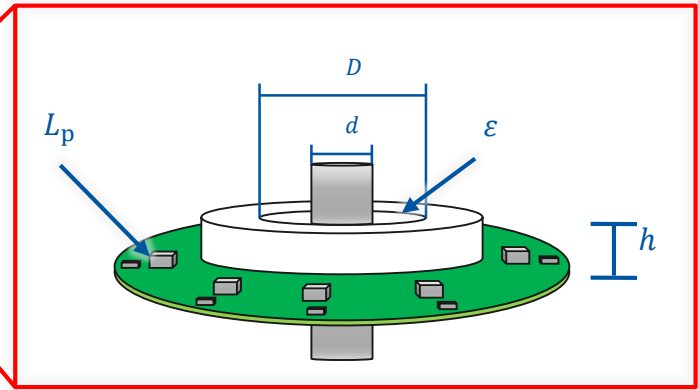
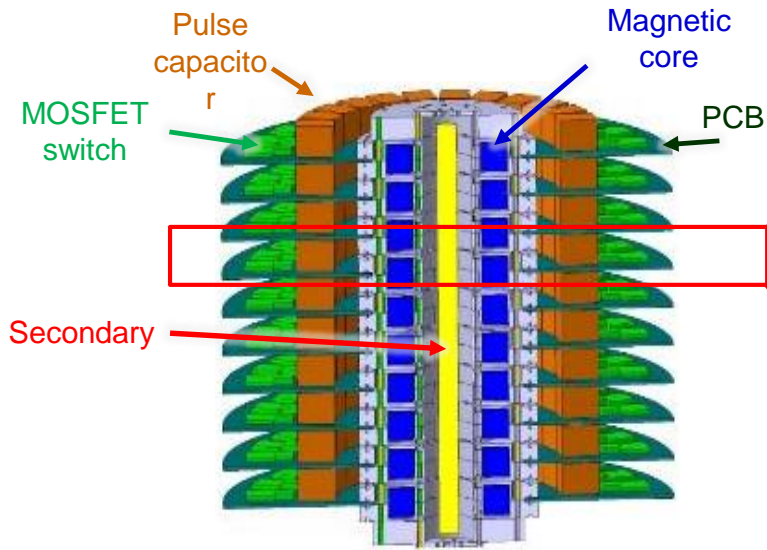
Challenges of the inductive adder design:

→ 0.350  $\mu\text{s}$  of **kicker magnet fill time**  
→ **0.075  $\mu\text{s}$**  remain for **pulse current rise time**

← Relatively high current

← Low impedance

# One layer of the Inductive Adder



## Content

- Impedance matching of the stack
- Layer design for fast rise times
- Biasing of magnetic cores

# Impedance matching of the stack

## Factors influencing the layer impedance:

- Ratio of primary inner diameter ( $D$ ) and stalk diameter ( $d$ )
- Insulation material between primary and secondary ( $\epsilon$ )
- Layer height ( $h$ )
- Inductance of primary winding ( $L_p$ )

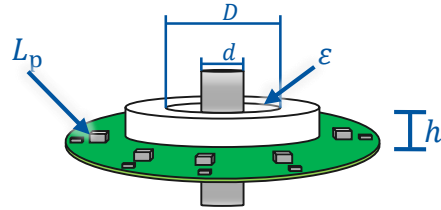
Examples for insulation materials:

- Air
- Oil
- Water
- Epoxy
- FC-77
- SF6
- Vacuum

Electric field in insulation:

$$E(r) = \frac{V_{out}}{r \cdot \ln \frac{D}{d}}$$

$$E_{max} = \frac{V_{out}}{\frac{d}{2} \cdot \ln \frac{D}{d}}$$



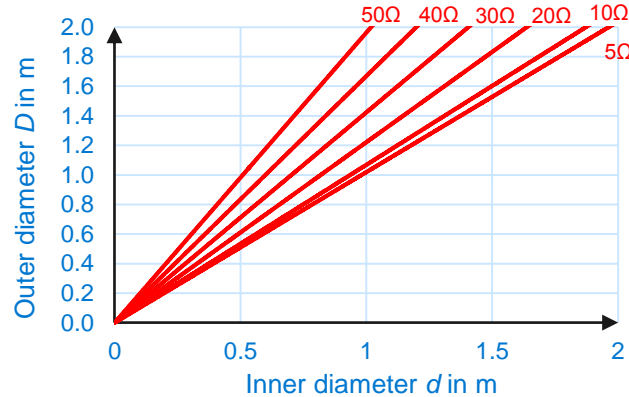
Impedance of IA:

$$C_{layer} = \frac{2\pi\epsilon h}{\ln \frac{D}{d}} \quad L_{layer} = \frac{\mu \cdot h \cdot \ln \frac{D}{d}}{2\pi}$$

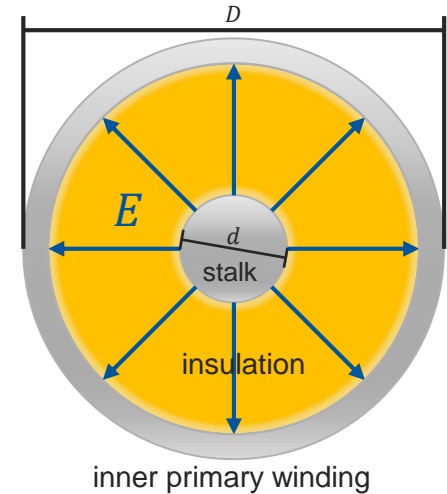
$$Z_{IA} = \sqrt{\frac{L_p + L_{cell}}{C_{cell}}} = \sqrt{\frac{L_p}{2\pi\epsilon h} \ln \frac{D}{d} + \frac{\mu}{4\pi^2\epsilon} \ln^2 \frac{D}{d}}$$

Outer diameter  $D$  over inner diameter  $d$  for different  $Z_{IA}$

$$D(d) = d \cdot e^{\frac{L_p \cdot \pi}{h\mu} + \sqrt{\left(\frac{L_p \cdot \pi}{h\mu}\right)^2 + Z_{IA}^2 \frac{4\pi^2\epsilon_0\epsilon_r}{\mu}}}$$



Low impedance -> small insulation gap



# Layer design for fast rise time

Propagation time of IA layer:  $t_{p,layer} = \sqrt{(L_p + L_{cell}) \cdot C_{cell}} = \sqrt{\left(L_p + \frac{\mu \cdot h \cdot \ln \frac{D}{d}}{2\pi}\right) \cdot \frac{2\pi\epsilon h}{\ln \frac{D}{d}}} = \sqrt{L_p \cdot \frac{2\pi\epsilon h}{\ln \frac{D}{d}} + \mu\epsilon h^2}$

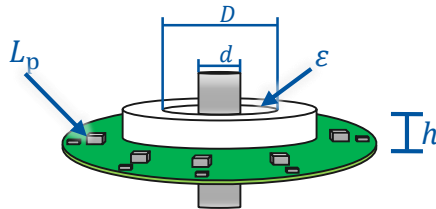
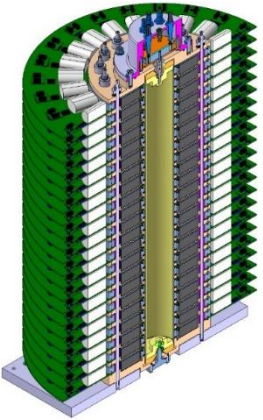
Propagation time of IA stack ( $n$  layers):  $t_{p,stack} = 2n \cdot t_{p,layer} = 2n \cdot \sqrt{L_p \cdot \frac{2\pi\epsilon h}{\ln \frac{D}{d}} + \mu\epsilon h^2}$

$$C_{cell} = \frac{2\pi\epsilon h}{\ln \frac{D}{d}} \quad L_{cell} = \frac{\mu \cdot h \cdot \ln \frac{D}{d}}{2\pi}$$

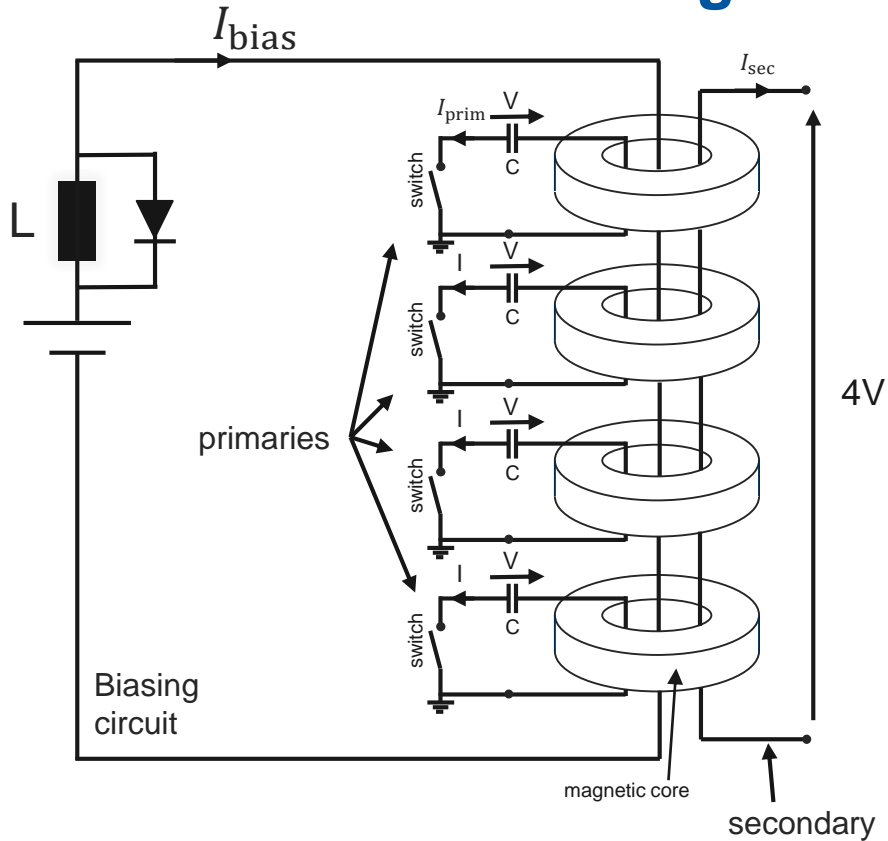
## Factors influencing the rise time:

- Layer height
- Insulation material
- Primary inductance
- Output voltage, layer voltage
- Switching time of switching device (SiC MOSFET)

The inductance of the secondary circuit should be low to not limit the rise time!



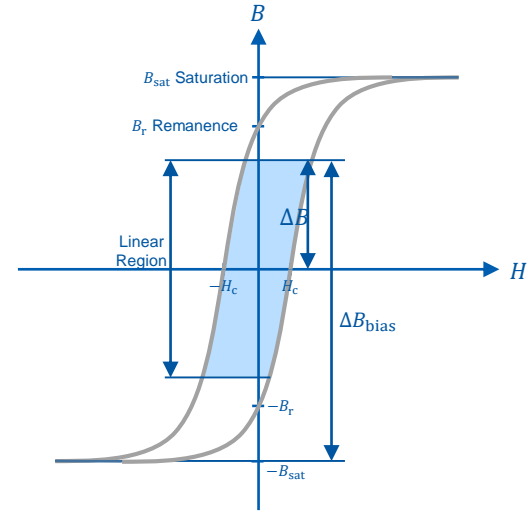
# Biasing of magnetic core



$$A_c = \frac{\int V_c dt}{\Delta B}$$

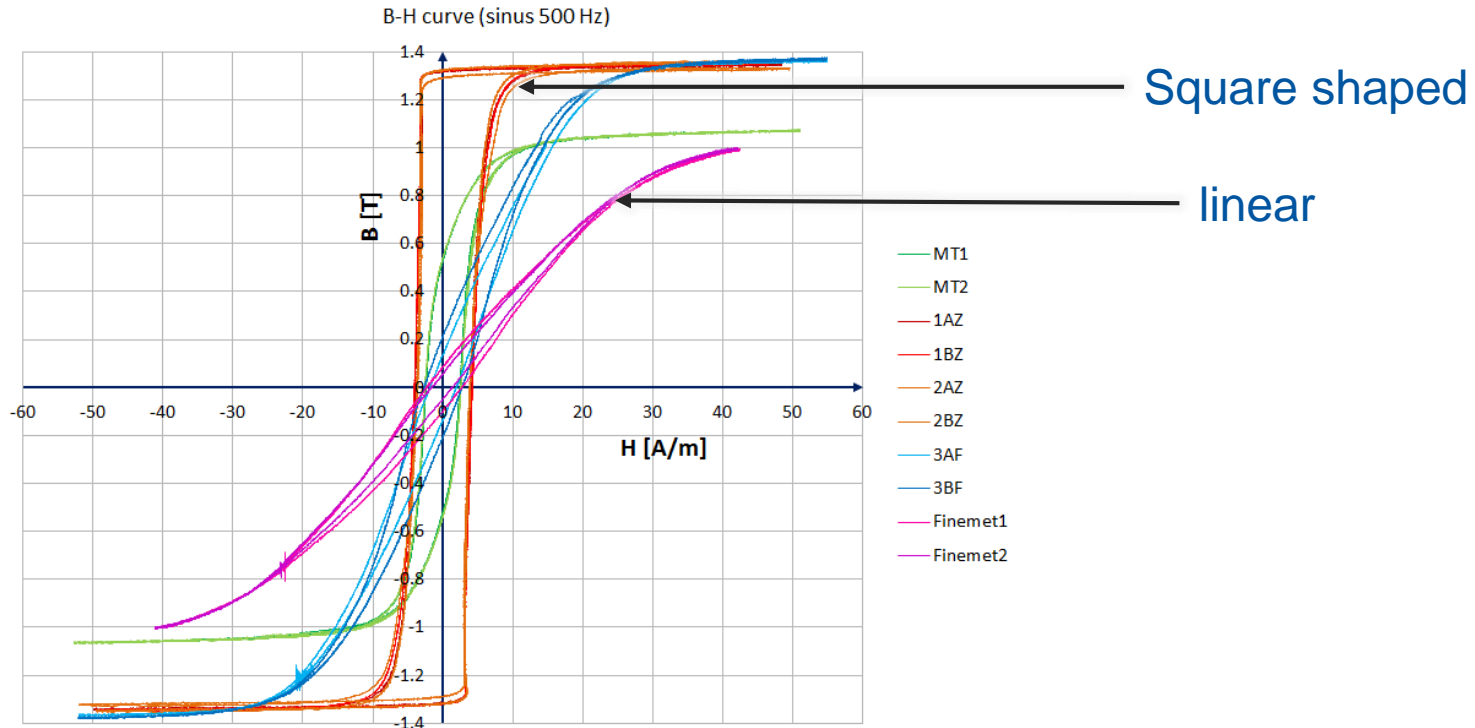
$$\Delta t = \frac{A_c \cdot \Delta B}{V_c}$$

$$\oint H ds = I_{prim} + I_{sec} + I_{bias}$$



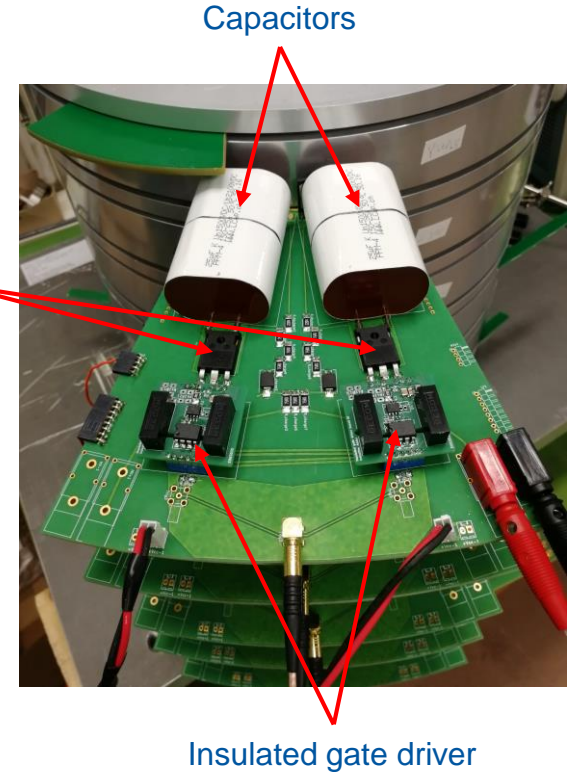
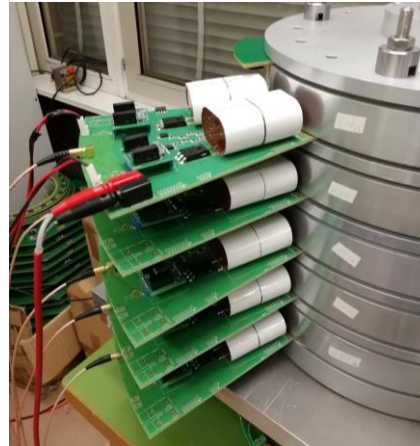
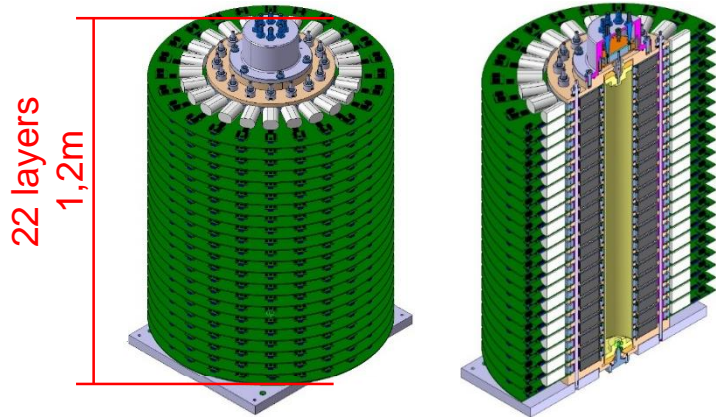
Biasing of the magnetic core can reduce the required core material and therefore **reduce the layer height.**

# Biasing of magnetic core



# Summary

- System impedance of 6.25 Ohm (2.5 kA, 15.7 kV)
- Oil insulation required
- Use of a biasing circuit
  - reduce magnetic material
  - Shorter layer height possible
  - Faster rise time achievable





# Thank you for your attention!

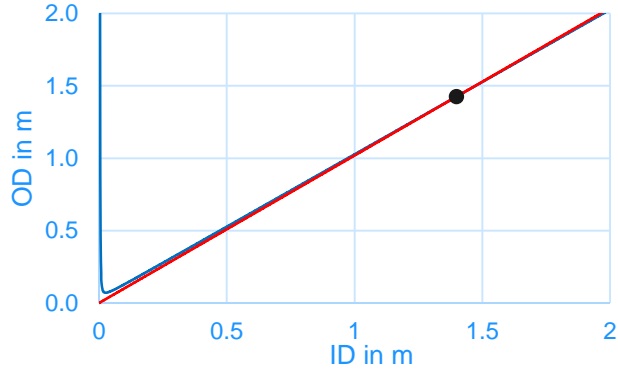
Questions?



[www.cern.ch](http://www.cern.ch)

# Evaluation of Dielectricum

Air



$$\begin{aligned} Z_{\text{out}} &= 5 \Omega \\ d &= 1.405 \text{ m} \\ D &= 1.431 \text{ m} \\ \delta &= 18.7 \text{ mm} \end{aligned}$$

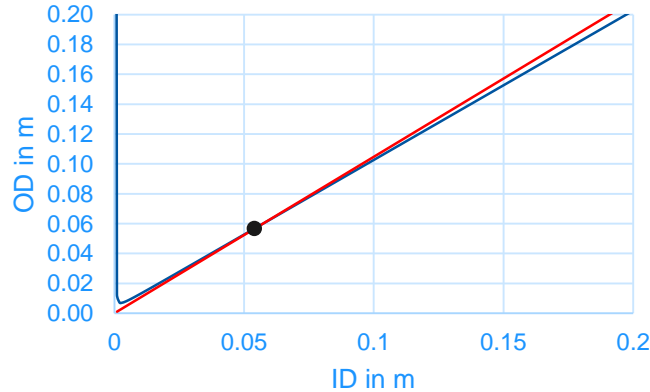
$$E_{\text{max,Air}} = 0.4 \cdot 2.5 \frac{\text{kV}}{\text{mm}}$$

$$\epsilon_{r,\text{Air}} = 1$$

Big diameters result in high costs for the magnetic cores.

Small insulation gaps are difficult to manufacture.

Oil



$$\begin{aligned} Z_{\text{out}} &= 5 \Omega \\ d &= 5.44 \text{ cm} \\ D &= 5.7 \text{ cm} \\ \delta &= 1.3 \text{ mm} \end{aligned}$$

$$E_{\text{max,Oil}} = 0.4 \cdot 25.7 \frac{\text{kV}}{\text{mm}}$$

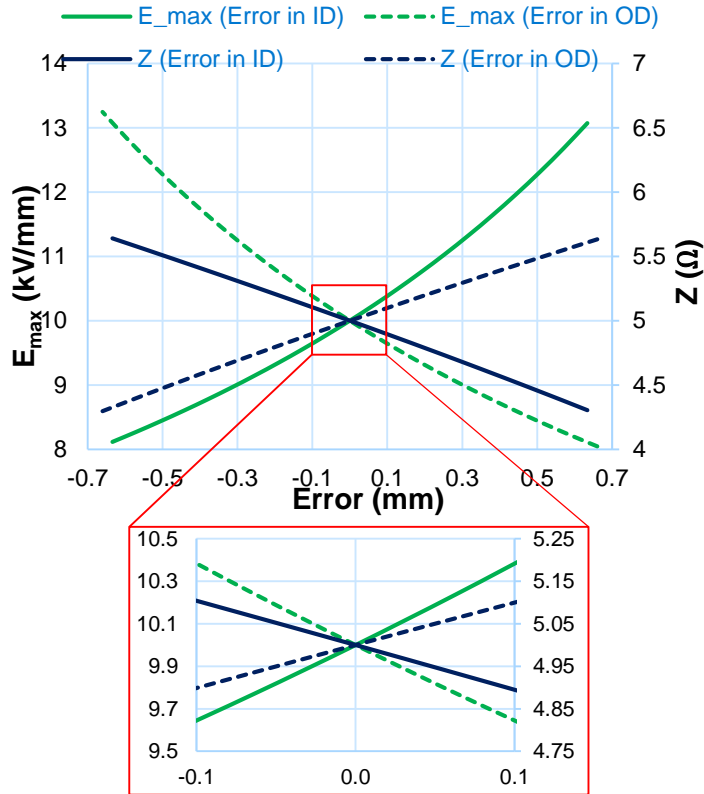
$$\epsilon_{r,\text{Oil}} = 2.7$$

Example for insulation materials:

- Air
- Oil
- Water
- Epoxy
- FC-77
- SF6
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# Tolerances in stalk

Precise manufacturing and adjustment of stalk and core is necessary!



- $E_{\max}$  can be reduced by using bigger diameters
- Impedance mismatch caused by an unprecise stalk is influencing the output pulse

PSpice simulations showed that the error needs to be  $<0.06$  mm, what is a reasonable value.

However, very precise production and alignment of the primary and secondary windings is necessary.

# BH curve measurement test setup from BE-BI-PI

Power supply

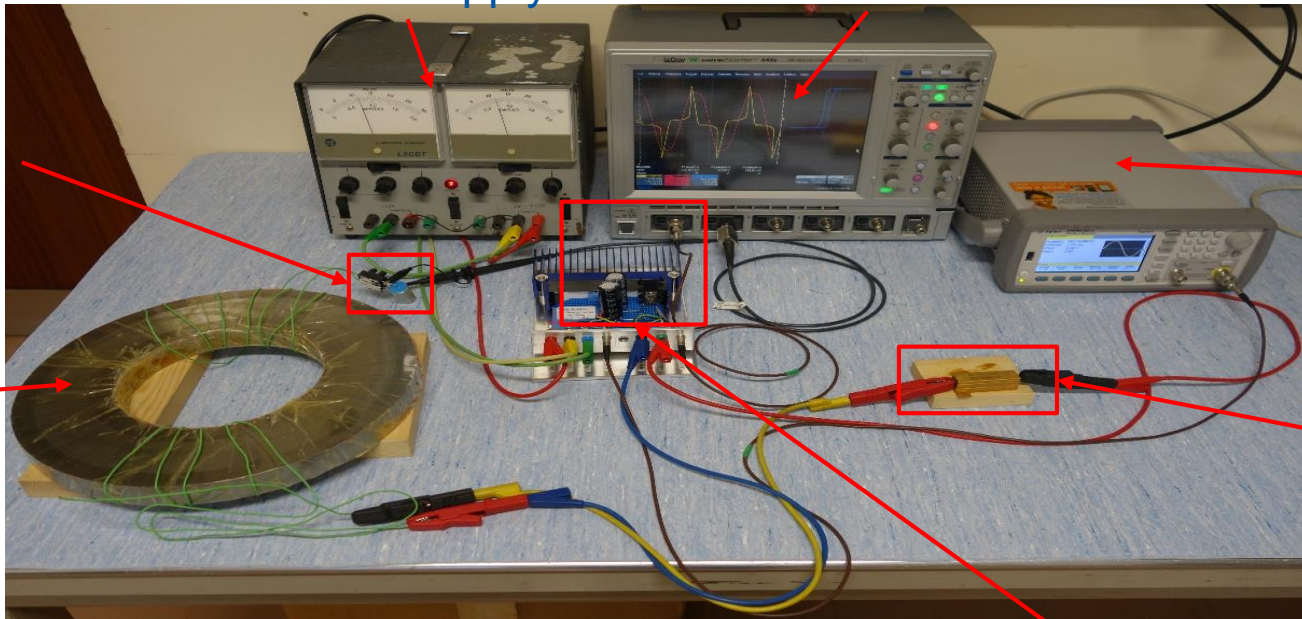
Oscilloscope

RC integrator  
to measure  
 $\int U_{\text{sec}} dt \sim B$

Function  
generator

Test core

Current  
limiting  
resistor



Other required parameters:  
Core dimensions, weight, fill factor,  
no of windings

Amplifier, incl.  $1 \Omega$  Shunt to measure  $I_{\text{prim}} \sim H$   
Thanks to S. Aguilera and M. Krupa