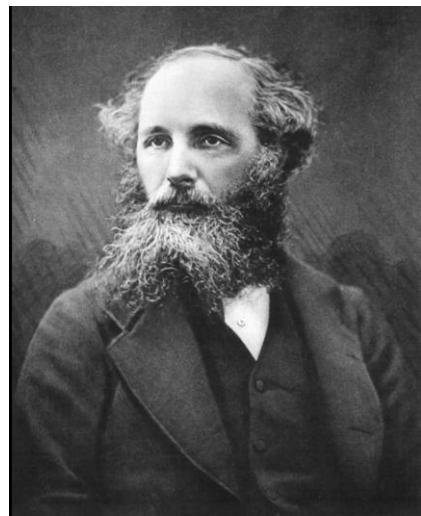


Introduction to RF

Andrea Mostacci
University of Rome “La Sapienza” and INFN, Italy



Outline



Goal of the lecture

Show **principles** behind the **practice** discussed in the RF engineering module

Maxwell equations

General review

The lumped element limit

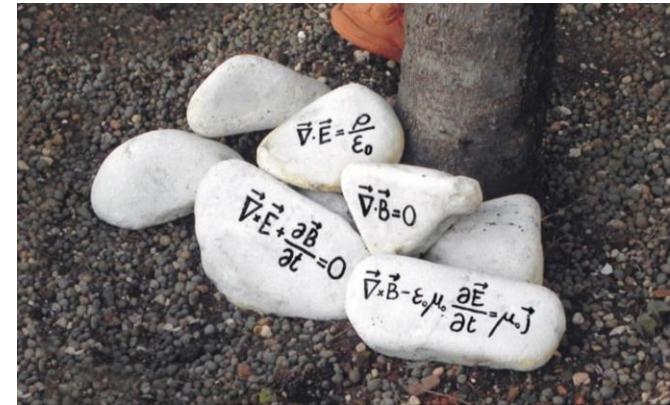
The wave equation

Maxwell equations for time harmonic fields

Fields in media and complex permittivity

Boundary conditions and materials

Plane waves



Boundary value problems for metallic waveguides

The concept of mode

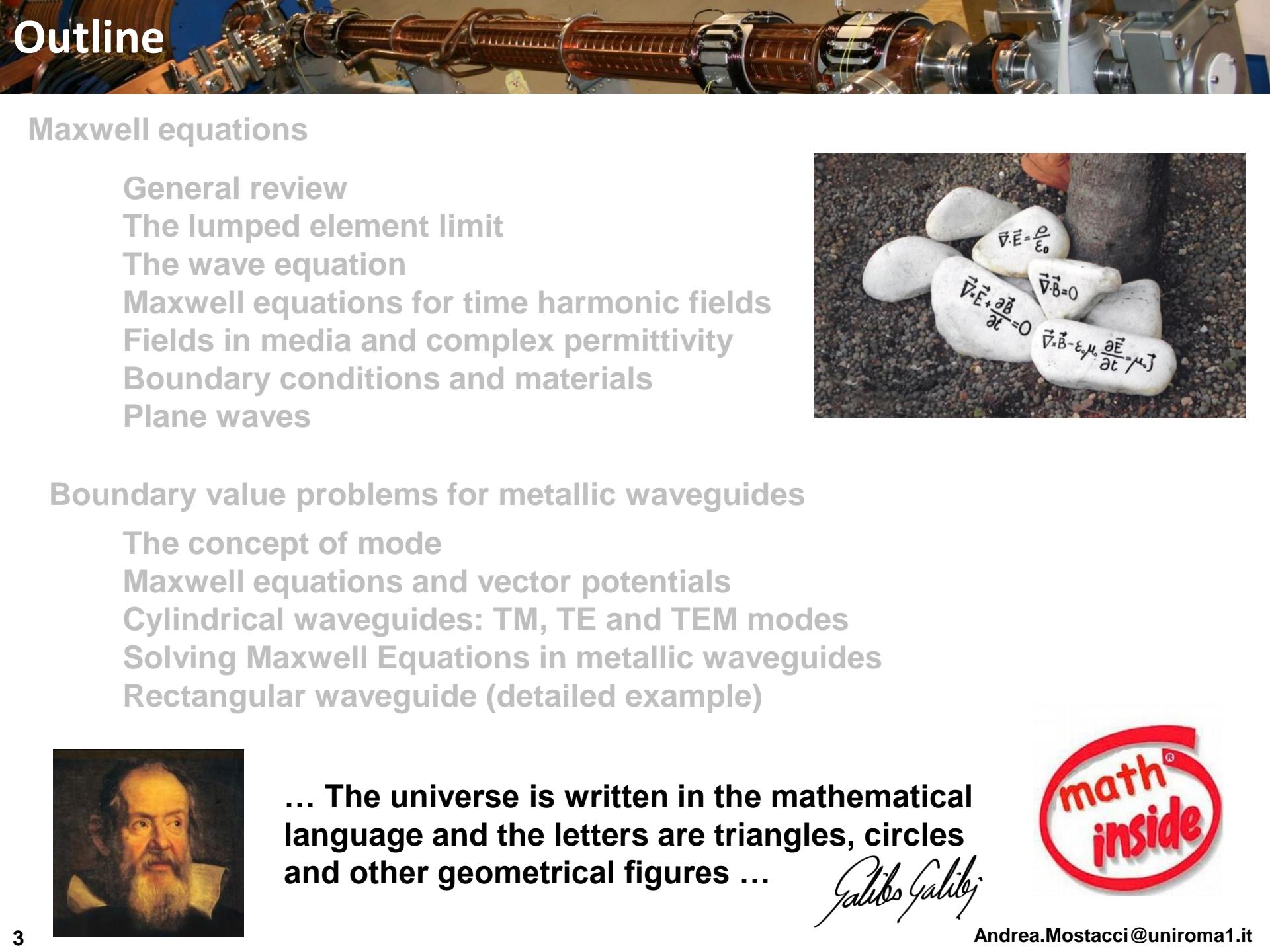
Maxwell equations and vector potentials

Cylindrical waveguides: TM, TE and TEM modes

Solving Maxwell Equations in metallic waveguides

Rectangular waveguide (detailed example)

Outline



Maxwell equations

General review

The lumped element limit

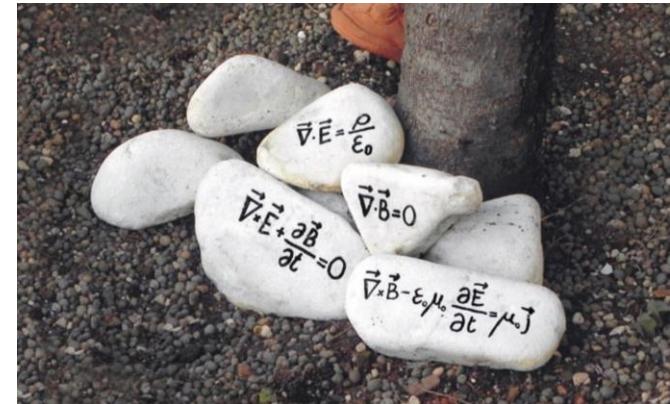
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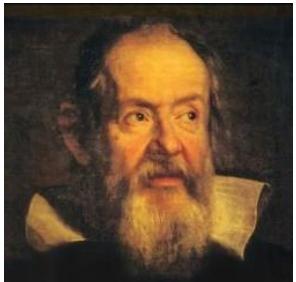
The concept of mode

Maxwell equations and vector potentials

Cylindrical waveguides: TM, TE and TEM modes

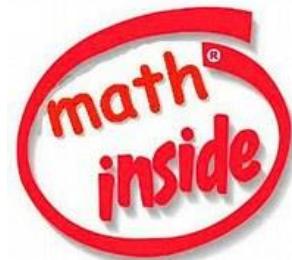
Solving Maxwell Equations in metallic waveguides

Rectangular waveguide (detailed example)



... The universe is written in the mathematical language and the letters are triangles, circles and other geometrical figures ...

Galileo Galilei



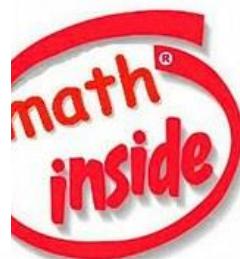
Outline



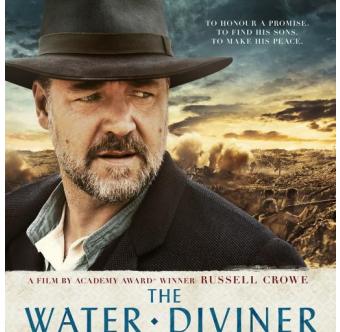
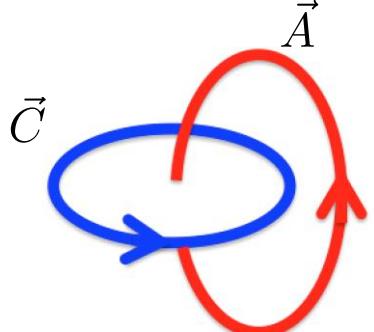
Maxwell equations



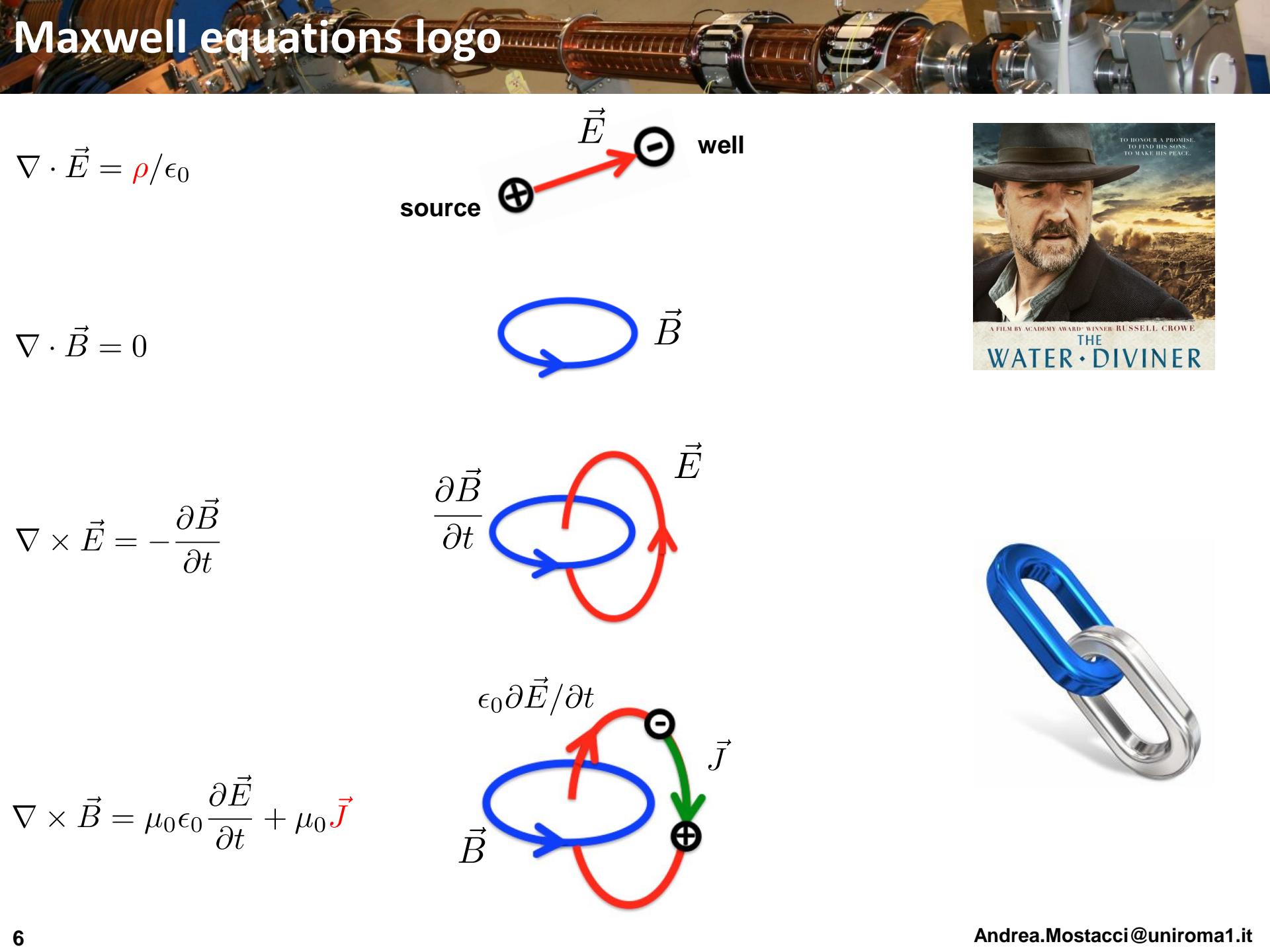
Schedule 2018	Monday Feb 12 th	Tuesday Feb 13 th	Wednesday Feb 14 th	Thursday Feb 15 th	Friday Feb 16 th
09:00					
		Introduction to RF lecture <i>A. Mostacci</i>	Vacuum systems lecture <i>V. Baglin</i>	RF Engineering lecture <i>F. Caspers</i>	RF Engineering lecture <i>F. Caspers</i>
		Coffee Break	Coffee Break	Coffee Break	RF Engineering tutorial <i>F. Caspers / M. Wendt</i>
		Introduction to RF lecture <i>A. Mostacci</i>	Vacuum systems lecture <i>V. Baglin</i>	Vacuum systems lecture <i>V. Baglin</i>	
		Vacuum systems lecture <i>V. Baglin</i>	Vacuum systems tutorial <i>V. Baglin / R. Kersevan</i>	Vacuum systems tutorial <i>V. Baglin / R. Kersevan</i>	Bus leaves at 11:30 from JUAS <i>(Lunch at CERN, R2, offered by ESI)</i>
	12:00 OFFICIAL OPENING (welcome & building visit)				
	13:00 WELCOME LUNCH	BREAK	BREAK	BREAK	
	14:00 Presentation of JUAS & Presentation of students <i>P. Lebrun</i>	Vacuum systems lecture <i>V. Baglin</i>	RF Engineering lecture <i>F. Caspers</i>	RF Engineering lecture <i>F. Caspers</i>	
	Introduction to CERN practical days <i>Magnet, Superconductivity</i>	RF Engineering lecture <i>F. Caspers</i>	RF Engineering tutorial <i>F. Caspers / M. Wendt</i>	RF Engineering tutorial <i>F. Caspers / M. Wendt</i>	VISIT AT CERN AD / ELENA LINAC / LEIR
	Coffee Break	Coffee Break	Coffee Break	Coffee Break	
	Introduction to CERN practical days <i>RF, Vacuum, CLEAR</i>	RF Engineering lecture <i>F. Caspers</i>	Accelerator driven system Seminar <i>J-L. Biarrotte</i>	RF Engineering lecture <i>F. Caspers</i>	
17:45	CHECK-IN AT THE RESIDENCE & SHOPPING FOR GROCERIES				Bus leaves at 18:00 from CERN
18:15					



Maxwell equations in vacuum

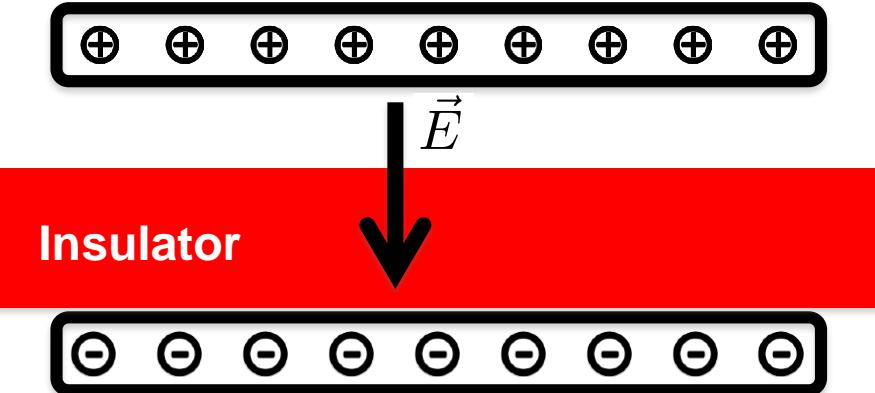
$\nabla \cdot \vec{E} = \rho/\epsilon_0$	\vec{E}	Electric Field	(V/m)	fields
$\nabla \cdot \vec{B} = 0$	\vec{B}	Magnetic Flux Density	(Wb/m^2)	
$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	ρ	Electric Charge Density	(C/m^3)	sources
$\nabla \times \vec{B} = \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} + \mu_0 \vec{J}$	\vec{J}	Electric Current Density	(A/m^2)	
$\mu_0 = 4\pi \cdot 10^{-7} \text{ (H/m)}$	$\epsilon_0 = 1/c^2 \mu_0 = 8.8542 \cdot 10^{-12} \text{ (F/m)}$	$c = 1/\sqrt{\mu_0 \epsilon_0} = 299792458 \text{ (m/s)}$		
Magnetic constant (permeability of free space)	Electric constant (permittivity of free space)			Speed of light
Divergence operator				Curl operator
$\nabla \cdot \vec{A} = \dots$			$\nabla \times \vec{A} = \vec{C}$	
				
The source of \vec{A} is ...				\vec{A} is chained to \vec{C}

Maxwell equations logo

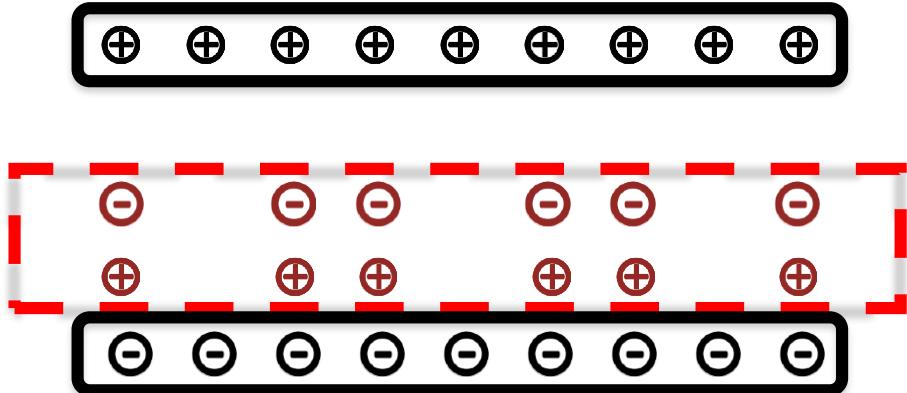


Maxwell equations in matter: the physical approach

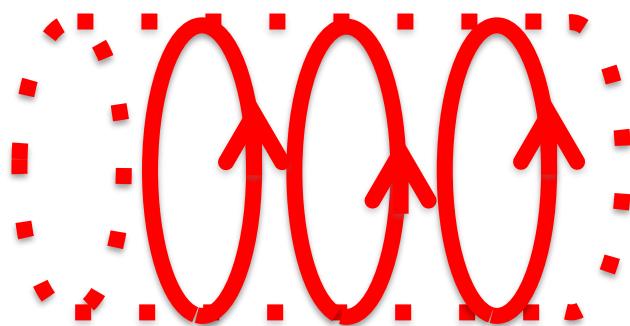
The reality ...



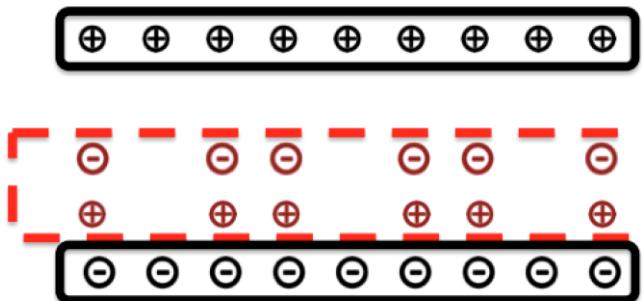
... the model



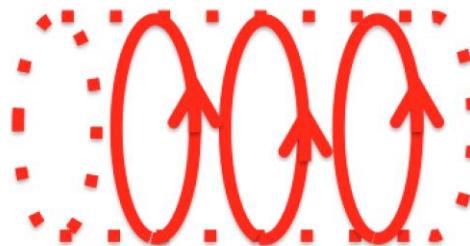
charges and currents IN VACUUM



Maxwell equations in matter: the mathematics



Electric insulators (dielectric)



Magnetic materials
(ferrite, superconductor)

Polarization charges

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}$$

Constitutive relations

$$\vec{H} = \frac{\vec{B}}{\mu_0} - \vec{M}$$

\vec{D} Electric Flux Density (C/m^2)

\vec{H} Magnetic Field (A/m)

\vec{P} Electric Polarization (C/m^2)

\vec{M} Magnetization (A/m)

Equivalence Principles in Electromagnetics Theory

Maxwell equations: general expression

$$\nabla \cdot \vec{D} = \rho$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} + \vec{J}$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

fields

\vec{E} Electric Field (V/m)

\vec{H} Magnetic Field (A/m)

\vec{B} Magnetic Flux Density (Wb/m^2)

\vec{D} Electric Flux Density (C/m^2)

sources

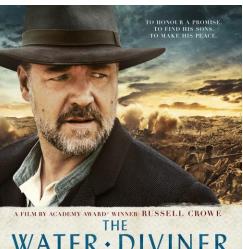
ρ Electric Charge Density (C/m^3)

\vec{J} Electric Current Density (A/m^2)

$$\vec{H} = \frac{\vec{B}}{\mu_0}$$

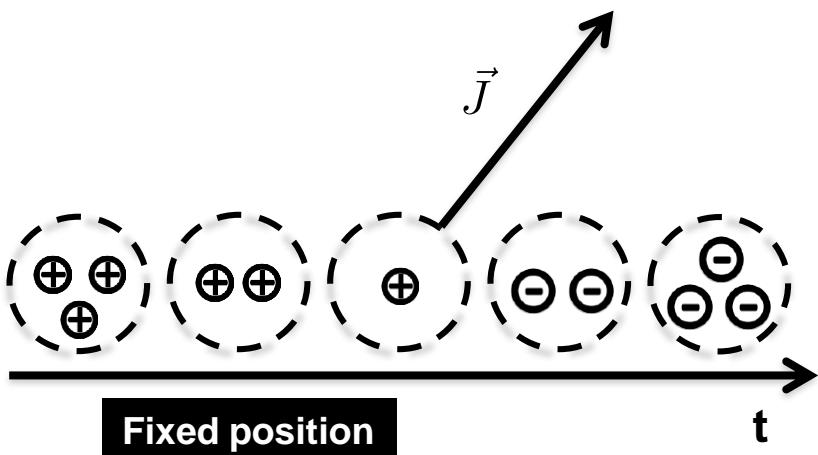
in vacuum

Continuity equation is included



$$\nabla \cdot \vec{J} = -\frac{\partial \rho}{\partial t}$$

At a given position, the source of \vec{J} is the decrease of charge in time



Fixed position

Maxwell equations: the static limit

$$\frac{\partial}{\partial t} = 0$$

$$\nabla \cdot \vec{J} = -\frac{\partial \rho}{\partial t} = 0$$

Ohm Law

Kirchhoff Laws

Lumped elements
(electric networks)

$$\frac{\partial}{\partial t} \approx 0$$

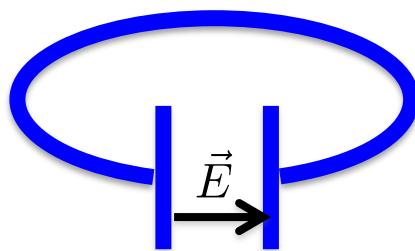
The **lumped elements model** for electric networks is used also when the field variation is negligible over the size of the network.

$$\frac{\partial}{\partial t} = 0$$

$$\nabla \times \vec{E} = 0$$

The E field is conservative.

The energy gain of a charge in closed circuit is zero.



No static, circular accelerators (RF instead!).

Electrostatics

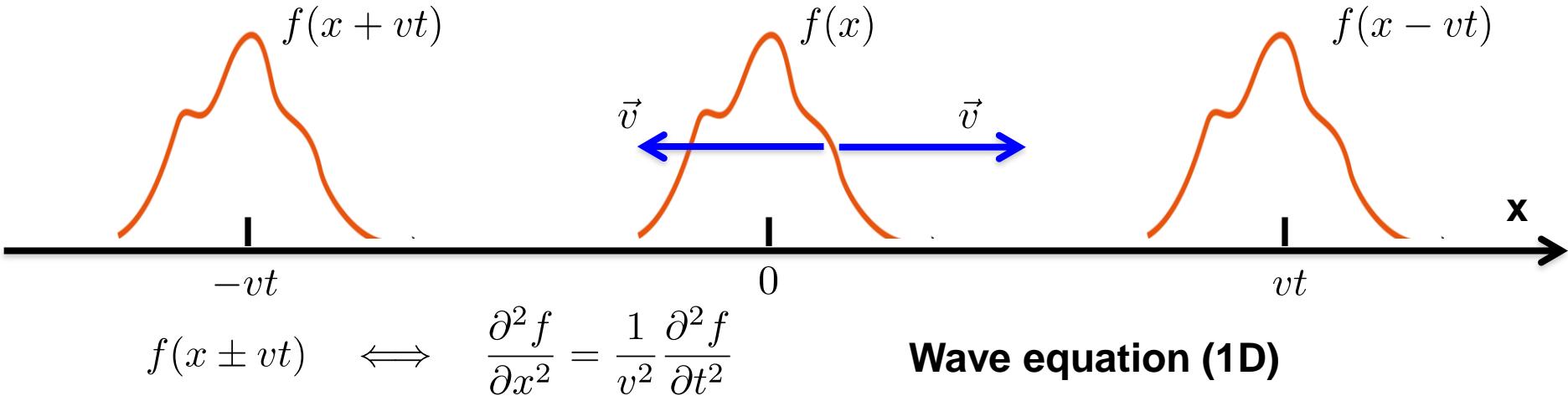
$$\nabla \times \vec{E} = 0 \rightarrow \vec{E} = -\nabla V$$

$$\xrightarrow{\text{free space}} \nabla \cdot \vec{E} = 0$$

$$\nabla^2 V = 0$$

Laplace
equation

Solution of Maxwell Equations: the EM waves



Maxwell Equations: free space, no sources

$$\left. \begin{array}{l} \nabla \cdot \vec{E} = 0 \\ \nabla \times \vec{E} = -\mu_0 \frac{\partial \vec{H}}{\partial t} \\ \nabla \times \vec{H} = \epsilon_0 \frac{\partial \vec{E}}{\partial t} \\ \nabla^2 \vec{E} = \mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2} \\ \nabla^2 \vec{H} = \mu_0 \epsilon_0 \frac{\partial^2 \vec{H}}{\partial t^2} \end{array} \right\}$$

$$\begin{aligned} \nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E} &= -\nabla^2 \vec{E} \\ \nabla \times \nabla \times \vec{E} &\parallel \\ -\mu_0 \frac{\partial}{\partial t} (\nabla \times \vec{H}) &= -\mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2} \end{aligned}$$

$$\frac{1}{v^2} = \mu_0 \epsilon_0 \implies v = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = c$$

Wave equation (3D)

Harmonic time dependence and phasors

Assuming sinusoidal electric field (Fourier)

Time dependence $\longrightarrow e^{j\omega t} = e^{j2\pi f t} \longrightarrow \frac{\partial}{\partial t} \dots = j\omega \dots$

$$\vec{E}(\vec{r}, t) = \text{Re} \left\{ \vec{E}(\vec{r}, \omega) e^{j\omega t} \right\}$$

Phasors are complex vectors

Power/Energy depend on **time average** of quadratic quantities

$$\left| \vec{E}(\vec{r}, t) \right|_{\text{average}}^2 = \frac{1}{T} \int_0^T \vec{E}(\vec{r}, t) \cdot \vec{E}(\vec{r}, t) dt = \dots = \frac{1}{2} \vec{E}(\vec{r}, \omega) \cdot \vec{E}^*(\vec{r}, \omega) = \left| \vec{E}_{\text{RMS}}(\vec{r}, \omega) \right|^2$$

↑
 $\left| \vec{E}_{\text{RMS}} \right| = \left| \vec{E} \right| / \sqrt{2}$

In the following we will use the same symbol for

Real vectors

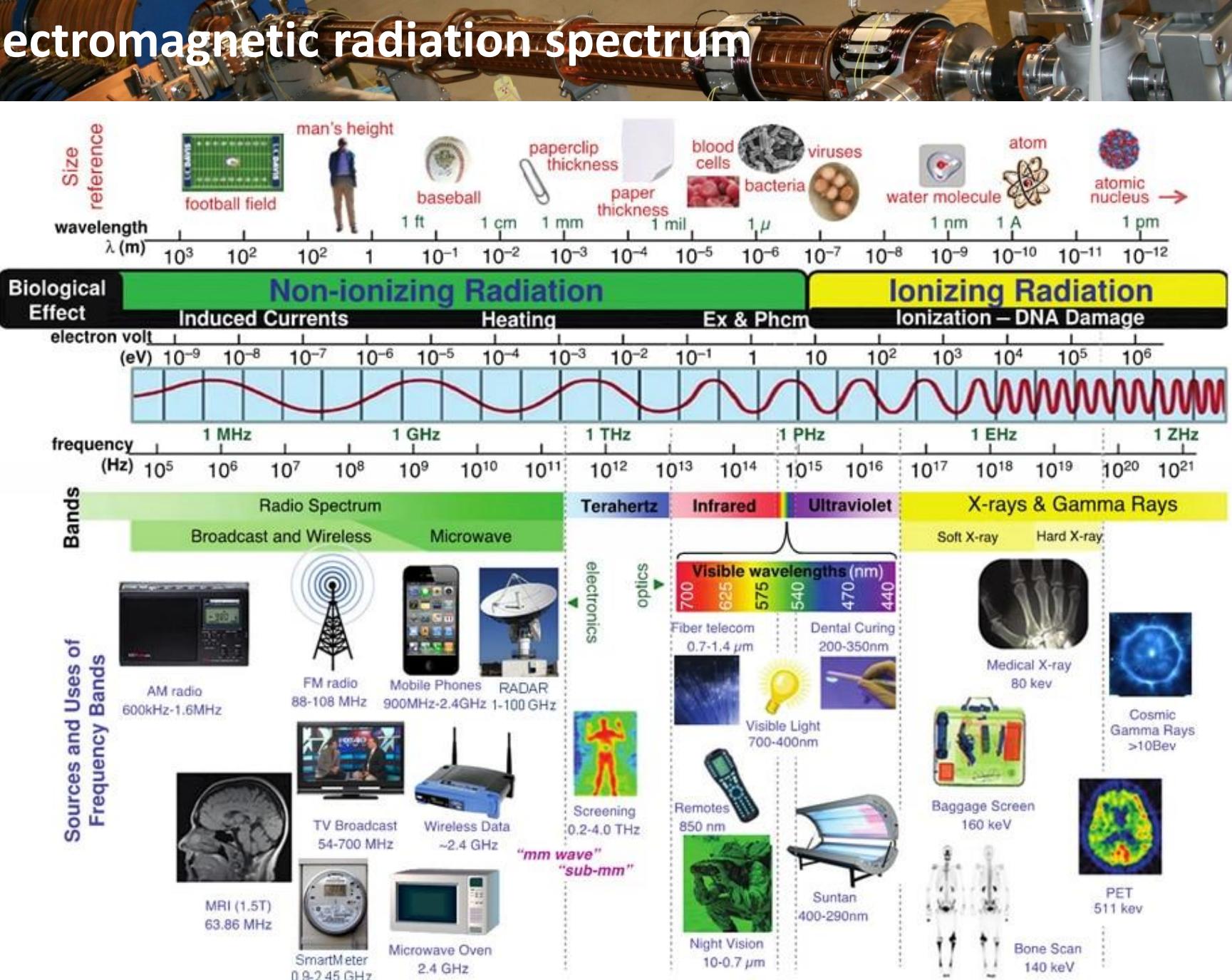
$$\vec{E}(\vec{r}, t), \vec{H}(\vec{r}, t), \dots$$

Complex vectors

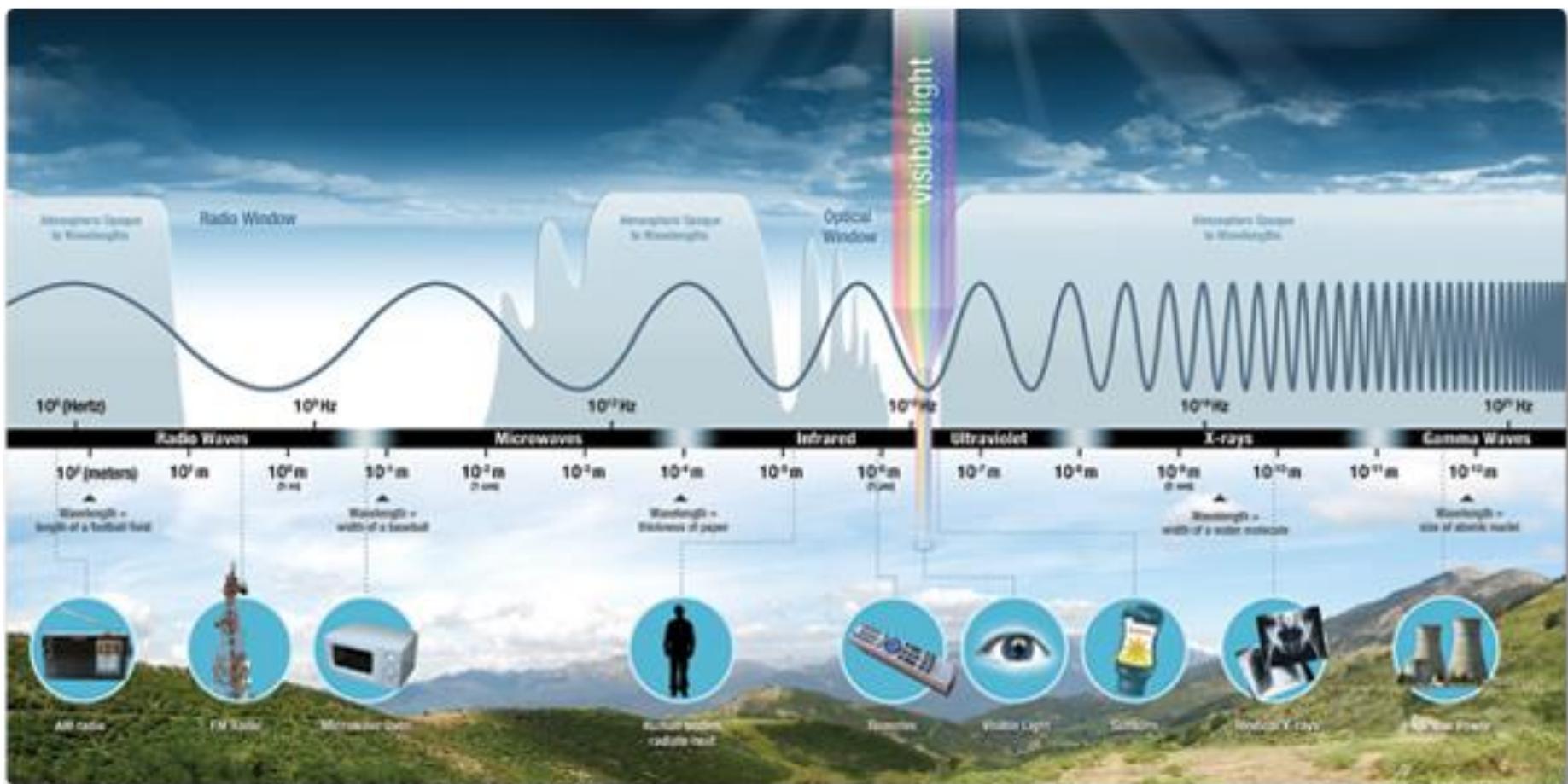
$$\vec{E}(\vec{r}, \omega), \vec{H}(\vec{r}, \omega), \dots$$

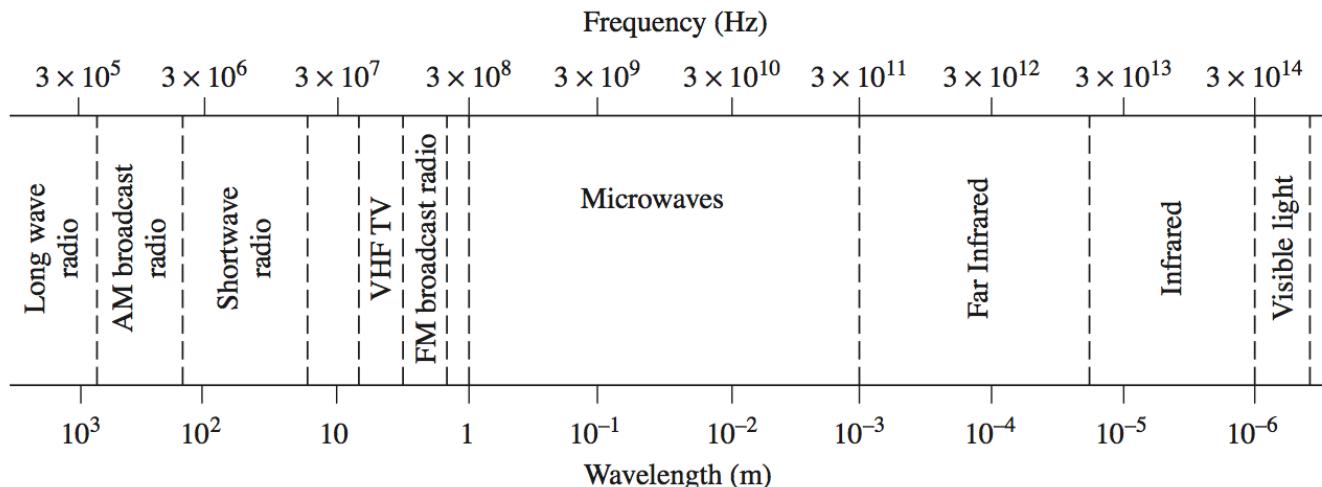
Note that, with phasors, a time animation is identical to phase rotation.

Electromagnetic radiation spectrum



Electromagnetic radiation spectrum: users point of view





Typical Frequencies

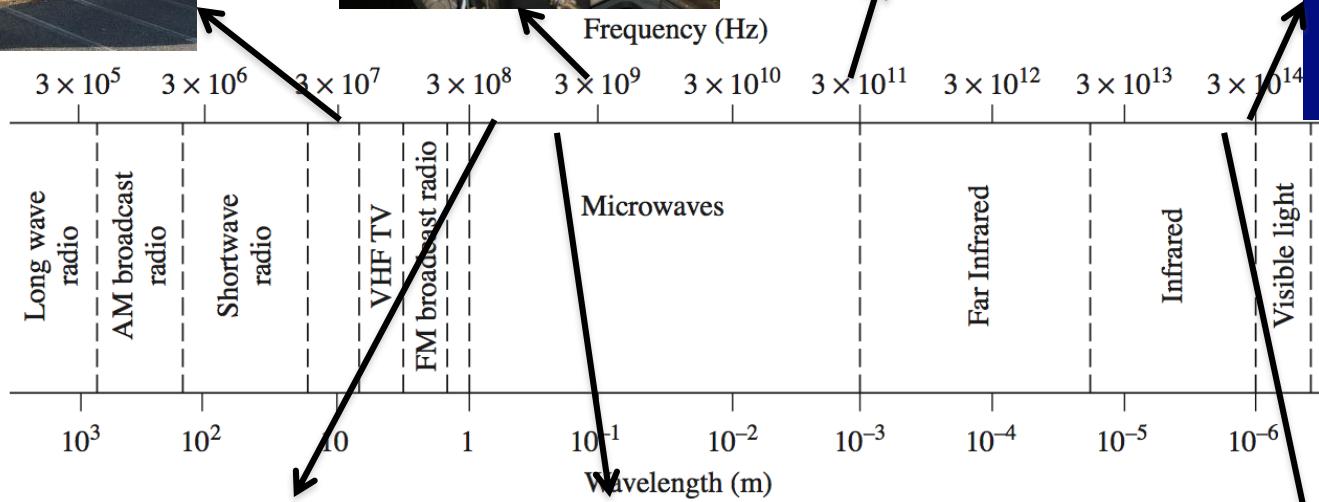
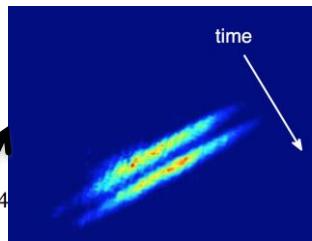
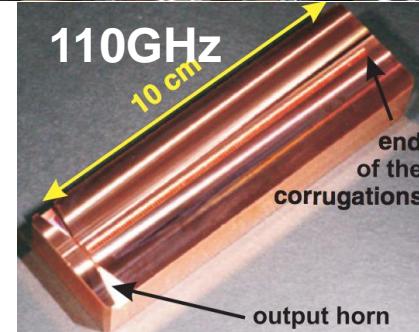
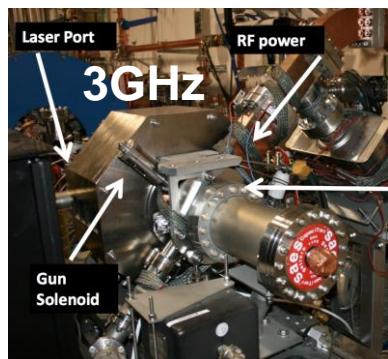
AM broadcast band	535–1605 kHz
Short wave radio band	3–30 MHz
FM broadcast band	88–108 MHz
VHF TV (2–4)	54–72 MHz
VHF TV (5–6)	76–88 MHz
UHF TV (7–13)	174–216 MHz
UHF TV (14–83)	470–890 MHz
US cellular telephone	824–849 MHz 869–894 MHz
European GSM cellular	880–915 MHz 925–960 MHz
GPS	1575.42 MHz 1227.60 MHz
Microwave ovens	2.45 GHz
US DBS	11.7–12.5 GHz
US ISM bands	902–928 MHz 2.400–2.484 GHz 5.725–5.850 GHz
US UWB radio	3.1–10.6 GHz

Approximate Band Designations

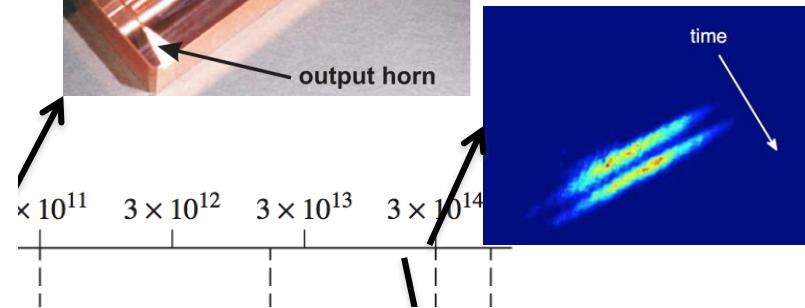
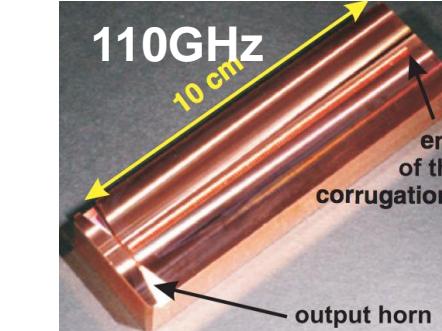
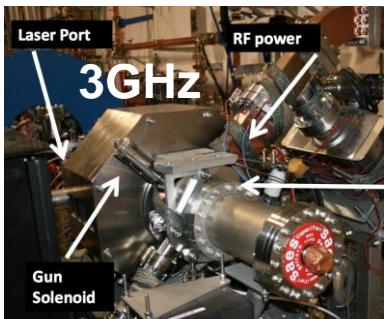
Medium frequency	300 kHz–3 MHz
High frequency (HF)	3 MHz–30 MHz
Very high frequency (VHF)	30 MHz–300 MHz
Ultra high frequency (UHF)	300 MHz–3 GHz
L band	1–2 GHz
S band	2–4 GHz
C band	4–8 GHz
X band	8–12 GHz
Ku band	12–18 GHz
K band	18–26 GHz
Ka band	26–40 GHz
U band	40–60 GHz
V band	50–75 GHz
E band	60–90 GHz
W band	75–110 GHz
F band	90–140 GHz

]

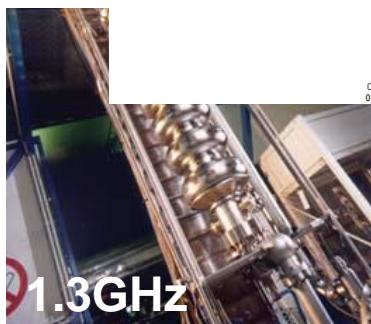
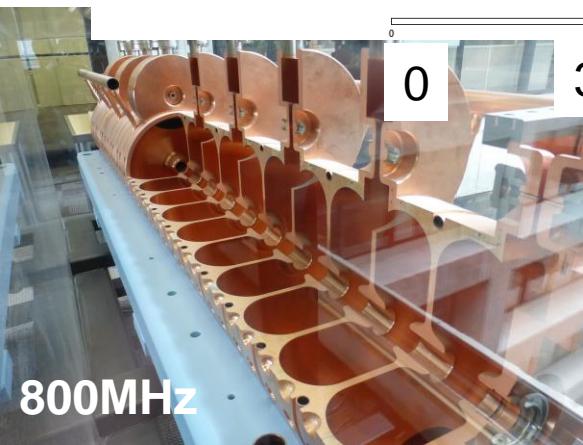
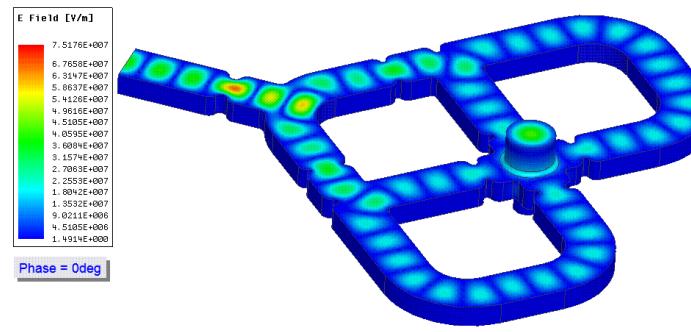
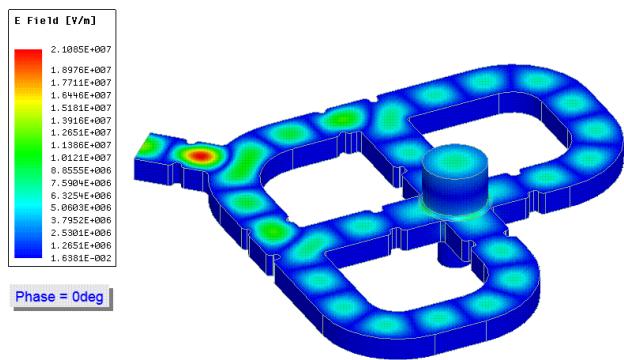
The RF spectrum and particle accelerators



The RF spectrum and particle accelerators

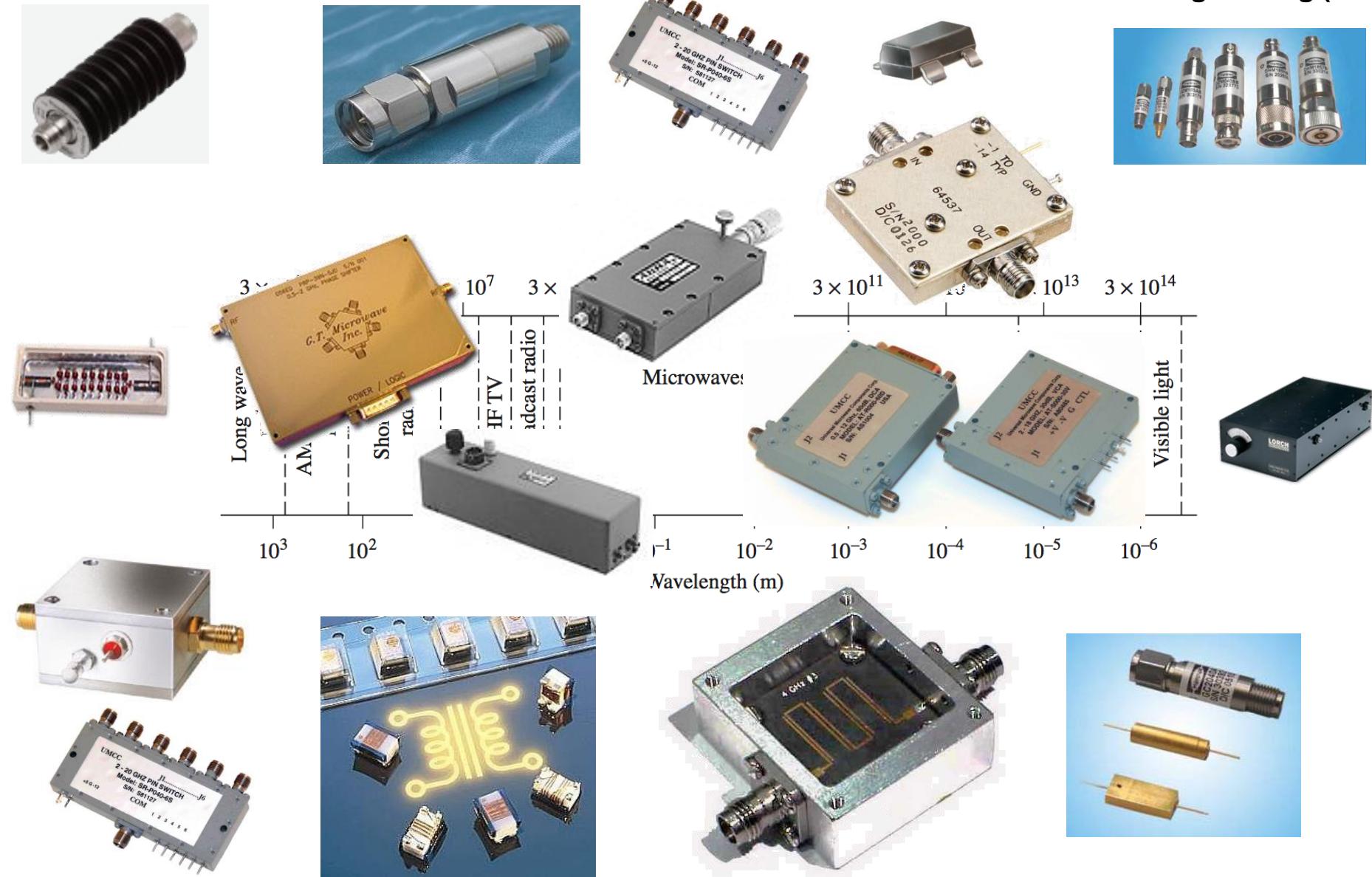


Animations by G. Castorina



The RF spectrum and particle accelerators

A. Gallo Lecture @ CAS RF engineering (2010)



Harmonic fields in media: constitutive relations

Hyp: Linear, Homogeneous, Isotropic and non Dispersive media

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}$$

$$\vec{D} = \epsilon_c \vec{E}$$

$$\epsilon_c = \epsilon' - j\epsilon''$$

complex permittivity



Losses (heat) due to damping of vibrating dipoles

$$\vec{H} = \frac{\vec{B}}{\mu_0} - \vec{M}$$

$$\vec{B} = \mu \vec{H}$$

$$\mu = \mu' - j\mu''$$

complex permeability

Ohm Law

$$\vec{J}_c = \sigma \vec{E}$$

σ **conductivity** (S/m)

Losses (heat) due to moving charges colliding with lattice

Material	Conductivity S/m (20°C)	Material	Conductivity S/m (20°C)
Aluminum	3.816×10^7	Nichrome	1.0×10^6
Brass	2.564×10^7	Nickel	1.449×10^7
Bronze	1.00×10^7	Platinum	9.52×10^6
Chromium	3.846×10^7	Sea water	3–5
Copper	5.813×10^7	Silicon	4.4×10^{-4}
Distilled water	2×10^{-4}	Silver	6.173×10^7
Germanium	2.2×10^6	Steel (silicon)	2×10^6
Gold	4.098×10^7	Steel (stainless)	1.1×10^6
Graphite	7.0×10^4	Solder	7.0×10^6
Iron	1.03×10^7	Tungsten	1.825×10^7
Mercury	1.04×10^6	Zinc	1.67×10^7
Lead	4.56×10^6		

Harmonic fields in media: Maxwell Equations

Hyp: Linear, Homogeneous, Isotropic and non Dispersive media

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P} \quad \vec{D} = \epsilon_c \vec{E} \quad \epsilon_c = \epsilon' - j\epsilon'' \quad \text{complex permittivity}$$

Losses (heat) due to damping of vibrating dipoles

$$\vec{H} = \frac{\vec{B}}{\mu_0} - \vec{M} \quad \vec{B} = \mu \vec{H} \quad \mu = \mu' - j\mu'' \quad \text{complex permeability}$$

Ohm Law

$$\vec{J}_c = \sigma \vec{E} \quad \sigma \quad \text{conductivity} \quad (S/m)$$

Losses (heat) due to moving charges colliding with lattice

$$\nabla \cdot \vec{D} = \rho \quad \nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -j\omega \mu \vec{H}$$

$$\nabla \times \vec{H} = j\omega \vec{D} + \vec{J}_c + \vec{J} = \dots = j\omega \epsilon \vec{E} + \vec{J} \quad \epsilon = \epsilon' - j\epsilon'' - j\frac{\sigma}{\omega}$$

$$\tan \delta = \frac{\omega \epsilon'' + \sigma}{\omega \epsilon'} = \frac{\text{Losses}}{\text{Displacement current}}$$

$$\epsilon' = \epsilon_r \epsilon_0$$

Loss tangent

$$\epsilon = \epsilon_r \epsilon_0 (1 - j \tan \delta)$$

Dielectric constant

Harmonic fields in media: Maxwell Equations

DIELECTRIC CONSTANTS AND LOSS TANGENTS FOR SOME MATERIALS

Material	Frequency	ϵ_r	$\tan \delta$ (25°C)
Alumina (99.5%)	10 GHz	9.5–10.	0.0003
Barium tetratitanate	6 GHz	$37 \pm 5\%$	0.0005
Beeswax	10 GHz	2.35	0.005
Beryllia	10 GHz	6.4	0.0003
Ceramic (A-35)	3 GHz	5.60	0.0041
Fused quartz	10 GHz	3.78	0.0001
Gallium arsenide	10 GHz	13.0	0.006
Glass (pyrex)	3 GHz	4.82	0.0054
Glazed ceramic	10 GHz	7.2	0.008
Lucite	10 GHz	2.56	0.005
Nylon (610)	3 GHz	2.84	0.012
Parafin	10 GHz	2.24	0.0002
Plexiglass	3 GHz	2.60	0.0057
Polyethylene	10 GHz	2.25	0.0004
Polystyrene	10 GHz	2.54	0.00033
Porcelain (dry process)	100 MHz	5.04	0.0078
Rexolite (1422)	3 GHz	2.54	0.00048
Silicon	10 GHz	11.9	0.004
Styrofoam (103.7)	3 GHz	1.03	0.0001
Teflon	10 GHz	2.08	0.0004
Titania (D-100)	6 GHz	$96 \pm 5\%$	0.001
Vaseline	10 GHz	2.16	0.001
Water (distilled)	3 GHz	76.7	0.157

1 Dispersive media

" complex permittivity

" complex permeability

Activity (S/m)

Losses (heat) due to moving charges colliding with lattice

$$\vec{E} + \vec{J}$$

$$\epsilon = \epsilon' - j\epsilon'' - j\frac{\sigma}{\omega}$$

Loss tangent

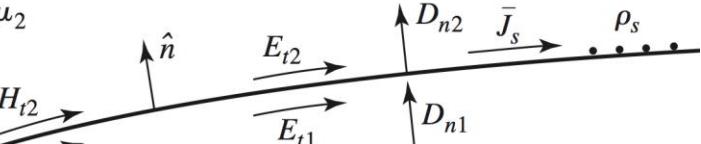
$$\epsilon = \epsilon_r \epsilon_0 (1 - j \tan \delta)$$

Dielectric constant

Boundary Conditions



Medium 2: ϵ_2, μ_2



Medium 1: ϵ_1, μ_1

Surface Charge Density

(C/m^2)

Surface Current Density

(A/m)

$$\hat{n} \cdot (\vec{D}_2 - \vec{D}_1) = \rho_s$$

$$\hat{n} \cdot (\vec{B}_2 - \vec{B}_1) = 0$$

$$\hat{n} \times (\vec{E}_2 - \vec{E}_1) = 0$$

$$\hat{n} \times (\vec{H}_2 - \vec{H}_1) = \vec{J}_s$$

Fields at a lossless dielectric interface

$$\rho_s = 0$$

$$\hat{n} \cdot \vec{D}_1 = \hat{n} \cdot \vec{D}_2$$

$$\hat{n} \cdot \vec{B}_1 = \hat{n} \cdot \vec{B}_2$$

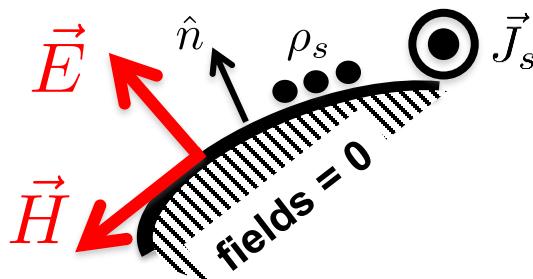
$$\vec{J}_s = 0$$

$$\hat{n} \times \vec{E}_1 = \hat{n} \times \vec{E}_2$$

$$\hat{n} \times \vec{H}_1 = \hat{n} \times \vec{H}_2$$

Perfect conductor (electric wall)

$$\sigma \rightarrow \infty$$



$$\hat{n} \cdot \vec{D} = \rho_s$$

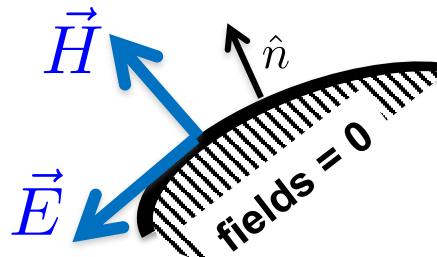
$$\hat{n} \cdot \vec{B} = 0$$

$$\hat{n} \times \vec{E} = 0$$

$$\hat{n} \times \vec{H} = \vec{J}_s$$

Magnetic Wall (dual of the E-wall)

approx.



$$\hat{n} \cdot \vec{D} = 0$$

$$\hat{n} \cdot \vec{B} = 0$$

$$\hat{n} \times \vec{H} = 0$$

$$\hat{n} \times \vec{E} \neq 0$$

Helmotz equation and its simplest solution

$$\nabla^2 \vec{E} = \mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2}$$

$$e^{j\omega t} \rightarrow \frac{\partial^2}{\partial t^2} \dots = -\omega^2 \dots$$

Helmotz equation

$$\nabla^2 \vec{E} + \omega^2 \mu \epsilon \vec{E} = 0$$

$$\nabla^2 \vec{H} + \omega^2 \mu \epsilon \vec{H} = 0$$

$$k = \omega \sqrt{\mu \epsilon} \quad (1/m)$$

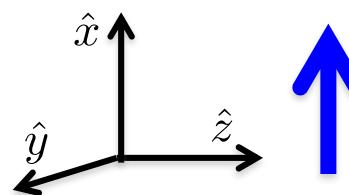
Propagation/phase constant

Wave number

The simples solution: the plane wave

$$\frac{\partial}{\partial x} = \frac{\partial}{\partial y} = 0$$

$$\frac{d^2 E_x}{dz^2} + k^2 E_x = 0$$



$$\vec{E} = E_x \hat{x}$$

Uniform in x, y

Lossless medium

$$E_x(z) = E^+ e^{-jkz} + E^- e^{jkz}$$

$$E_x(z, t) = \operatorname{Re} \{ E(x, \omega) e^{j\omega t} \} = E^+ \cos(\omega t - kz) + E^- \cos(\omega t + kz)$$

It is a wave, moving in the +z direction or -z direction

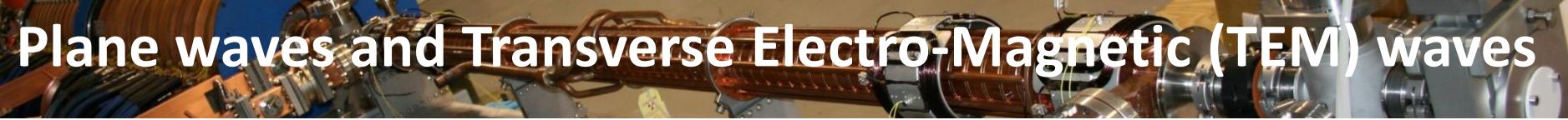
Phase velocity

Velocity at which a fixed phase point on the wave travels

$$\omega t \mp kz = \text{const}$$

$$v_p = \frac{dz}{dt} = \frac{d}{dt} \left(\frac{\omega t \mp \text{const}}{k} \right) = \frac{\omega}{k} = \frac{1}{\sqrt{\mu \epsilon}}$$

Speed of light



Plane waves and Transverse Electro-Magnetic (TEM) waves

Wave length **Distance between two consecutive maxima (or minima or ...)**

$$(\omega t - kz) - [\omega t - k(z + \lambda)] = 2\pi$$
$$\lambda = \frac{2\pi}{k} = \frac{2\pi v_p}{\omega} = \frac{v_p}{f}$$

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

Compute H ...

$$E_x(z) = E^+ e^{-jkz} + E^- e^{jkz}$$

Plane waves and Transverse Electro-Magnetic (TEM) waves

Wave length **Distance between two consecutive maxima (or minima or ...)**

$$(\omega t - kz) - [\omega t - k(z + \lambda)] = 2\pi$$

$$\lambda = \frac{2\pi}{k} = \frac{2\pi v_p}{\omega} = \frac{v_p}{f}$$

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$H_x = H_z = 0$$

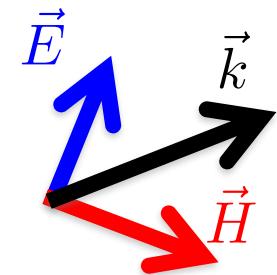
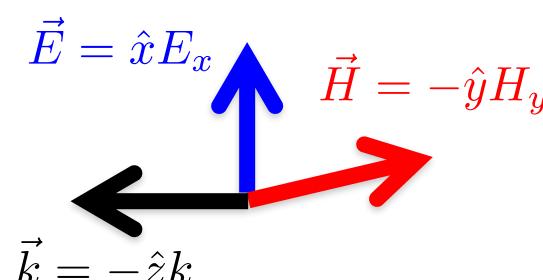
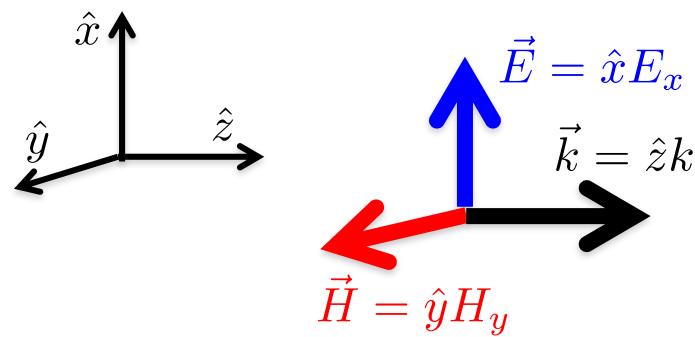
$$H_y = \frac{j}{\omega\mu} \frac{\partial E_x}{\partial z} = \frac{1}{\eta} (E^+ e^{-jkz} - E^- e^{jkz})$$

$$\eta = \frac{\omega\mu}{k} = \sqrt{\frac{\mu}{\epsilon}}$$

Intrinsic impedance of the medium (Ω)

$$\eta_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377 \Omega$$

The ratio of E and H component is an impedance called **wave impedance**



$$\vec{H} = \frac{1}{\eta} \hat{k} \times \vec{E}$$

TEM wave

E and H field are transverse to the direction of propagation.

$$Z_{TEM} = \eta$$

Plane wave in lossy media

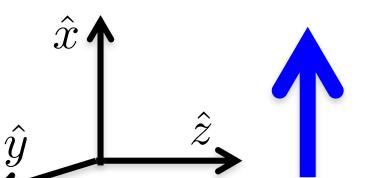
$$\nabla^2 \vec{E} + \omega^2 \mu \epsilon \vec{E} = 0$$

$$\epsilon = \epsilon_r \epsilon_0 (1 - j \tan \delta)$$

$$\tan \delta = \frac{\omega \epsilon'' + \sigma}{\omega \epsilon'}$$

Definition: $\gamma = \alpha + j\beta = j\omega\sqrt{\mu\epsilon} = j\omega\sqrt{\mu\epsilon_0\epsilon_r(1 - j \tan \delta)}$

Attenuation constant Phase constant



\hat{x} \hat{y} \hat{z}

$\vec{E} = E_x \hat{x}$
Uniform in x, y

$\frac{d^2 E_x}{dz^2} - \gamma^2 E_x = 0$

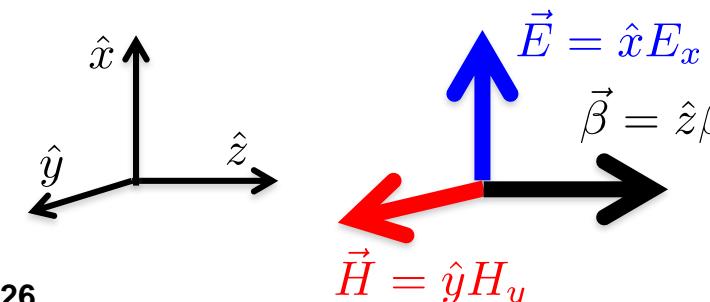
$E_x(z) = E^+ e^{-\gamma z} + E^- e^{\gamma z}$

$e^{-\gamma z} = e^{-\alpha z} e^{-j\beta z}$ — time — $e^{-\alpha z} \cos(\omega t - \beta z)$

$v_p = \frac{\omega}{\beta}$ $\lambda = \frac{2\pi}{\beta}$

$$H_y = \frac{j}{\omega \mu} \frac{\partial E_x}{\partial z} = -\frac{j\gamma}{\omega \mu} (E^+ e^{-\gamma z} - E^- e^{\gamma z}) = \frac{1}{\eta} (E^+ e^{-\gamma z} - E^- e^{\gamma z})$$

$\eta = \frac{j\omega \mu}{\gamma} \rightarrow \sqrt{\frac{\mu}{\epsilon}}$



\hat{x} \hat{y} \hat{z}

$\vec{E} = \hat{x} E_x$

$\vec{H} = \hat{y} H_y$

$\vec{\beta} = \hat{z} \beta$

$Z_{TEM} = \eta$ complex

$\vec{H} = \frac{1}{\eta} \hat{\beta} \times \vec{E}$

Attenuating TEM “wave” ...

Plane waves in good conductors

Good conductor

Conduction current >> displacement current

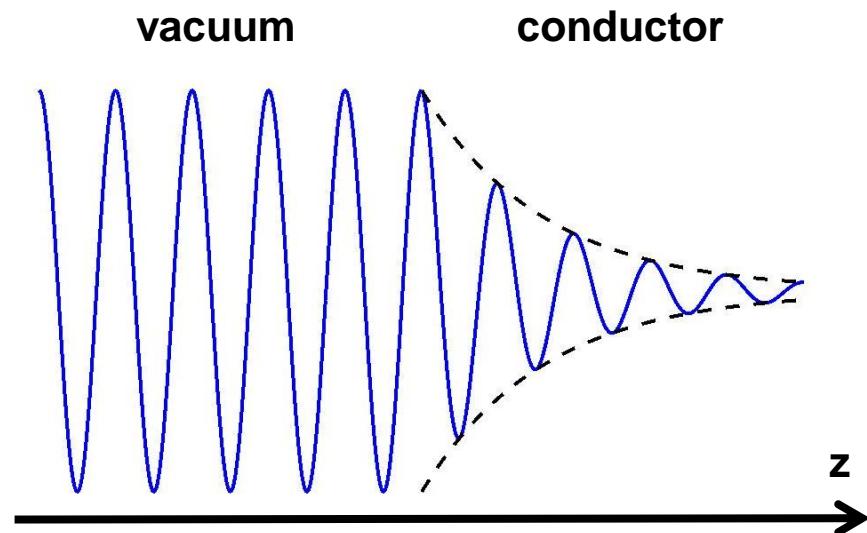
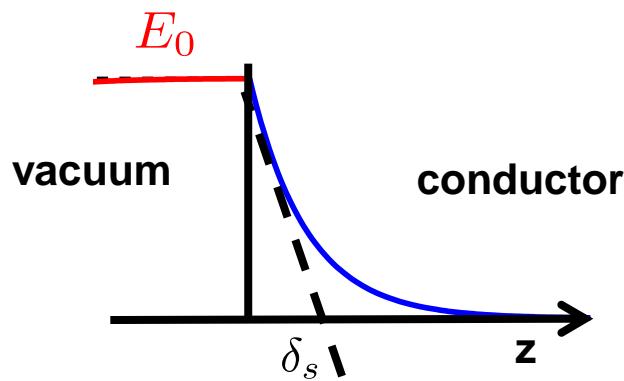
$$\sigma E \gg \omega \epsilon_c E$$

$$\tan \delta = \frac{\omega \epsilon'' + \sigma}{\omega \epsilon'} \approx \frac{\sigma}{\omega \epsilon_0 \epsilon_r}$$

$$\gamma = \alpha + j\beta = j\omega\sqrt{\mu\epsilon} \simeq (1+j)\sqrt{\frac{\omega\mu\sigma}{2}}$$

Characteristic depth of penetration: skin depth

$$\delta_s = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega\mu\sigma}}$$



Plane waves in good conductors



Good conductor

Conduction current >> displacement current

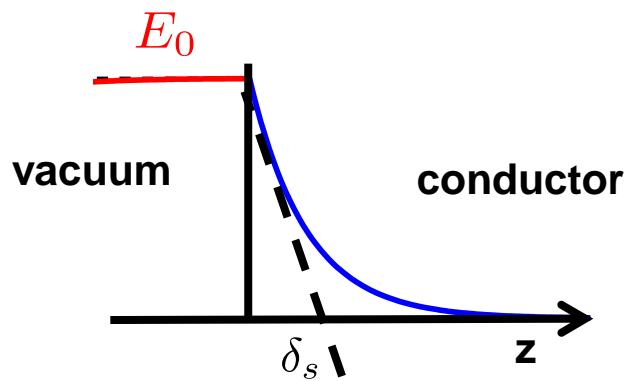
$$\sigma E \gg \omega \epsilon_c E$$

$$\tan \delta = \frac{\omega \epsilon'' + \sigma}{\omega \epsilon'} \approx \frac{\sigma}{\omega \epsilon_0 \epsilon_r}$$

$$\gamma = \alpha + j\beta = j\omega\sqrt{\mu\epsilon} \simeq (1+j)\sqrt{\frac{\omega\mu\sigma}{2}}$$

Characteristic depth of penetration: skin depth

$$\delta_s = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega\mu\sigma}}$$



Al $\delta_s = 8.14 \cdot 10^{-7} \text{ m}$

Cu $\delta_s = 6.60 \cdot 10^{-7} \text{ m}$

Au $\delta_s = 7.86 \cdot 10^{-7} \text{ m}$

Ag $\delta_s = 6.40 \cdot 10^{-7} \text{ m}$

@ 10 GHz

impedance of
the medium

$$\eta = \frac{j\omega\mu}{\gamma} \simeq (1+j)\sqrt{\frac{\omega\mu}{2\sigma}} = (1+j)\frac{1}{\sigma\delta_s}$$

? Copper @ 100 MHz



Maxwell equations and boundary value problem

Maxwell equation with sources + boundary conditions = boundary value problem

Homogeneous medium

$$\nabla \cdot \vec{E} = \rho/\epsilon$$

$$\nabla \cdot \vec{H} = 0$$

Sources

$$\vec{J}, \rho$$

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\nabla \times \vec{H} = +j\omega\epsilon\vec{E} + \vec{J}$$

Do you see asymmetries?



Maxwell equations and boundary value problem

Maxwell equation with sources + boundary conditions = boundary value problem

Homogeneous medium

$$\nabla \cdot \vec{E} = \rho/\epsilon$$

$$\nabla \cdot \vec{H} = \rho_m/\mu$$

Sources

$$\vec{J}, \rho$$

Actual or equivalent

$$\nabla \times \vec{E} = -j\omega\mu\vec{H} - \vec{J}_m$$

$$\nabla \times \vec{H} = +j\omega\epsilon\vec{E} + \vec{J}$$

$$\vec{J}_m, \rho_m$$

equivalent

Vector Helmholtz Equation

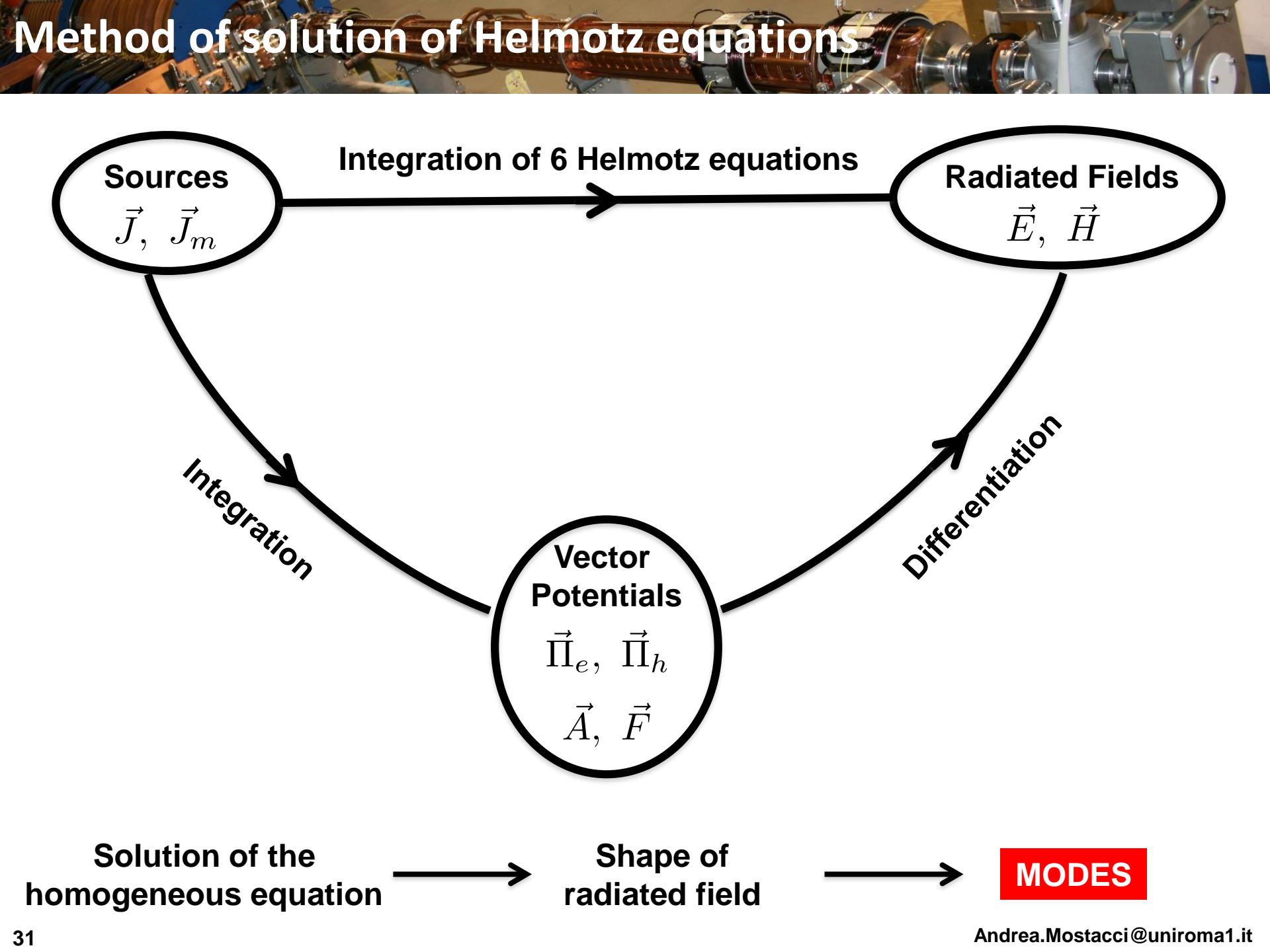
$$\nabla^2 \vec{E} + k^2 \vec{E} = \nabla \times \vec{J}_m + j\omega\mu\vec{J} + \frac{1}{\epsilon} \nabla \rho \quad k^2 = \omega^2 \mu \epsilon$$

$$\nabla^2 \vec{H} + k^2 \vec{H} = -\nabla \times \vec{J} + j\omega\epsilon\vec{J}_m + \frac{1}{\mu} \nabla \rho_m$$

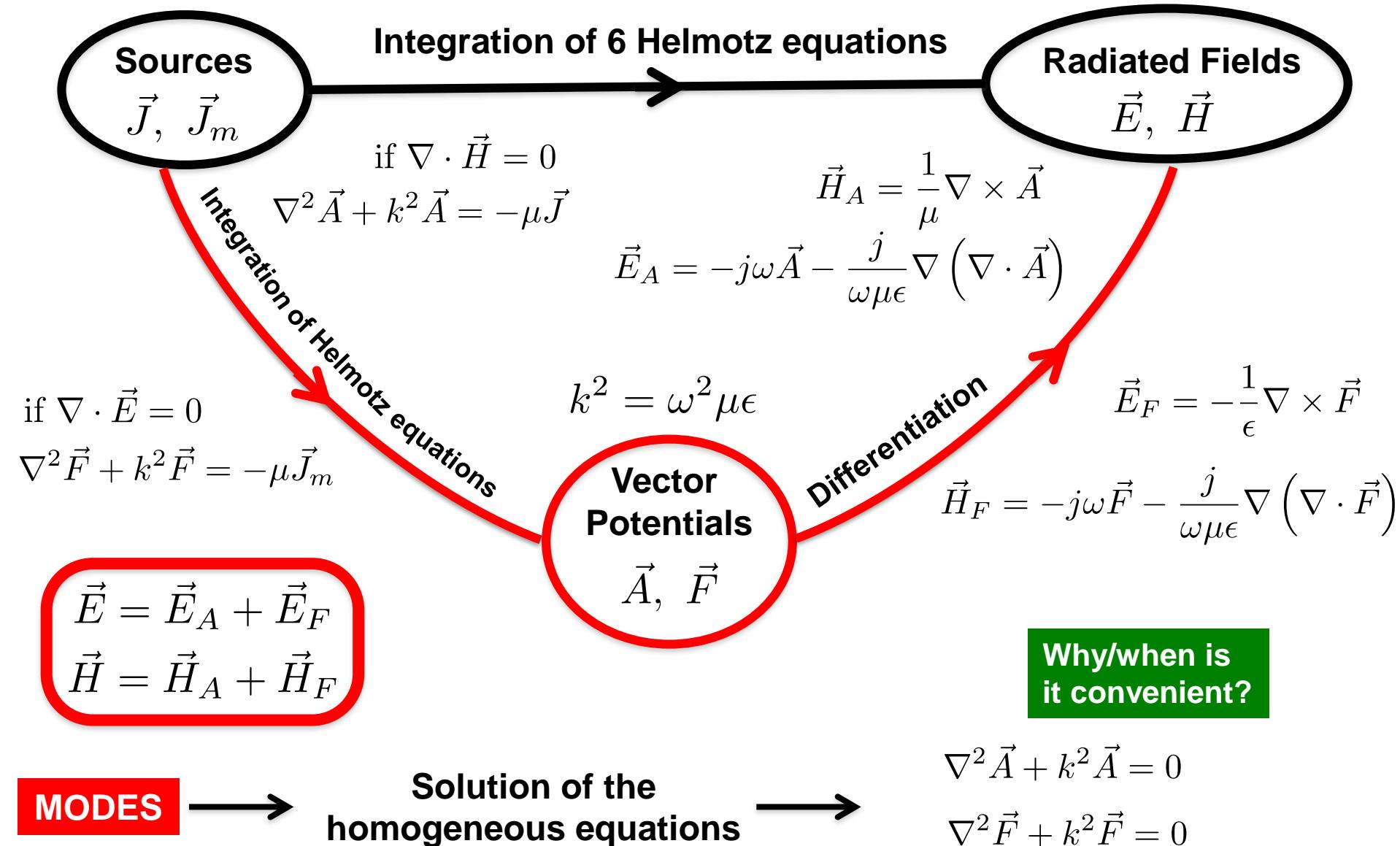
Step 1 Source free region $\vec{J} = \vec{J}_m = \rho_m = \rho = 0$ **Homogeneous problem**

Step 2 Solution $= \sum_k C_k (\vec{J}, \vec{J}_m, \rho_m, \rho)$ Solution-Homogeneous-Problem_k

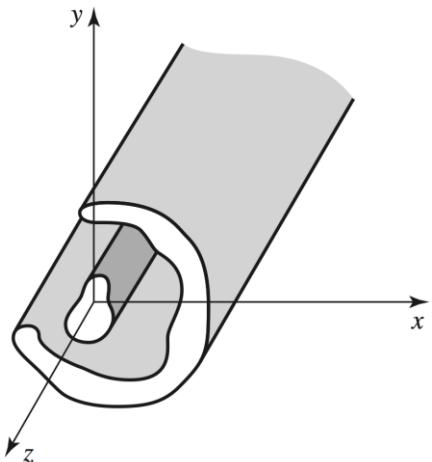
Method of solution of Helmotz equations



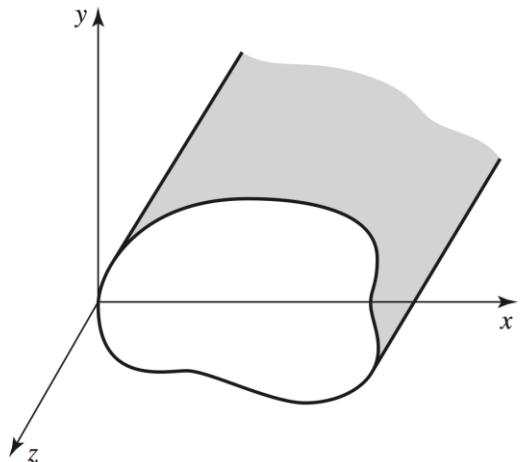
Solution of Helmholtz equations using potentials



Modes of cylindrical waveguides: propagating field



$$\nabla^2 = \nabla_t^2 + \frac{\partial^2}{\partial z^2} \quad \longrightarrow$$



$$\begin{aligned}\nabla_t^2 A_z + (k^2 - \beta^2) A_z &= 0 \\ \nabla_t^2 F_z + (k^2 - \beta^2) F_z &= 0\end{aligned}$$

Field propagating in the positive z direction

$$\vec{A} = \hat{z} \ A_z(x, y) e^{-j\beta z} = \hat{z} \ A$$

$$\vec{F} = \hat{z} \ F_z(x, y) e^{-j\beta z} = \hat{z} \ F$$

**2 Helmotz equations
(transverse coordinates)**

$$\vec{H}_A = \frac{1}{\mu} \nabla \times (\hat{z} A) \quad \longrightarrow \quad \vec{H}_A = \vec{h}_t e^{-j\beta z}$$

$$\vec{E}_A = -j\omega A \hat{z} - \frac{\beta}{\omega \mu \epsilon} \nabla A \quad \longrightarrow \quad \vec{E}_A = [\vec{e}_t + \hat{z} \ \vec{e}_z] e^{-j\beta z}$$

**Only E field along z
E-mode**

Transverse Magnetic (TM)

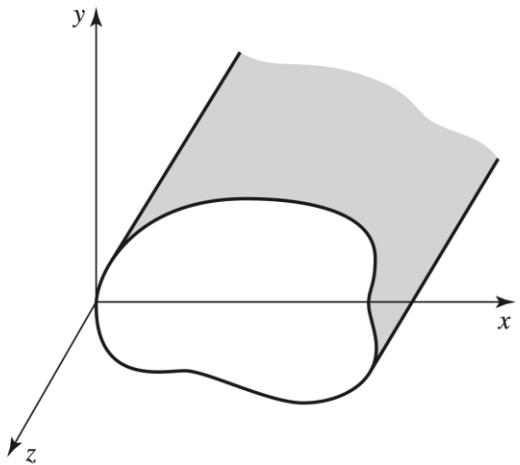
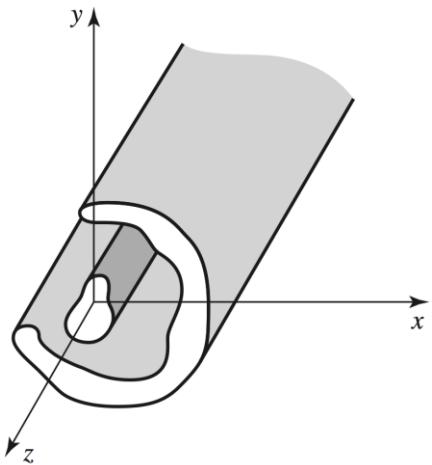
$$\vec{E}_F = -\frac{1}{\epsilon} \nabla \times (\hat{z} F) \quad \longrightarrow \quad \vec{E}_F = \vec{e}_t e^{-j\beta z}$$

$$\vec{H}_F = -j\omega F \hat{z} - \frac{\beta}{\omega \mu \epsilon} \nabla F \quad \longrightarrow \quad \vec{H}_F = [\vec{h}_t + \hat{z} \ \vec{h}_z] e^{-j\beta z}$$

**Only H field along z
H-mode**

Transverse Electric (TE)

Modes of cylindrical waveguides: propagating field



Field propagating in the positive z direction

$$\vec{A} = \hat{z} \ A_z(x, y) e^{-j\beta z} = \hat{z} \ A$$

$$\vec{F} = \hat{z} \ F_z(x, y) e^{-j\beta z} = \hat{z} \ F$$

$$\vec{H}_A = \frac{1}{\mu} \nabla \times (\hat{z} A) \quad \rightarrow \quad \vec{H}_A = \vec{h}_t e^{-j\beta z}$$

$$\vec{E}_A = -j\omega A \hat{z} - \frac{\beta}{\omega \mu \epsilon} \nabla A \quad \rightarrow \quad \vec{E}_A = [\vec{e}_t + \hat{z} \ \textcolor{red}{e}_z] e^{-j\beta z}$$

**Only E field along z
E-mode**

Transverse Magnetic (TM)

$$\vec{E}_F = -\frac{1}{\epsilon} \nabla \times (\hat{z} F) \quad \rightarrow \quad \vec{E}_F = \vec{e}_t e^{-j\beta z}$$

$$\vec{H}_F = -j\omega F \hat{z} - \frac{\beta}{\omega \mu \epsilon} \nabla F \quad \rightarrow \quad \vec{H}_F = [\vec{h}_t + \hat{z} \ \textcolor{red}{h}_z] e^{-j\beta z}$$

**Only H field along z
H-mode**

Transverse Electric (TE)

$$\vec{E} = \vec{E}_A + \vec{E}_F$$

$$\vec{H} = \vec{H}_A + \vec{H}_F$$



**TM
modes**

+

**TE
modes**



Exercise

Look for a Transverse Electric Magnetic mode $E_z = H_z = 0$

$\vec{E}, \vec{H}, v_p?$

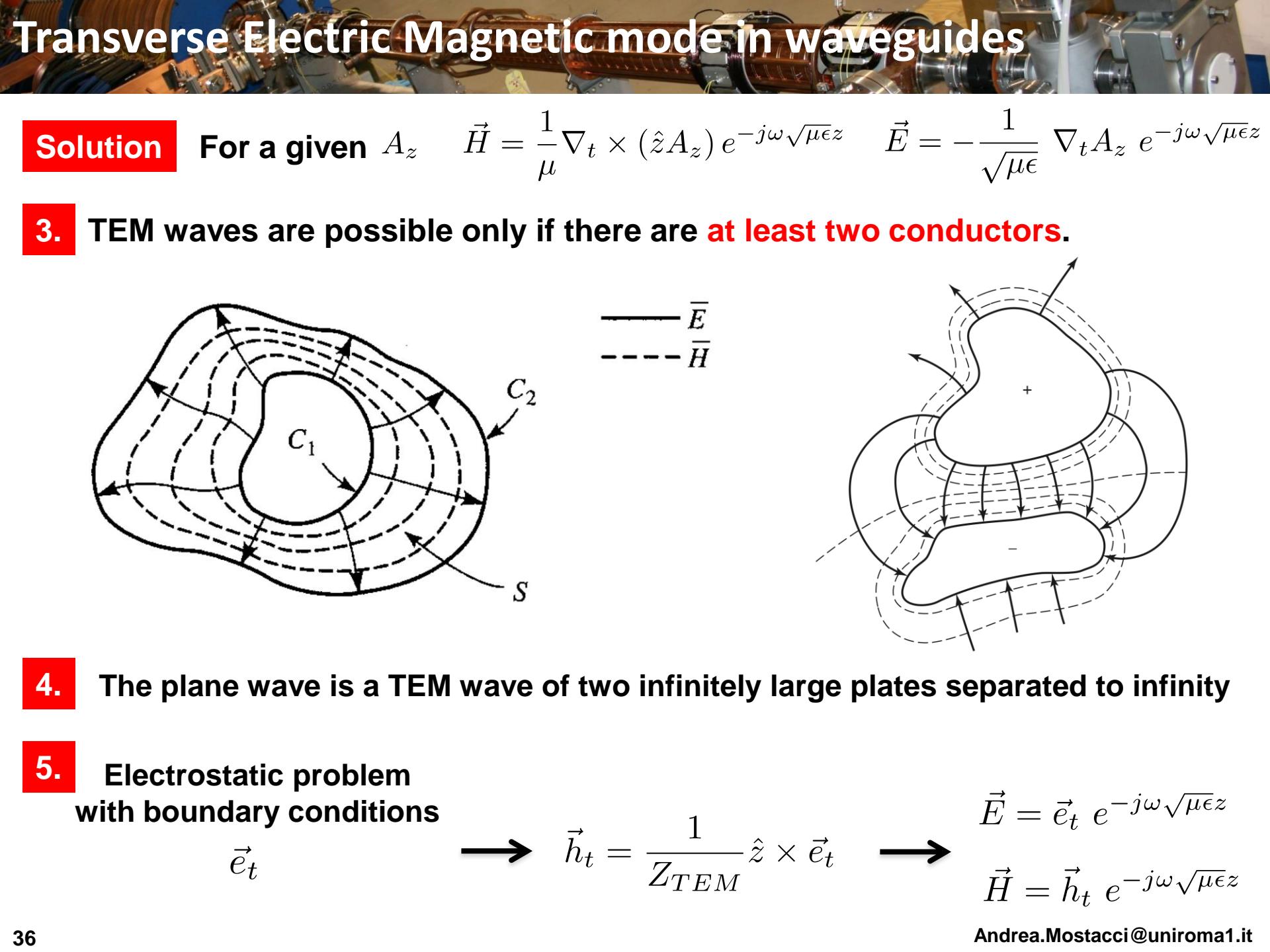
Hint 1 Start from a TM mode (vector potential A) $H_z = 0$

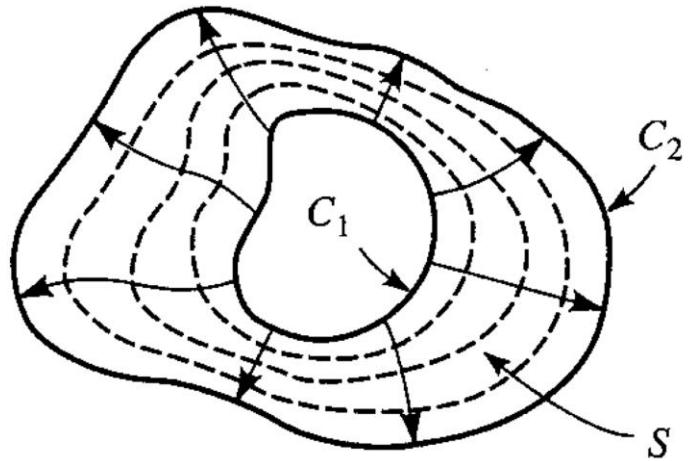
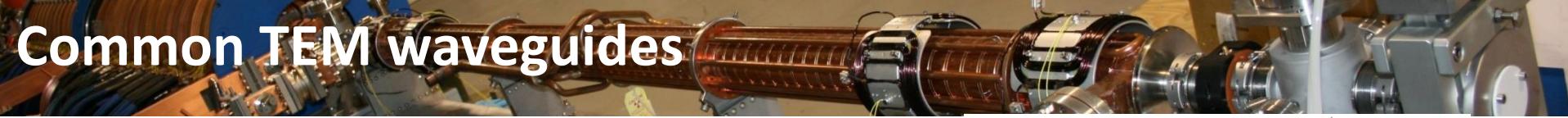
$$\nabla = \nabla_t + \hat{z} \frac{\partial}{\partial z} \quad \nabla \cdot \vec{A} = \dots$$

Hint 2 $\vec{E}_A = \dots$

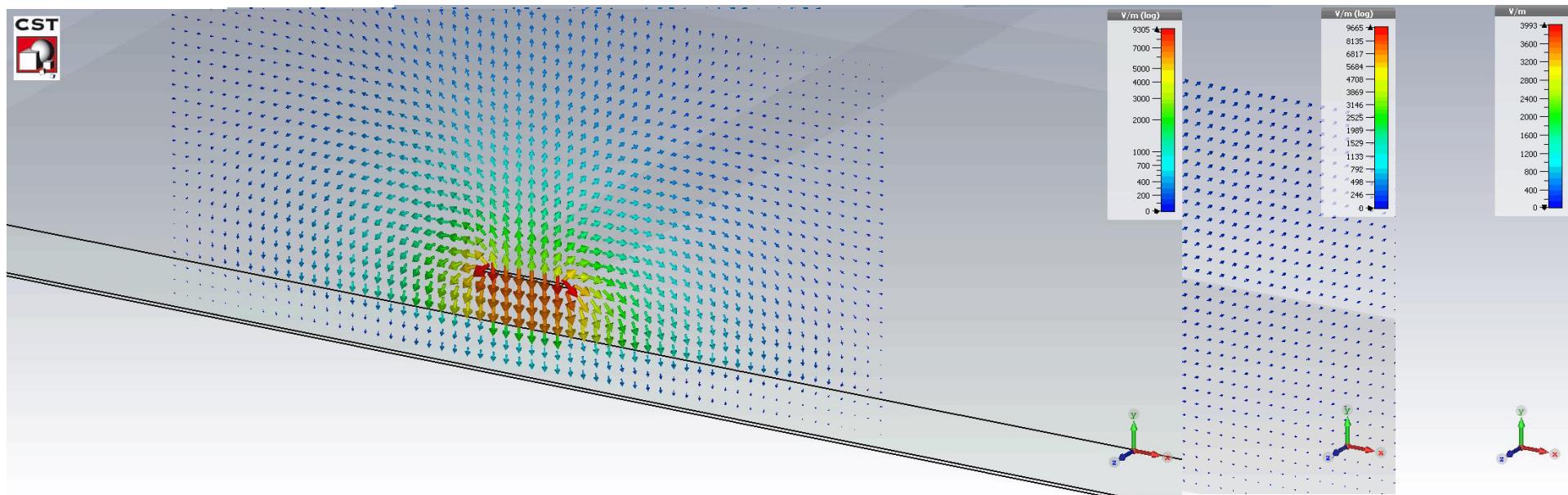
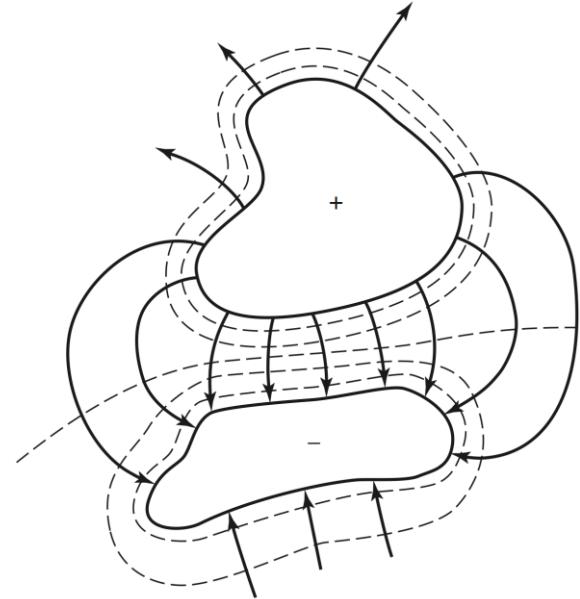
Solution

Transverse Electric Magnetic mode in waveguides





— \overline{E}
- - - \overline{H}



Animations by G. Castorina

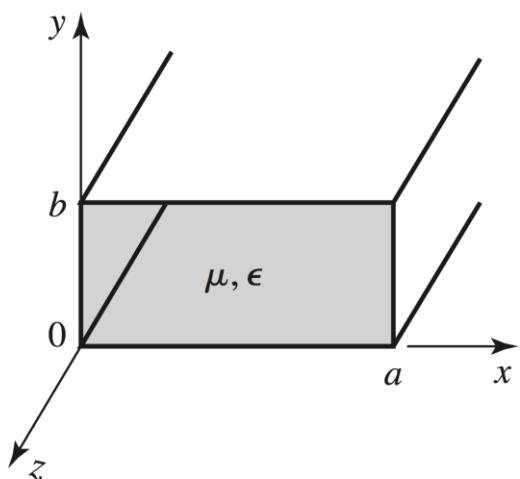
Andrea.Mostacci@uniroma1.it

General solution for fields in cylindrical waveguide

1. Write the Helmholtz equations for potentials

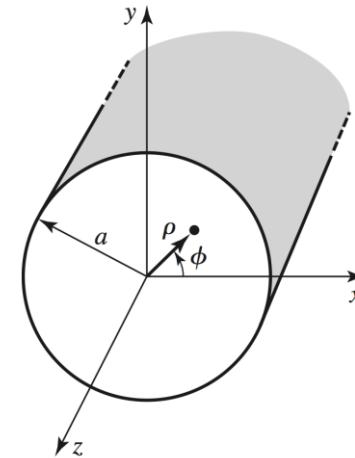
TM waves $\nabla_t^2 A_z + k_t^2 A_z = 0$ $k_t^2 = k^2 - \beta^2 = \omega^2 \mu \epsilon - \beta^2$

TE waves $\nabla_t^2 F_z + k_t^2 F_z = 0$ $\epsilon = \epsilon_r \epsilon_0 (1 - j \tan \delta)$



Cartesian coordinates

$$\nabla_t^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$$



Cylindrical coordinates

$$\nabla_t^2 = \frac{\partial^2}{\partial \rho^2} + \frac{1}{\rho} \frac{\partial}{\partial \rho} + \frac{1}{\rho^2} \frac{\partial^2}{\partial \phi^2}$$

2.

$$A_z(x, y) = X(x)Y(y)$$

$$A_z(\rho, \phi) = R(\rho)\Phi(\phi)$$

Separation of variables

General solution for fields in cylindrical waveguide

3. Eigenvalue problem: Eigenvalues + Eigen-function

TM $\nabla_t^2 A_z + k_t^2 A_z = 0$ k_t A_z, F_z

TE $\nabla_t^2 F_z + k_t^2 F_z = 0$

4. Compute the fields and apply the boundary conditions

$$\vec{e} = \vec{e}_t + \hat{z} e_z$$

$$\vec{h} = \vec{h}_t + \hat{z} h_z$$



$$\begin{array}{c} \vec{e}_{m,n} \quad \vec{h}_{m,n} \\ \beta_{m,n} = \sqrt{\omega^2 \mu \epsilon - k_t^2} \end{array}$$

Mode (m,n)

5.

$$\vec{E} = \sum_{m,n} a_{m,n} \vec{e}_{m,n} e^{-j\beta_{m,n} z}$$

It can be complex

$$\vec{H} = \sum_{m,n} b_{m,n} \vec{h}_{m,n} e^{-j\beta_{m,n} z}$$

It depends on the sources



Rectangular waveguides: TE mode

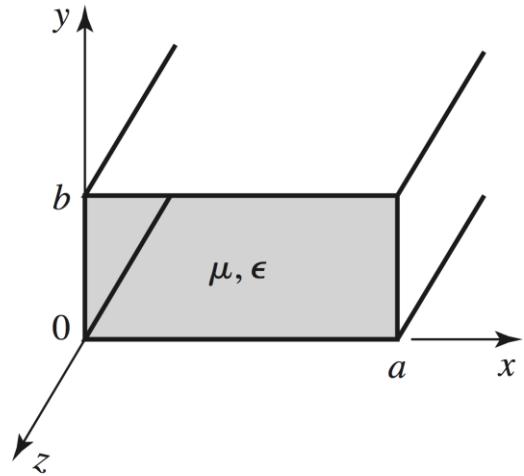
Example

$$F_z = X(x)Y(y)$$

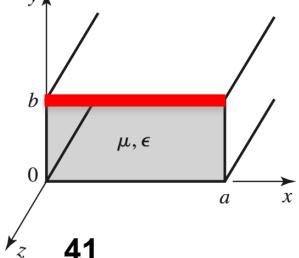
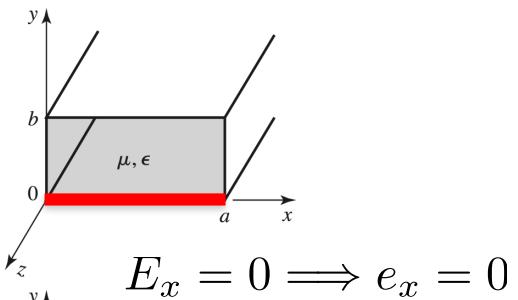
Write the Helmotz equation

$$X(x) =$$

$$Y(y) =$$



$$e_x = -\frac{1}{\epsilon} \frac{\partial F_z}{\partial y} = -\frac{1}{\epsilon} XY' :$$



Rectangular waveguides: TE mode

Example

$$F_z = X(x)Y(y) \quad \nabla_t^2 F_z + k_t^2 F_z = YX'' + XY'' + k_t^2 XY = 0$$

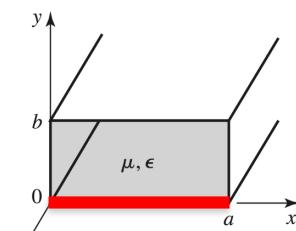
$$\frac{X''}{X} + \frac{Y''}{Y} + k_t^2 = 0 \quad -k_x^2 - k_y^2 + k_t^2 = 0$$

constraint condition

$$\frac{X''}{X} = -k_x^2 \quad \rightarrow \quad X(x) = C_1 \cos(k_x x) + D_1 \sin(k_x x)$$

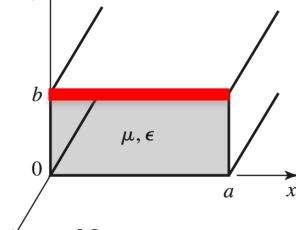
$$\frac{Y''}{Y} = -k_y^2 \quad \rightarrow \quad Y(y) = C_2 \cos(k_y y) + D_2 \sin(k_y y)$$

$$e_x = -\frac{1}{\epsilon} \frac{\partial F_z}{\partial y} = -\frac{1}{\epsilon} XY' = -\frac{k_y}{\epsilon} [C_1 \cos(k_x x) + D_1 \sin(k_x x)] [-C_2 \sin(k_y y) + D_2 \cos(k_y y)]$$

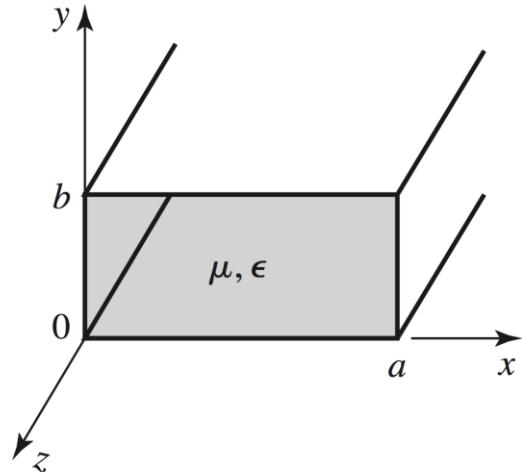


$$e_x(0 \leq x \leq a, y = 0) = \dots [-C_2 \cdot 0 + D_2 \cdot 1] = 0 \iff D_2 = 0$$

$$E_x = 0 \implies e_x = 0$$



$$e_x(0 \leq x \leq a, y = b) = \dots [-C_2 \sin(k_y b)] = 0 \iff \begin{aligned} k_y b &= n\pi \\ n &= 0, 1, 2, \dots \end{aligned}$$



Eigenvalues and cut-off frequencies (TE mode, rect. WG)

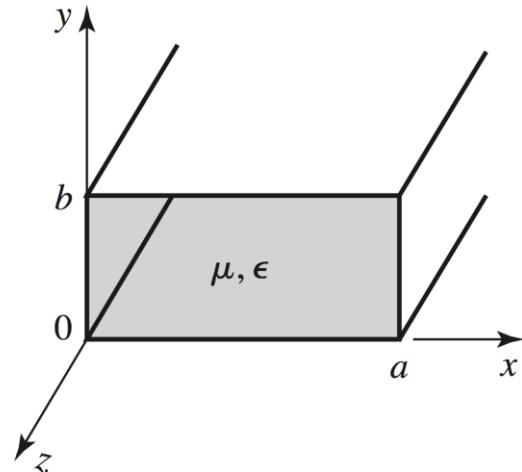
$$k_t^2 = k_x^2 + k_y^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 = \omega^2 \mu \epsilon - \beta^2$$

constraint condition

$$\vec{H} = \sum_{m,n} b_{m,n} \vec{h}_{m,n} e^{-j\beta_{m,n}z}$$

$$\beta_{m,n} = \sqrt{\omega^2 \mu \epsilon - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

$$\vec{E} = \sum_{m,n} a_{m,n} \vec{e}_{m,n} e^{-j\beta_{m,n}z}$$



Cut-off frequencies f_c such that $\beta_{m,n} = 0$

$$(f_c)_{m,n} = \frac{1}{2\pi\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2} \quad m, n = 0, 1, 2, \dots$$

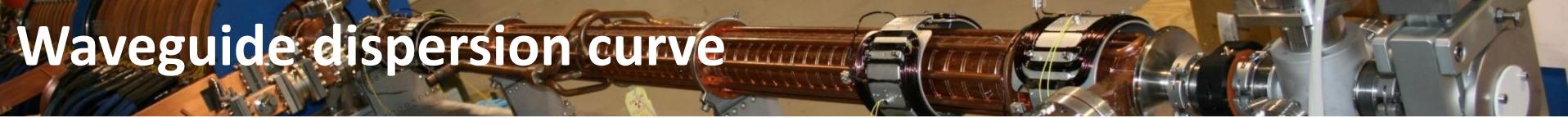
$m = n \neq 0$

$$f < (f_c)_{m,n}$$

mode m, n is attenuated exponentially (evanescent mode)

$$f > (f_c)_{m,n}$$

mode m, n is propagating with no attenuation

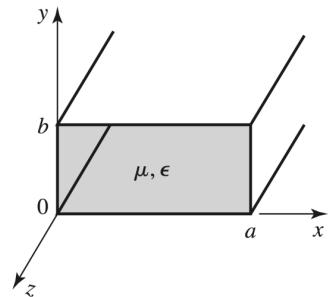
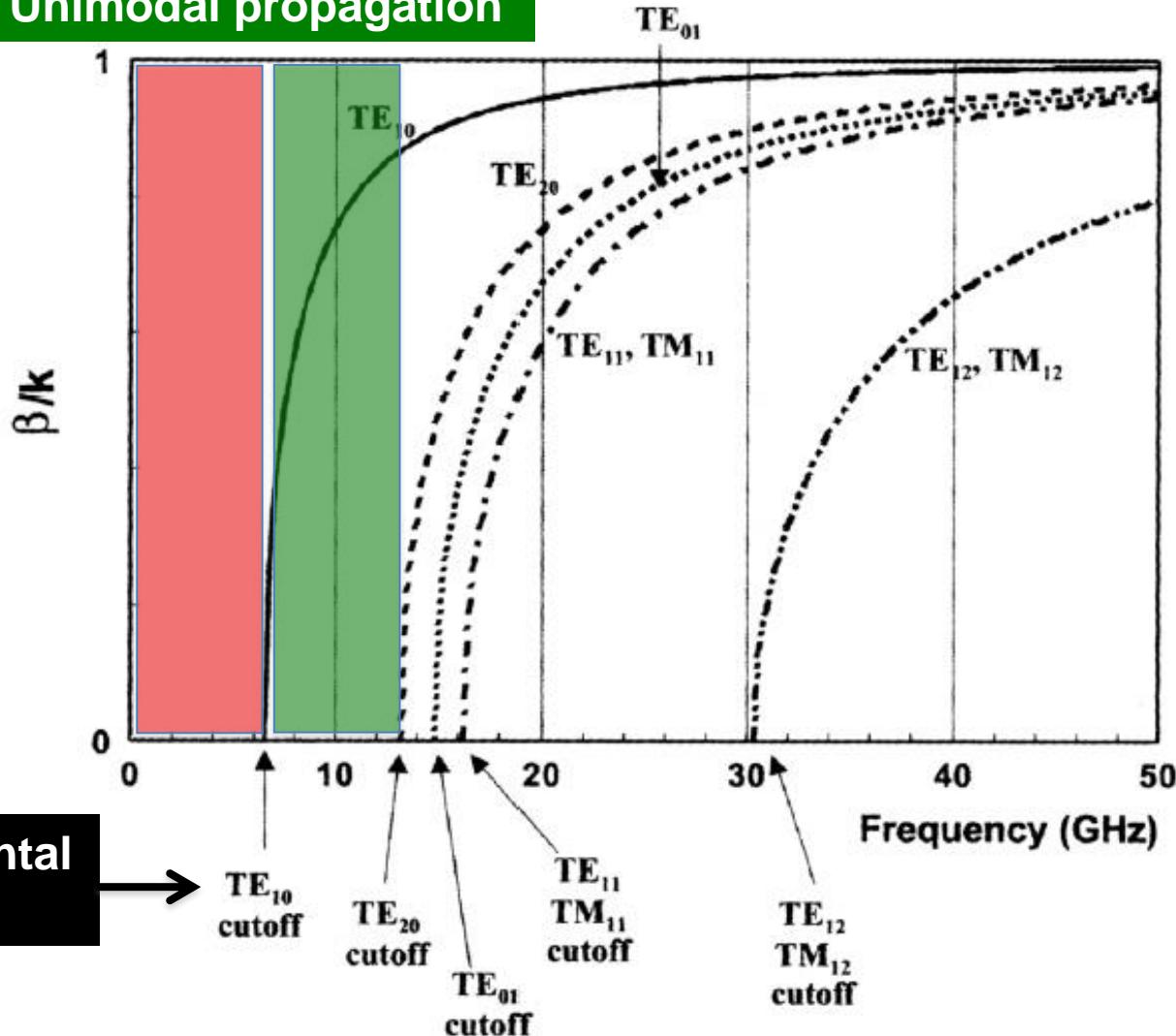


Waveguide dispersion curve

Cut-off

Unimodal propagation

Courtesy of S. Pisa



Same curve for TE and TM mode, but n=0 or m=0 is possible only for TE modes.

In any metallic waveguide the fundamental mode is TE.

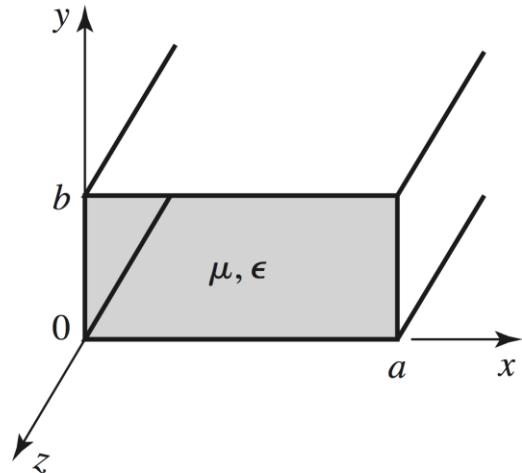
Single mode operation of a rectangular waveguide

Exercise

1. Find the smallest ratio a/b allowing the largest bandwidth of single mode operation
2. State the largest bandwidth of single mode operation
3. Defining the single mode bandwidth as

$$1.25 (f_c)_1 < f < 0.95 (f_c)_2$$

Find the single mode BW for WR-90 waveguide ($a=22.86\text{mm}$ and $b=10.16\text{ mm}$)



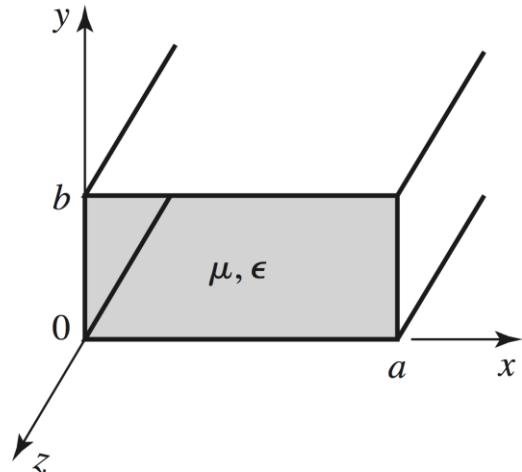
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Eigenfunctions and mode pattern (TE mode, rect. WG)

$$E_x^{+, (m,n)} = a_{m,n} \frac{k_y}{\epsilon} \cos(k_x x) \sin(k_y y) e^{-j\beta z}$$

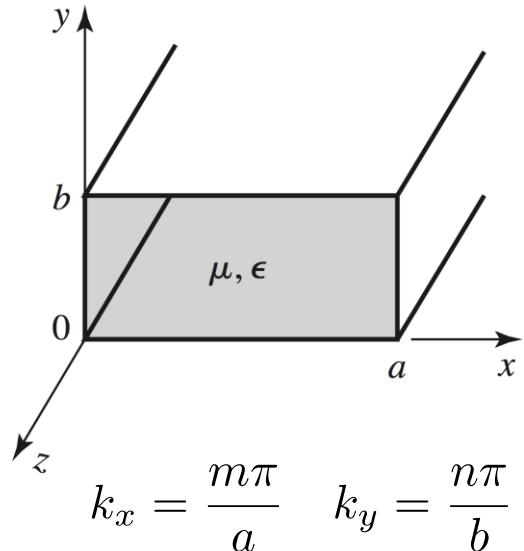
$$E_y^{+, (m,n)} = a_{m,n} \frac{k_y}{\epsilon} \sin(k_x x) \cos(k_y y) e^{-j\beta z}$$

$$E_z^{+, (m,n)} = 0$$

$$H_x^{+, (m,n)} = a_{m,n} \frac{k_x \beta}{\omega \mu \epsilon} \sin(k_x x) \cos(k_y y) e^{-j\beta z}$$

$$H_y^{+, (m,n)} = a_{m,n} \frac{k_y \beta}{\omega \mu \epsilon} \cos(k_x x) \sin(k_y y) e^{-j\beta z}$$

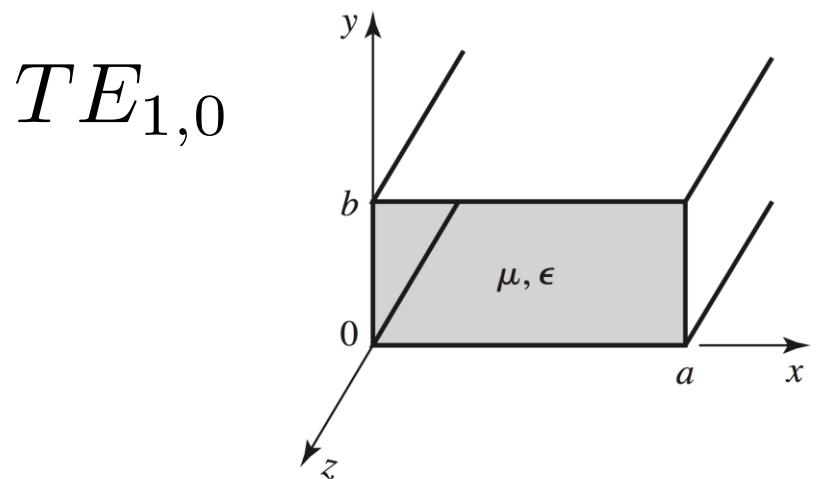
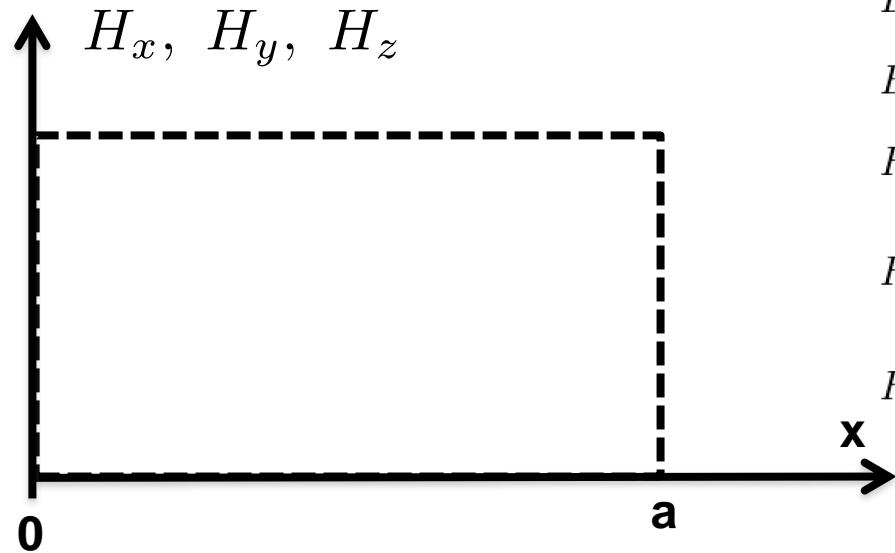
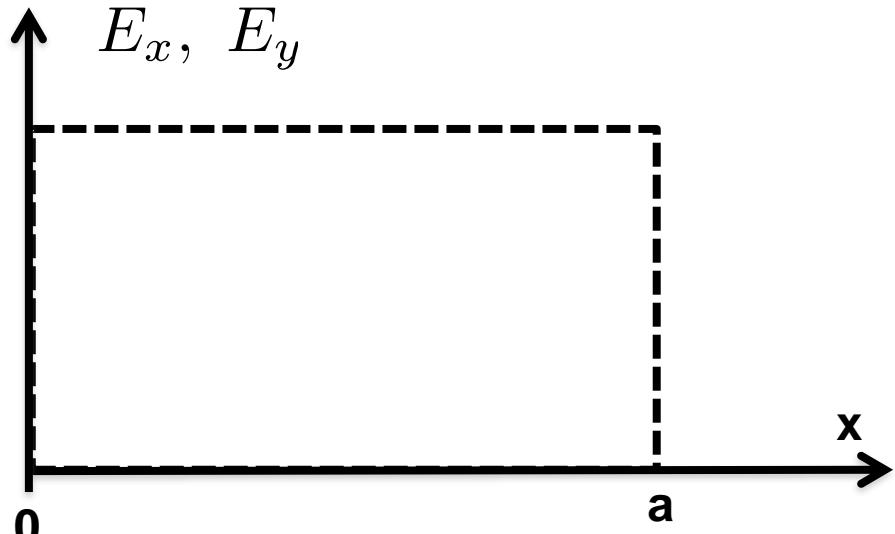
$$H_z^{+, (m,n)} = -ja_{m,n} \frac{k_t^2}{\omega \mu \epsilon} \cos(k_x x) \cos(k_y y) e^{-j\beta z}$$



$$\beta = \sqrt{\omega^2 \mu \epsilon - k_x^2 - k_y^2}$$

$TE_{m,n}^{+z}$

You can draw ...



$$E_x^{+, (m,n)} = a_{m,n} \frac{k_y}{\epsilon} \cos(k_x x) \sin(k_y y) e^{-j\beta z}$$

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Eigenfunctions and mode pattern (TE mode, rect. WG)

$$E_x^{+, (m,n)} = a_{m,n} \frac{k_y}{\epsilon} \cos(k_x x) \sin(k_y y) e^{-j\beta z}$$

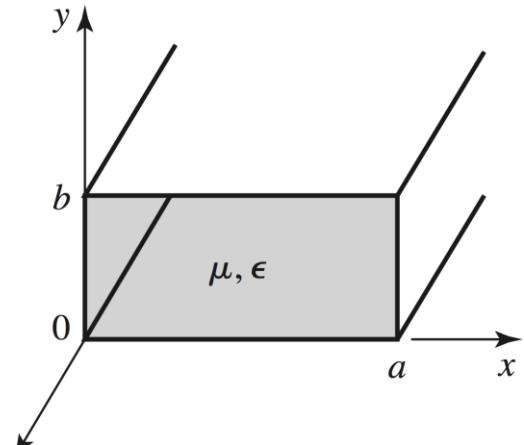
$$E_y^{+, (m,n)} = a_{m,n} \frac{k_y}{\epsilon} \sin(k_x x) \cos(k_y y) e^{-j\beta z}$$

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$$k_x = \frac{m\pi}{a} \quad k_y = \frac{n\pi}{b}$$

$$\beta = \sqrt{\omega^2 \mu \epsilon - k_x^2 - k_y^2}$$

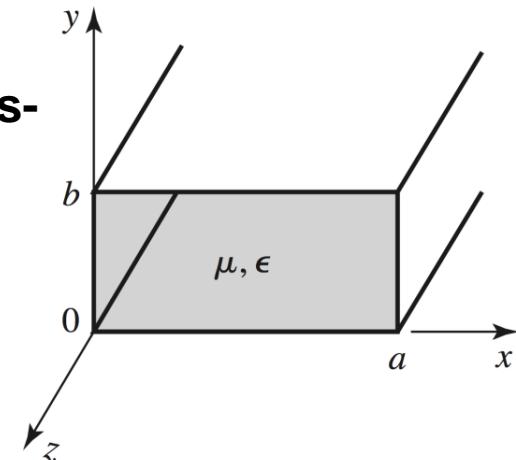
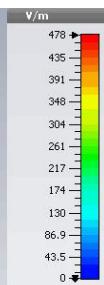
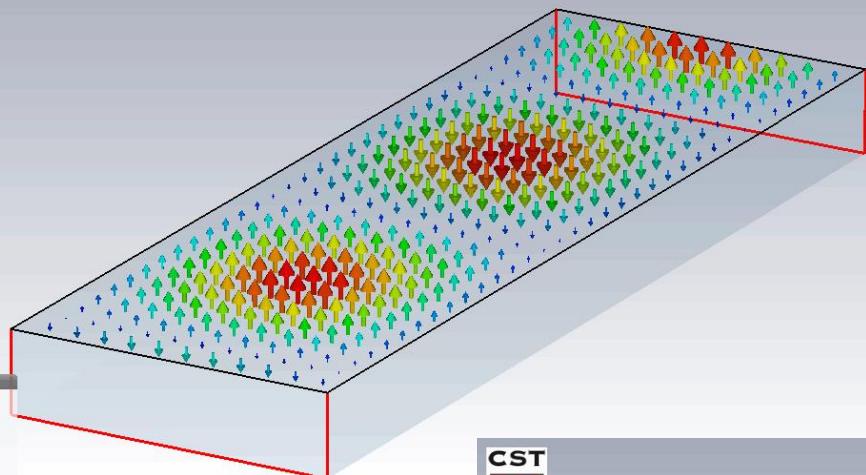
$$TE_{m,n}^{+z}$$

$$TE_{1,0}$$

Field pattern (TE10 mode, rect. WG)

$TE_{m,n}^{+z}$

m (n) is the number of half periods (or maxima/minima) along the x (y) axis in the cross-section.



h-field (f=2) [1] (peak)
Cutplane Name: Cross Section A
Cutplane Normal: 0, 1, 0
Cutplane Position: 0
2D Maximum [A/m]: 0.9531
Frequency: 2
Phase: 0

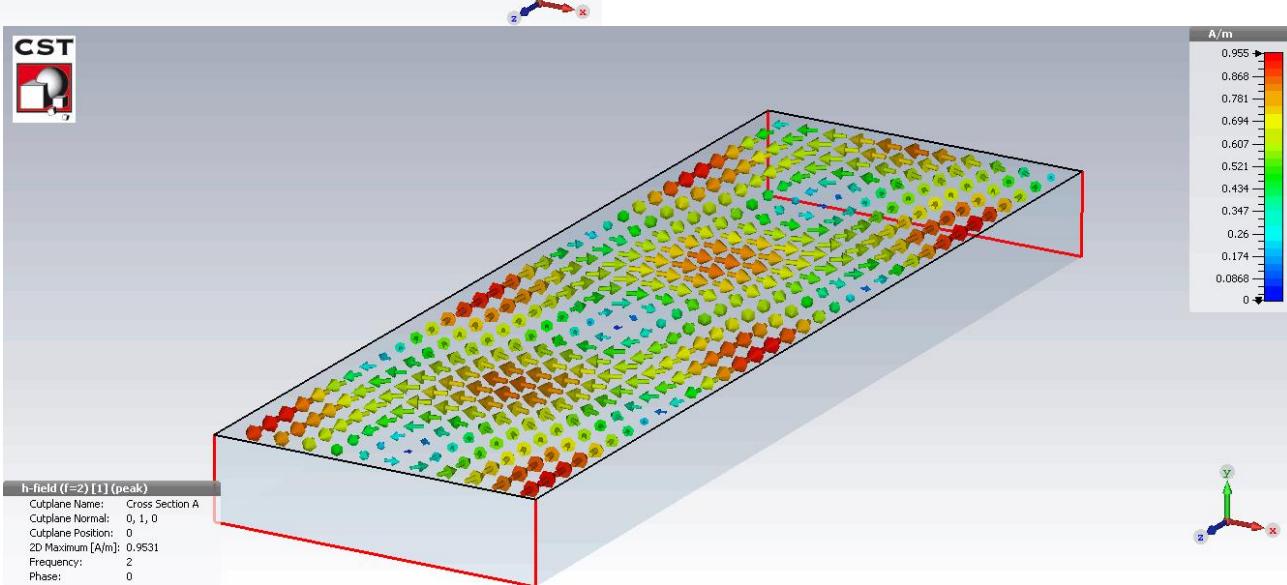
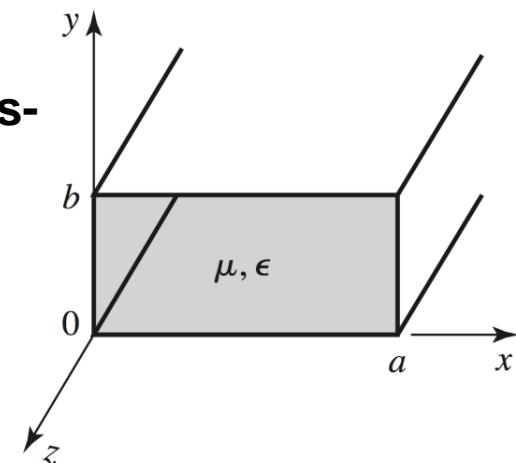
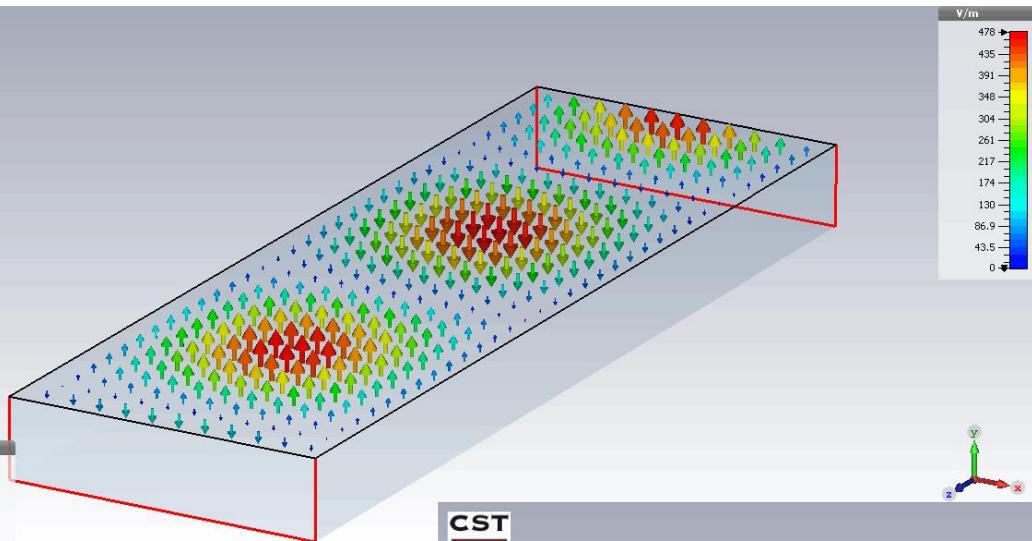


Simulations by L. Ficcadenti

Field pattern (TE₁₀ mode, rect. WG)

$TE_{m,n}^{+z}$

m (n) is the number of half periods (or maxima/minima) along the x (y) axis in the cross-section.



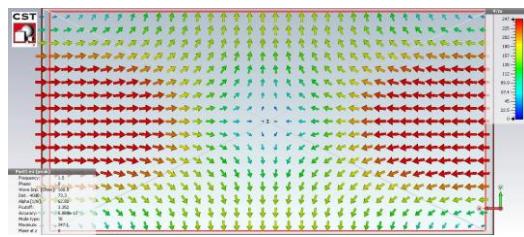
Animations by L. Ficcadenti

Field pattern at the cross section

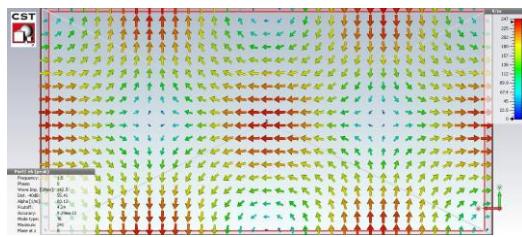
$TE_{m,n}^{+z}$

m (n) is the number of half periods (or maxima/minima) along the x (y) axis in the cross-section.

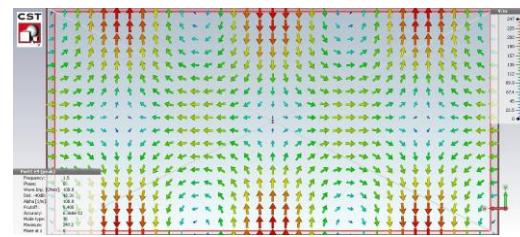
TE??



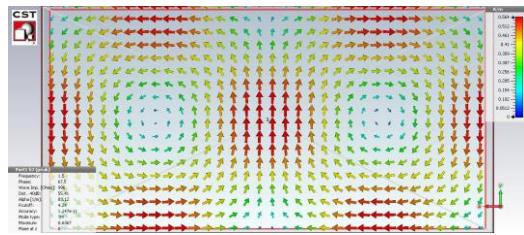
TE??



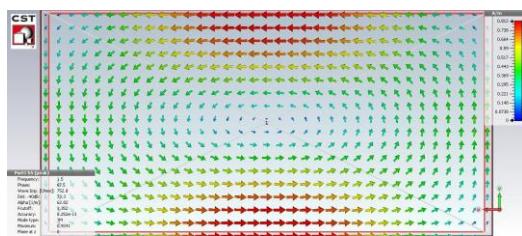
TE??



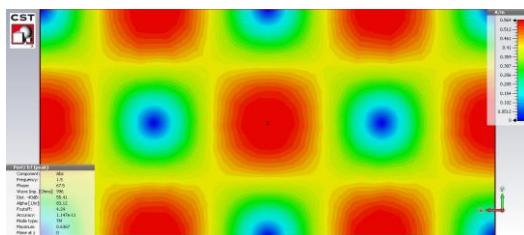
TM??



TM??



TM??



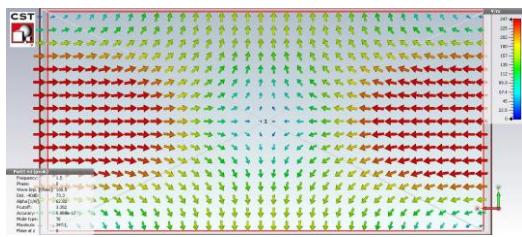
Simulations by L. Ficcadenti

Field pattern at the cross section

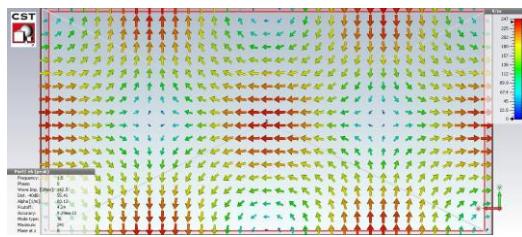
$$TE_{m,n}^{+z}$$

m (n) is the number of half periods (or maxima/minima) along the x (y) axis in the cross-section.

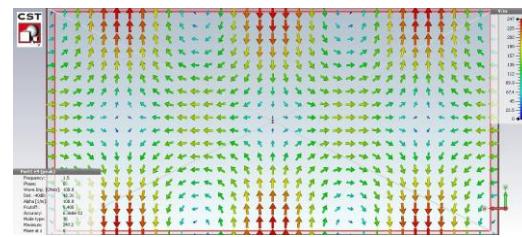
TE11



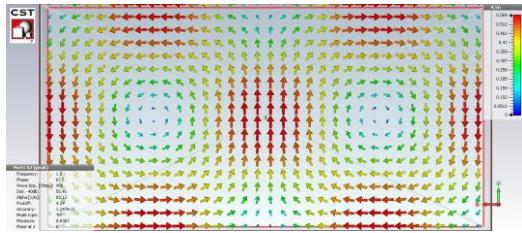
TE21



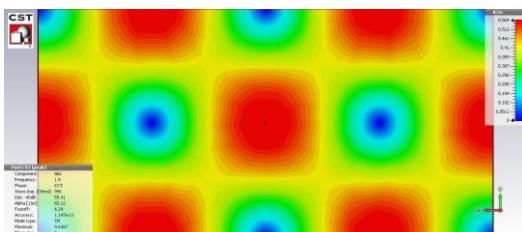
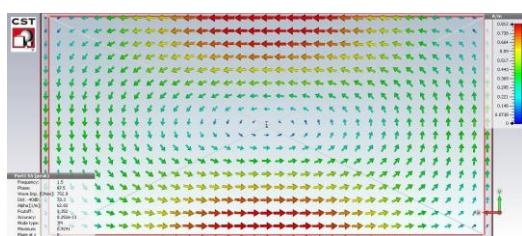
TE31



TM21



TM11



TM31

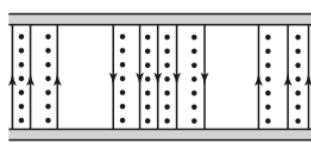
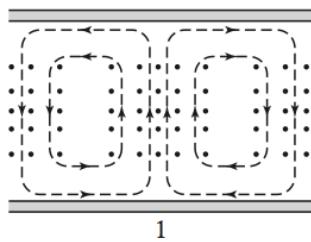
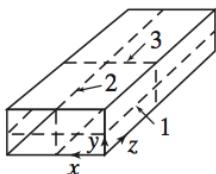
Simulations by L. Ficcadenti

Field pattern (TE mode, rect. WG)

$TE_{m,n}^{+z}$

m (n) is the number of half periods (or maxima/minima) along the x (y) axis in the cross-section.

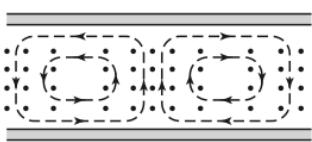
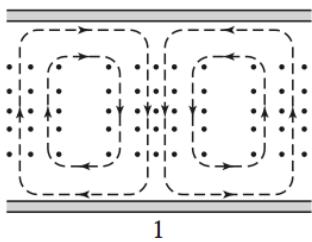
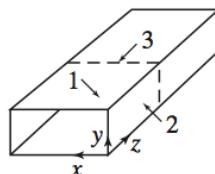
TE_{10}



3

2

TE_{11}

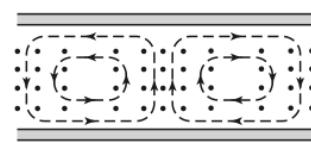
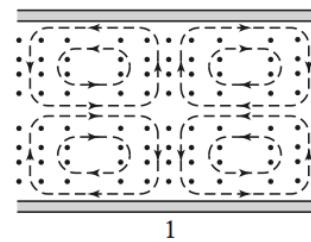
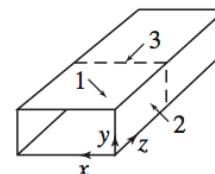


1

2

3

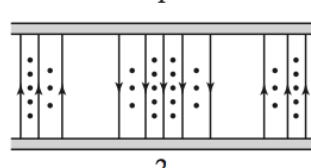
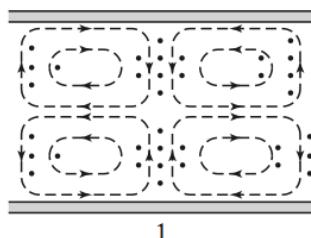
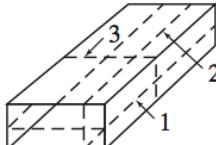
TE_{21}



1

2

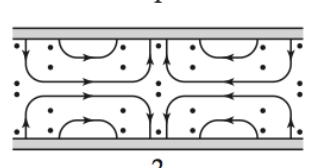
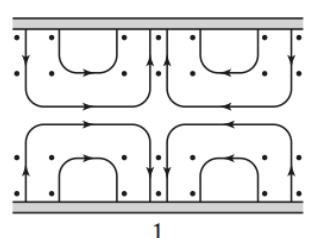
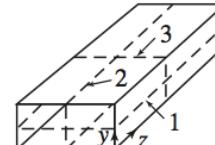
TE_{20}



3

2

TM_{11}

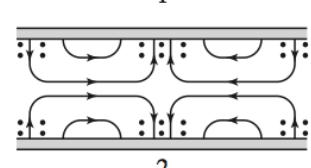
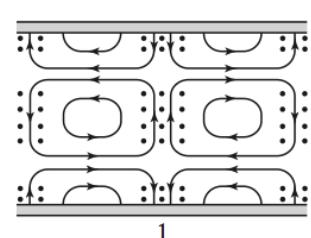
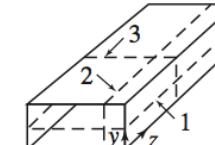


1

2

3

TM_{21}



1

2

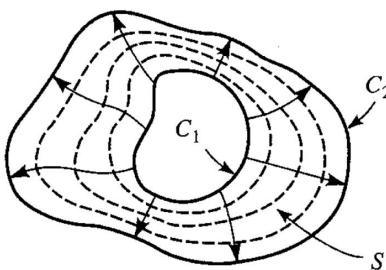
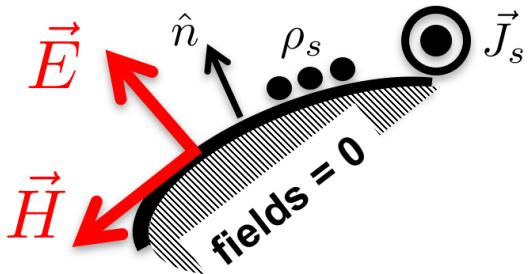
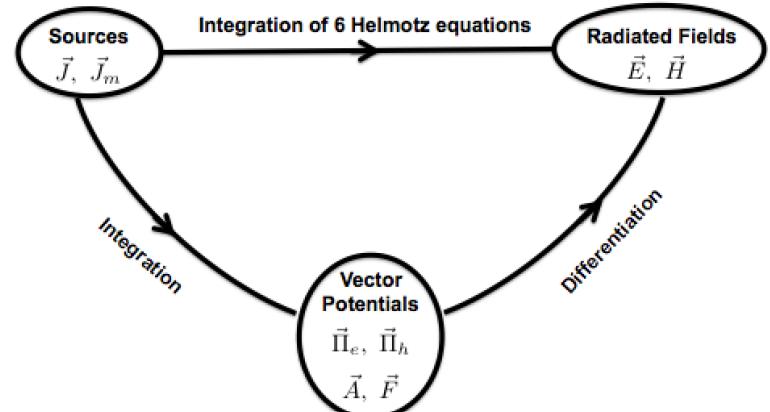
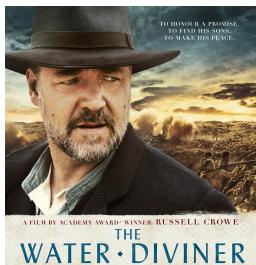
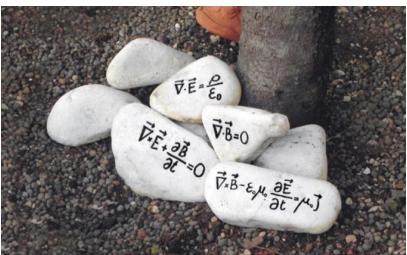
Conclusions



... The universe is written in the mathematical language and the letters are triangles, circles and other geometrical figures ...

Galileo Galilei

$$\nabla \times \nabla \cdot$$



$$\begin{array}{c} \overrightarrow{E} \\ \overrightarrow{H} \end{array}$$

