

Thermal simulations of the DQW HOM coupler

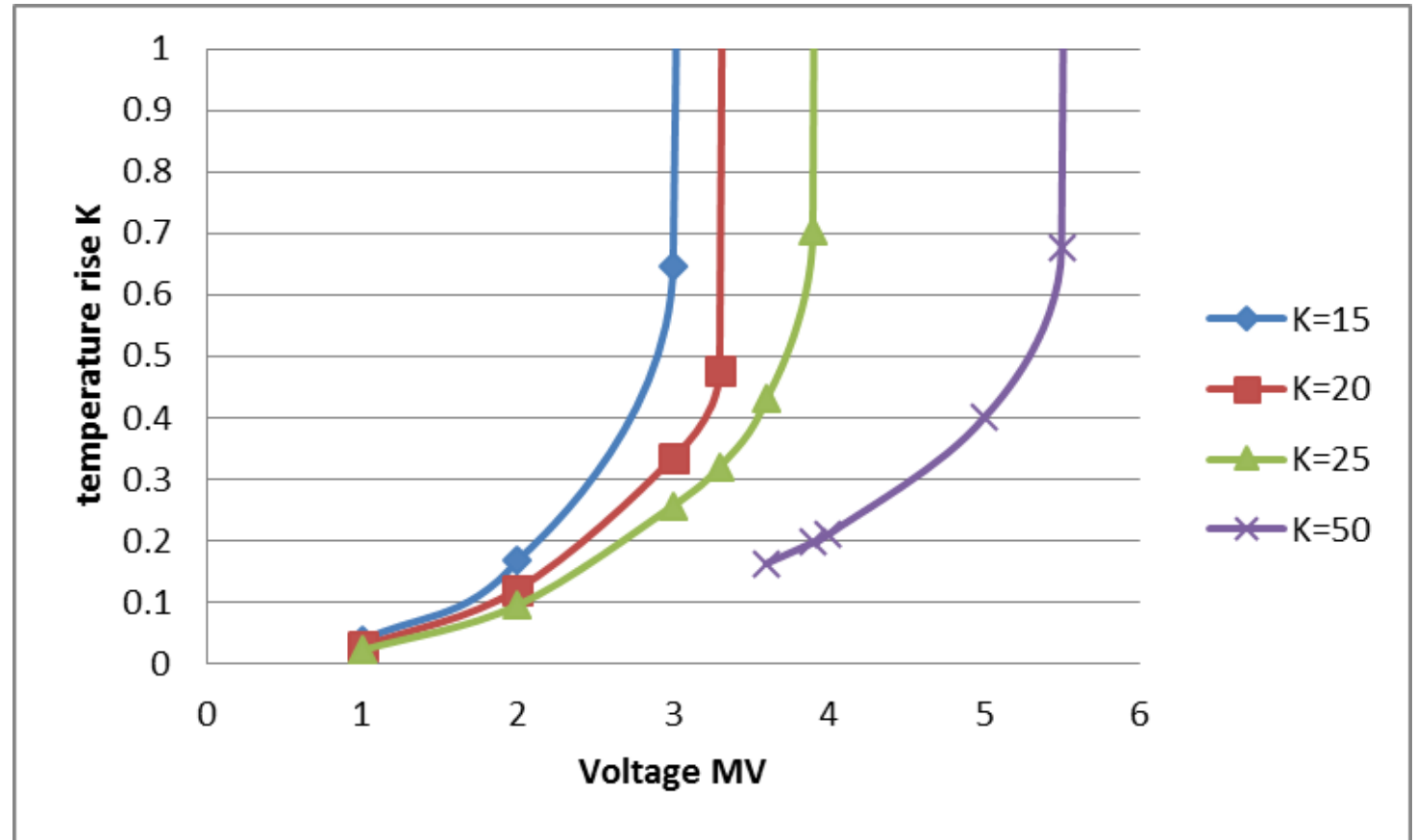
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Original thermal modelling

- Did a simulation with the properties at 2K Nb and calculate dT/dR .
- Then do an iterative solve to find steady state temperature using

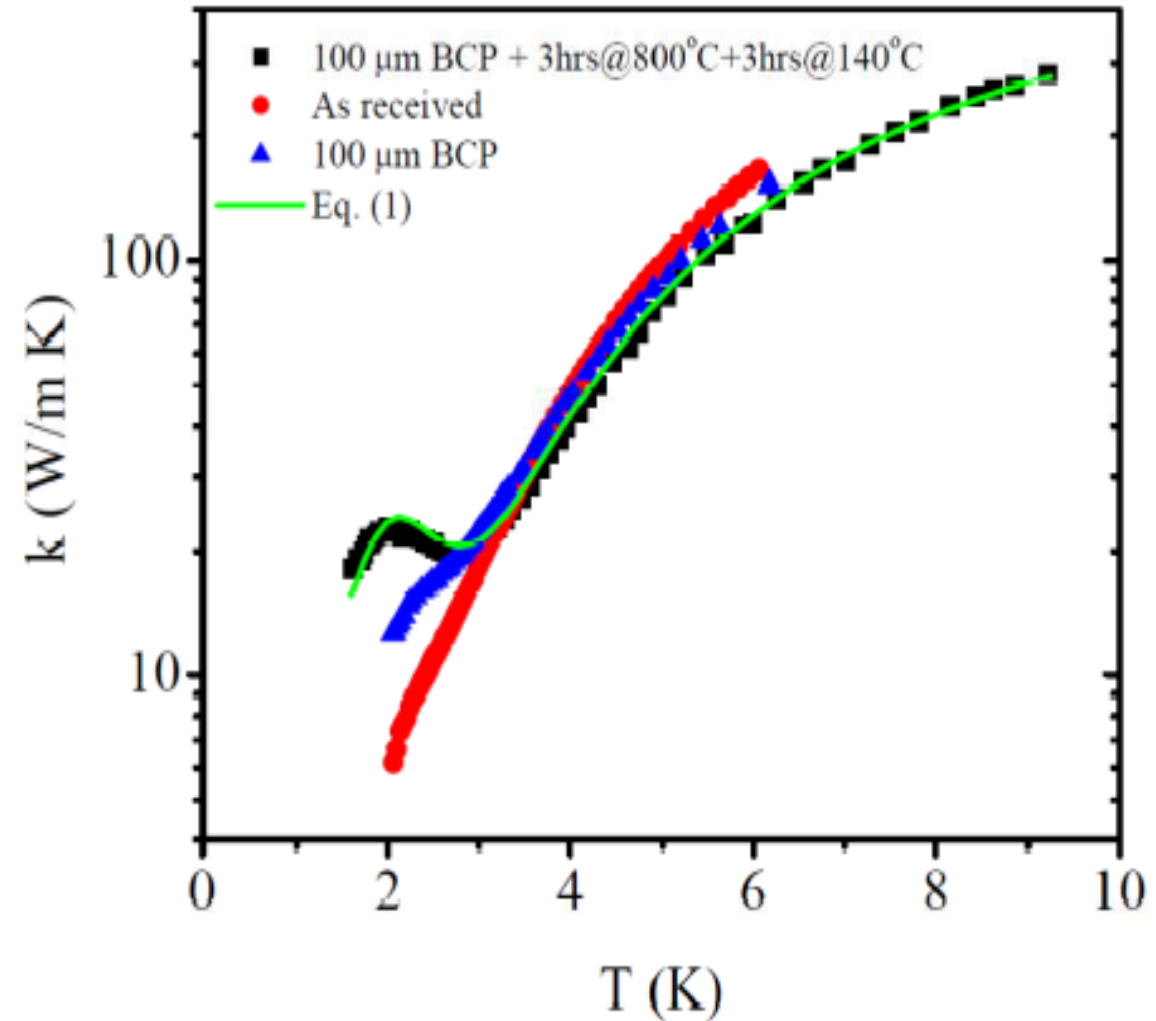
$$R_{BCS} = 2 \times 10^{-4} \frac{1}{T} \left(\frac{f}{1.5} \right)^2 \exp\left(-\frac{17.67}{T} \right)$$

$$T_{n+1} = \frac{dT}{dR} [R B_{CS}(T_n) + R r_{es}] * \frac{K_{CST}}{K_{scaled}}$$



Variation of thermal conductivity

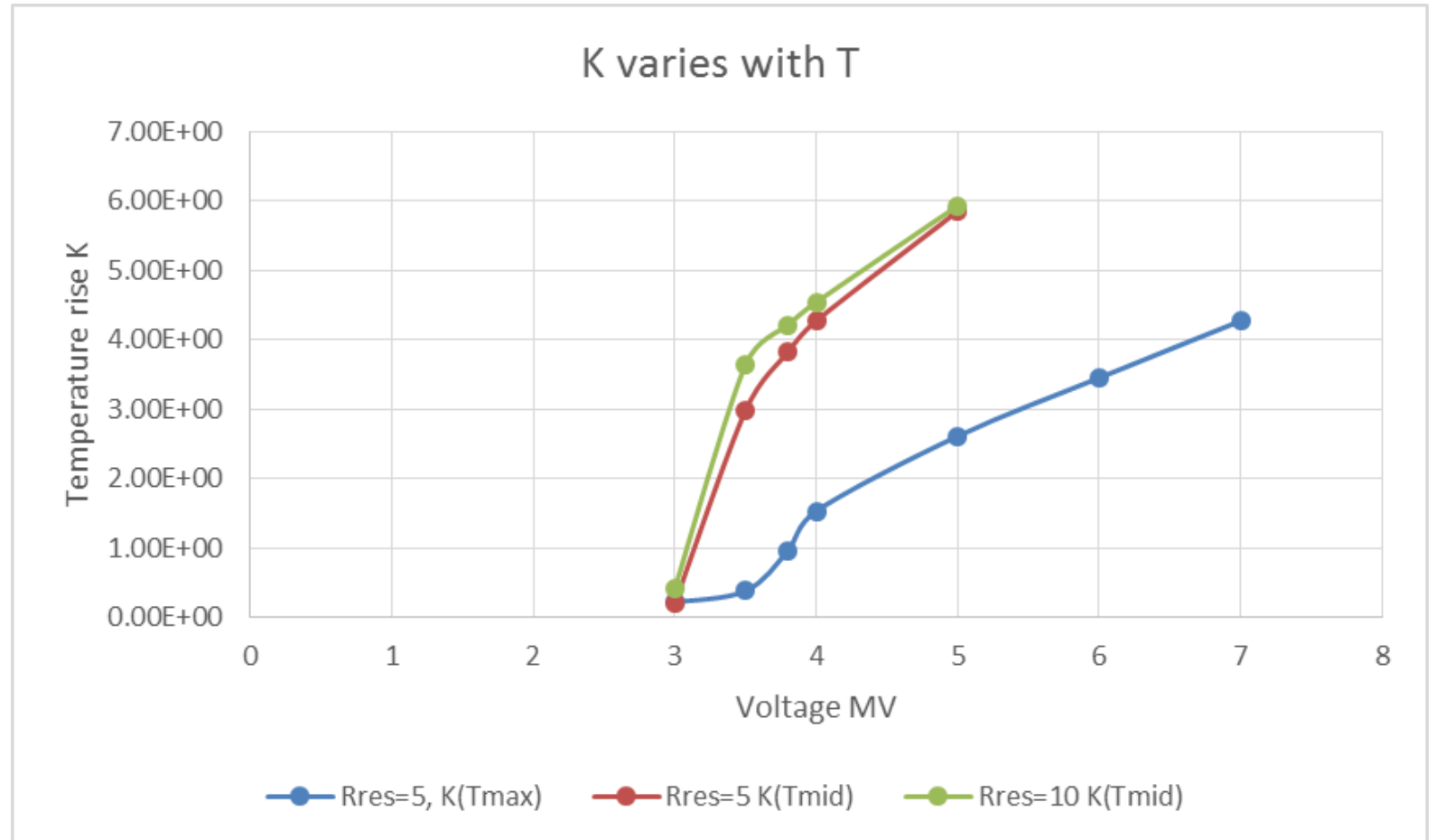
- Use a fit to the green line opposite



Analytical model for scaling assuming constant thermal and electrical properties

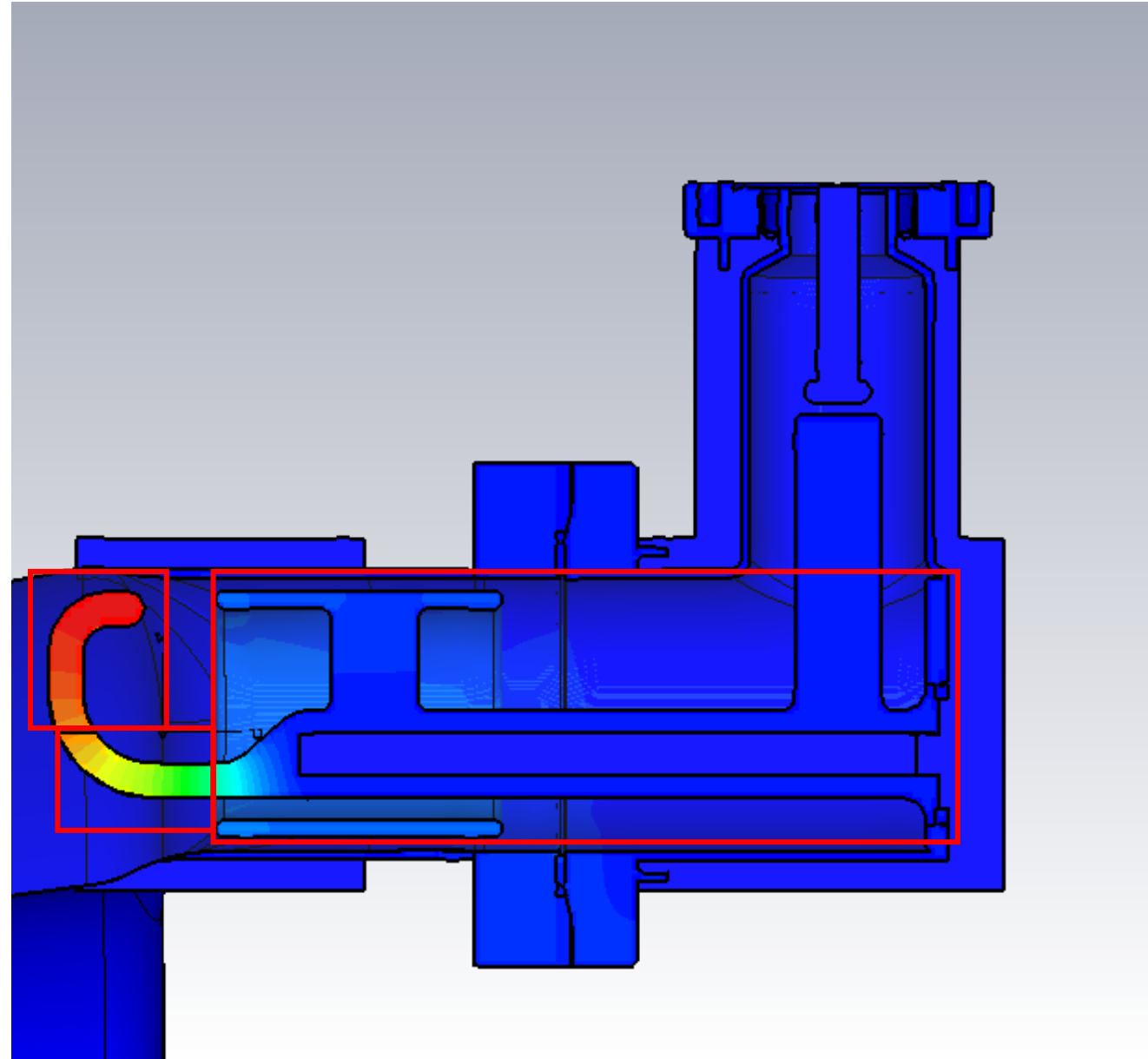
- Previous simulations did the simulations with a constant thermal conductivity
- Here we now use a temp dependant K
- Tmax means using the thermal conductivity at the tip, Tmid means using thermal conductivity of the mid point

$$T_{n+1} = \frac{dT}{dR} [RB_{CS}(T_n) + Rr_{es}] * \frac{K_{CST}}{K(T_n)}$$



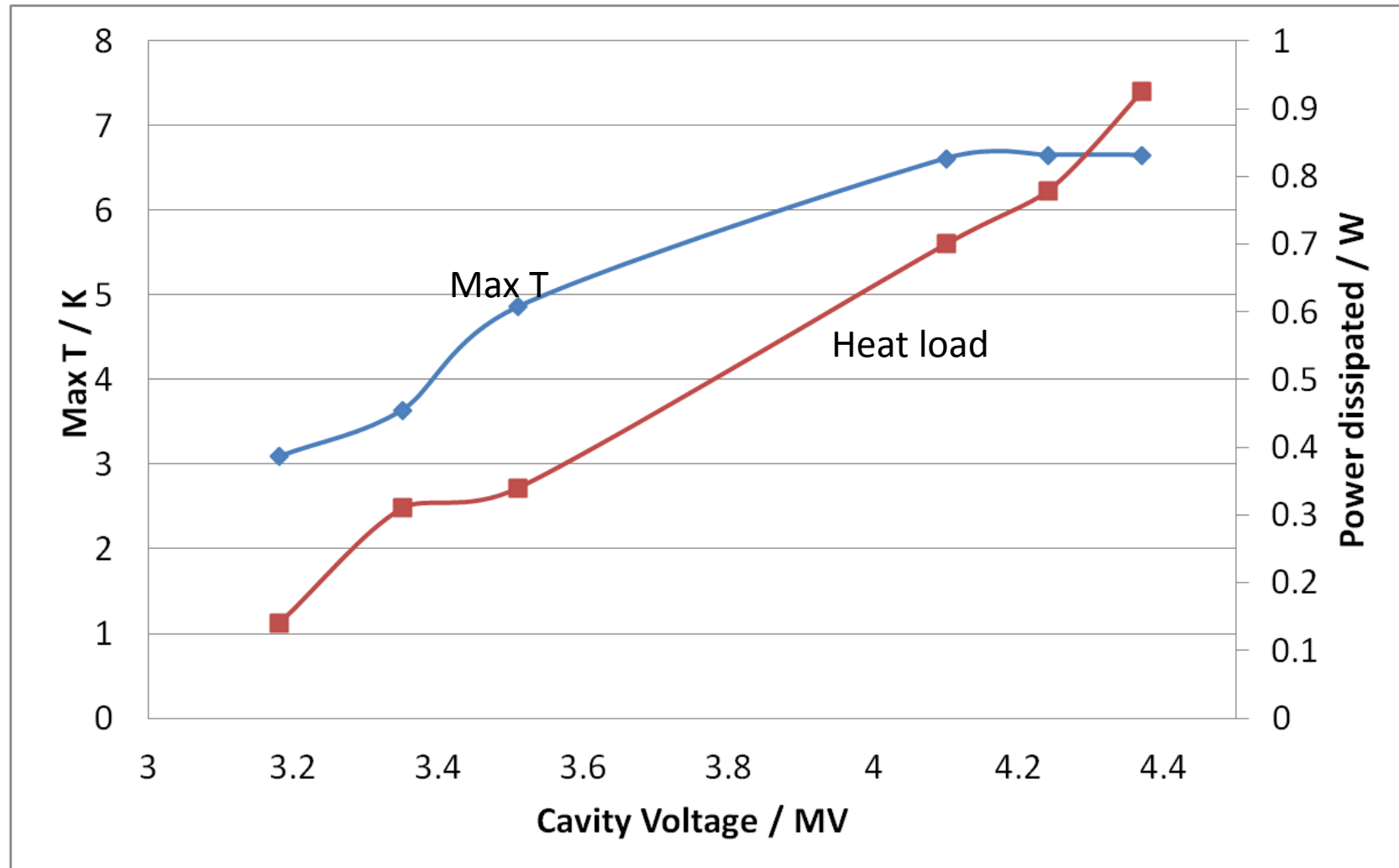
CST simulation

- Split the coupler into 3 regions and set thermal conductivity and surface resistance of each based on the previous simulation and iterate

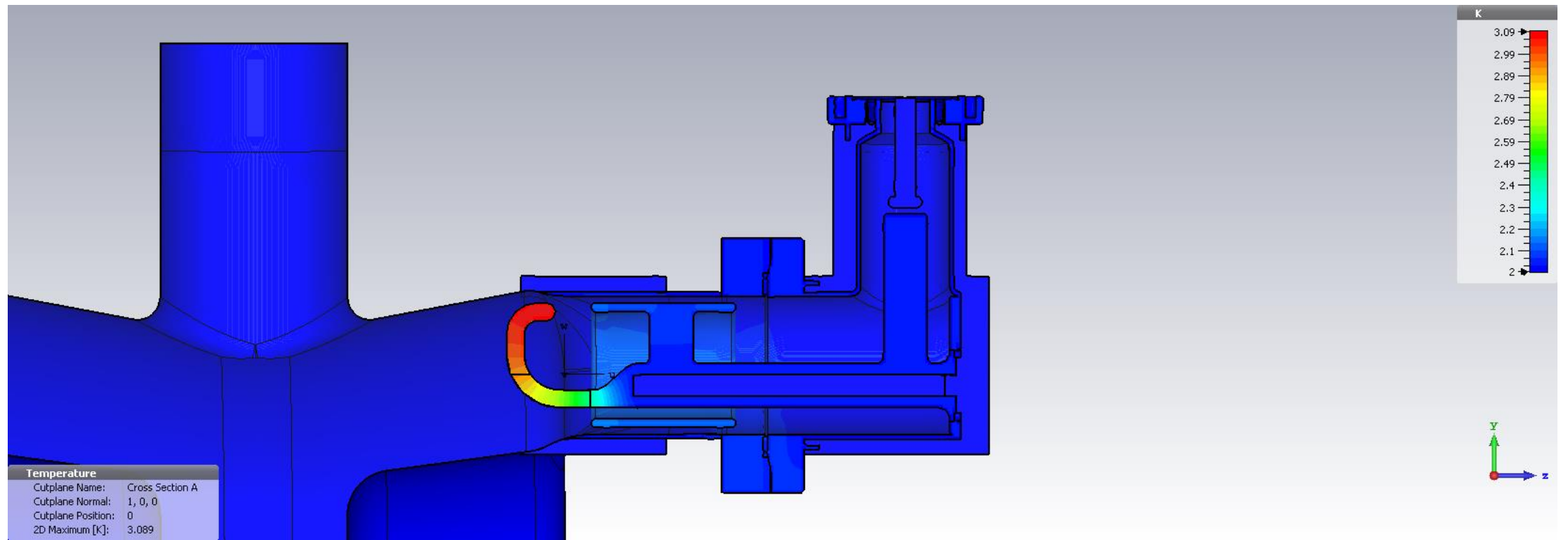


CST simulations with $R_{res}=5$ nOhms

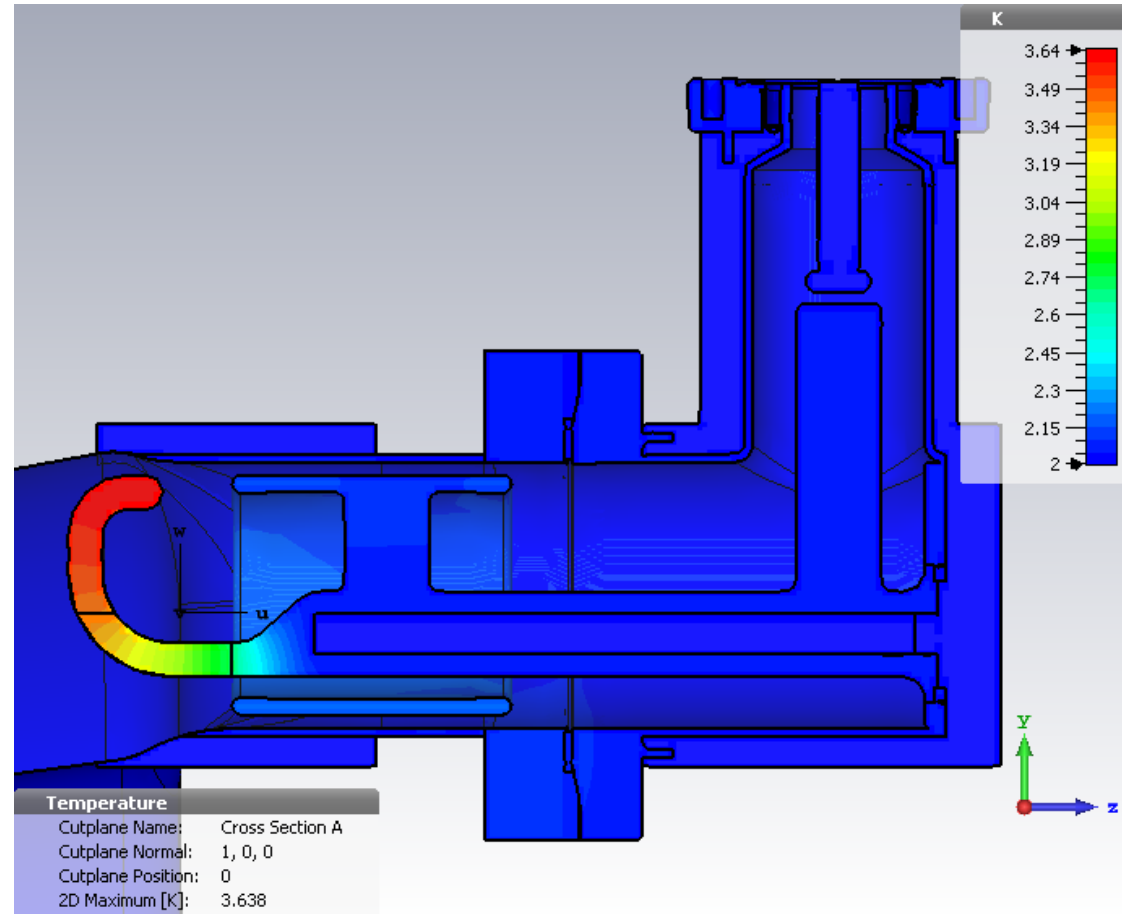
- In self-consistent CST sims where K varies with T along the hook we find the low temperature end dominates as it has a very low K .
- We also find that at high voltage the temperature stabilises as the base heats up.
- At just under 4.5 MV the heat load is 1 watt per HOM coupler in CST which would be above the limit for heat transport in the hollow inner conductor (1 Watt/cm^2)



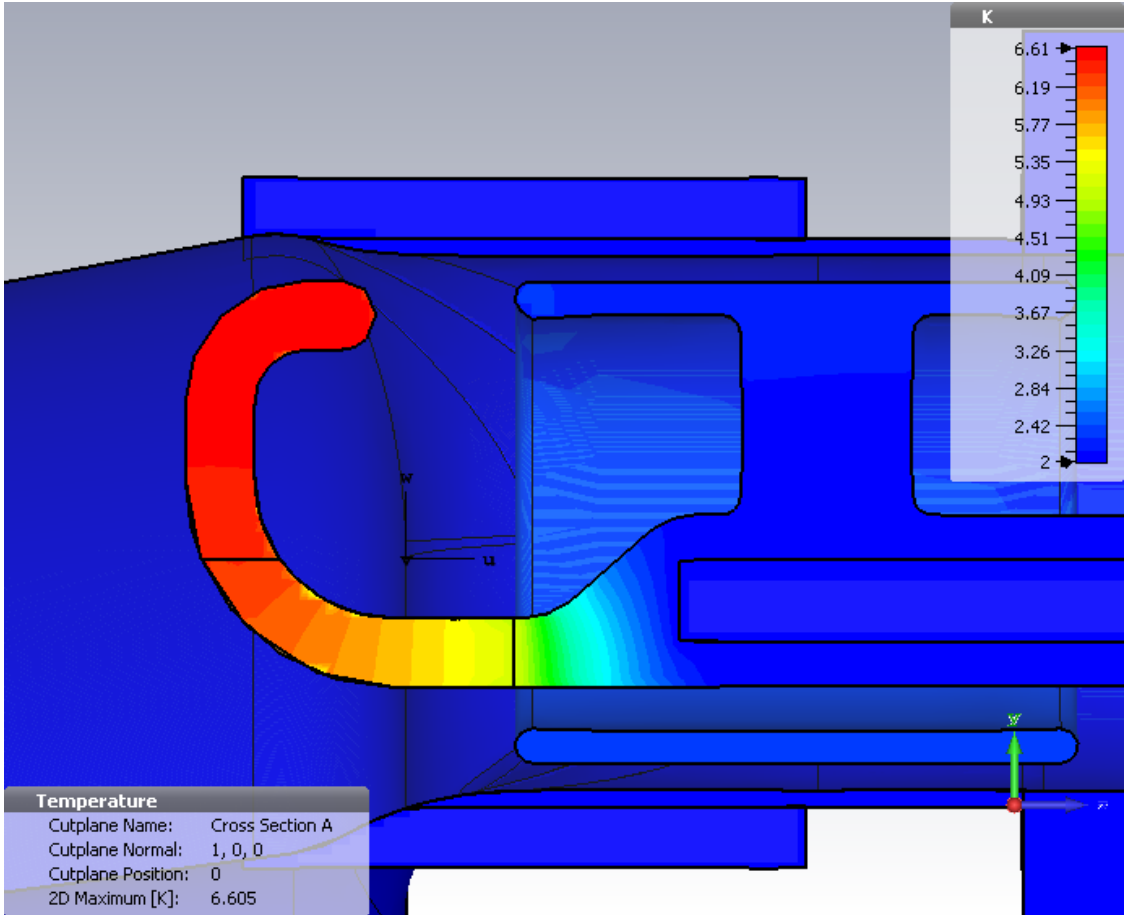
3.18 MV



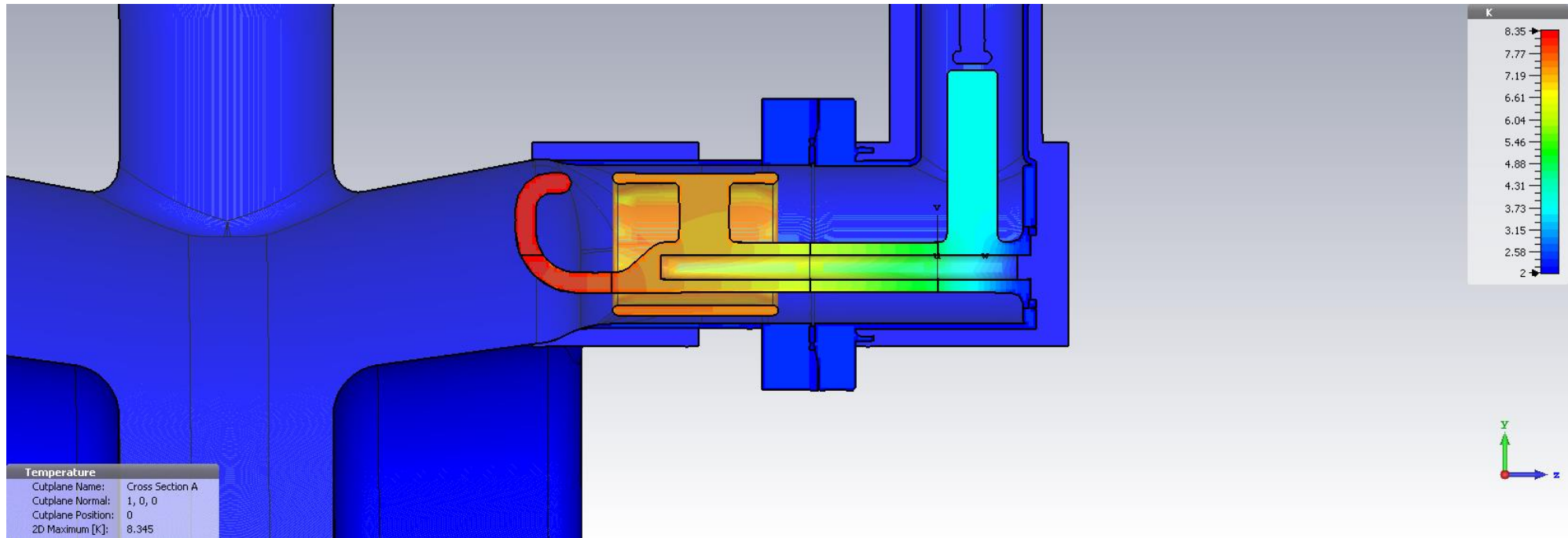
3.5 MV



4.1 MV



Cooling channel filled with gas



- Quenches at around 3.5 MV

Next steps

- Look at rotating the coupler
- Look at 4.2 K operation
- Look at the effect of the notch being off resonance
- Look at multipactor