




**POLITECNICO  
MILANO 1863**



## Radiochemistry and Monte Carlo integrated approach to radiological characterization for nuclear facilities decommissioning

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## **i. INTRODUCTION**

- Radiological characterization for Decommissioning
- L-54M reactor

## **ii. SCOPE OF THE WORK**

### **iii. STEP 1**

- Why MCNP?
- Model development
- Model Verification

### **iv. STEP 2**

- Activation reactions
- Impurities distributions

### **v. STEP 3**

- Assessment of activation
- Model Validation

## **vi. CONCLUSIONS AND FUTURE WORKS**

After nuclear reactor shut-down

... several possible strategies

1. Immediate dismantling → *Decon*
2. Postponed dismantling → *Safe storage*
3. *Entombment*

*Technical, economical, social and political factors influence the strategy choice*

## PURPOSES:

1. Restoration of **unrestricted re-use condition** (greenfield/brownfield);
2. Reduction of **costs** and financial risk;
3. Reduction of **radiological/contamination risk** to operators/public/environment;
4. Optimization of **material recycling**;
5. Better resources exploitation



## MAIN OPERATIONS

1. Preliminary radiological characterization
2. Decontamination
3. Dismantling and Confinement

### In-situ characterization



### In-lab characterization

Sample preparation and radiochemical separation





## POLITECNICO di MILANO DEPARTMENT OF ENERGY

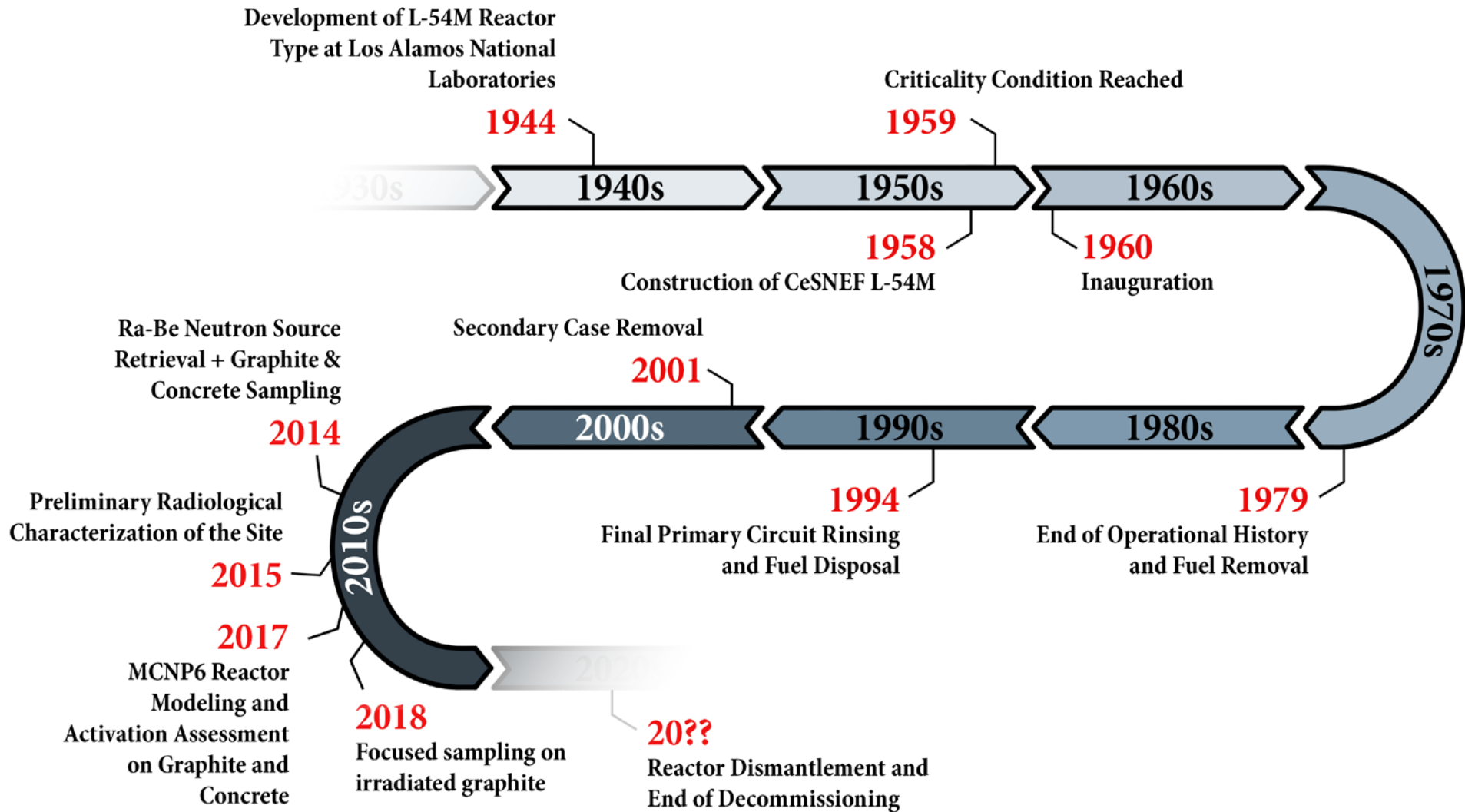
New B18 building with  
nuclear integrated labs

- Radiochemistry
- Radioprotection...



### L-54M Reactor

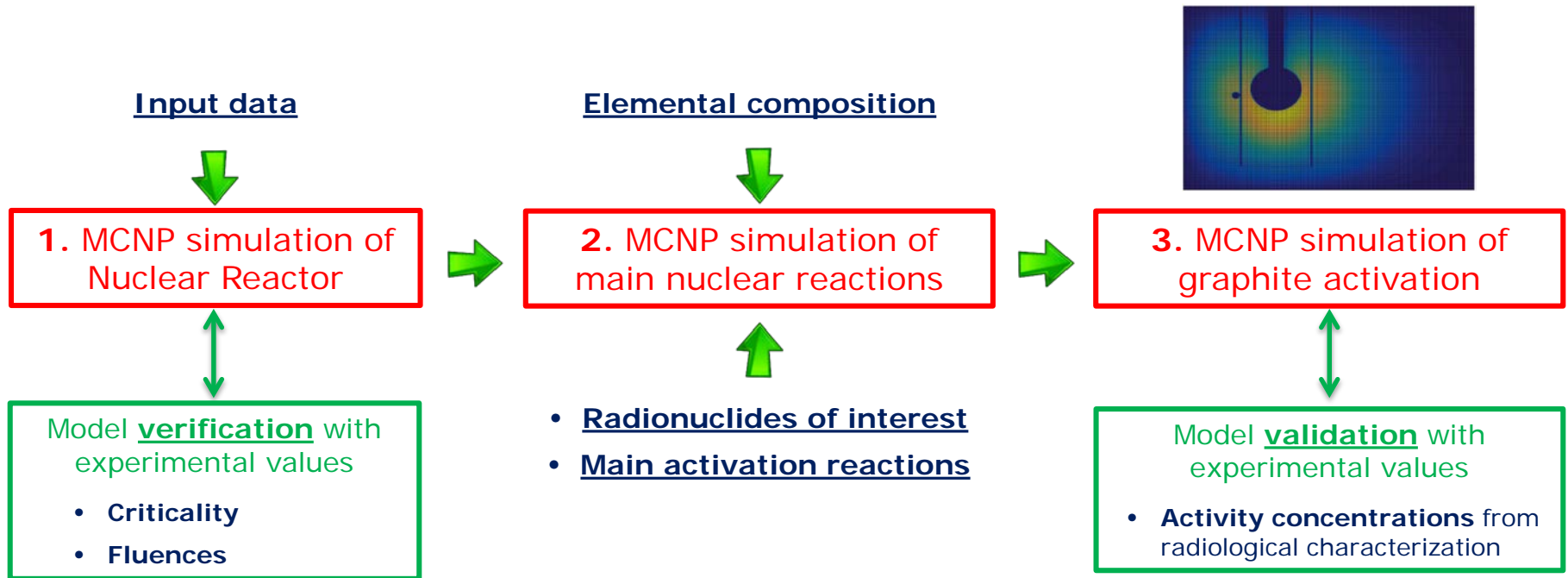


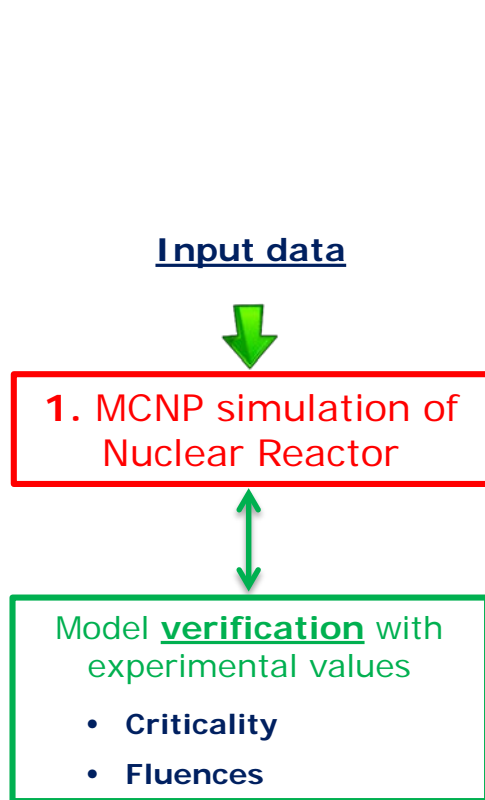


## Preliminary radiological characterization

**SCOPE:** 3D-computational assessment of neutron activated radionuclides distribution by means of **Monte Carlo N-Particles code (MCNP6)**

**PURPOSE:** cost savings and support to forthcoming characterization efforts





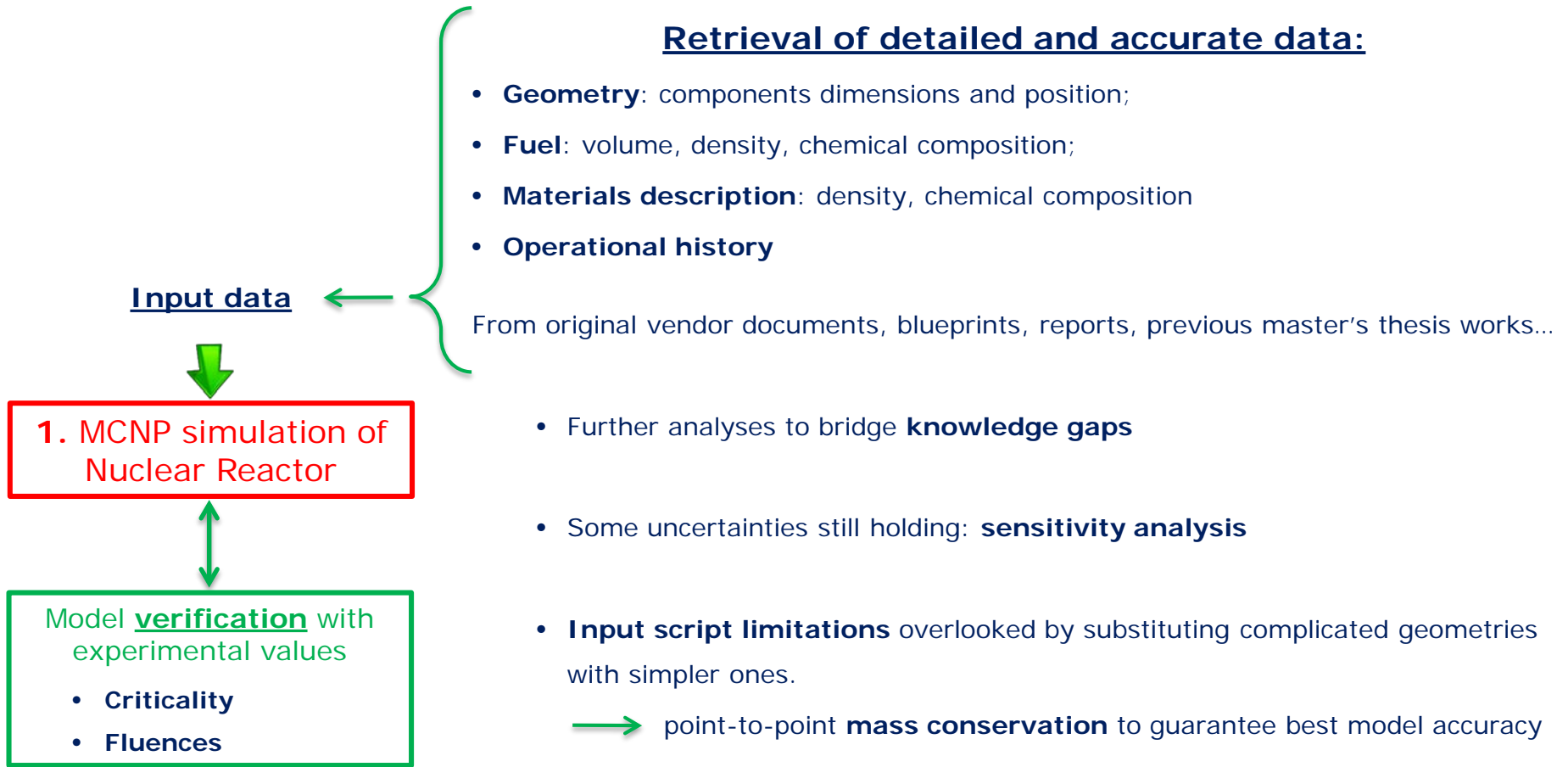
1. **MCNP** (Monte Carlo N-Particle, version 6) transport code has been chosen to develop the Radiochemistry and Monte Carlo integrated approach

- Well-established and validated;
- Reliable;
- Suitable to study thermal neutron diffusion and activation reaction rates;
- Possible coupling with CAD



T. Goorley et al. Nuclear Technology, 180(3):298 – 315, 2012

2. **ENDF** and **JEFF** cross-section libraries have been selected for the simulations





## Example: L-54M model

Input data

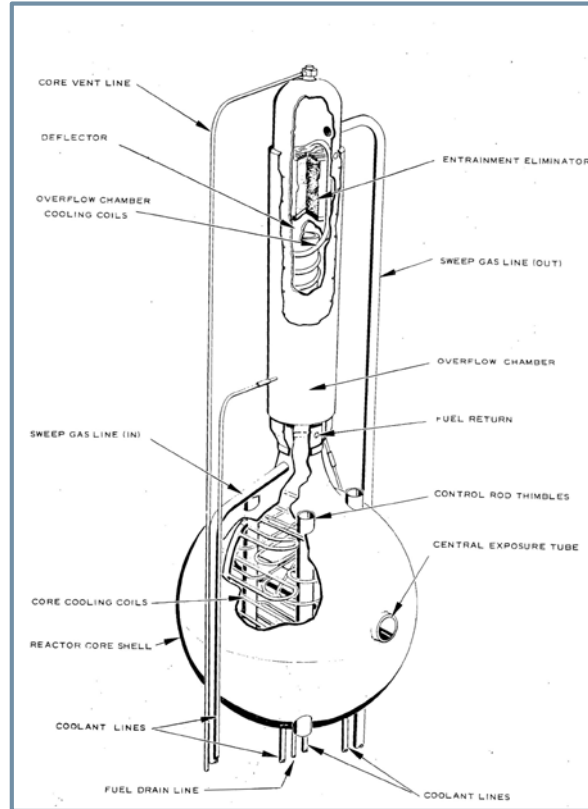


1. MCNP simulation of Nuclear Reactor

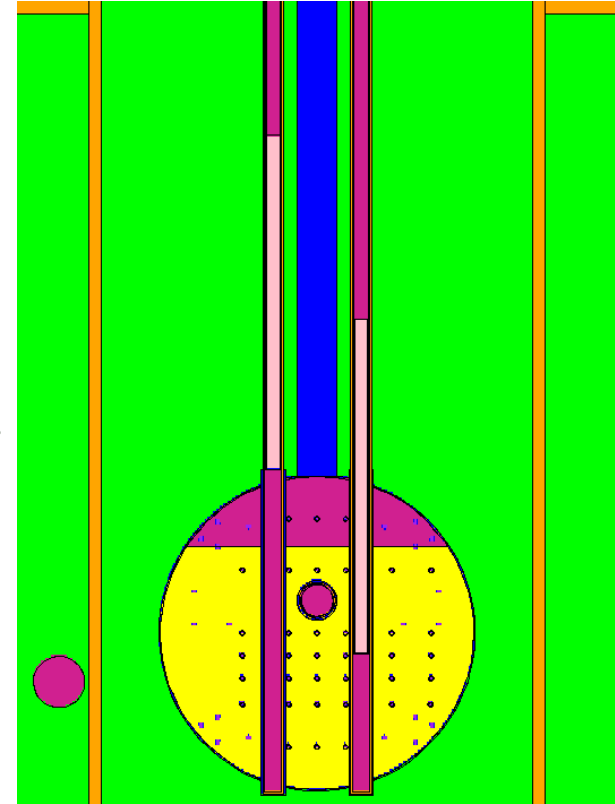


Model verification with experimental values

- Criticality
- Fluences



Reactor Core section



Implemented Core section

within IAEA collaborative research project on irradiated GRAPhite Processing Approaches (GRAPA)



Input data

1. MCNP simulation of Nuclear Reactor



Model verification with experimental values

- Criticality
- Fluences

Criticality verification

**KCODE card** has been used for criticality simulations to determine neutron multiplication factor ( $k_{eff}$ ) in a multiplying medium

Examples of criticality parameters:

- **Subcritical reactivity** → *control rods completely inserted*
- **Supercritical reactivity** → *control rods completely withdrawn*
- **Total rod worth** → *sum of Subcritical and Supercritical reactivity*
- **Control rods inventory** → *control rod inserted and others withdrawn*
- **Control rod calibration** → *control rod stepwisely moved from fully inserted to completely extracted position, with others withdrawn*

**TMP card** has been used with **makxsf code** to perform simulations at real working conditions (*i.e.* at non ambient temperature), thus considering temperature effect on cross sections and collision kinematics.

Fluences verification

**F2** and **F4 tallies** have been used to determine the flux of particles with determined Energy crossing a surface or volume respectively.

**F7 tally** has been used to normalize the flux on the energy produced by fission events in the core region

$$\Phi_{norm} [cm^{-2} \cdot J^{-1}] = \frac{F2 \text{ or } F4 [cm^{-2}]}{F7 [MeV \cdot g^{-1}] \cdot F7_{mass} \cdot (MeV \rightarrow J)} \xrightarrow{\cdot P[W]} \Phi_{norm} [cm^{-2} \cdot s^{-1}]$$

## Example: L-54M model verification

Input data

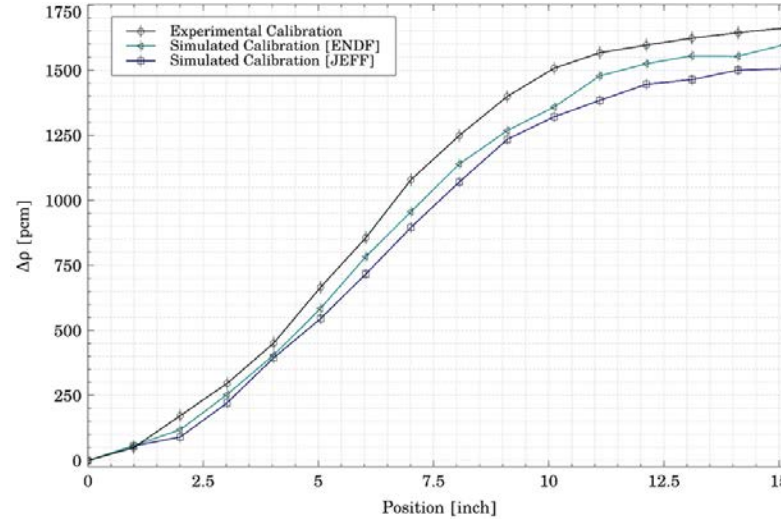


1. MCNP simulation of Nuclear Reactor



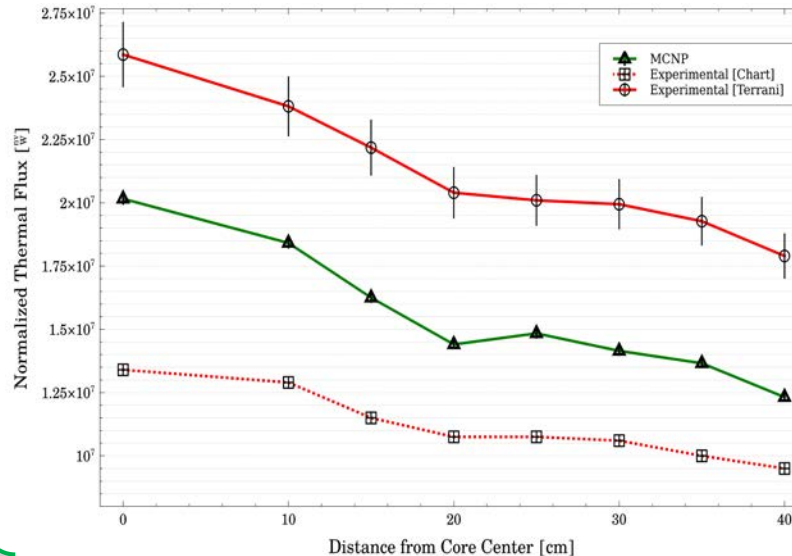
Model verification with experimental values

- Criticality
- Fluences



**Simulated vs Experimental control rod calibration**

4<sup>th</sup> control rod simulated moving it from the fully inserted position to the fully extracted one with all other rods withdrawn.



**Simulated vs Experimental thermal neutron flux in the central channel**

The flux is normalized per energy deposited by fission events

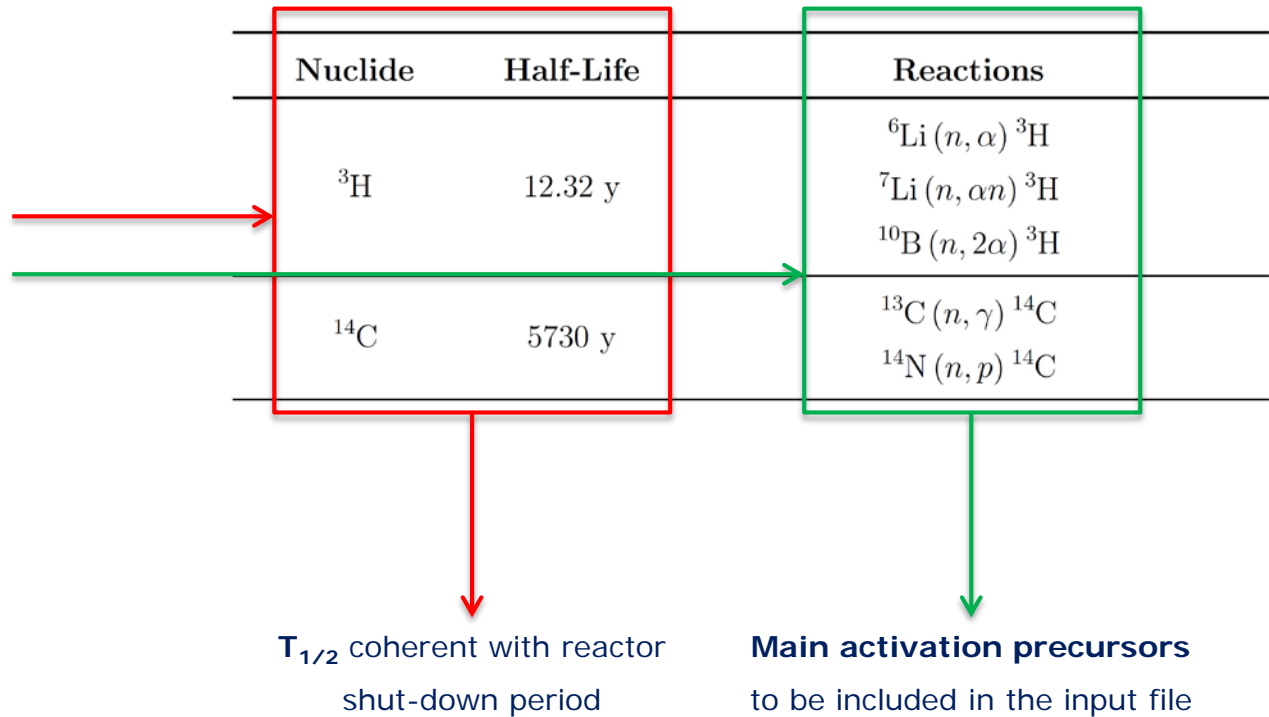
- Elemental composition



**2. MCNP simulation of main nuclear reactions**



- Radionuclides of interest
- Main activation reactions



- Elemental composition



2. MCNP simulation of main nuclear reactions



- Radionuclides of interest
- Main activation reactions

## Example: L-54M simulated activation reactions

- $T_{1/2} > 2y$  since L-54M shut-down in 1979;
- **Scarce information in the literature about AGOT composition:**  
**Activation precursors** to be determined in virgin graphite

Nuclide	Half-Life	Reactions
$^3\text{H}$	12.32 y	$^6\text{Li}(n, \alpha) ^3\text{H}$
		$^7\text{Li}(n, \alpha n) ^3\text{H}$
		$^{10}\text{B}(n, 2\alpha) ^3\text{H}$
$^{14}\text{C}$	5730 y	$^{13}\text{C}(n, \gamma) ^{14}\text{C}$
		$^{14}\text{N}(n, p) ^{14}\text{C}$
$^{36}\text{Cl}$	$3 \cdot 10^5$ y	$^{35}\text{Cl}(n, \gamma) ^{36}\text{Cl}$
		$^{39}\text{K}(n, \alpha) ^{36}\text{Cl}$
		$^{40}\text{Ca}(n, \alpha p) ^{36}\text{Cl}$
$^{41}\text{Ca}$	$10^5$ y	$^{40}\text{Ca}(n, \gamma) ^{41}\text{Ca}$
$^{55}\text{Fe}$	2.73 y	$^{54}\text{Fe}(n, \gamma) ^{55}\text{Fe}$
		$^{56}\text{Fe}(n, 2n) ^{55}\text{Fe}$
$^{59}\text{Ni}$	$7.6 \cdot 10^4$ y	$^{58}\text{Ni}(n, \gamma) ^{59}\text{Ni}$
		$^{60}\text{Ni}(n, 2n) ^{59}\text{Ni}$
$^{60}\text{Co}$	5.27 y	$^{59}\text{Co}(n, \gamma) ^{60}\text{Co}$

Nuclide	Half-Life	Reactions
$^{59}\text{Ni}$	$7.6 \cdot 10^4$ y	$^{58}\text{Ni}(n, \gamma) ^{59}\text{Ni}$
		$^{60}\text{Ni}(n, 2n) ^{59}\text{Ni}$
$^{60}\text{Co}$	5.27 y	$^{59}\text{Co}(n, \gamma) ^{60}\text{Co}$
$^{63}\text{Ni}$	100 y	$^{63}\text{Cu}(n, p) ^{63}\text{Ni}$
		$^{62}\text{Ni}(n, \gamma) ^{63}\text{Ni}$
$^{93}\text{Mo}$	4000 y	$^{92}\text{Mo}(n, \gamma) ^{93}\text{Mo}$
$^{94}\text{Nb}$	$2.03 \cdot 10^4$ y	$^{93}\text{Nb}(n, \gamma) ^{94}\text{Nb}$
$^{99}\text{Tc}$	$2.111 \cdot 10^5$ y	$^{98}\text{Mo}(n, \gamma) ^{99}\text{Mo} \xrightarrow[2.74 \text{ d}]{\beta^-} ^{99m}\text{Tc} \xrightarrow[6.01 \text{ h}]{\text{IT}} ^{99}\text{Tc}$
$^{108m}\text{Ag}$	418 y	$^{107}\text{Ag}(n, \gamma) ^{108m}\text{Ag}$
$^{152}\text{Eu}$	13.54 y	$^{151}\text{Eu}(n, \gamma) ^{152}\text{Eu}$
$^{154}\text{Eu}$	8.59 y	$^{153}\text{Eu}(n, \gamma) ^{154}\text{Eu}$
$^{233}\text{U}$	$1.592 \cdot 10^5$ y	$^{232}\text{Th}(n, \gamma) ^{233}\text{Th} \xrightarrow[21.8 \text{ m}]{\beta^-} ^{233}\text{Pa} \xrightarrow[26.97 \text{ d}]{\beta^-} ^{233}\text{U}$
$^{239}\text{Pu}$	24110 y	$^{238}\text{U}(n, \gamma) ^{239}\text{U} \xrightarrow[23.5 \text{ m}]{\beta^-} ^{239}\text{Np} \xrightarrow[2.36 \text{ d}]{\beta^-} ^{239}\text{Pu}$
fission products	-	$^{235}\text{U}(n, f); ^{238}\text{U}(n, f); ^{232}\text{Th}(n, f)$

• Elemental composition



Development of dedicated ICP-MS procedure



2. MCNP simulation of main nuclear reactions



- i. **Oxidation** of graphite powder in a muffle at 650°C for 24 h;
- ii. **Multistep digestion** of ashes by mixture of acids (HNO<sub>3</sub>, HCl, HF);
- iii. **Dilution** by 1% HNO<sub>3</sub>;
- iv. **ICP-MS** analysis.

- Radionuclides of interest
- Main activation reactions

Element	ppm
Li	0.0194 ± 2.7%
Al	1.18 ± 2.9%
K	1.22 ± 11%
Ca	7.97 ± 9.8%
Ti	0.622 ± 4.8%
V	22.1 ± 1.1%
Fe	2.81 ± 3.2%
Ni	1.00 ± 1.3%
Cu	0.208 ± 1.6%
Mo	0.144 ± 1.3%
Ba	0.0595 ± 1.9%

Element	ppb
B	< LOQ (13.9 ppb)
Co	9.3 ± 1.5%
Nb	5.0 ± 8.0%
Ag	< LOQ (0.71 ppb)
Cs	0.47 ± 4.8%
La	2.8 ± 2.9%
Ce	3.2 ± 4.6%
Nd	0.38 ± 29%
Eu	0.55 ± 4.0%
Th	886 ppt ± 5.0 %
U	66 ppt ± 33%



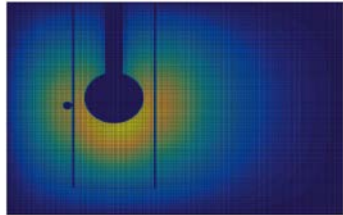
Under definition collaboration to determine light and volatile elements (such as Li, B, N, Cl) by **Prompt-Gamma Neutron Activation Analysis (PGNAA)**.

The **Reaction Rate** could be obtained by:

$$RR[\text{atom} \cdot \text{cm}^{-3} \cdot \text{J}^{-1}] = C \cdot \iiint d^3r \int dE \cdot \Phi_{\text{norm}}(E, \vec{r}) \cdot \Sigma(E)$$

where:

- the **precursor nuclide density**,  $C[\text{atom} \cdot \text{barn}^{-1} \cdot \text{cm}^{-1}]$ , is a normalization factor;
- the **cross-sections** of activation reaction,  $\Sigma[\text{barn}]$ , is a response function.



$$A[\text{Bq/g}] = \frac{\lambda [\text{s}^{-1}]}{\rho[\text{g} \cdot \text{cm}^{-3}]} \sum_{\text{month}} RR[\text{atoms} \cdot \text{cm}^{-3} \cdot \text{J}^{-1}] * \text{Energy}(i)[\text{J}] * e^{-\lambda \Delta t(i)}$$

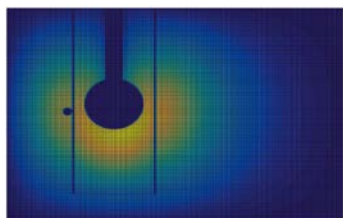
Decay from production

Monthly energy production

3. MCNP simulation of graphite activation

Model **validation** with experimental values

- **Activity concentrations** from radiological characterization



### 3. MCNP simulation of graphite activation



Model **validation** with experimental values

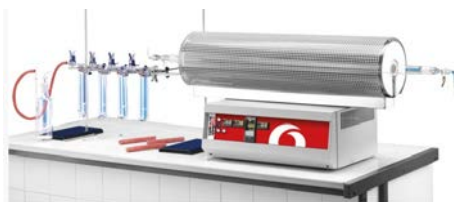
- **Activity concentrations** from radiological characterization



## Example: L-54M pre-characterization



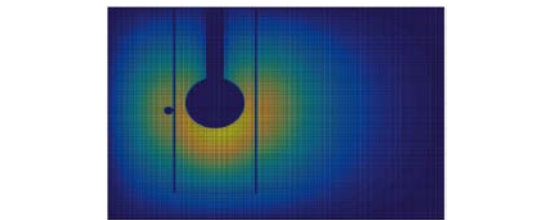
- Extraction of the graphite block;
- Drilling of graphite samples at several radial distances;



- **Gamma spectrometry;**
- Sample pre-treatment by **pyrolysis** and **<sup>3</sup>H** and **<sup>14</sup>C** trapping for following **Liquid Scintillation Counting** quantification

Radionuclide	0 cm	80 cm	120 cm
<sup>3</sup> H [Bq·g <sup>-1</sup> ]	9170 ± 597	811 ± 54	51.5 ± 3.4
<sup>14</sup> C [Bq·g <sup>-1</sup> ]	370 ± 25	37.5 ± 2.6	4.1 ± 0.3
<sup>152</sup> Eu [Bq·g <sup>-1</sup> ]	253.9 ± 18.8	34.3 ± 2.3	4.1 ± 0.3





3. MCNP simulation of graphite activation



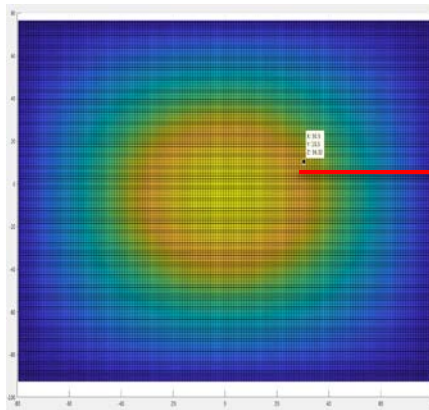
Model **validation** with experimental values

- **Activity concentrations** from radiological characterization



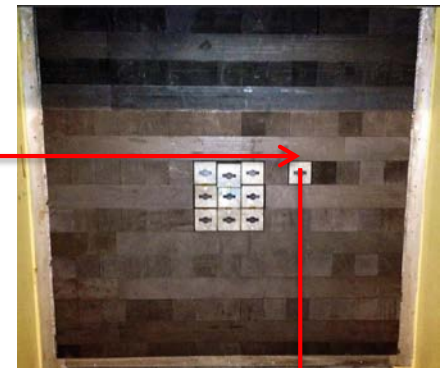
## Example: L-54M model validation

<sup>152</sup>Eu neutron activation (MCNP6)  
(about 0.6 ppb Eu in virgin graphite)



2D slice at 80 cm

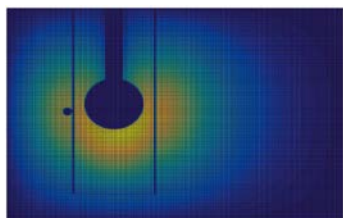
Comparison with few experimental data available



Radial distance from the core

0 cm                      80 cm                      120 cm

<sup>152</sup> Eu [Bq·g <sup>-1</sup> ]	0 cm	80 cm	120 cm
MCNP Simulation	207 ± 1	21.5 ± 0.2	1.8 ± 0.1
Experiment	253.9 ± 18.8	34.3 ± 2.3	4.1 ± 0.3



3. MCNP simulation of graphite activation



Model **validation** with experimental values

- **Activity concentrations** from radiological characterization



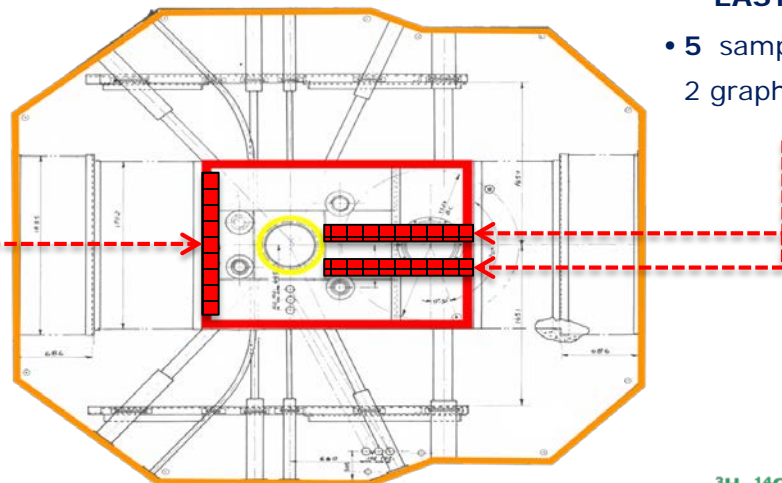
### Example: further L-54M model validation

**WEST side**

- 7 samples on external graphite surface

**EAST side**

- 5 samples along 2 graphite rods



- **$\gamma$  emitting radionuclides by HPGe**

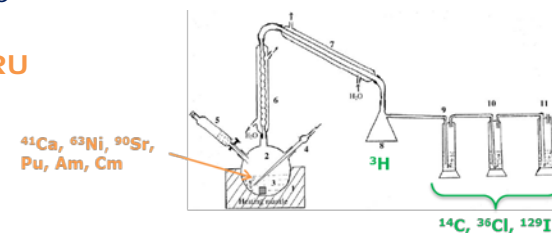
- **Pure  $\beta$  and  $\alpha$  emitting radionuclides**

- $^3\text{H}$ ,  $^{14}\text{C}$ ,  $^{36}\text{Cl}$ ,  $^{129}\text{I}$  (volatiles)

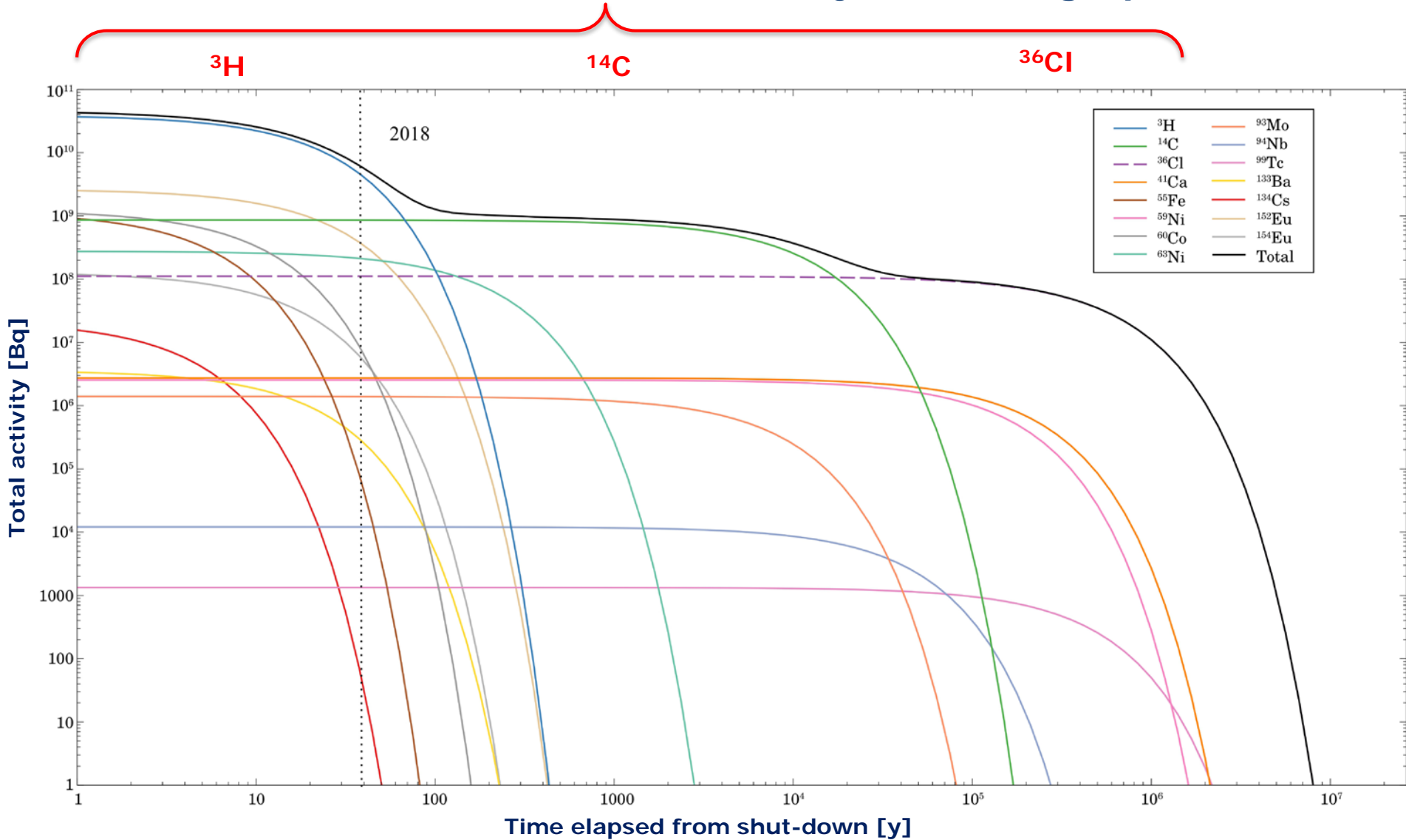
Pyrolysis + radiochemical separation + LSC

- $^{41}\text{Ca}$ ,  $^{63}\text{Ni}$ ,  $^{90}\text{Sr}$ , TRU

Acid digestion +  
radiochemical separation +  
LSC/alpha spectrometry



## Main contributors to Total Activity of L-54M graphite



## 3D-Model of Reactor Graphite Activation

1. The integrated computational approach prompted to be a **valid support to radiological characterization campaign**

In fact, L-54M neutronic model

1. **proficiently developed**,
2. **verified** by comparing simulated and experimental criticality and fluences data;
3. **validated** by comparing simulated and experimental radiometric data.

2. The approach is **general and applicable to other nuclear facilities**

### Future works on L-54M reactor model

- **Light and volatile impurities** determination in virgin graphite by PGNA and NAA.
- **Ultimate model validation** by additional radiometrical analyses on recently collected graphite samples:  $^3\text{H}$ ,  $^{14}\text{C}$ ,  $^{36}\text{Cl}$ ,  $^{41}\text{Ca}$ ,  $^{63}\text{Ni}$ ...



