



Powerful energy
recovery linac experiments

Preliminary studies : Quadrupoles & Arc - Splitter dipoles

P.A THONET (CERN) - C. VALLERAND (LAL)

27th June 2018



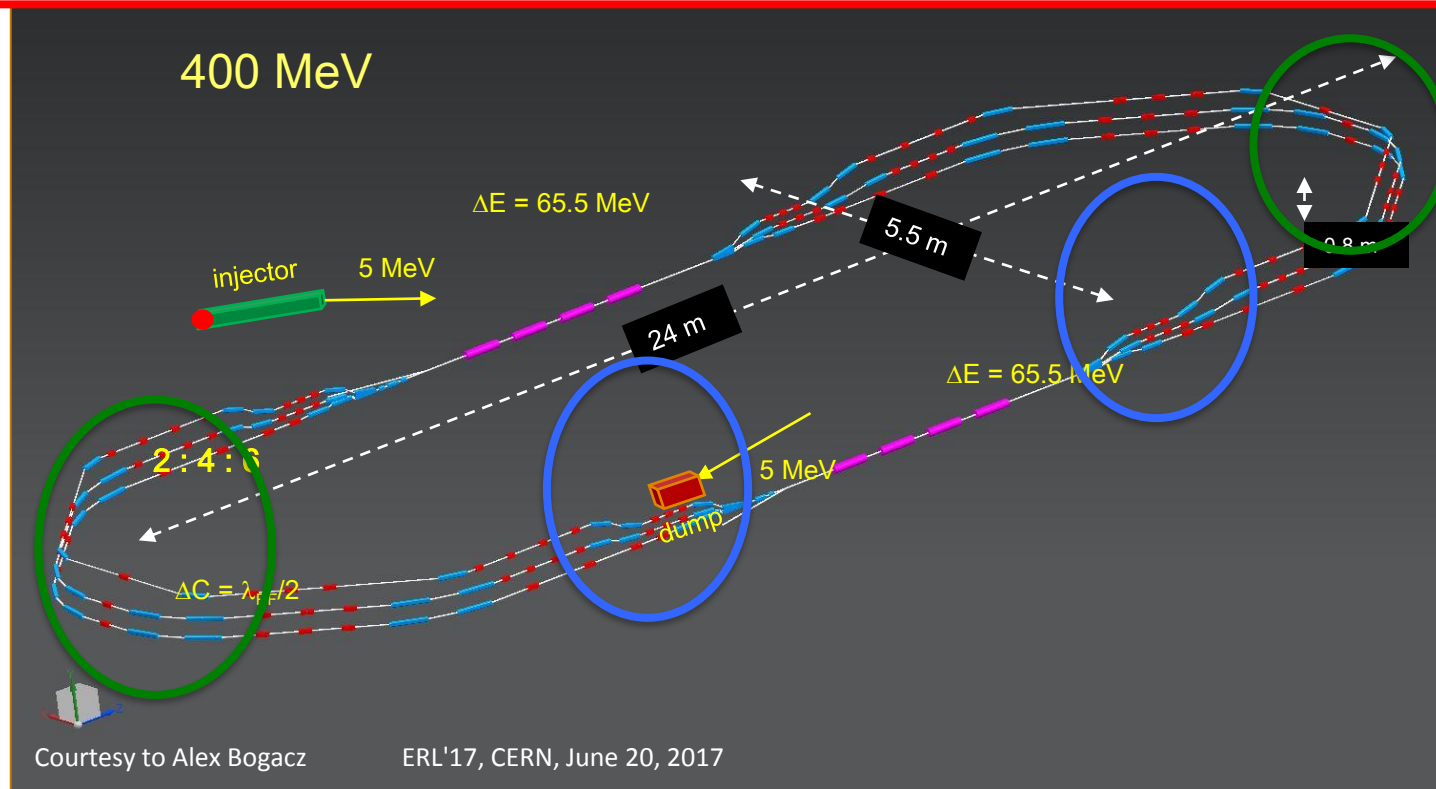
- **Summary of magnet inventory**
- **Arc region :**
 - **Quadrupole magnets :**
 - Requirements & constraints
 - 3D design
 - **Arc bending magnets :**
 - Requirements & constraints
 - 3D design
- **Spreader region :**
 - **Splitter magnet**
 - Requirements & constraints
 - 3D preliminary design
- **Points to be highlighted**

Summary of magnet inventory

- 6 arcs, one each for 80, 155, 230, 305, 380, 455 MeV beams.
- Each arc contains : 4 dipoles, powered in series within that arc
114 quadrupoles, which are powered individually
Number of sextupoles and correctors to be defined
- 4 splitters and 46 spreader/recombiner dipoles are placed at each end of the linacs in order to provide/suppress the vertical separation between the beams at different energies.

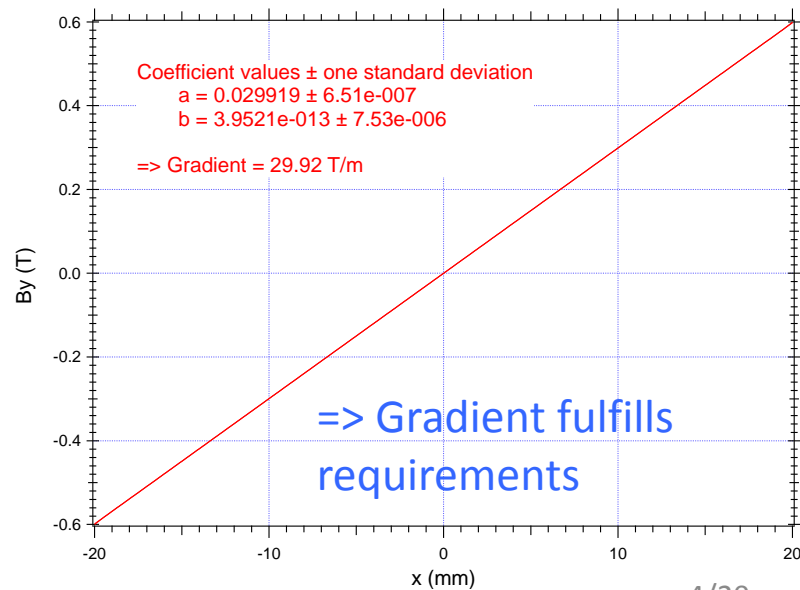
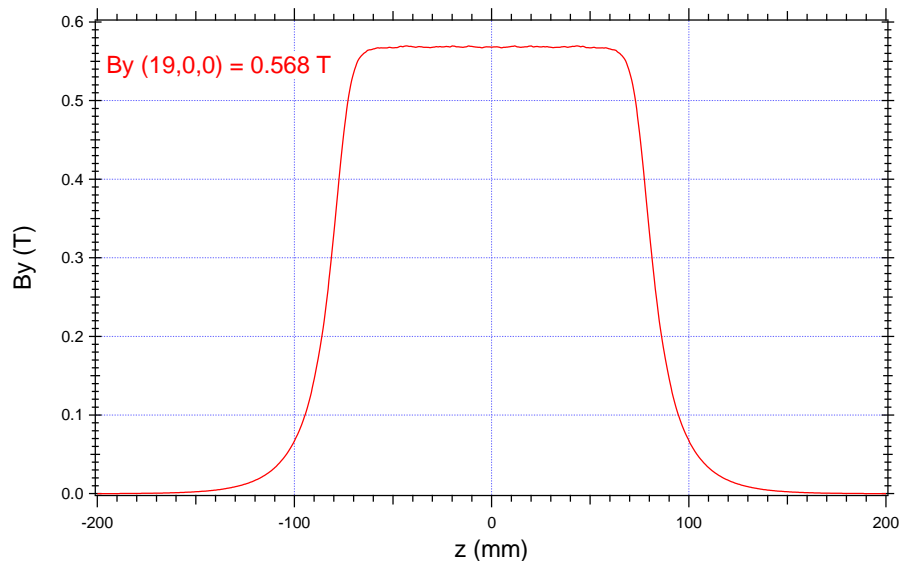
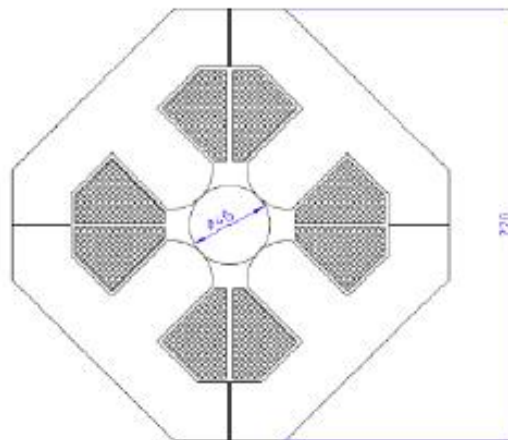
168 magnets without including sextupoles with correctors

=> Need to optimize design of magnets by considering cost and dimensions as a key parameter

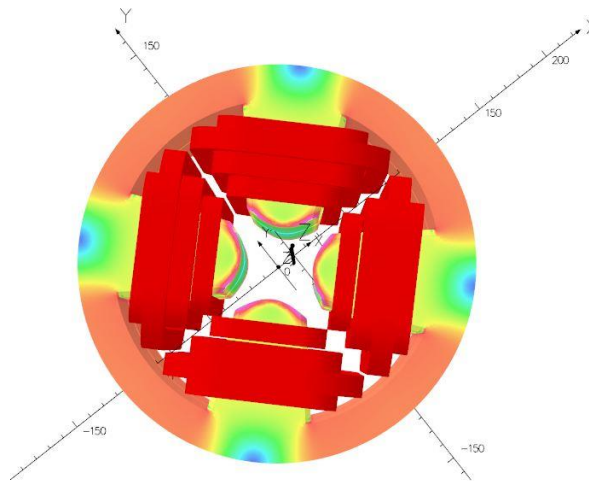
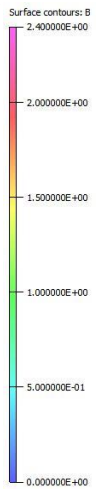
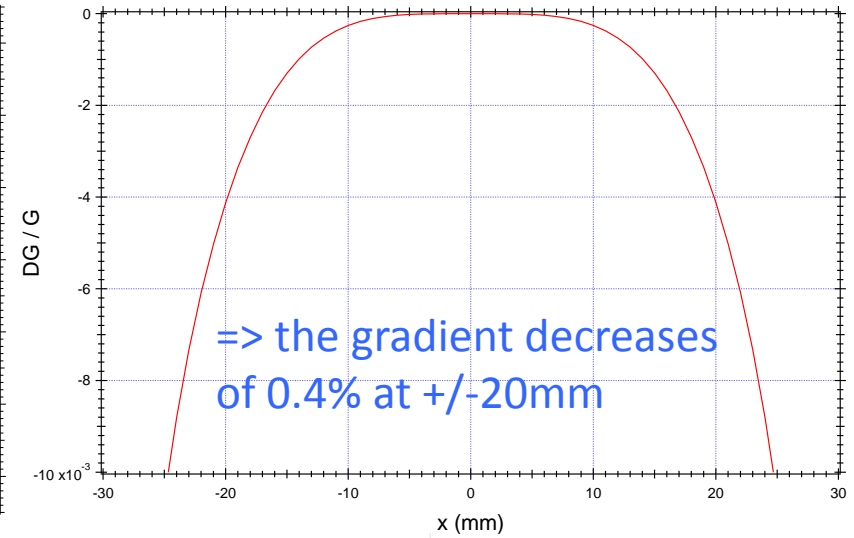
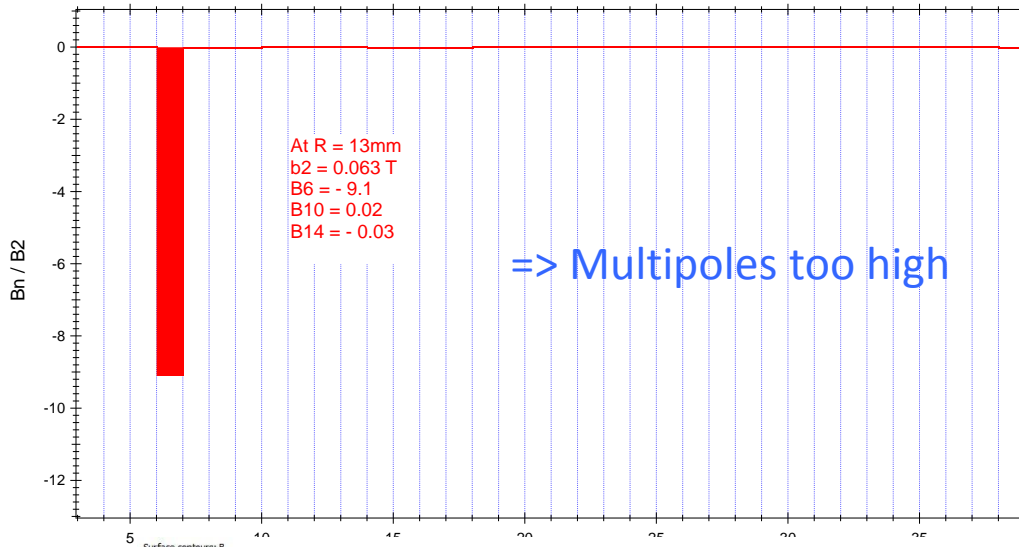


Features of quadrupoles magnets

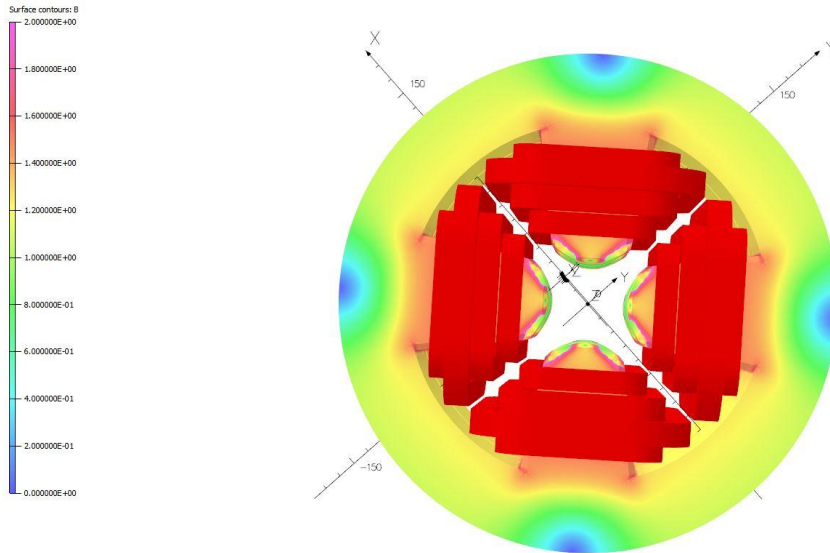
Quantity	114 + 1 (pre-serie)
Magnetic length	100 - 200 mm
Main gradient G_0	30T/m
Gap	40 mm
Good field region	+/- 20mm
Beam energy	From 50 to 400 MeV



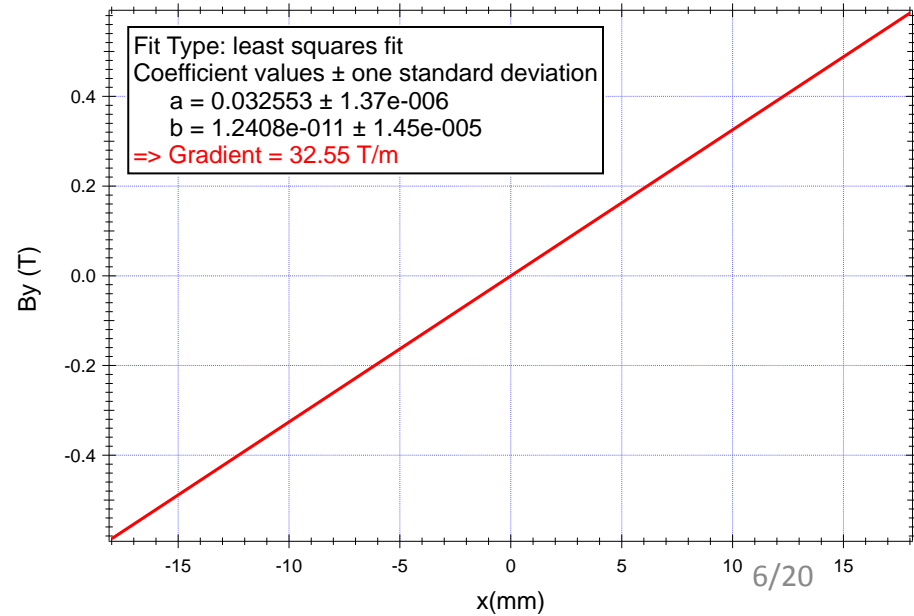
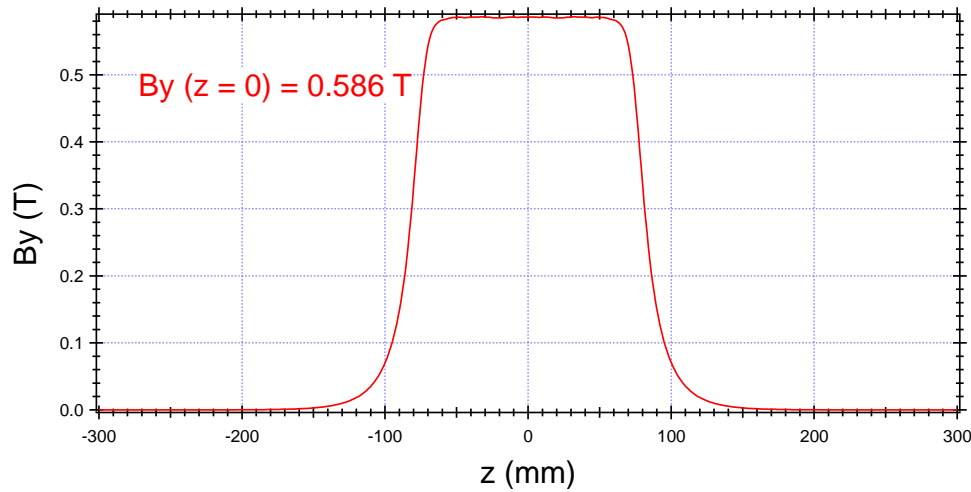
• **BUT**

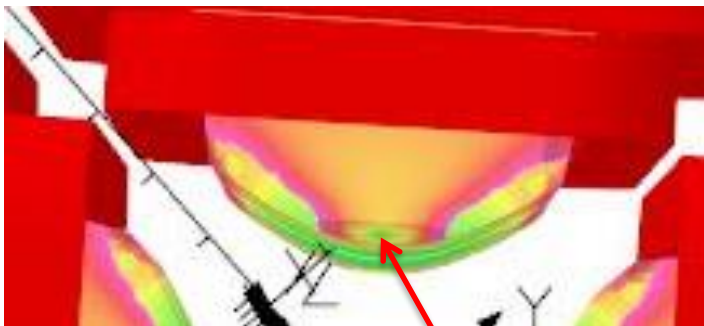


⇒ Iron totally saturated

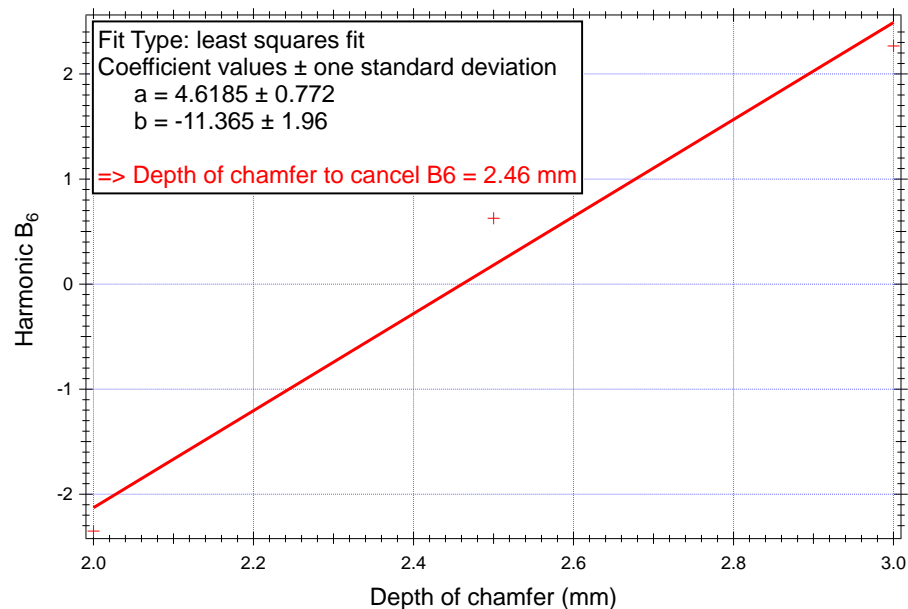


Opera
Simulation Software
CERN/EP/ST





Study of the chamfer deepness at the entrance/exit of the pole



	Harmonic @ 13 mm
B_6/b_2	$0.63 \cdot 10^{-4}$
B_{10}/b_2	$-0.45 \cdot 10^{-4}$
B_{14}/b_2	$-0.05 \cdot 10^{-4}$
B_{18}/b_2	$-0.003 \cdot 10^{-4}$

Conclusion :

Quadrupoles are designed and optimized :

- $B_y(0) = 0.586$ T
- Gradient = 32.55 T/m > 30 T/m
- Harmonic content $\ll 5 \cdot 10^{-4}$

IF

diameter can be 250 mm instead of 220mm

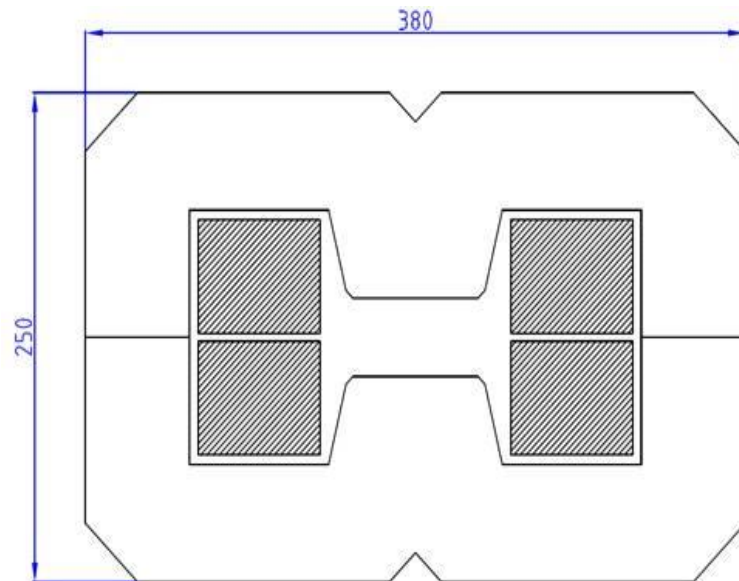
Arc bending magnets : Requirements & constraints

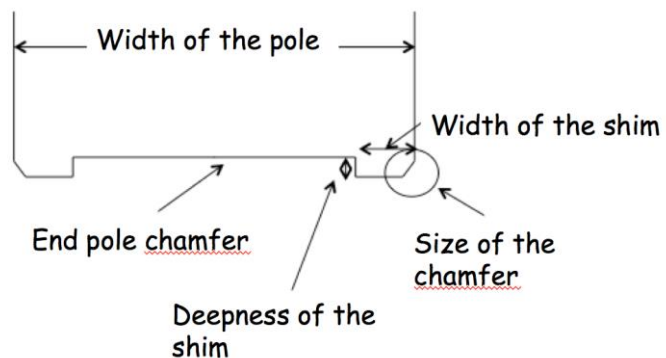
- Iron-dominated resistive magnets preferred for improving tunability
- Engineering current density of 7-8 A/mm²
- H design to reduce the height of magnet for stacking
- Homogeneous field as low as possible due to the use of one power supply by a series of converters, the vacuum system and cooling as well as a common structure with a 45° deflection

Features of arc bending magnet

Quantity	(pre-serie)	
Deflection angle	45°	
Magnet length	1192 mm	596 mm
Operating field B ₀	1.25 - 1.3 T	1.25 - 1.3 T
Gap	40 mm	40 mm
Good field region	+/- 20mm	+/- 20mm
Mechanical length	936 mm	468 mm
Current max.	Not defined	Not defined
Beam energy	From 305 to 455 MeV	From 80 MeV to 230 MeV

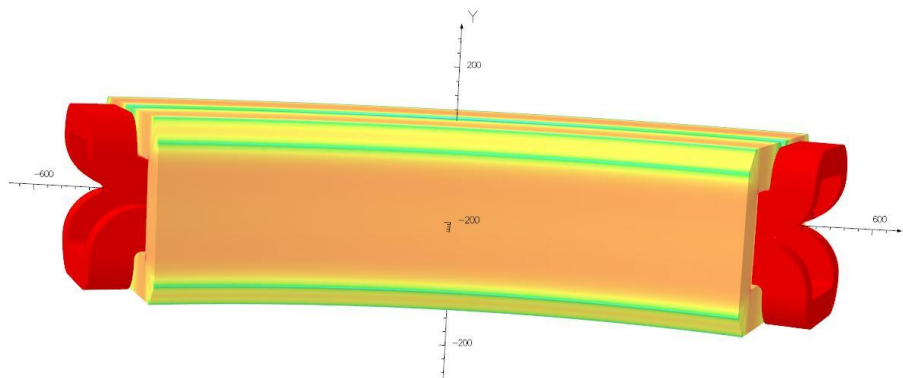
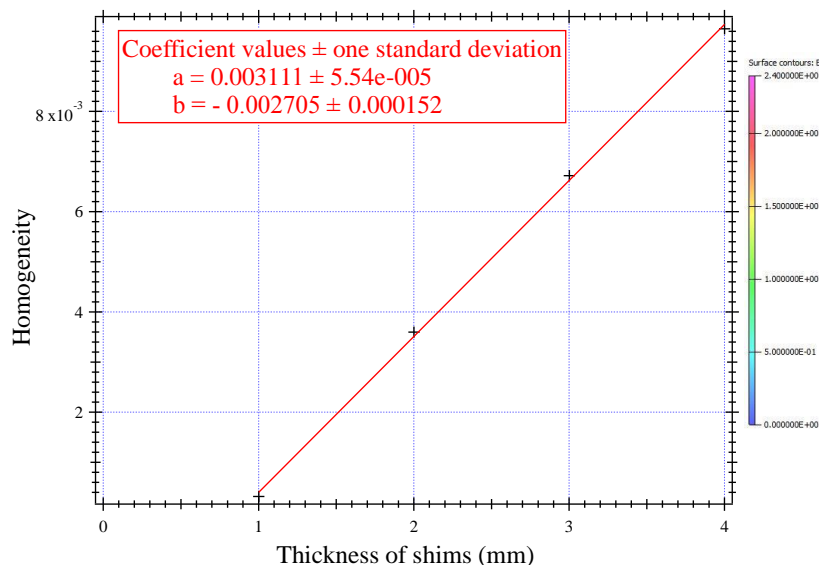
Challenge to highlight : Very compact bending magnet while keeping a reasonable current density for 6 arcs and using the same structure for Arc 1 up to 3 and for Arc 4 up to 6.



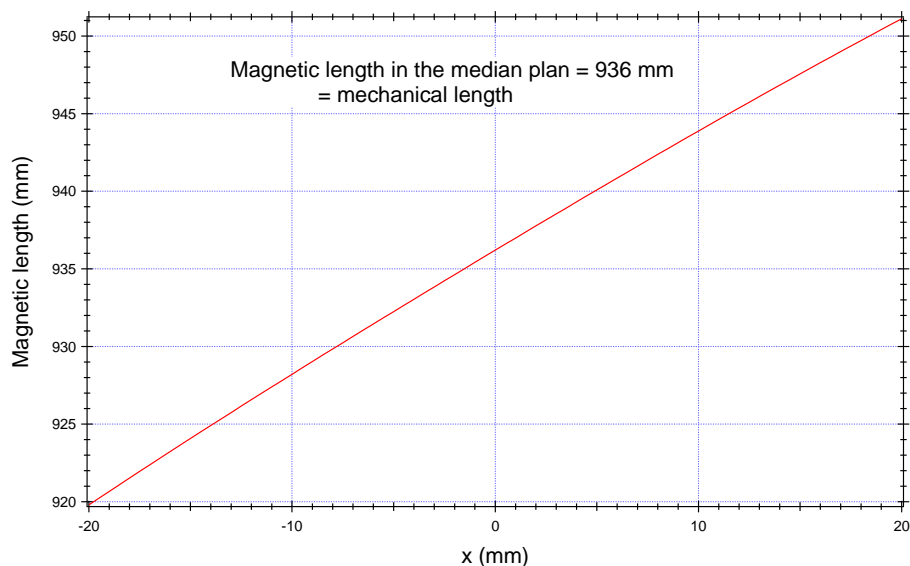
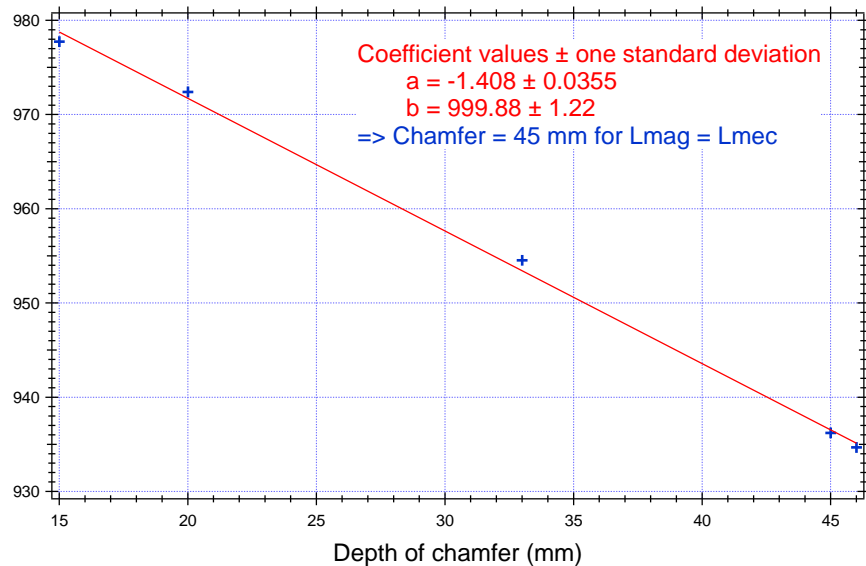
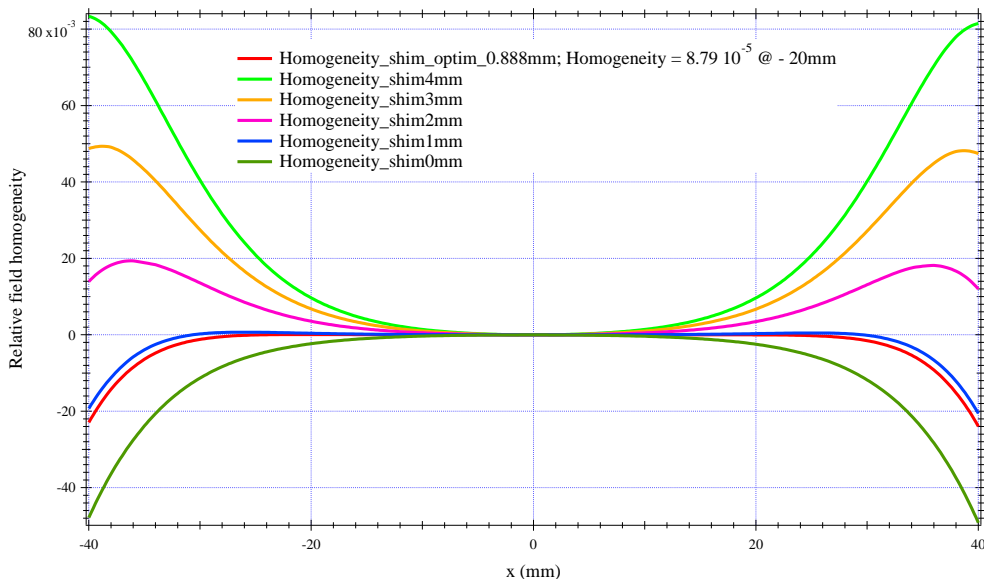


Improvements :

- Enlargement of the pole base width (50mm instead of 40mm) to desaturate iron
- Add-on of shims (10mm) to improve the homogeneity of field
- Height of coils allowing superposition
- Use of bedstead coils to get $j < 7 \text{ A/mm}^2$



Simulation results with 4 thickness of shims to obtain a field homogeneity of 5.10^{-4} expected
By fitting, we obtained a thickness of 0.888mm



Conclusion in January :

Magnetic field = 1.26 T

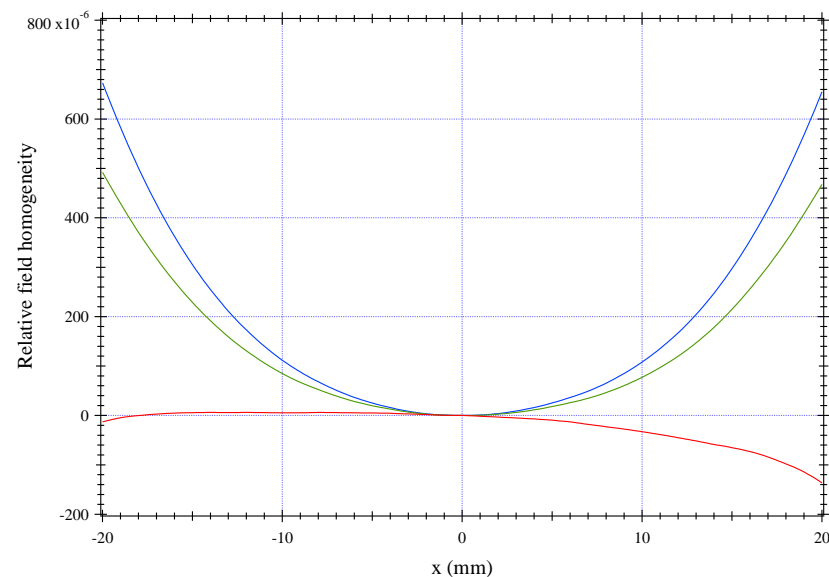
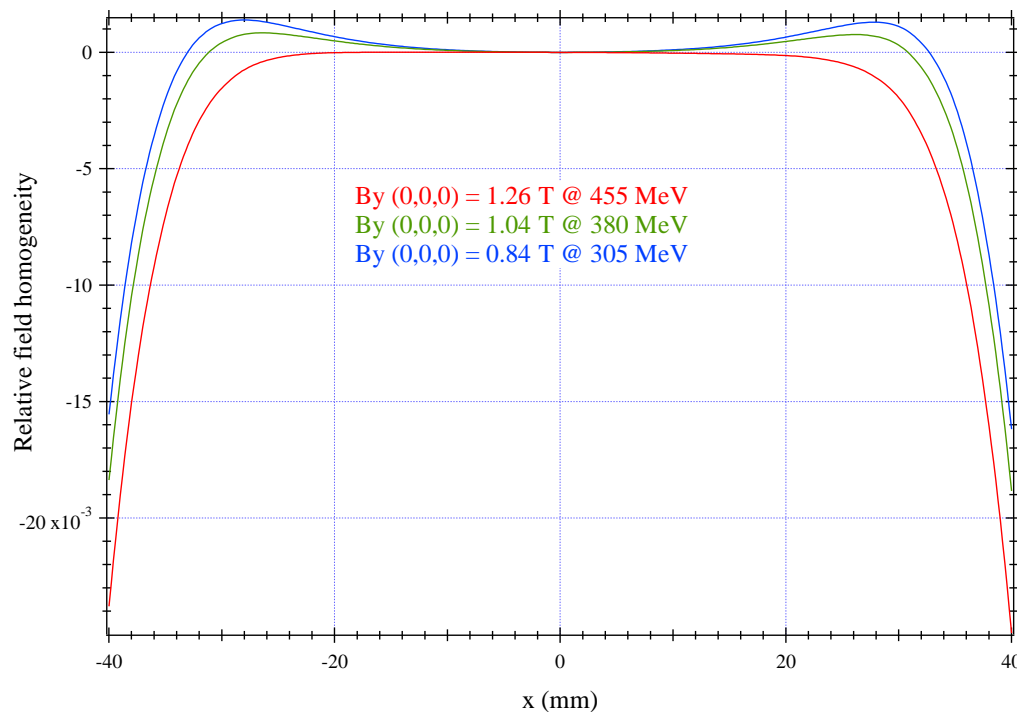
Homogeneity $8.8 \cdot 10^{-5}$ with a shim 0.88 mm $< 5 \cdot 10^{-4}$

Magnetic length = Mechanical length = 936mm

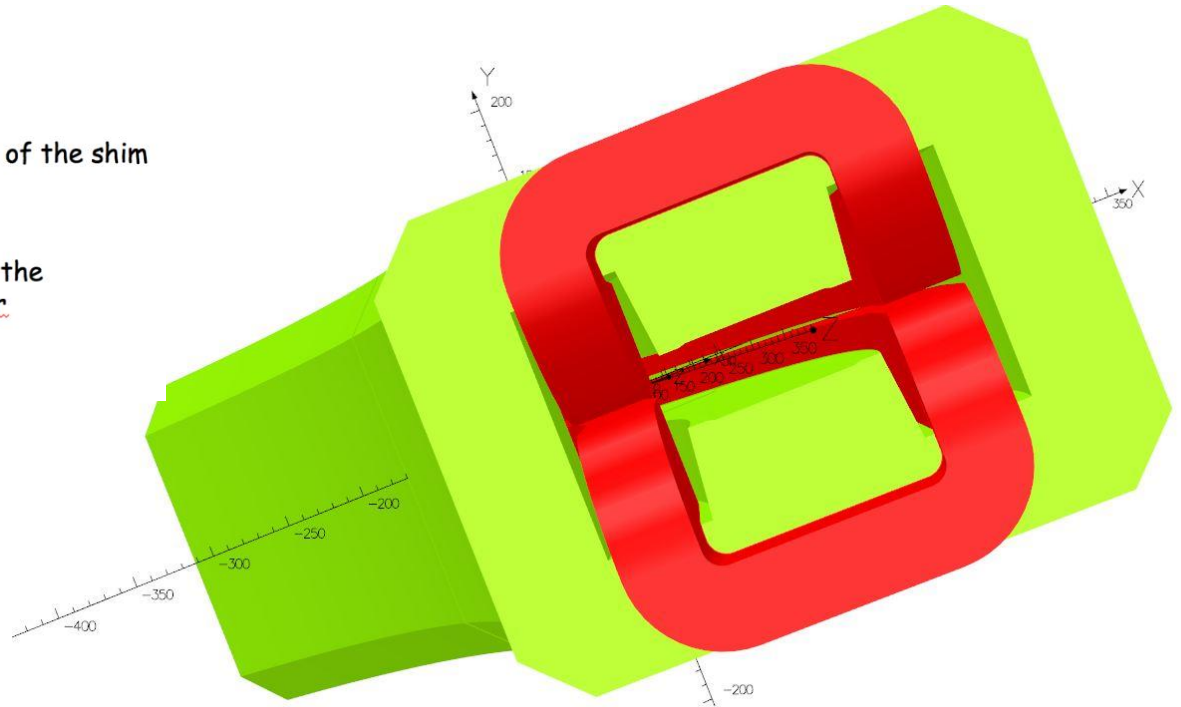
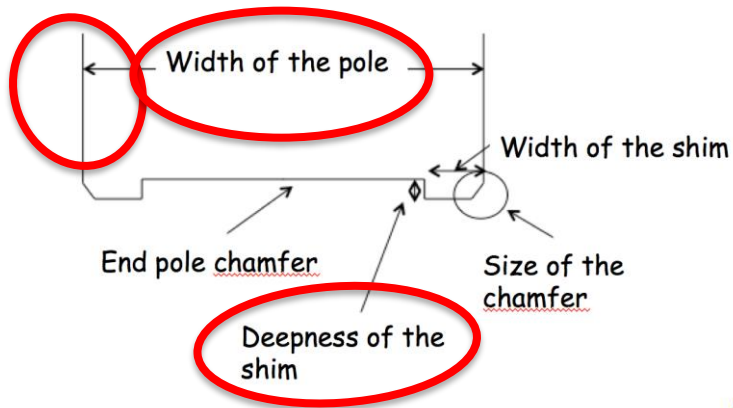
$J = 5.5 \text{ A/mm}^2$

\Rightarrow Feasibility has been proved for using same structure for long radius

- BUT** : Homogeneity of $B_y(x)$ for 3 last arcs with the shim optimized for 455 MeV



Shim optimized for 455 MeV doesn't match for others energies with this design of magnet.
 \Rightarrow Need to adjust shims for each beam energy or change the design to use a same shim.



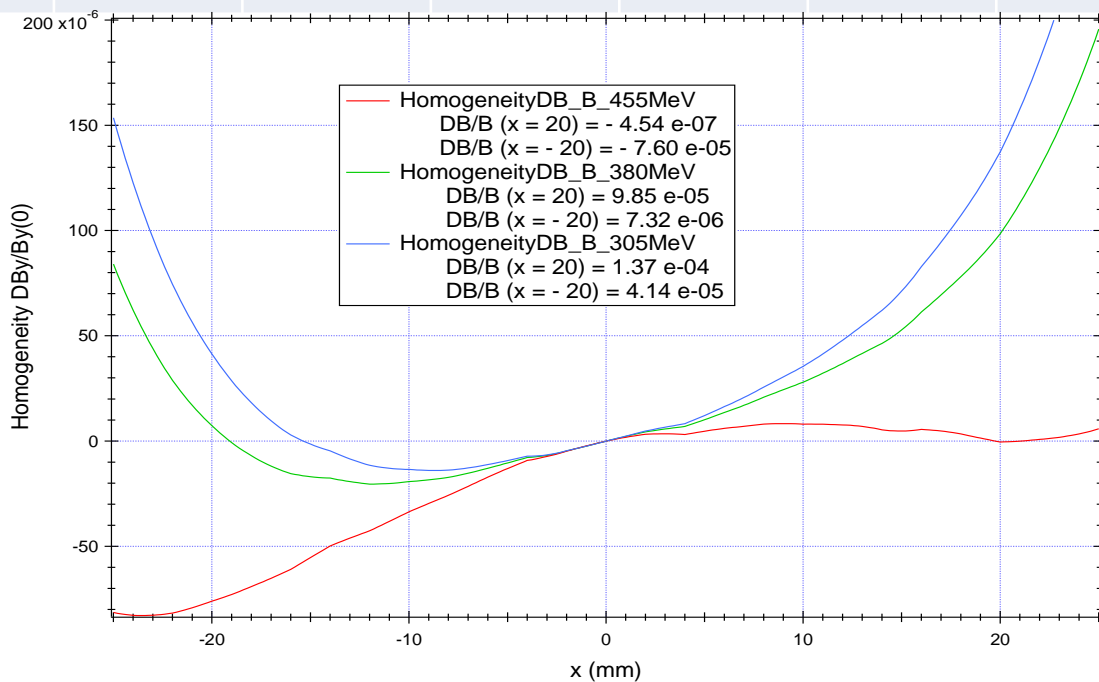
9 cases have been carried out for 3 energies 305 – 380 - 455 MeV :

- Width of pole : 90 – 105 – 120 mm**
- Deepness of the shim : 1 – 2 – 3 mm**

Optimisation for keeping same shims

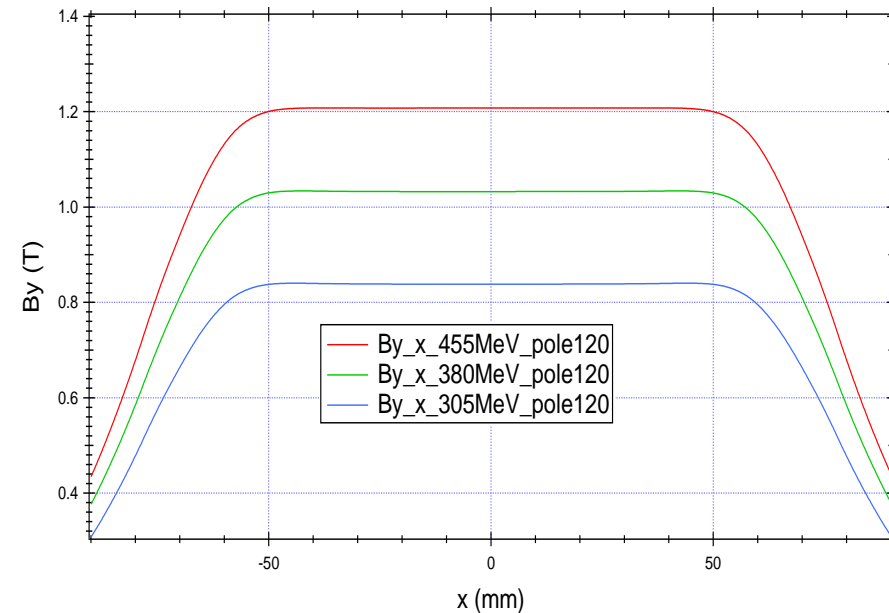
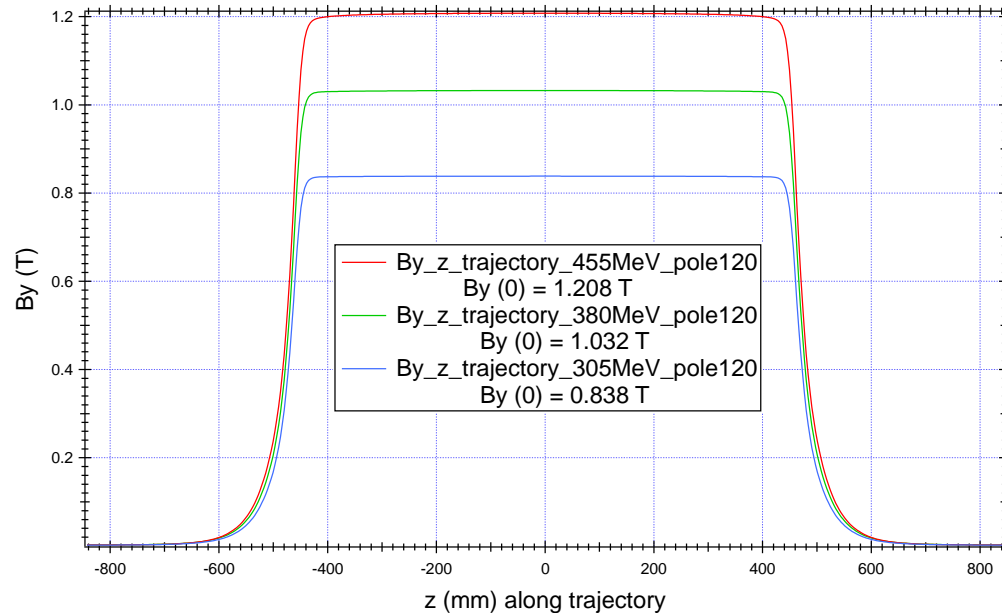
- Results for 3 energies of homogeneity results vs depth shim

Depth shim (mm)	Homogeneity ($\cdot 10^{-4}$) with a pole width 90 mm @ 20mm			Homogeneity ($\cdot 10^{-4}$) with a Pole width 105 mm @ 20 mm			Homogeneity($\cdot 10^{-4}$) with a pole width 120 mm @ 20 mm		
	305 MeV	380 MeV	455 MeV	305 MeV	380 MeV	455 MeV	305 MeV	380 MeV	455 MeV
1	9.2	6.5	-2.5	3.5	2.5	-8	1.4	1	0
2	45	40.5	26	15	13	9	5	4.4	3
3	86	78	53	28	26	18	9	8	6



With a shim of 1 mm, Homogeneity $\ll 5 \cdot 10^{-4}$ for 3 higher energies

- By(z) along the trajectory and By (x) for R 1192 mm with a shim =1 mm

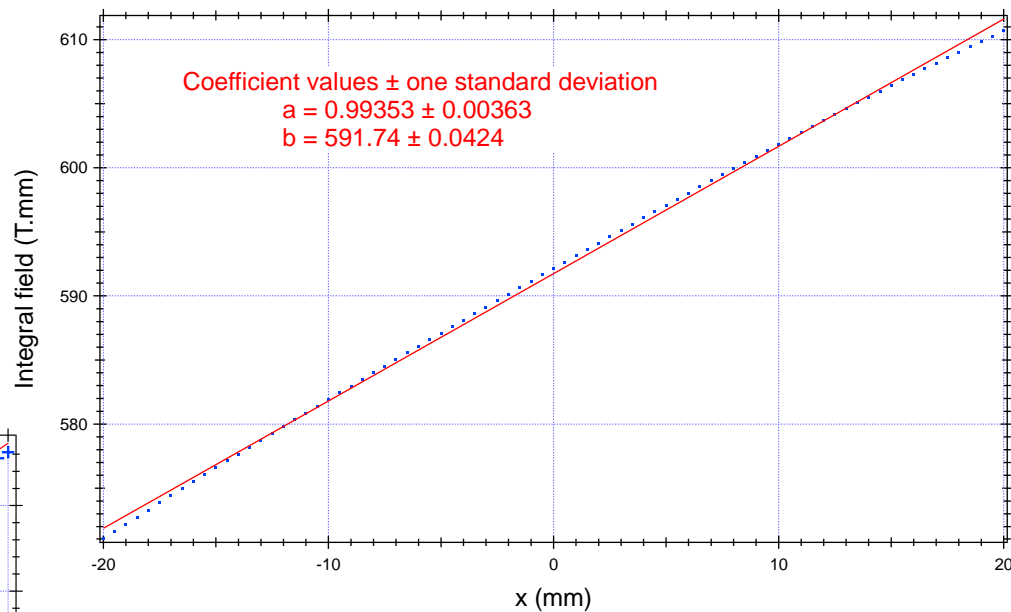
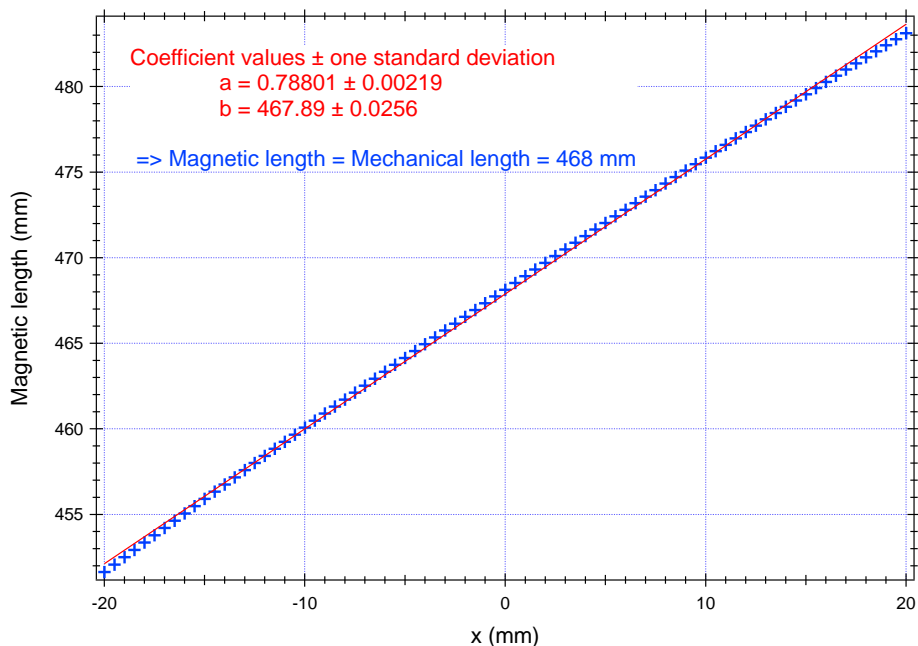
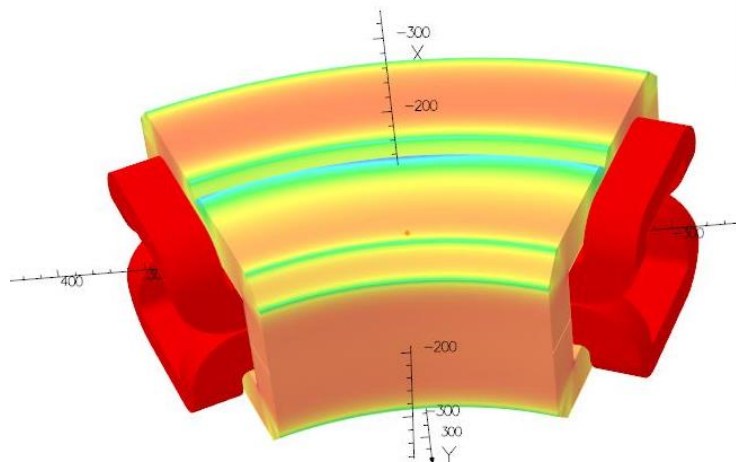


Conclusion :

Shim is optimized for 3 energies to get a field homogeneity lower than $5 \cdot 10^{-4}$
Magnetic design is done for the arc bending magnet R1192 mm

Same way of design for R=1192 mm model.

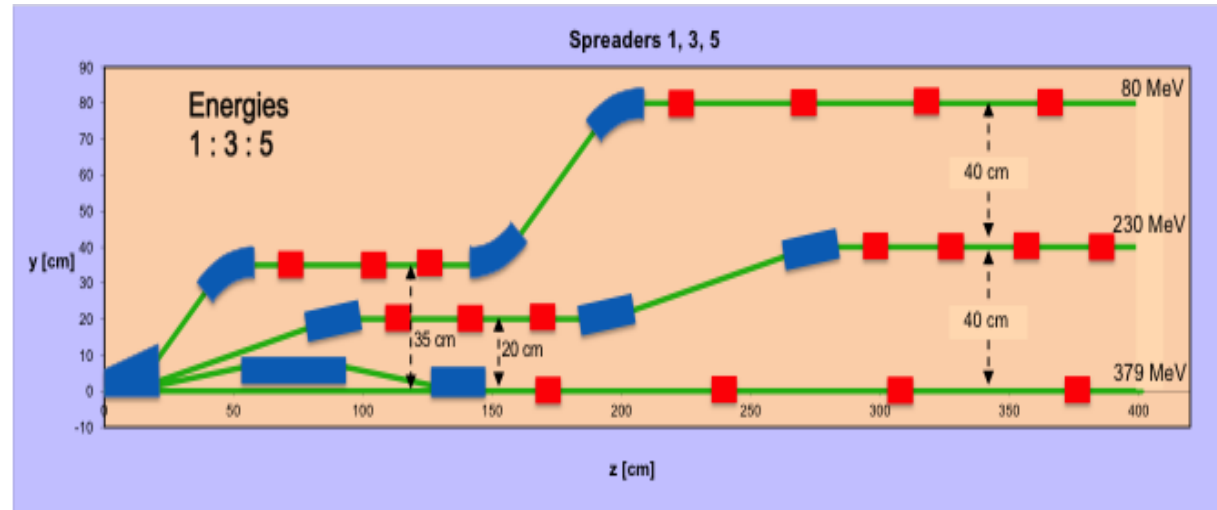
Use of shims optimized for 455MeV (0.88 mm) and studies to optimize chamfer



With a chamfer of 51.1 mm :
 Magnetic length = mechanical length
 along the central trajectory
 \Rightarrow 1st model optimized for short radius
 \Rightarrow Need to check that shim 1mm is right
 for 3 lower energies

- The spreaders and recombiners separate the bunches at different energies coming from the linac, in order to route them to the corresponding arc, and recombine them to the same orbit before entering the next linac.

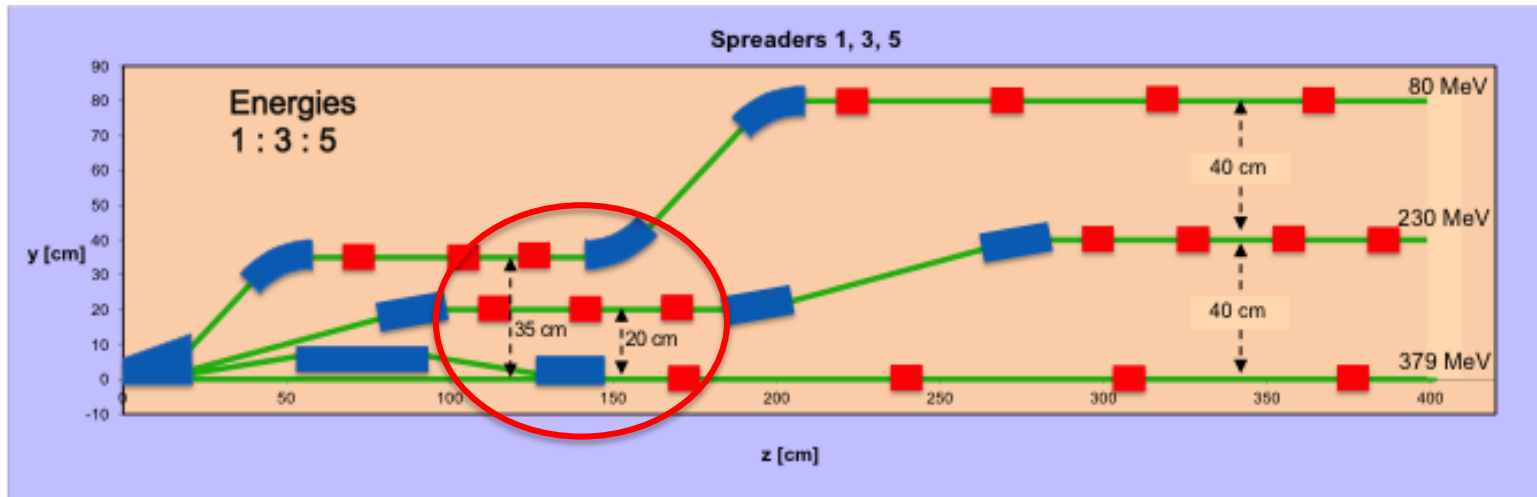
- The spreader consists of a vertical bending magnet that initiates the separation.



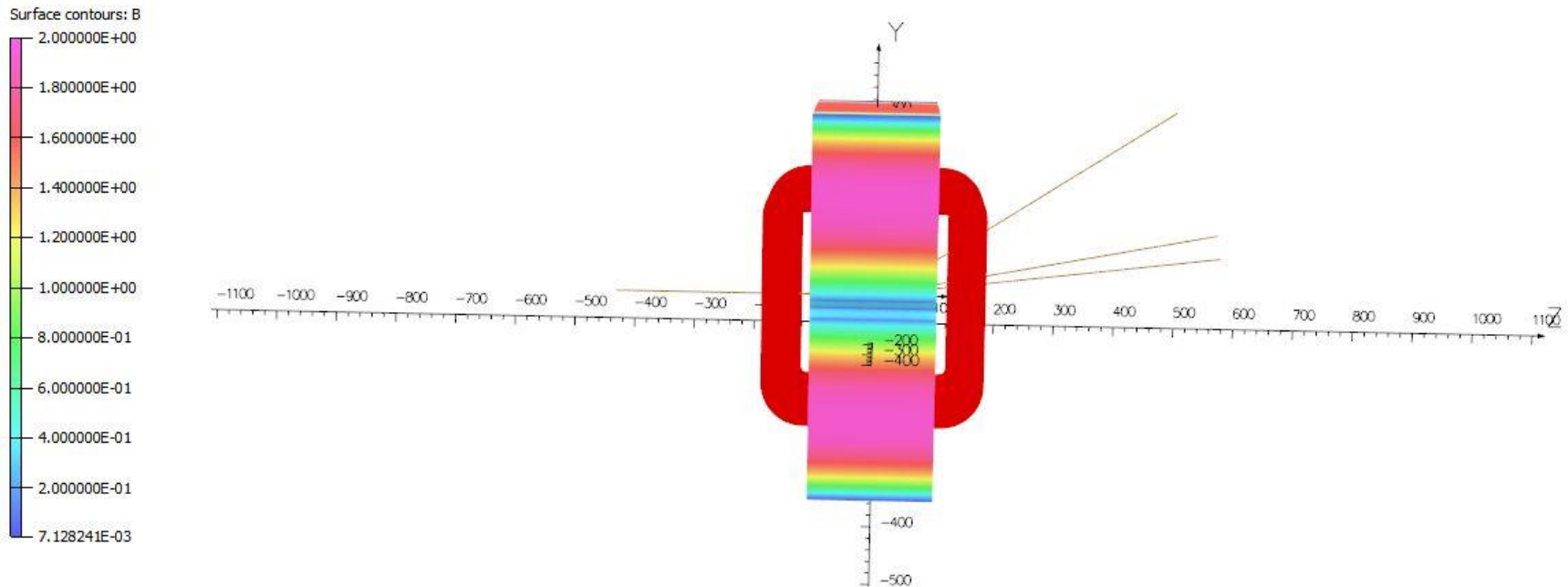
- The highest energy, at the bottom, is brought back to the horizontal plane with a chicane.
- The lower energies are captured with two-steps vertical bendings.

Spreader Requirements

An H-magnet design was chosen for the dipoles in order to minimize stray fields given the close proximity of the four beamlines. The maximum field is restricted to 6 kG in order to limit flux leakage out of the central pole iron as for CBETA project.



	Energy [?] (MeV)	Brho [?] (T.m)	Angle [?] (deg)	BI [?] (T.m)	Vertical [?] coordinate [?] of [?] beam [?] axis [?] at [?] z=400 [?] (mm)/spreader	Distance [?] between [?] beams [?] z=400 [?] (mm)	Vertical [?] coordinate [?] of [?] beam [?] axis [?] at [?] z=500 [?] (mm)/spreader	Distance [?] between [?] beams [?] z=500	Vertical [?] coordinate [?] of [?] beam [?] axis [?] at [?] z=800 [?] (mm)/spreader	Distance [?] between [?] beams [?] z=800
Arc [?] ₁	80	0,269	41	0,19217	347,71		434,64		695,43	
Arc [?] ₃	230	0,769	14,32	0,19217	102,11	151,54	127,63	307,01	204,21	491,22
Arc [?] ₅	380	1,269	8,67	0,19217	61,03	43,90	76,29	51,35	122,06	82,15



=> Trajectory at 80 MeV – 230 MeV and 380 MeV is correct.

⇒ Feasibility is done but need to go ahead simulations due to

- the saturation of the iron.
- the necessity to improve magnetic field homogeneity ($1 \cdot 10^{-3}$)
- the necessity to assure the design of following dipoles with these angles

- Magnetic design of arc quadrupoles is optimized
- Magnetic model for long radius arc bending magnets is optimized
- Feasibility of splitter is done

What remains to do

- Finalization of short radius bending magnet design : 1 day if shim 1mm is adapted – 4 days
- Simulation of the cross-talk between arc magnets : 4 days
- Finalization of the spreader design : 15 days
- Design of combiner magnets : 4 months
- Need sextupoles with integrated correctors ? Design of these sextupoles : 8 weeks

What we need to know to go ahead

- Arc bending magnets :
 - Homogeneity requirements : integrated homogeneity, flat field...
- If sextupoles and octupoles :
 - Strength, Homogeneity
- Spreader/Combiner magnets :
 - Deflection angle possibilities, Size of the beams, Homogeneity
 - Possibility to envisage septa solution ?

Thank you for your attention

Thank you to Fabrice Marteau from SOLEIL