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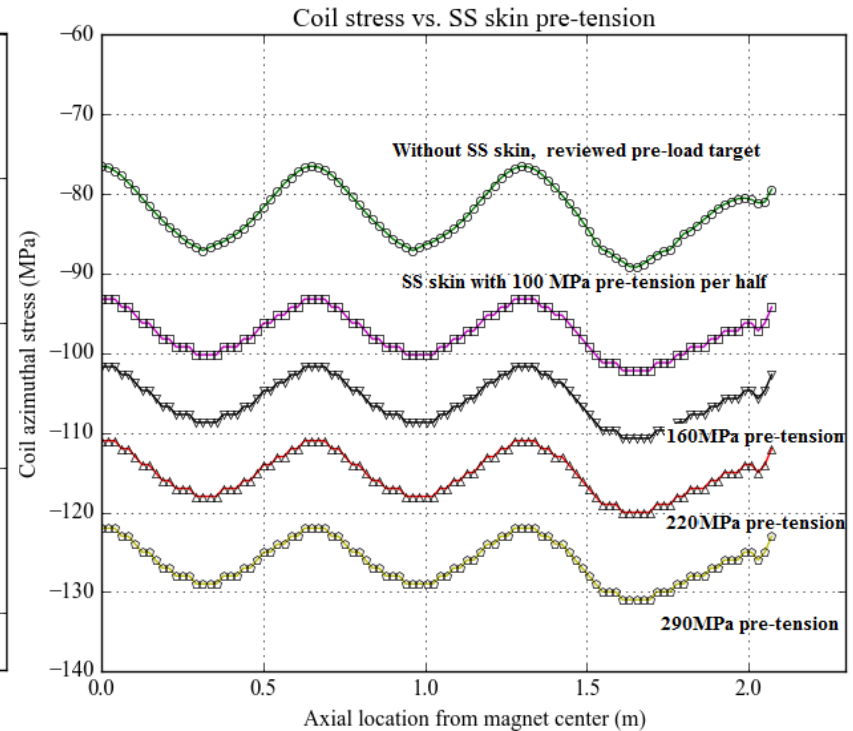
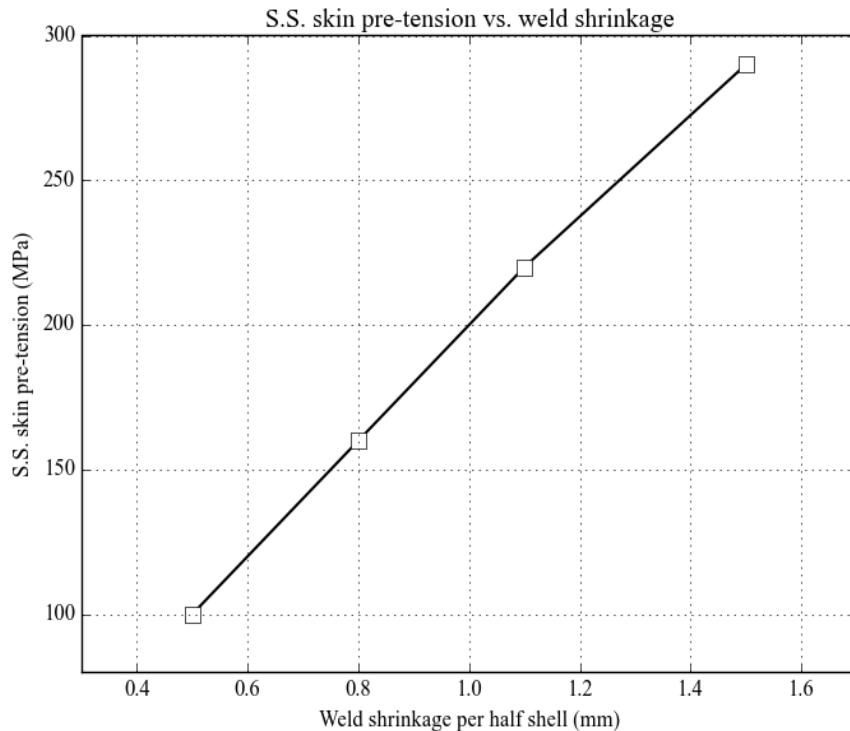
MQXFS1d Welding Status

Antonios Vouris

Cold Mass Status Meeting

25 January 2018

Coil pre-stress changes with SS skin pre-tensions

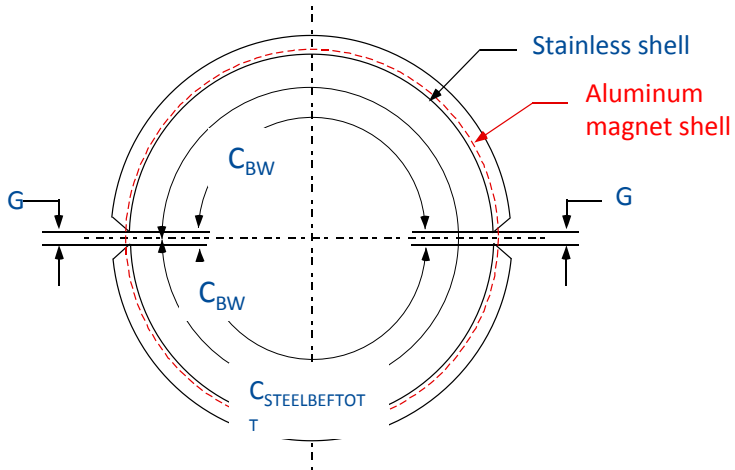
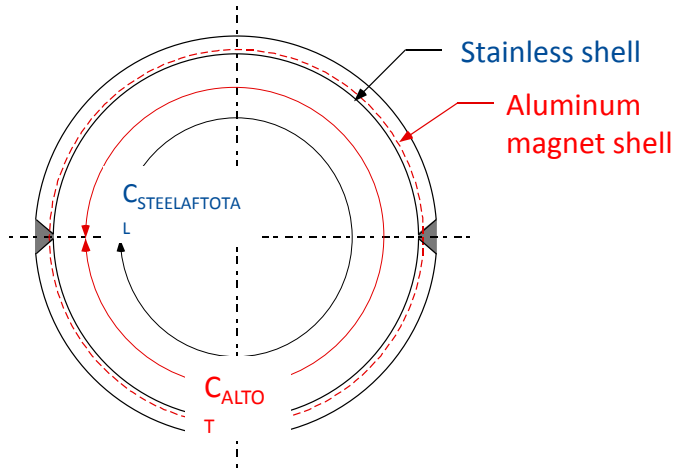


- Impact of the SS skin has been performed in our 3D model by applying different interferences between S.S. vessel and the magnet structure.
- The plot on the right presents the coil (pole) azimuthal stress along the magnet length with different SS skin pre-tensions induced by welding shrinkage.

$\Delta \sigma_{\text{Coil}}$ compared with Giorgio's results

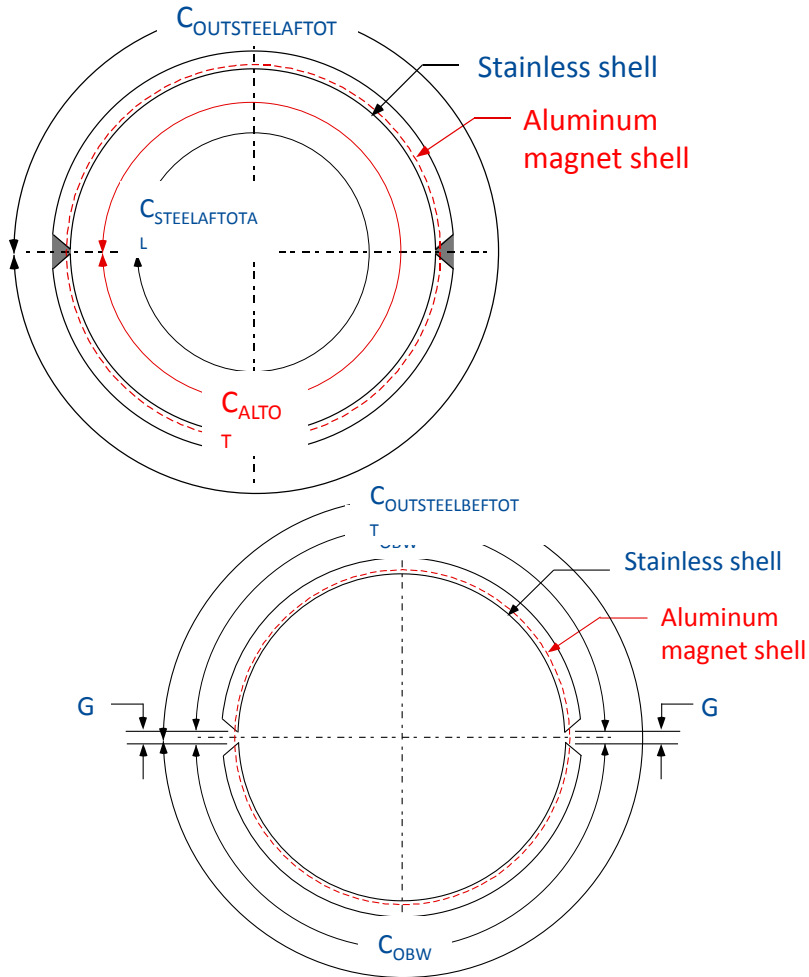
- The coil stress increases by ~ 3.2 MPa / 0.1mm weld shrinkage (half shell). This denotes about 48 MPa coil stress increasing is expected for a 50 mil (1.5 mm) weld shrinkage (half shell).
- This value is close to the results Giorgio presented in the his slides “MQXF – Vessel Welding” (05/12/2017) .
- Both 2D and 3D results shows the current weld shrinkage is relatively high for the coil pre-stress.

Calculation of Shell Weld Preparation



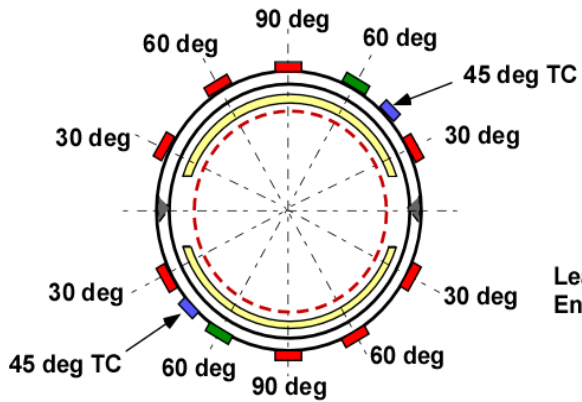
- C_{ALTOT} = Total Circumference of Outside surface of Aluminum shell
- $C_{STEELAFTOT}$ = Total Circumference of Inner surface of Steel shell after welding
- Measured dia. of Aluminum Shell O.D. = 614.657 mm = 24.199 in.
- *Criteria to achieve correct tightness after welding:* $C_{STEELAFTOT} = C_{ALTOT} - .020$ in.
- $C_{ALTOT} = 24.199 \text{ in.} \times \pi = 76.023$ in.
- $C_{STEELBEFTOT} = C_{STEELAFTOT} + \text{Total Shrinkage during welding}$
- Total shrinkage during welding = .090 in. (over entire azimuth) = .045 in. per side.
- Therefore, $C_{STEELBEFTOT} = 76.023 \text{ in.} - .020 \text{ in.} + .090 \text{ in.} = 76.093$ in.
- And the inside diameter of the steel before welding is $76.093 / \pi = 24.221$ in.
- C_{BW} = Circumference of inside of steel shell half before welding
- G = Gap size before welding per side = .094 in.
- $C_{STEELBEFTOT} = C_{BW} + C_{BW} + G + G$
- Therefore, $C_{BW} = (C_{STEELBEFTOT} - 2G) / 2$
- Therefore, $C_{BW} = (76.093 \text{ in.} - .188 \text{ in.}) / 2 = 37.952$ in.

Calculation of Shell Weld Preparation (Using Outside Diameter)

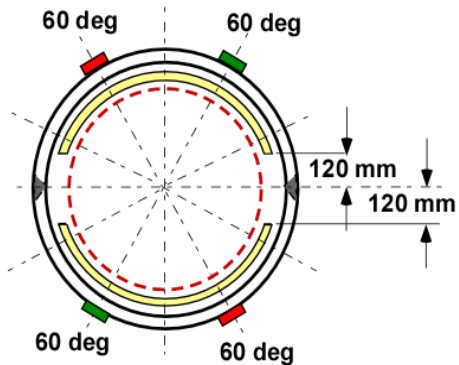


- C_{ALTO} = Total Circumference of Outside surface of Aluminum shell
- $C_{STEELAFTOT}$ = Total Circumference of Inner surface of Steel shell after welding
- Measured dia. of Aluminum Shell O.D. = 614.657 mm = 24.199 in.
- Outside dia. Stainless Shell after welding = 24.199 in. + (.330)(2) = 24.859 in.
- *Criteria to achieve correct tightness after welding:* $C_{STEELAFTOT} = C_{ALTO} - .020$ in.
- Outside circumference of steel after welding = $C_{OUTSTEELAFTOT} = 24.859$ in. $\times \pi = 78.096$ in.
- $C_{OUTSTEELEBTOT} = C_{OUTSTEELAFTOT} + \text{Total Shrinkage during welding}$
- Total shrinkage during welding = .090 in. (over entire azimuth) = .045 in. per side.
- Therefore, $C_{OUTSTEELEBTOT} = 78.096$ in. - .020 in. + .090 in. = 78.166 in.
- And the outside diameter of the steel before welding is $78.166 / \pi = 24.881$ in.
 - C_{OBW} = Circumference of outside of steel shell half before welding
 - G = Gap size before welding per side = .094 in.
 - $C_{OUTSTEELEBTOT} = C_{OBW} + C_{OBW} + G + G$
 - Therefore, $C_{OBW} = (C_{OUTSTEELEBTOT} - 2G) / 2$
 - Therefore, $C_{OBW} = (78.166$ in. - .188 in.) / 2 = 38.989 in.

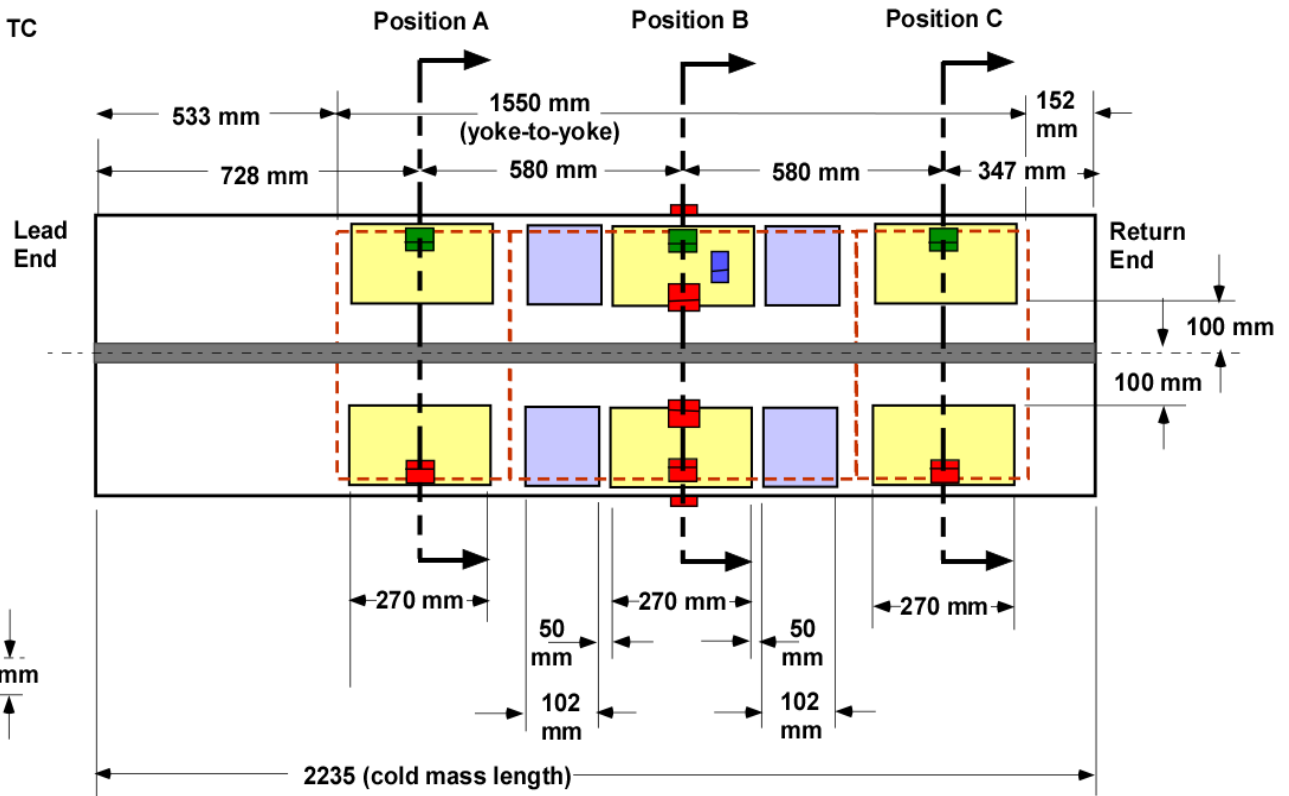
Fuji film plan



Position B
(looking from LE to RE)

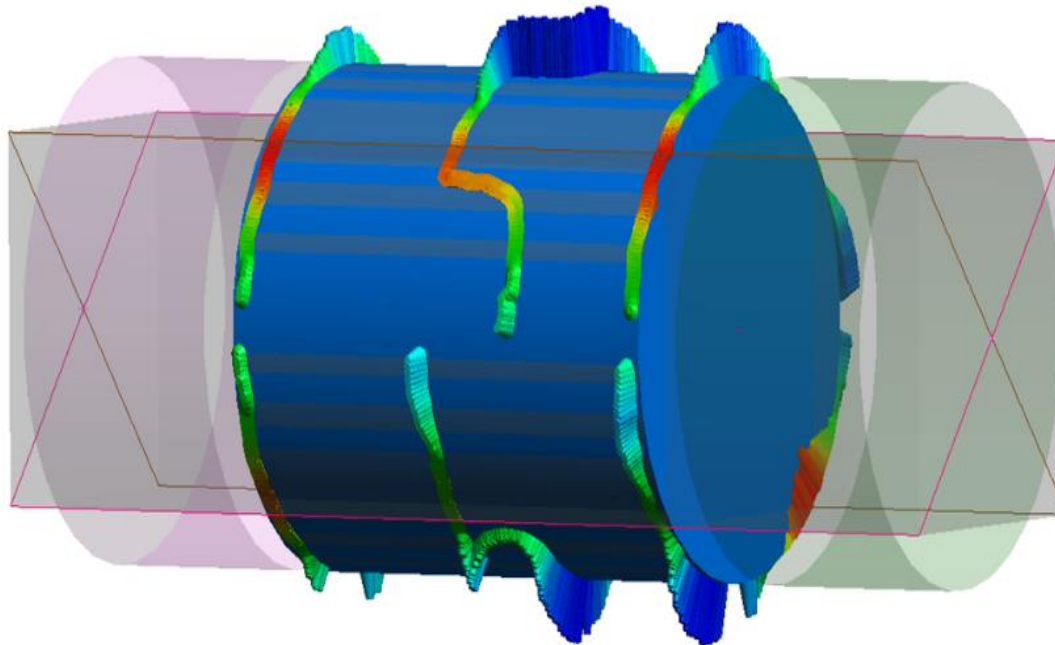


Positions A and C
(looking from LE to RE)



Yellow = Low Pressure Fuji Film
Blue = Medium Pressure Fuji Film

Note: all (yellow) low pressure film pieces are centered axially on the center of an aluminum section



Measurements of center section of MQXFS1C shell.

Status



Next steps:

- Wire up the strain gauges
- Scribe the centerline both sides
- Insert the Fuji films
- Fit up the shells
- Welding
 - Final shell leveling wrt. equipment
 - Monitor temperatures
 - Measure strain gauges after each passes