



**Design of the Electron gun for the GSI  
space charge compensation lens**  
ARIES Annual Meeting, 23.5.2018, Riga

Kathrin Schulte-Urlichs, GSI/IAP

# Objectives

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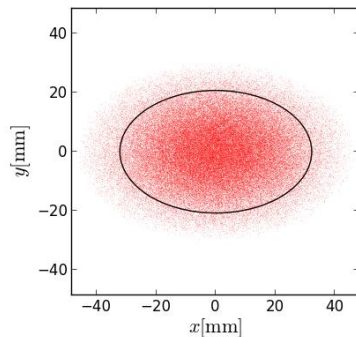
- Requirements for SCC gun
- Basic Gun Design
- Modulation Options & Challenges
- Commissioning of Electron Gun
- Outlook

# Requirements for SCC gun

## Electron beam for space charge compensation in SIS18

number of electron lenses	$N=3$
interaction region	$l=3$ m
electron beam current	$I_B = 10$ A

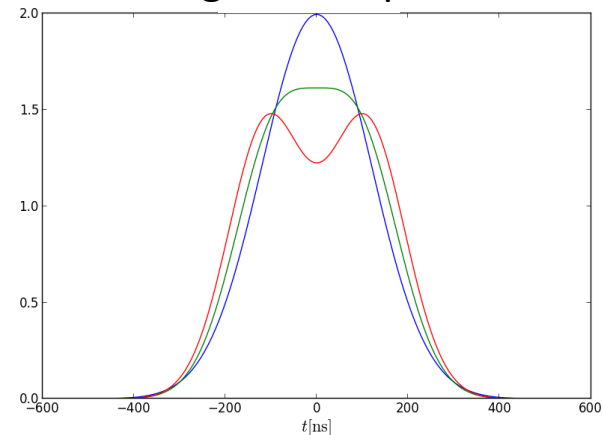
transverse profile



$$2\sigma_x = 35 \text{ mm}$$

$$2\sigma_y = 20 \text{ mm}$$

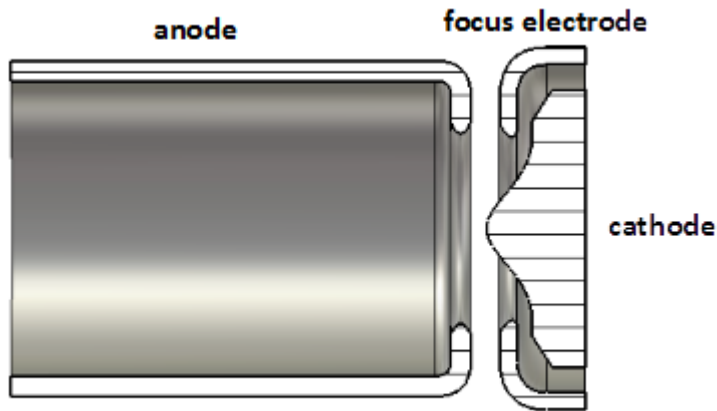
longitudinal profile



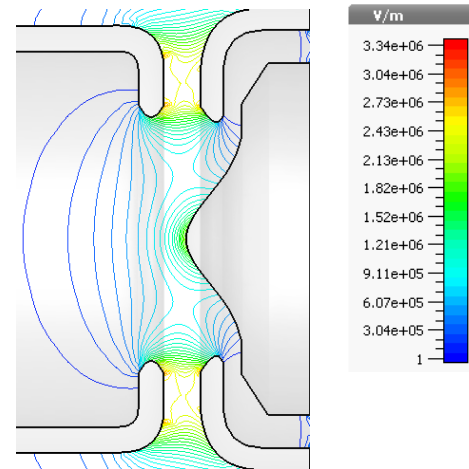
$$f = 5 \text{ MHz}$$

# Basic Gun Design

Layout of electron gun

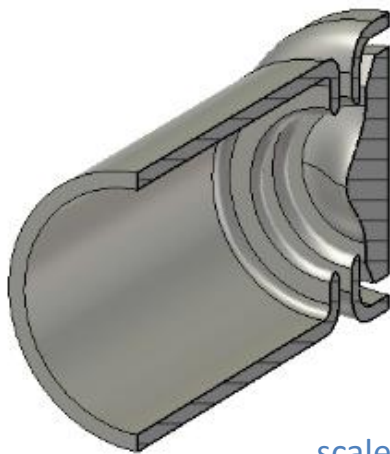


Gun electric field



$$E_{\max} = 3.3 \text{ kV/mm}$$
$$E_{\text{Kilpatrick}} = 9.5 \text{ kV/mm}$$

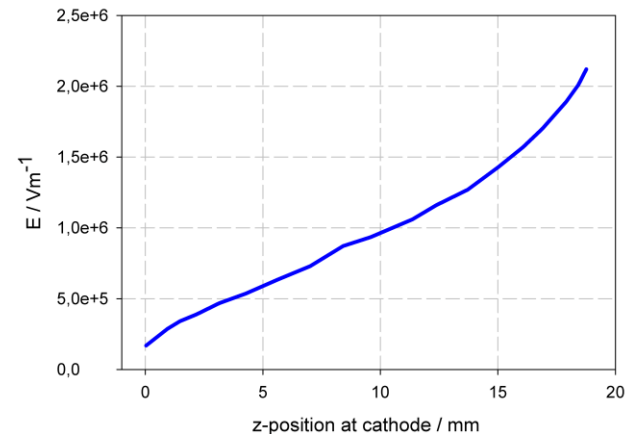
homogeneous  
magnetic field  
 $B_z = 0.2 \text{ T}$



$$P = 5.3 \cdot 10^{-6} \text{ A/V}^{3/2}$$
$$U = 30 \text{ kV}$$
$$I = 30.8 \text{ A}$$
$$B_z = 0.2 \text{ T}$$
$$J_e = 2.2 \text{ Acm}^{-2}$$
$$r_c = 35 \text{ mm}$$

scaled design of BNL  
e-gun by A. Pikin

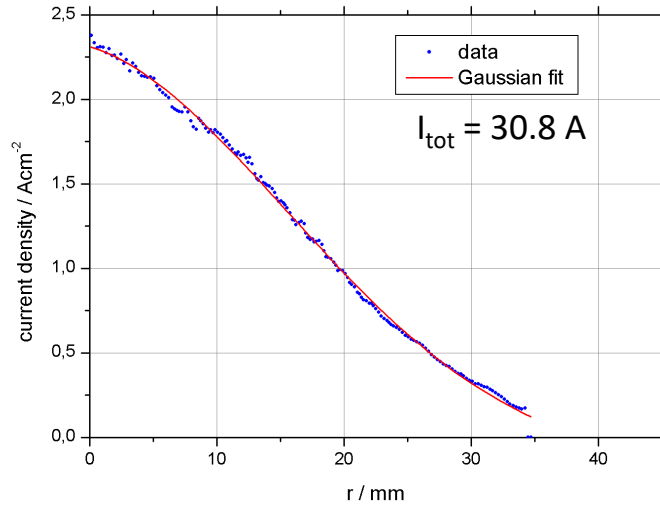
Electric field along cathode



# Basic Gun Design

## Current density profile

TRAK (2D)

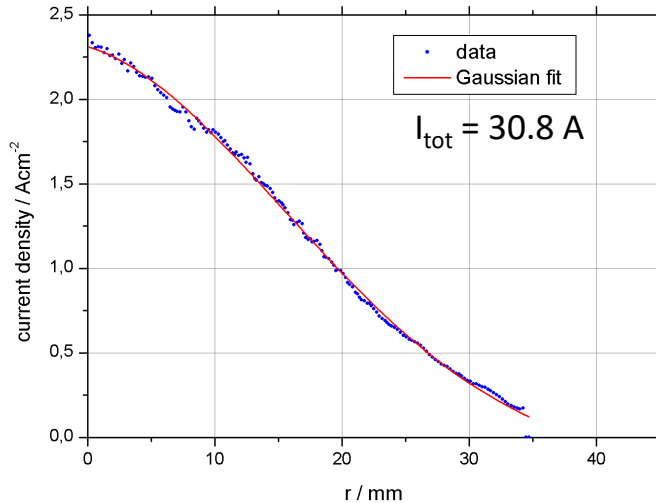


Gun  
parameters:  
 $U_c = 0 \text{ V}$   
 $U_{CE} = 0 \text{ V}$   
 $U_a = 30 \text{ kV}$   
 $B_z = 0.22 \text{ T}$

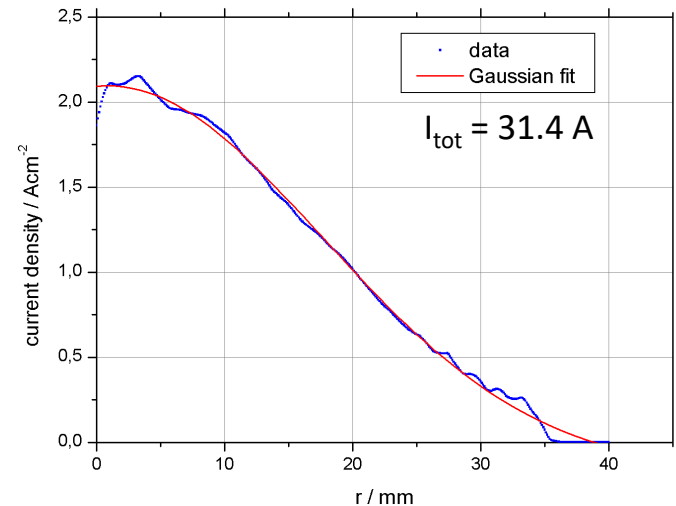
# Basic Gun Design

## Current density profile

TRAK (2D)



CST PS (3D)



Gun  
parameters:  
 $U_c = 0 \text{ V}$   
 $U_{CE} = 0 \text{ V}$   
 $U_a = 30 \text{ kV}$   
 $B_z = 0.22 \text{ T}$

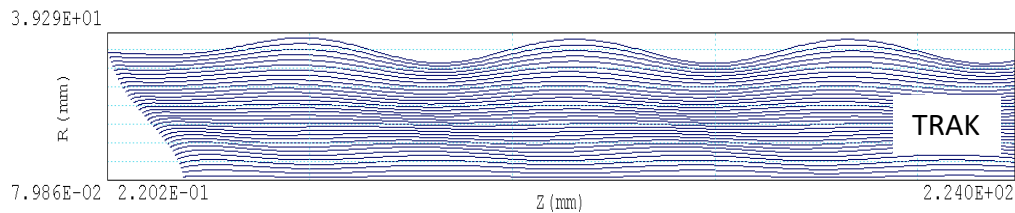
Two codes (2D and 3D) are used

- validation of simulation results using CST PS
  - Basic design studies using 2D code
- Advanced studies (elliptical beam, modulation) using 3D code

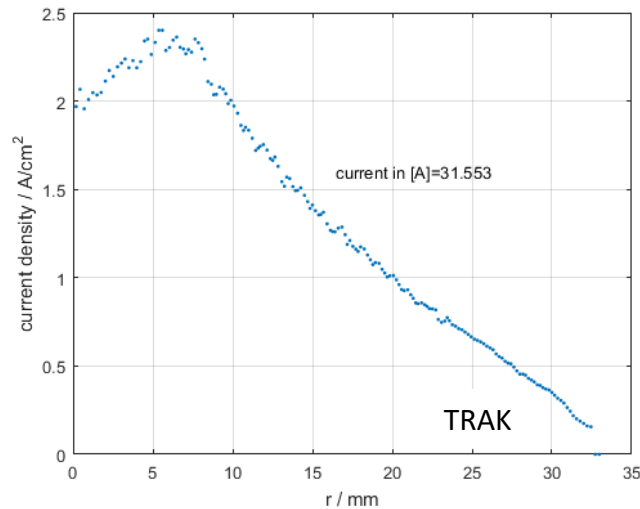
# Basic Gun Design

## Influence of magnetic field on current density profile

Electron trajectories for  $B_z=0.05\text{T}$

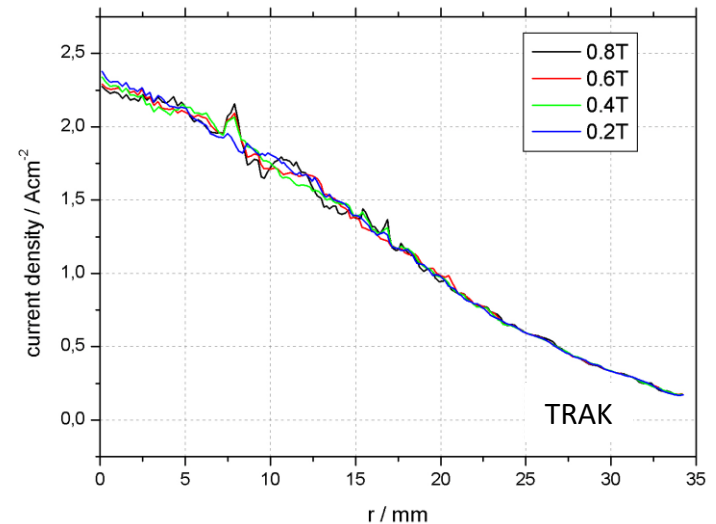


Current density profile for  $B_z=0.05\text{T}$



Gun  
parameters:  
 $U_c = 0\text{ V}$   
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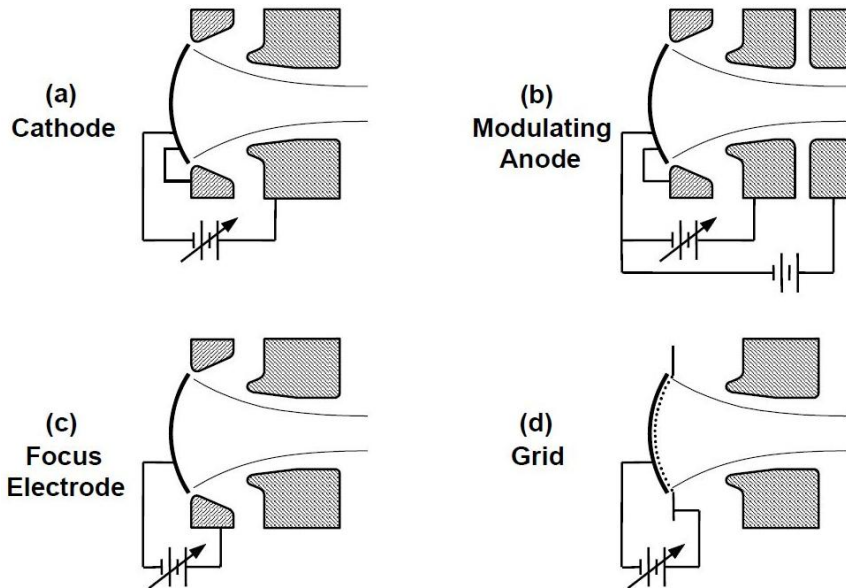
Current density profiles for  $B_z=0.2-0.8\text{T}$



Above certain threshold only minor changes in current density profile are observed.

# Modulation Options & Challenges

## Typical Modulation Options



Anode modulation:

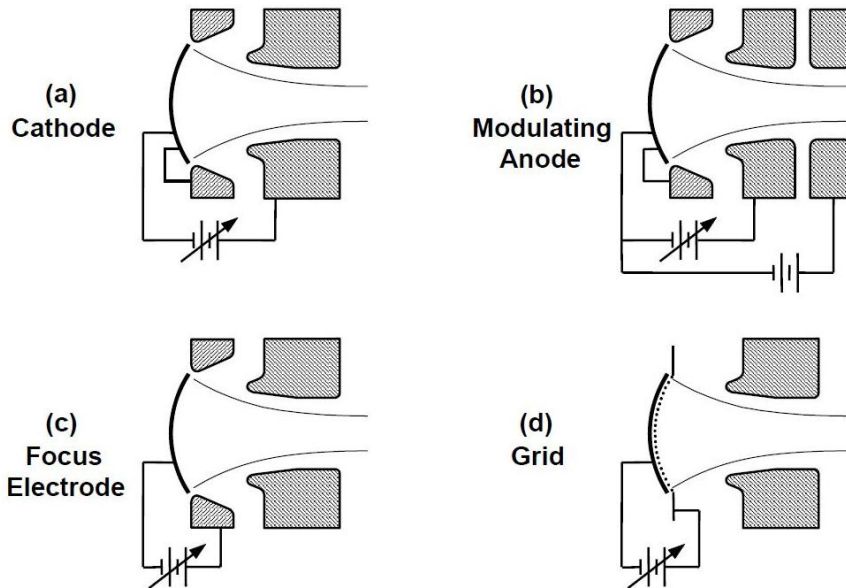
$$P_{diss} = \frac{1}{2} C U_a^2 \cdot f$$
$$P_{diss} = \frac{1}{2} \cdot 200\text{pF} \cdot 25\text{kV}^2 \cdot 5\text{MHz} = 313\text{kW}$$





# Modulation Options & Challenges

## Typical Modulation Options



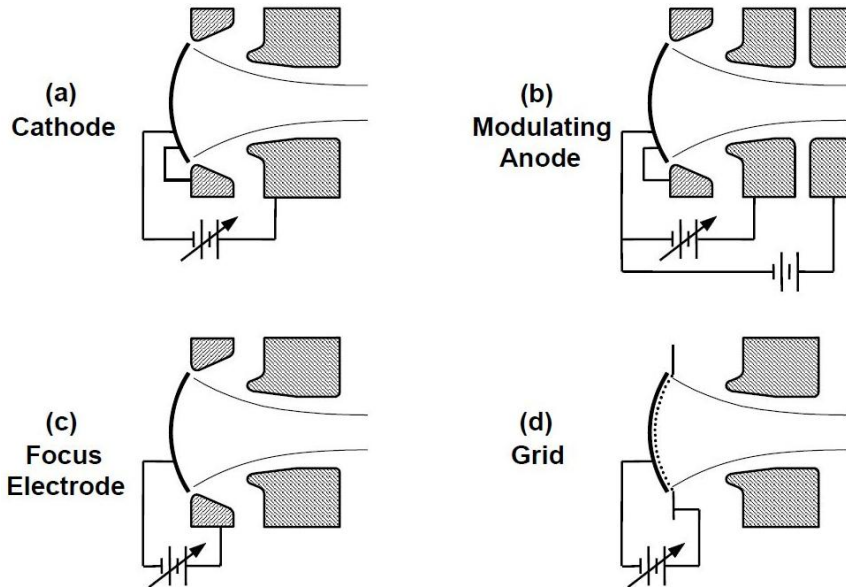
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# Modulation Options & Challenges

## Typical Modulation Options

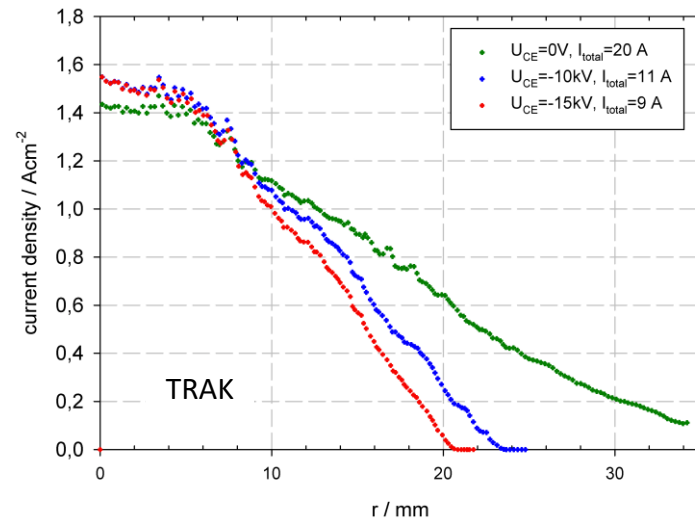


Anode modulation:

$$P_{diss} = \frac{1}{2} C U_a^2 \cdot f$$

$$P_{diss} = \frac{1}{2} \cdot 200\text{pF} \cdot 25\text{kV}^2 \cdot 5\text{MHz} = 313\text{kW}$$

Focus electrode modulation

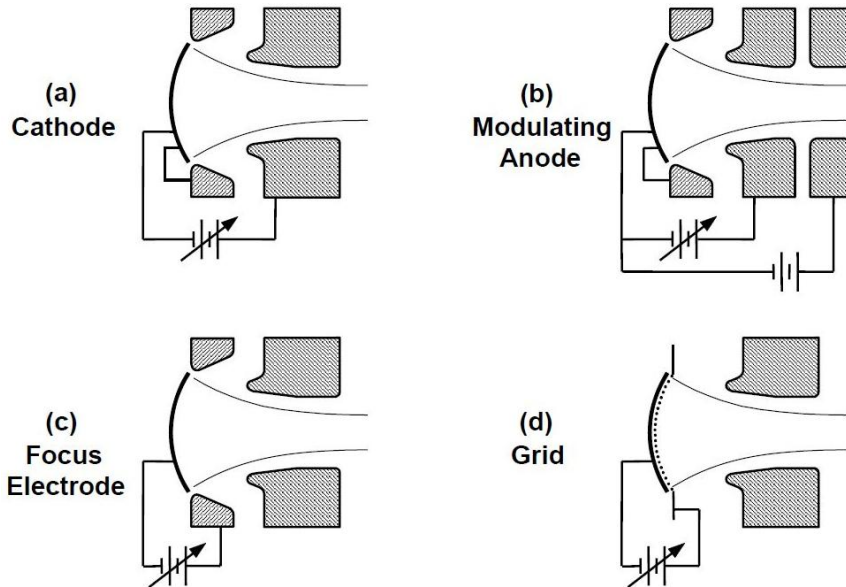


Gun parameters:  
 U<sub>c</sub> = 0 V  
 U<sub>a</sub> = 22 kV  
 B<sub>z</sub> = 0.4 T

High voltages required to depress beam current.

# Modulation Options & Challenges

## Typical Modulation Options

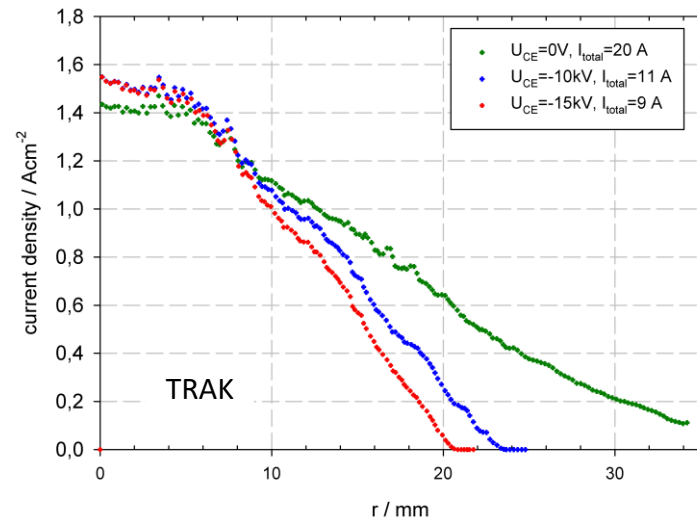


Anode modulation:

$$P_{diss} = \frac{1}{2} C U_a^2 \cdot f$$

$$P_{diss} = \frac{1}{2} \cdot 200\text{pF} \cdot 25\text{kV}^2 \cdot 5\text{MHz} = 313\text{kW}$$

Focus electrode modulation

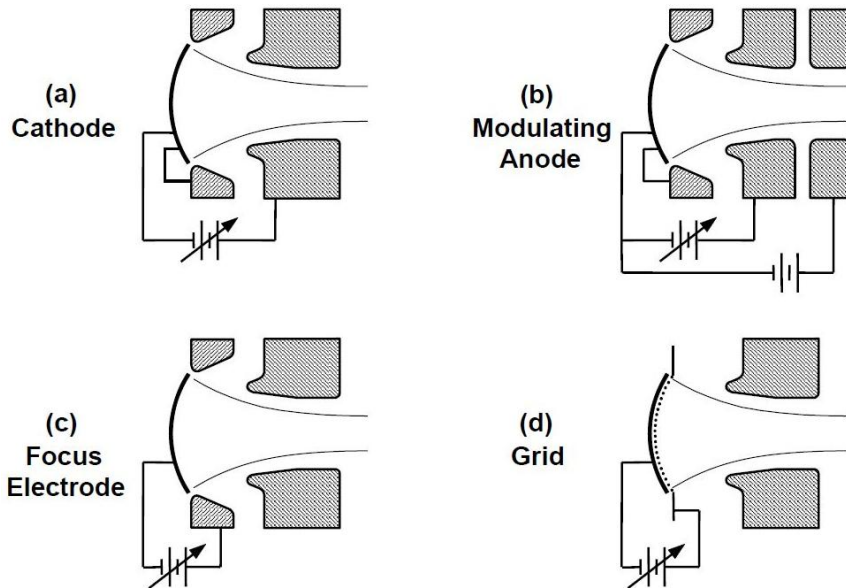


Gun parameters:  
 U<sub>c</sub> = 0 V  
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High voltages required to depress beam current.

# Modulation Options & Challenges

## Typical Modulation Options



### Grid modulation:

Low grid voltages, low dissipated power

$$P_{diss} = \frac{1}{2} C U_g^2 \cdot f$$

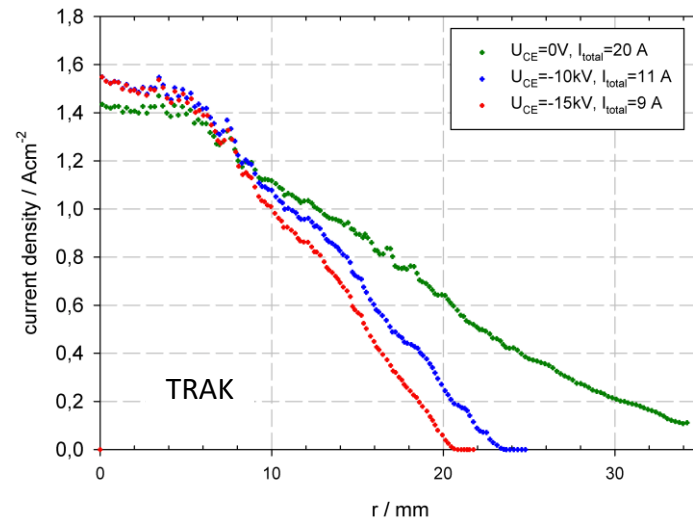
$$P_{diss} = \frac{1}{2} \cdot 150\text{pF} \cdot 1\text{kV}^2 \cdot 5\text{MHz} = 375\text{W}$$

### Anode modulation:

$$P_{diss} = \frac{1}{2} C U_a^2 \cdot f$$

$$P_{diss} = \frac{1}{2} \cdot 200\text{pF} \cdot 25\text{kV}^2 \cdot 5\text{MHz} = 313\text{kW}$$

### Focus electrode modulation

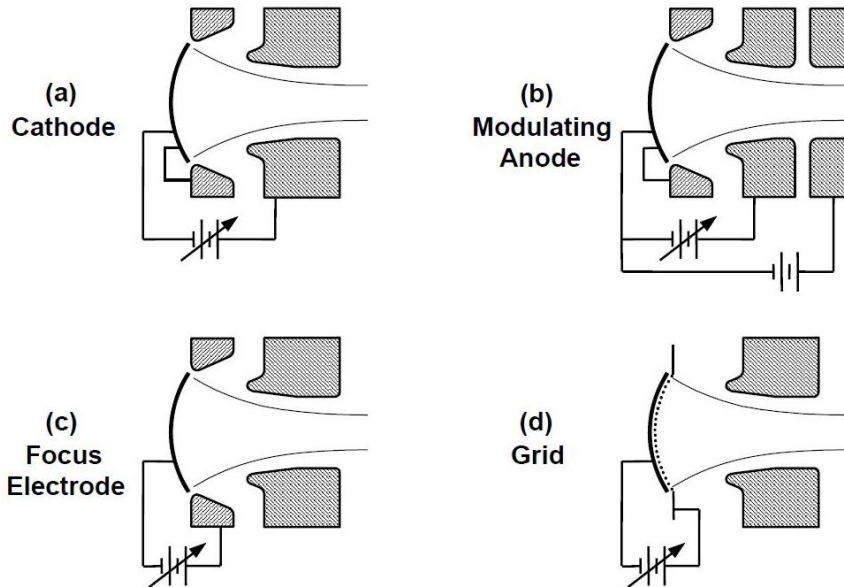


Gun parameters:  
 U<sub>c</sub> = 0 V  
 U<sub>a</sub> = 22 kV  
 B<sub>z</sub> = 0.4 T

High voltages required to depress beam current.

# Modulation Options & Challenges

## Typical Modulation Options



### Grid modulation:

Low grid voltages, low dissipated power

$$P_{diss} = 1/2 CU_g^2 \cdot f$$

$$P_{diss} = 1/2 \cdot 150\text{pF} \cdot 1\text{kV}^2 \cdot 5\text{MHz} = 375\text{W}$$

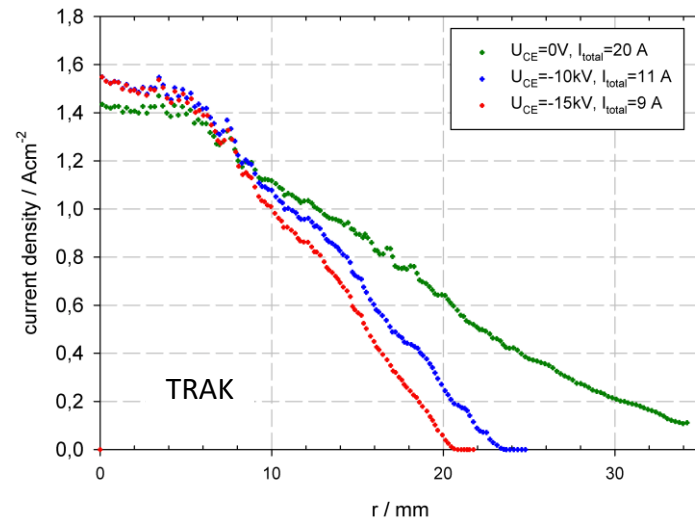
reduced current, beamlets

### Anode modulation:

$$P_{diss} = 1/2 CU_a^2 \cdot f$$

$$P_{diss} = 1/2 \cdot 200\text{pF} \cdot 25\text{kV}^2 \cdot 5\text{MHz} = 313\text{kW}$$

### Focus electrode modulation



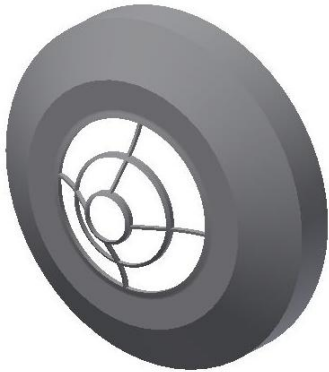
Gun parameters:  
 $U_c = 0\text{ V}$   
 $U_a = 22\text{ kV}$   
 $B_z = 0.4\text{ T}$

High voltages required to depress beam current.

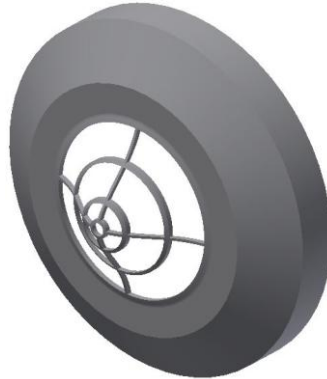
# Grid Design

Different grid designs are studied:

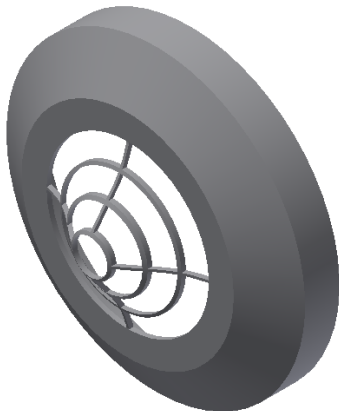
Grid 1



Grid 2



Grid 3



Grid 4



distance cathode-grid  $d_{cg}=2\text{mm}$

Transverse current density preserved?

Total emitted current?

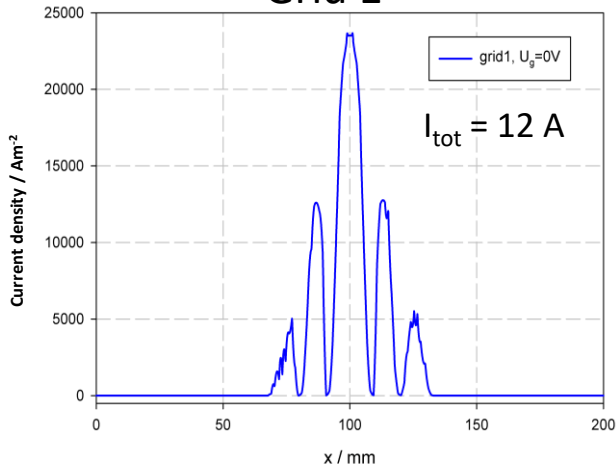
Grid voltages to depress current?

Losses on grid?

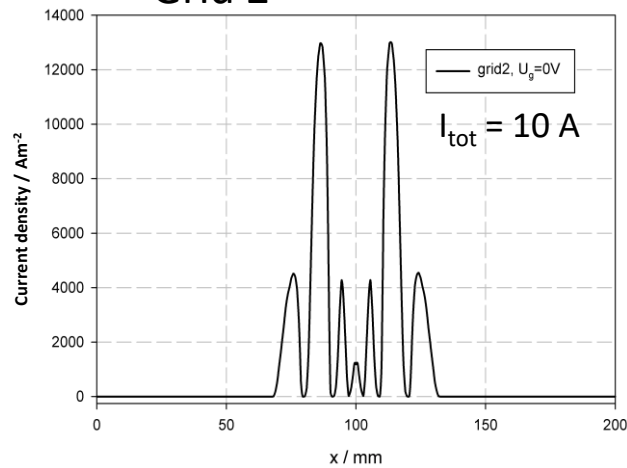
# Grid Design

Current density profile for  $U_g=0V$  and total emitted current:

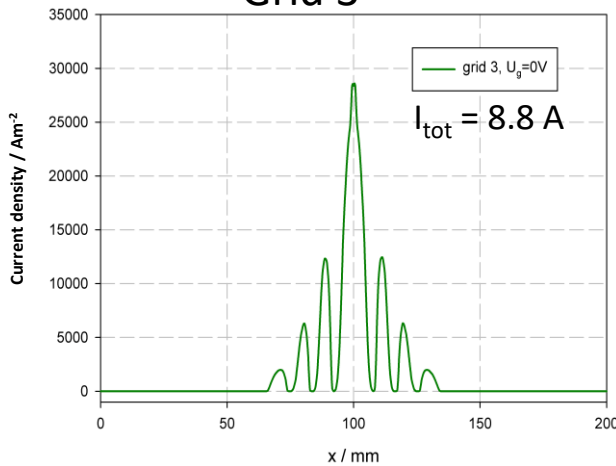
Grid 1



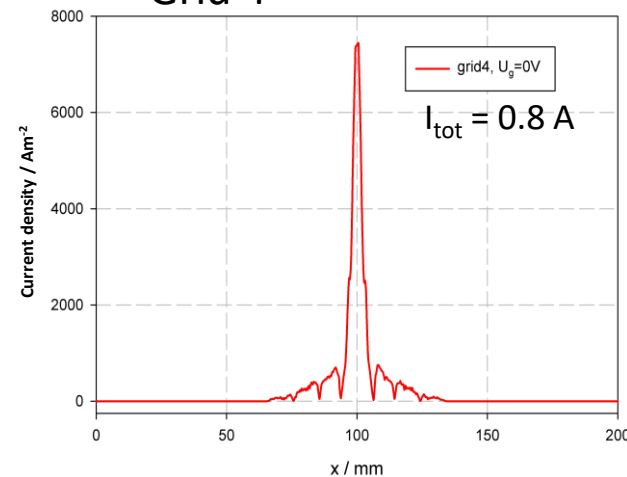
Grid 2



Grid 3



Grid 4



Gun parameters:

$$U_c = 0 V$$

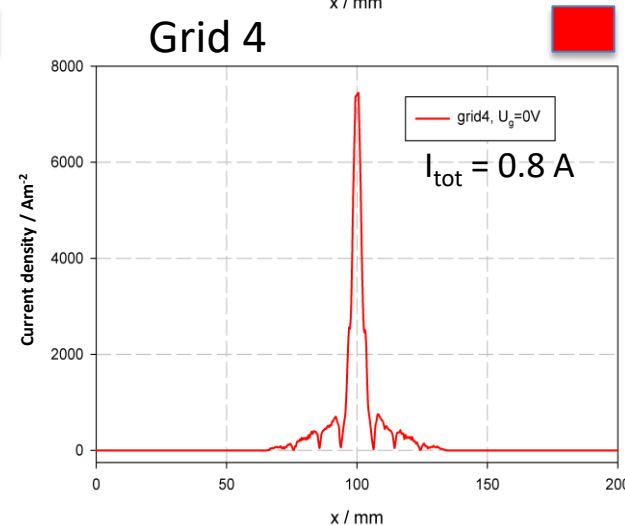
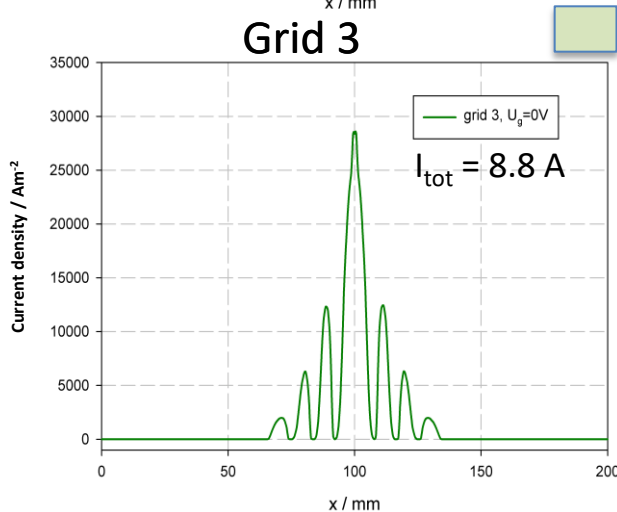
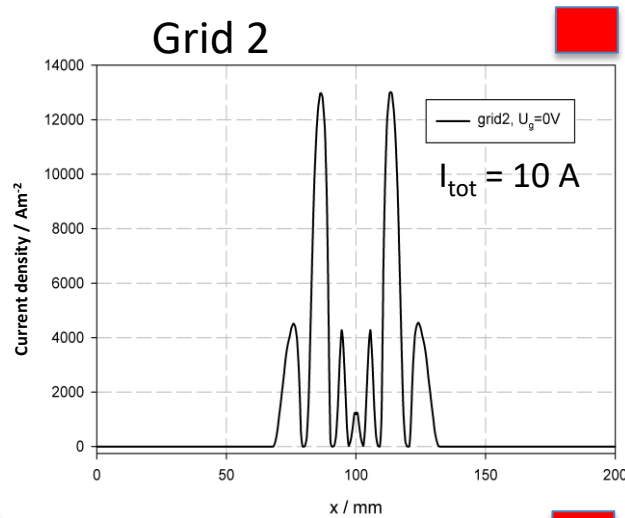
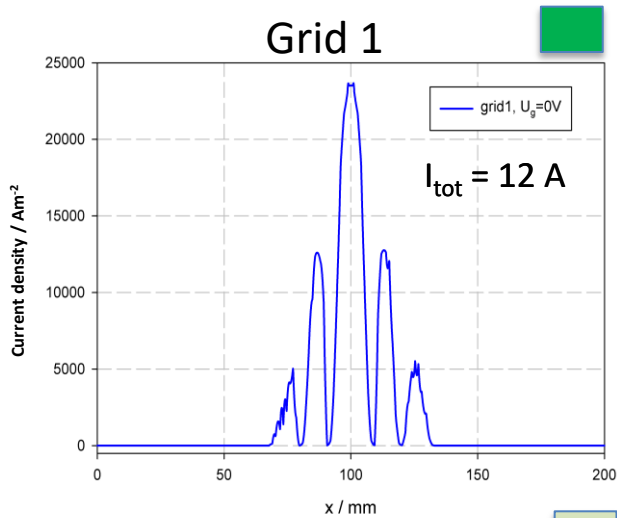
$$U_{CE} = 0 V$$

$$U_a = 25 kV$$

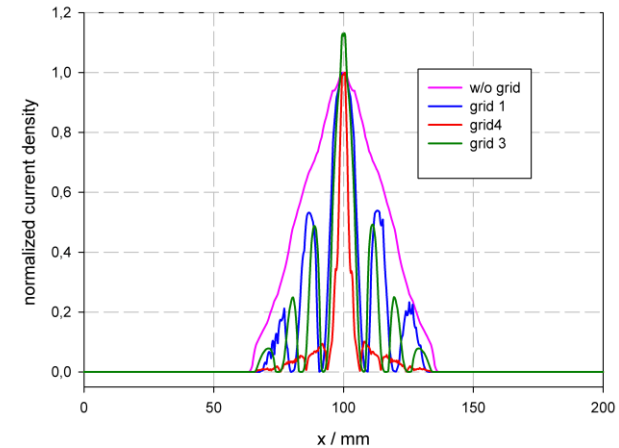
$$B_z = 0.2 T$$

# Grid Design

Current density profile for  $U_g=0V$  and total emitted current:



Perservation of current density profile



Gun parameters:

$$U_c = 0 V$$

$$U_{CE} = 0 V$$

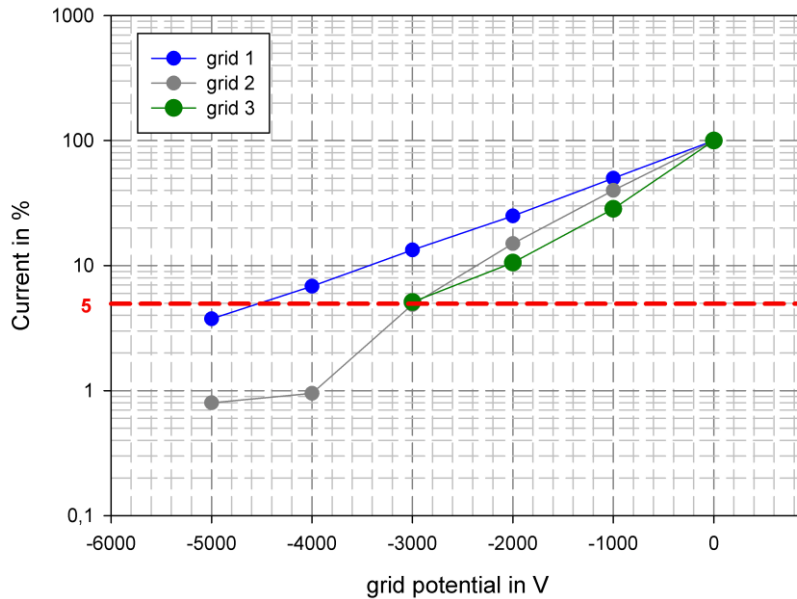
$$U_a = 25 kV$$

$$B_z = 0.2 T$$

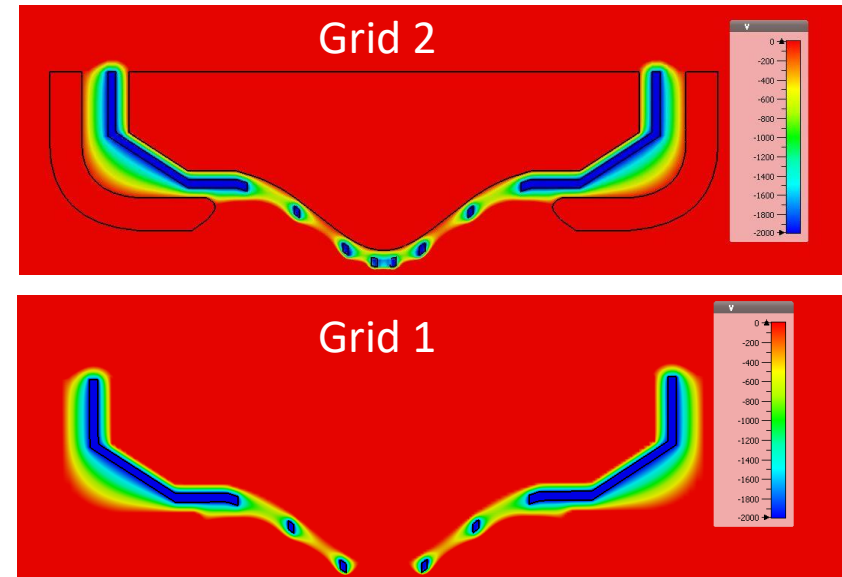


# Grid Design

Required grid voltages to suppress electron current:



Example of potential distribution

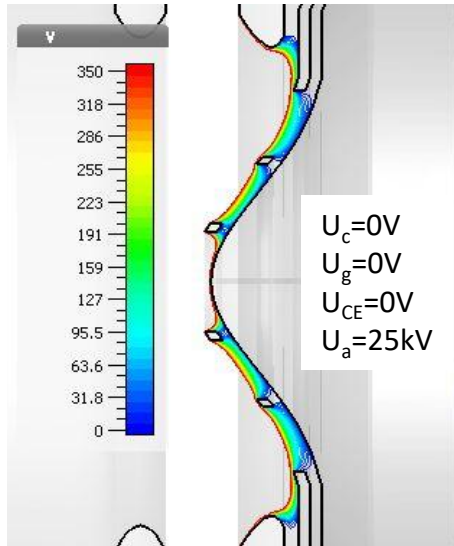


Grid 3 nearly preserves transverse current density profile and requires  $U_g = -3$  kV to depress current to 5% of initial value. This leads to a dissipated power of 1.7kW for  $C_g = 75$  pF.

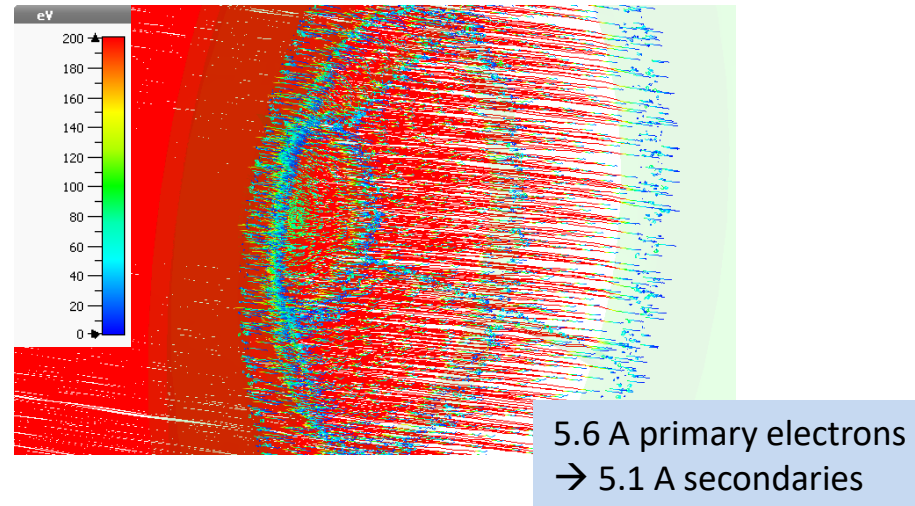
**The design of grid 3 still needs to be improved in order to exactly match Gaussian current density profile. Furthermore, the final results have to be validated by simulations performed with smaller mesh size.**

# Grid Design

Potential distribution at grid1 for  $U_g=0V$ :



Secondaries produced at tungsten grid for  $U_g=100V$ :



Grid temperature estimate:

$$I_l = 6A, U = 100 V$$

$$P/A = 156 \cdot 10^3 W/m^2$$

$$T = \sqrt[4]{P/A \cdot \sigma_{SB}} = 1288 K$$

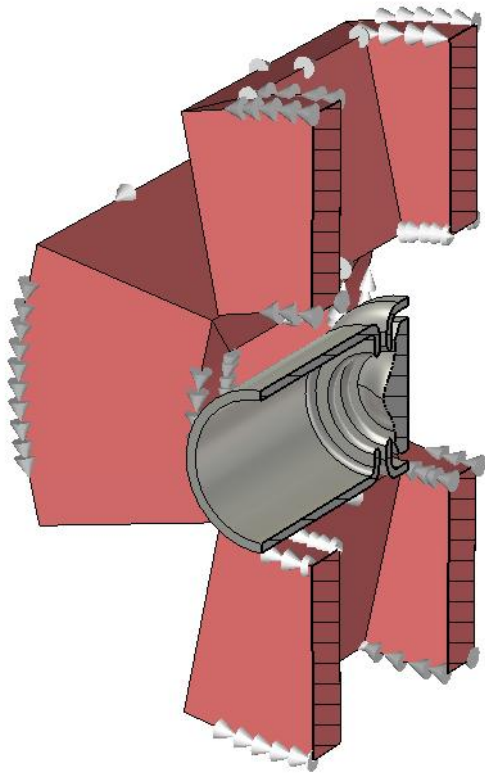
if only radiation is assumed as cooling mechanism

cathode temperature  $\sim 1273K$

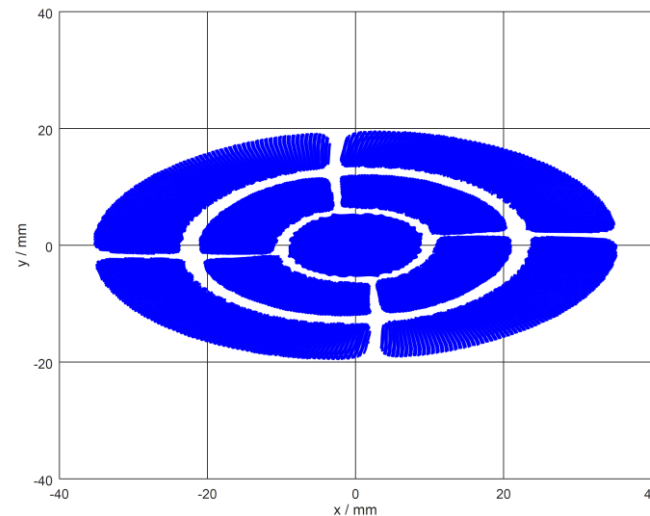
further studies needed

# Beam Shaping Options

- Cathode shaping
- Beam pipe shaping
- Internal quadrupol field



Elliptical beam distribution  
created by quadrupol field



Gun parameters:

$$U_c = 0 \text{ V}$$

$$U_{CE} = 0 \text{ V}$$

$$U_a = 25 \text{ kV}$$

$$B_z = 0.2 \text{ T}$$

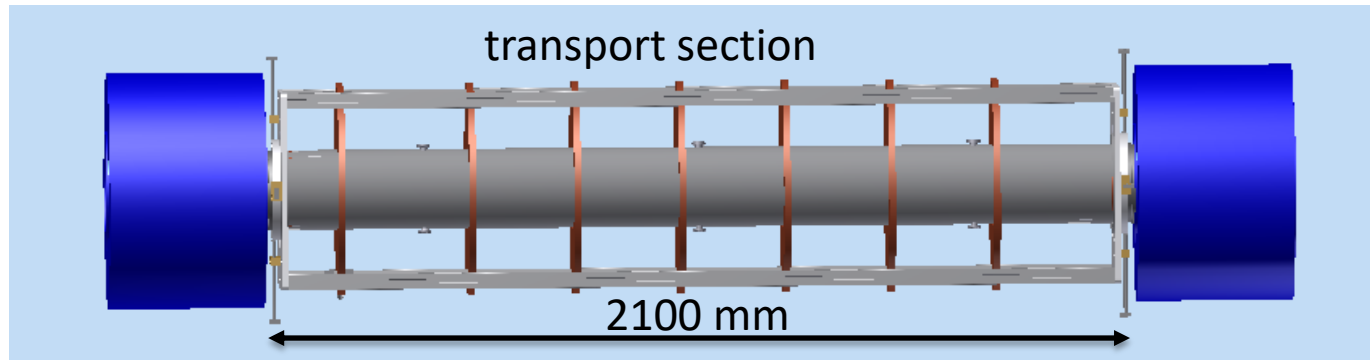
$$B_{x,Q} = 0.07 \text{ T}$$

- adjustable of beam distribution
- reduction of cathode radius from 35 mm to 26.5 mm
- needs to be integrated into solenoid chamber

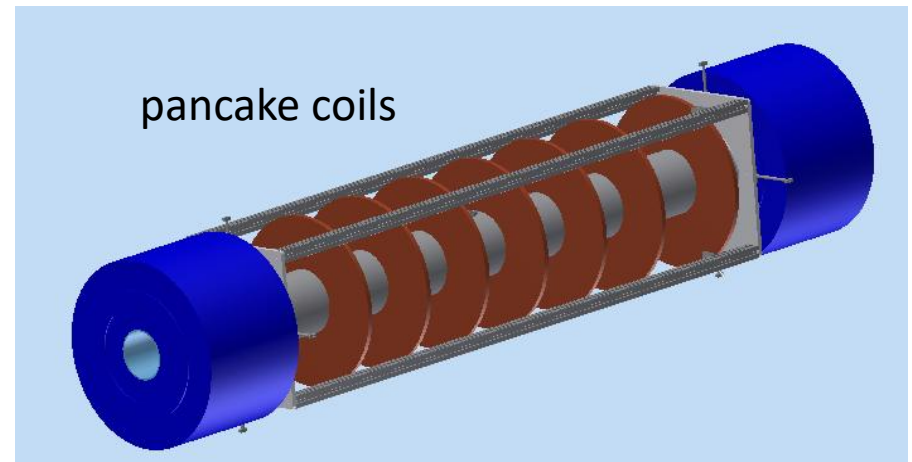
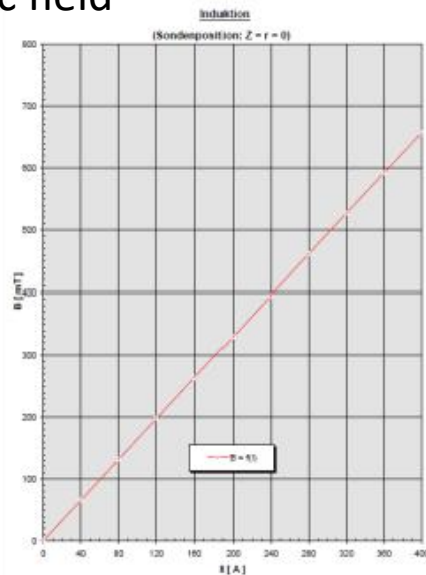
# Electron gun commissioning at IAP

gun solenoid

collector solenoid



Magnetic field



- Finalization of test bench layout
- Purchasing of gun and collector solenoids
- Preparation of diagnostics and data acquisition

# Outlook

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## Electron gun

- Grid design to be finalized (affects also  $U_a$ )
  - simulations performed with smaller mesh size
  - beam load and grid material
  - Secondary electron emission
  - cut-off frequency
- Technical integration of quadrupol magnet
- Adaptation of present design to allow for exchange of cathode to deliver homogeneous beam as well
- Choice of cathode material
- Technical layout

## Test Bench

- Finalization of design
- Purchasing solenoids



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Thank you!

Thanks to my colleagues from IAP and GSI supporting this work.  
My special thanks go to A. Pikin for helping to get started with my studies on  
electron gun design and for fruitful discussions!

