



Status of WP-6 Development of Nb-Ti Quadrupole Magnet Prototype

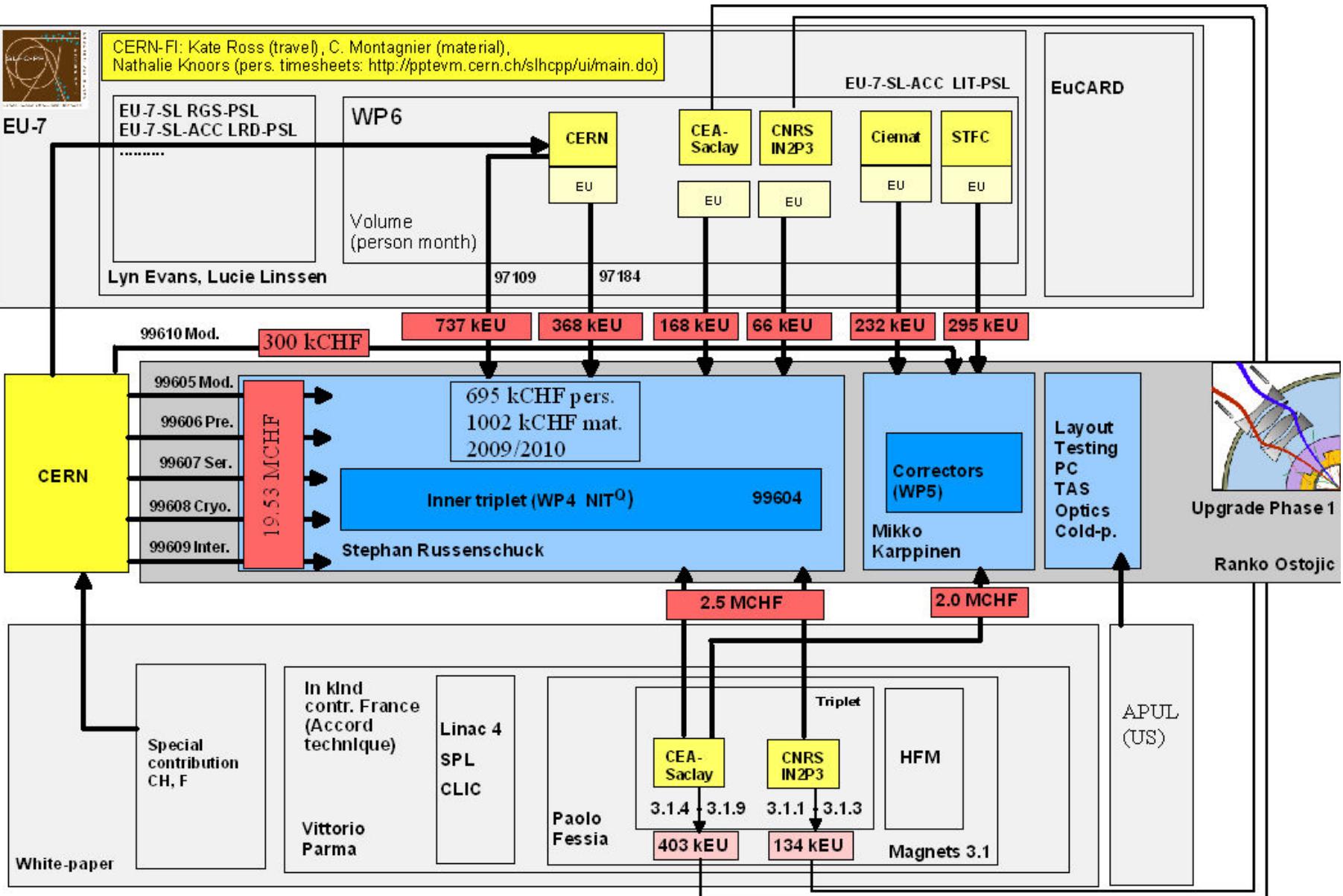
Stephan Russenschuck

for the WP-6 team

05.02.2010

- Framework: EU-WP6 and White-Paper
 - Deliverables and Milestones
- Design and construction activities/challenges
 - Challenges (Heat load, powering and protection, axial forces, collaring)
 - New features (Porous cable and ground-plane insulation, tuning shims)
 - Integrated design process (quench simulation, end-spacer design)
- Planning issues (How much R&D)

The EU and White-paper Framework



EU-FP7 and Accord-Technique (F)

Year	Q	Deliverables	Milestones	Accord-Technique
2008	4		Component qualification (6.1)	
2009	1		Basic magnetic design (6.2)	
	2	Basic MQXC design (6.1.1)		Cryostat proto. design review
	3		Coldmass design (6.3)	
	4	Model construction (6.2.1)	Cryomagnet design (6.4)	Cryostat proto. production review Cryostat f. corrector package design review Corrector magnet design Cold-bore tube tech. spec.
2010	1			Cryostat f. corrector package production readiness review Quench heater tech. spec. Collars for MQXC tech spec.
	2	Model cold-test and design assesment (6.2.2)		
	3	Corrector package construction (6.3.1)		
	4	Prototype construction (6.3.2)	Corrector package cold-test (6.7) MQXC ELQA (6.6)	Cryostat prototype tooling installation Cryostat component delivery Corrector magnet series production start First quench-heater delivery Collar delivery for MQXC
2011	1	MQXC prototype cold-test (6.3.3)		Cryostat f. corrector package ready
	2	Complete IR design (6.3.4)		
	3			
	4			All corrector magnets delivered

EU-FP7 and Accord-Technique (F)

Year	Q	Deliverables	Milestones	Accord-Technique
2008	4		Component qualification (6.1)	
2009	1-4		Basic magnet design (6.2)	
2010	1	Basic MQXC design (6.1.1)		
	2			Cryostat proto. design review
	3		Coldmass design (6.3)	
	4	Model construction (6.2.1)	Cryomagnet design (6.4)	Cryostat proto. production review Cryostat f. corrector package design review Corrector magnet design Cold-bore tube tech. spec.
2011	1			Cryostat f. corrector package production readiness review Quench heater tech. spec. Collars for MQXC tech spec.
	2	Model cold-test and design assesment (6.2.2)		
	3	Corrector package construction (6.3.1)		
	4	Prototype construction (6.3.2)	Corrector package cold-test (6.7) MQXC ELQA (6.6)	Cryostat prototype tooling installation Cryostat component delivery Corrector magnet series production start First quench-heater delivery Collar delivery for MQXC
2012	1	MQXC prototype cold-test (6.3.3)		Cryostat f. corrector package ready
	2	Complete IR design (6.3.4)		
	3			
	4			All corrector magnets delivered

EU-FP7 and Accord-Technique (F)

Year	Q	Deliverables	Milestones	Accord-Technique
2010	1	Basic MQXC design (6.1.1)		Parameters fixed for all correctors (except for orbit correctors in Q2)
	2	All drawings (magnet, instrumentation and tooling)		
	3	All tooling (winding, curing, collaring, lifting, assembly, coil finishing, yoking) All components Coil measurements	Coldmass design (6.3)	
	4	Model construction (6.2.1)	Cryomagnet design (6.4)	Cryostat f. corrector package design review Corrector magnet design
2011	1	Test in vertical cryostat Integration in horizontal cryostat, test-bench preparation, cycling, field measurements		Cryostat f. corrector package production readiness review Quench heater tech. spec. Collars for MQXC tech spec.
	2	Model cold-test and design assesment (6.2.2)		
	3	Corrector package construction (6.3.1)		
	4	Prototype construction (6.3.2)	Corrector package cold-test (6.7) MQXC ELQA (6.6)	Corrector magnet series production start First quench-heater delivery Collar delivery for MQXC
2012	1	MQXC prototype cold-test (6.3.3)		Cryostat f. corrector package ready
	2	Complete IR design (6.3.4)		
	3			
	4			All corrector magnets delivered

List of Components, Tooling, Assembly Activities, and Tests (MQXC)

Components	Tooling	Assembly	Tests/Studies
Concept design	Concept design	Started	
Drawing	Drawing	Finished	
Specifications	Manufacture		
Prototype	Installation		
(Series) manufacture			
Coil (50%)	Coil winding mandrel (20%)	Insulate and cut wedges	Arch curing tests
End-spacers (80%)	Curing mold assembly (50%)	Cure and measure coil packs	Arch E-modulus test
Ramp and splice box (50%)	Collar pack assembly tooling (0%)	Calculate best position of coils	Cold test 150 mm model
Copper wedges (100%)	Assembly for collar packs on coil (100%)	Assemble collar packs	
Quench heaters (80%)	Multipurpose test press (Hydraulics) (100%)	Assemble 150 mm model	
Wiring diagrams (0%)	Collaring press horizontal (100%)		
Capacitance gauges (100%)	Auxiliary tooling for collaring press (50%)	Insulate cable	Quench heater discharge
Strain gauges (100%)	Ground insulation former (0%)	Insulate Cu wedges	Quench heater high-pot
Spot heaters (0%)	Layer jump and splice former (0%)	Coil winding	Connection box
Head shims (0%)	E-mod size press (straight section) (80%)	Coil curing	
Collars (Instrumented) (100%)	E-mod size press (end section) (0%)	Coil size measurements	
Collar (Non-instrumented) (0%)	Steel dummy coils (straight section)	Collaring	Warm magnetic field meas. 1
Collar (Punched) (0%)	Steel dummy coils (end section)	Mechanical measurements	Warm magnetic field meas. 2
Collaring shoe (100%)	Collapsible mandrel for apert. assemb. (short)	Warm magnetic field measurements	
Collaring keys (100%)	Collar rectification table	Mount end flanges	Cold test in vertical cryostat:
Ground insulation (50%)	Longitudinal compaction press	Solder electrical joints	Field quality
Pole turn fishbones (60%)	Lifting tooling	Yoke assembly	Quench behavior
Outer layer fish-bone (60%)	Quench heater fabrication tooling	Warm magnetic field measurements	
Yoke laminations (Wire, punched) (100%)	Soldered joint tooling		Cold test in horizontal cryostat
Yoking tie rods and nut assembly (0%)			Dump
Aperture end plate components (0%)			Quench heater delay
Joint box components (0%)			Propagation velocity
Yoke end plates (0%)			RRR
Main assembly drawing (20%)			Field quality
Instrumentation feedthrough system			Dynamic effects
Helium vessel			
End-domes			

MQXA (KEK)

5 years

- [1996_asc_Design.pdf](#)
- [1998_asc_Model_test.pdf](#)
- [1998_epac_TUP20G.pdf](#)
- [1999_mt16_00828194.pdf](#)
- [1999_mt16_Mech_tolerance.pdf](#)
- [2000_asc_5Model_comp..pdf](#)
- [2000_asc_00920090.pdf](#)
- [2000_asc_00920094.pdf](#)
- [2001_mt17_01018377.pdf](#)
- [2001_mt17_01018386.pdf](#)
- [2001_mt17_01018733.pdf](#)
- [2001_mt17_Prototype_testing.pdf](#)
- [2002_asc_01211840.pdf](#)

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IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY, VOL. 12, NO. 1, MARCH 2002

Quench Protection Study of a Prototype for the LHC Low-Beta Quadrupole Magnets

Tatsushi Nakamoto, Earle E. Burkhardt, Toru Ogitsu, Akira Yamamoto, Takakazu Shintomi, and Kiyosumi Tsuchiya

IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY, VOL. 7, NO. 2, JUNE 1997

Design Study of a Superconducting Insertion Quadrupole Magnet for the Large Hadron Collider

A. Yamamoto, K. Tsuchiya, N. Higashi, T. Nakamoto, T. Ogitsu, N. Ohuchi, T. Shintomi, and A. Terashima
National Laboratory for High Energy Physics (KEK), Tsukuba, Ibaraki, 305, Japan

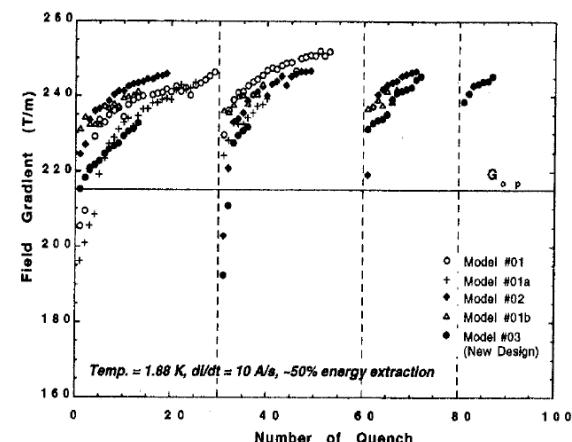
G. Kirby*, R. Ostoja, and T. M. Taylor
European Laboratory for Particle Physics (CERN), 23 Geneve, CH-1211, Switzerland

IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY, VOL. 9, NO. 2, JUNE 1999

Quench and Mechanical Behavior of an LHC Low- β Quadrupole Model

T. Nakamoto, K. Tanaka, A. Yamamoto, K. Tsuchiya, E. Burkhardt, N. Higashi,
N. Kimura, T. Ogitsu, N. Ohuchi, K. Sasaki, T. Shintomi, and A. Terashima,
High Energy Accelerator Research Organization (KEK), 1-1 Oho, Tsukuba, Ibaraki 305-0801, Japan

G. A. Kirby, R. Ostoja, and T. M. Taylor
European Laboratory for Particle Physics (CERN), 1211 Geneva 23, Switzerland



5 Models built (revision of inner layer)



MQXB (Fermilab)

5 years

- 1996_asc_00614571.pdf
- 1996_epac_Design.pdf
- 1996_epac_MOP045G.pdf
- 1997_pac_6P001.pdf
- 1997_pac_6P004.pdf
- 1998_asc_00783334.pdf
- 1998_asc_Model_test.pdf
- 1999_mt16_00828186.pdf
- 1999_mt16_00828187.pdf
- 1999_mt16_00828189.pdf
- 1999_pac_THP96.pdf
- 1999_pac_THP103.pdf
- 2000_asc_9Model_performance.pdf
- 2001_mt17_01018352.pdf
- 2001_mt17_01018368.pdf
- 2001_mt17_Protoype_result.pdf
- 2002_asc_01211835.pdf
- 2003_pac_WPAE015.pdf
- 2004_asc_01439830.pdf
- 2004_asc_01439834.pdf
- 2005_mt19_01642881.pdf
- 2005_nim.pdf
- 2006_epac_WEPLS109.pdf

Field Measurement of a Fermilab-Built Full Scale Prototype Quadrupole Magnet for the LHC Interaction Regions

R. Bossert, R. Carcagno, J. DiMarco, S. Feher, H. Glass, J. Kerby, M. J. Lamm, A. Nobrega, T. Nicol, T. Ogitsu, D. Orris, T. Page, R. Rabehl, G. Sabbi, P. Schlabach, J. Strait, C. Sylvester, M. Tartaglia, J. C. Tompkins, G. Velev, and A. V. Zlobin

DESIGN OF A HIGH GRADIENT QUADRUPOLE FOR THE LHC INTERACTION REGIONS

R. Bossert, S.A. Gourlay, T. Heger, Y. Huang, J. Kerby, M.J. Lamm, P.J. Limon, P.O. Mazur, F. Nobrega, J.P. Ozelis, G. Sabbi, J. Strait, A.V. Zlobin
Fermilab, Batavia, Illinois, USA;

S. Caspi, D. Dell'orco, A.D. McInturff, R. M. Scanlan, J.M. Van Oort
Lawrence Berkeley National Laboratory, Berkeley, California, USA;
R.C. Gupta, Brookhaven National Laboratory, Upton, New York, USA

IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY, VOL. 9, NO. 2, JUNE 1999

Design, Development and Test of 2m Quadrupole Model Magnets for the LHC Inner Triplet

J. Kerby, A.V. Zlobin, R. Bossert, J. Brandt, J. Carson, D. Chichili, J. Dimarco, S. Feher, M.J. Lamm, P.J. Limon, A. Makarov, F. Nobrega, I. Novitski, D. Orris, J.P. Ozelis, B. Robotham, G. Sabbi, P. Schlabach, J.B. Strait, M. Tartaglia, J.C. Tompkins, Fermi National Accelerator Laboratory, Batavia, Illinois, USA

S. Caspi, A.D. McInturff, R. Scanlan,
Lawrence Berkeley National Laboratory, Berkeley, California, USA

TABLE V
Quench current and b_6 as a function of coil curing cycle

	coil curing cycle		I_c	$\Delta b_6, 6kA$
	temperature	pressure	300 A/s	40 A/s
HGQ01	135°	low	10965	0.02
HGQ02	190°	low	11335	0.21
HGQ03	195°	low	11298	0.16
HGQ05	130°	low	10519	0.12
HGQ06	190°	high	6433	-1.04
HGQ07	190°	high	4487	-0.55
HGQ08	190°	high	3941	-0.72
HGQ09	190/135°	low/high	12946	0.13

9 Models (change of cables)

Can we do Better than 4-5 Years ?

Pro

Contra

More advanced simulation tools

Cable available

Heat load
(porous insulation; coil modulus)

Integrated design and manufacture for end-spacers

Large aperture

Busbar design and routing

Faster link between CAD and FE modeling

EU-Industrial suppliers

Horizontal collaring (new press to be procured)

More sophisticated CAD/CAM

EU/White paper

Magnet protection (nested PCs, heaters)

Existing specifications

Technical experience

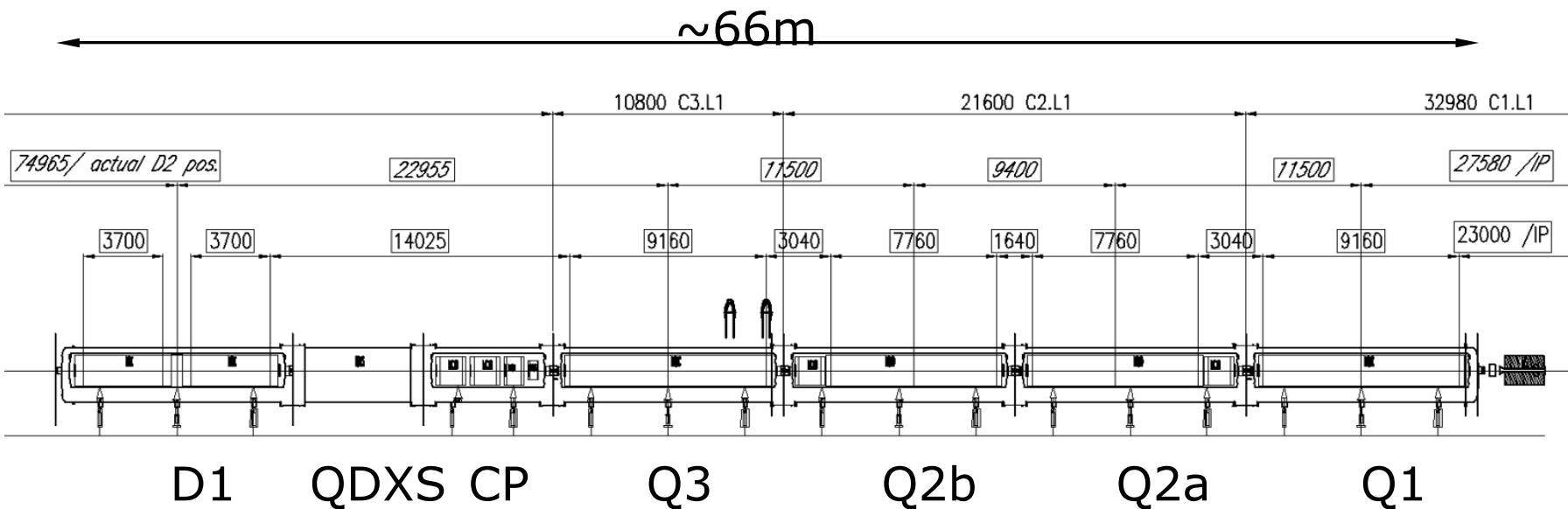
Axial forces

Cryostat identical to MB

In-house production

EU-Certification of tooling

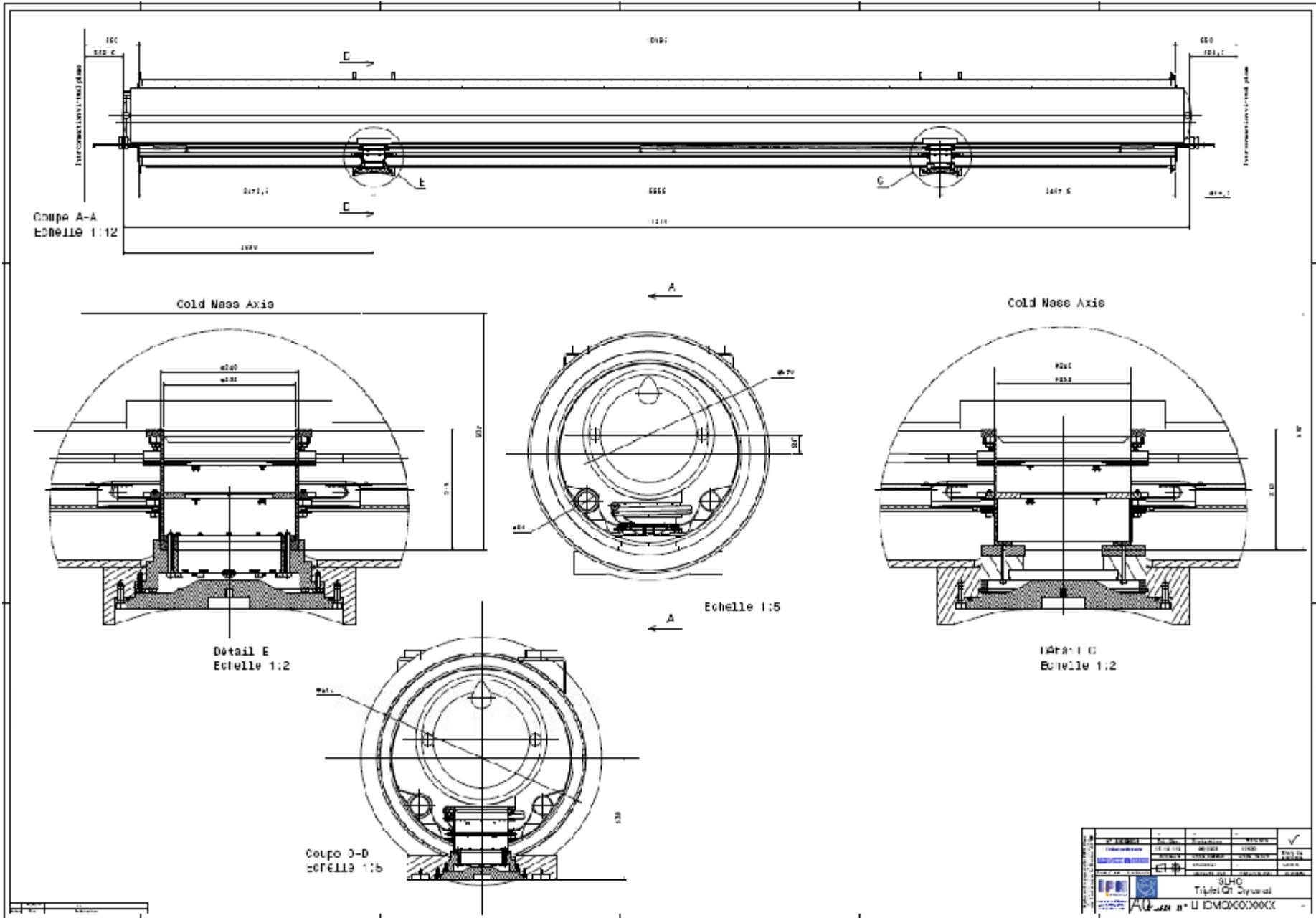
Layout – General Overview



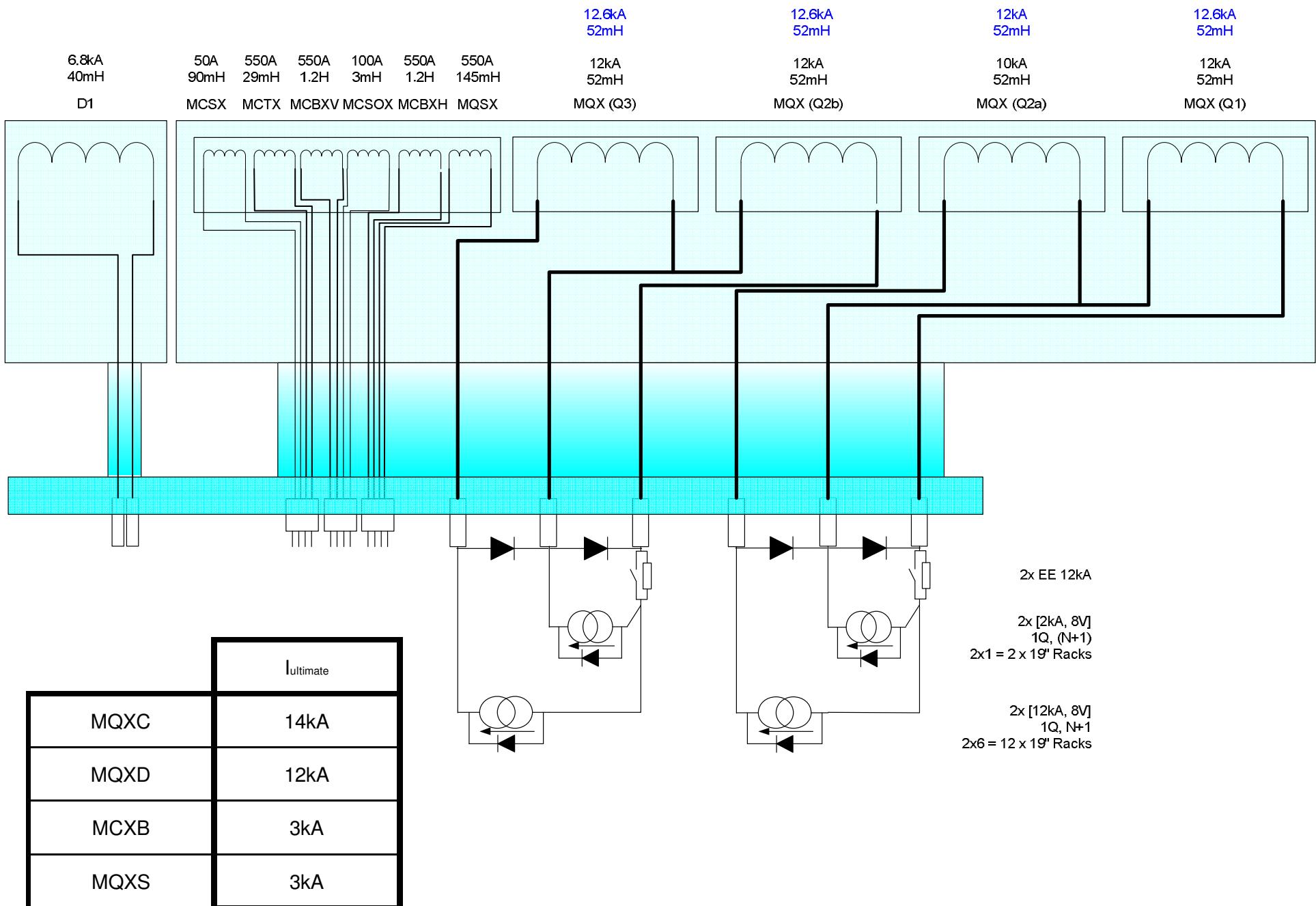
- One cryostated cold mass per main magnet
- Part of the correctors located in an individual cold mass (CP)
- Distribution feed box removed from the tunnel
- Magnets, cold masses and cryostating performed at CERN (except D1&DFX)
- Maximum standardization with the existing LHC components
- Matching section magnets are left in their current position

	Drawing	Magnets	Cold mass length	Cryostat length	Dist btw supports
Q1 = Q3		MQXC (Lmag = 9160mm)			
Q2a		MQXD + MCXB (Lmag = 7760mm) (Lmag ≈ 1040mm)			3.594m
Q2b		MQXD + MCXB (Lmag = 7760mm) (Lmag ≈ 1040mm)	10.080m	9.7m	Depending on W bellows Identical to the ones in separation dipoles D2, D3, D4
D1		MBXC x 2 (Lmag = 3700mm)			

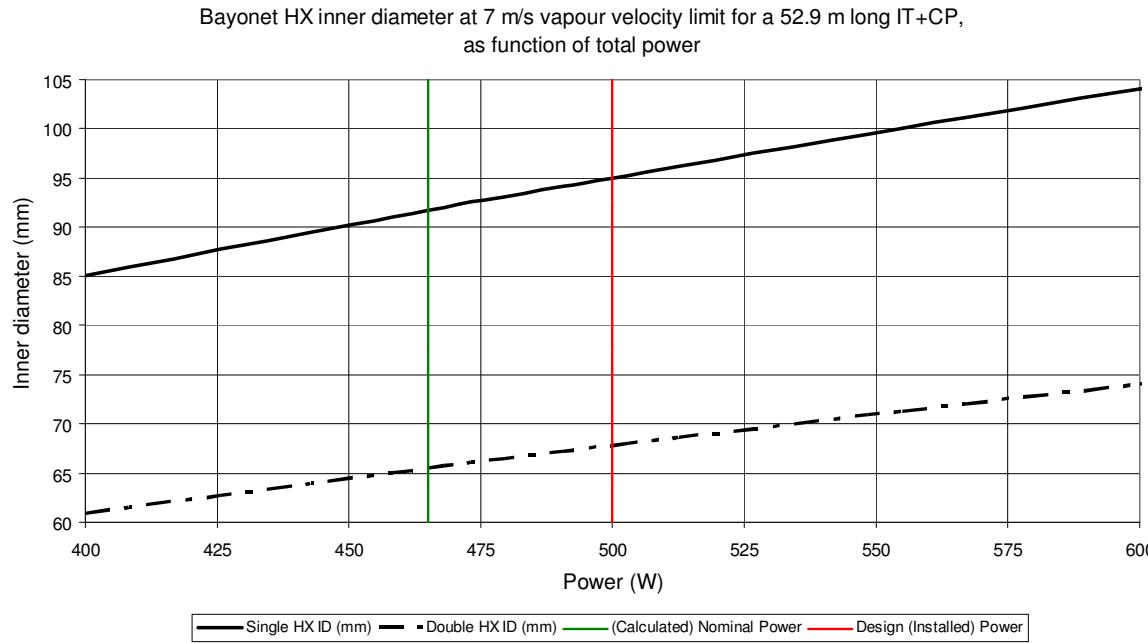
Cryostat Design identical to MB



Electrical Powering Scheme

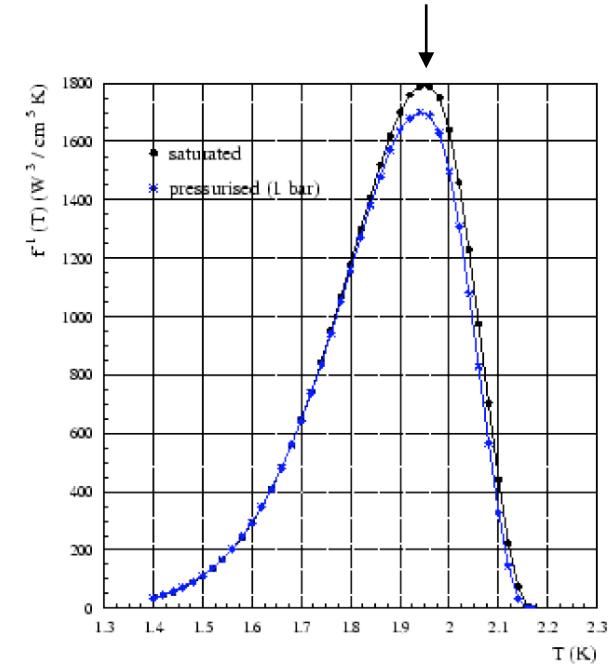
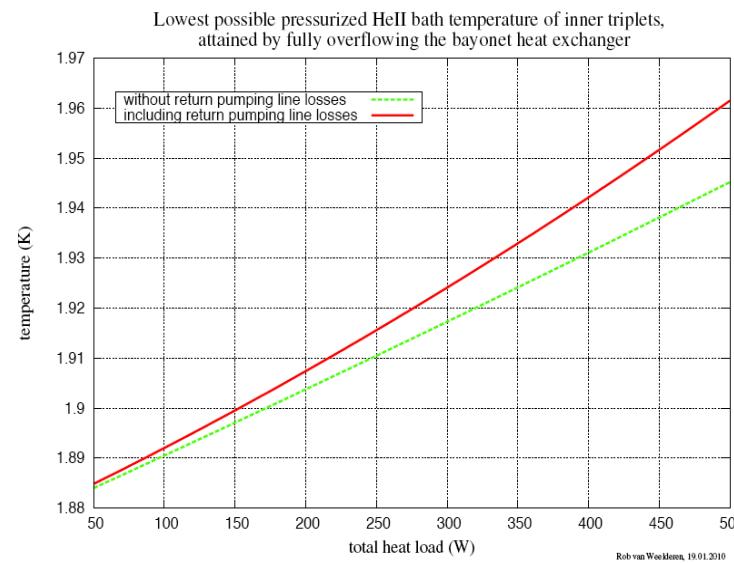


Heat-Load and Cooling Requirements

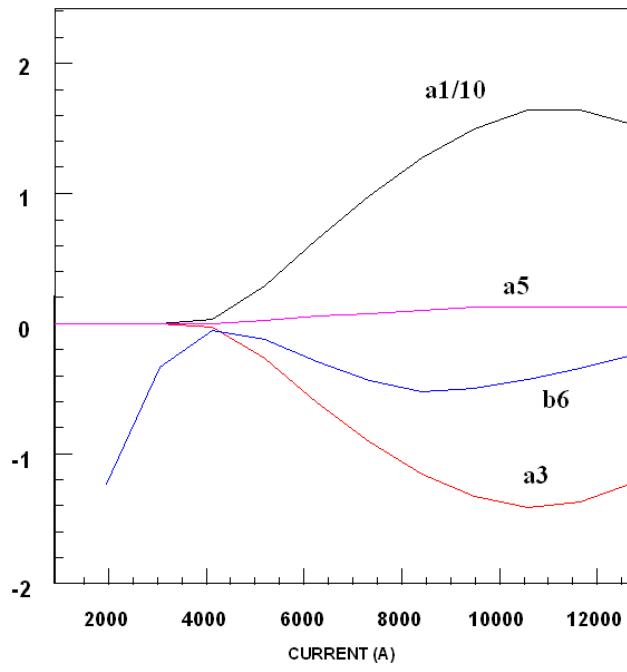
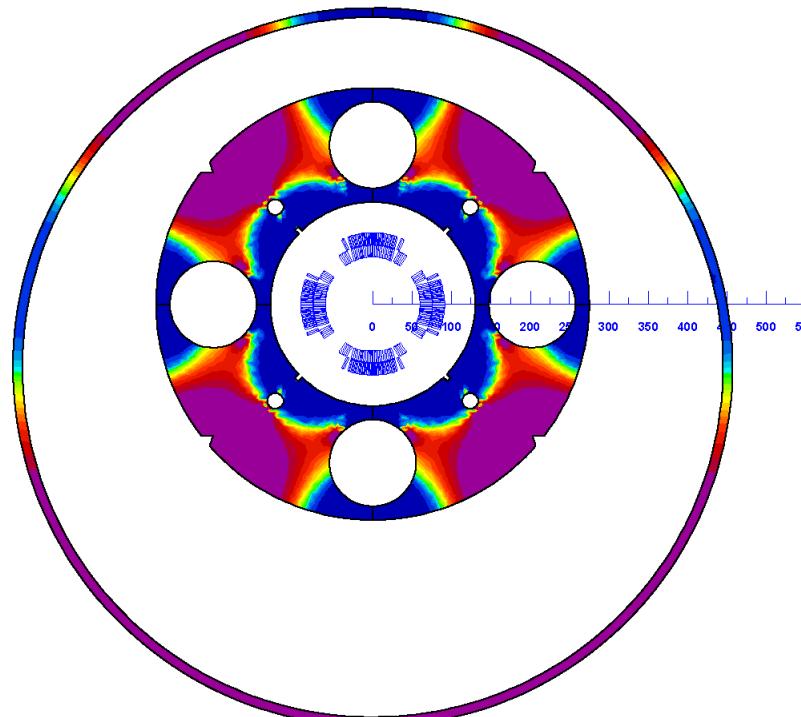
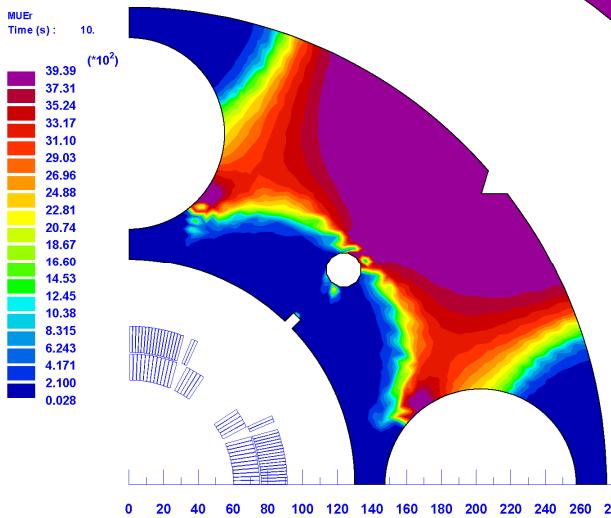


Consequence:
Redesign of magnet cross section

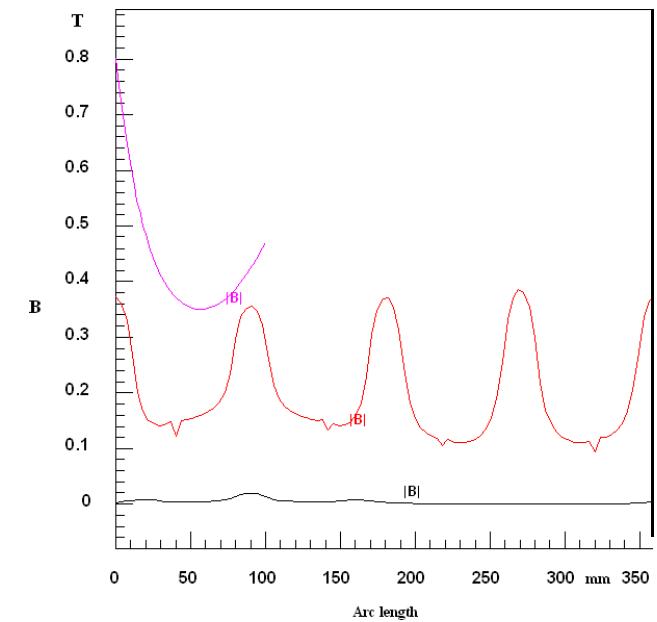
Consequence:
More porous insulation (coil and ground-plane)



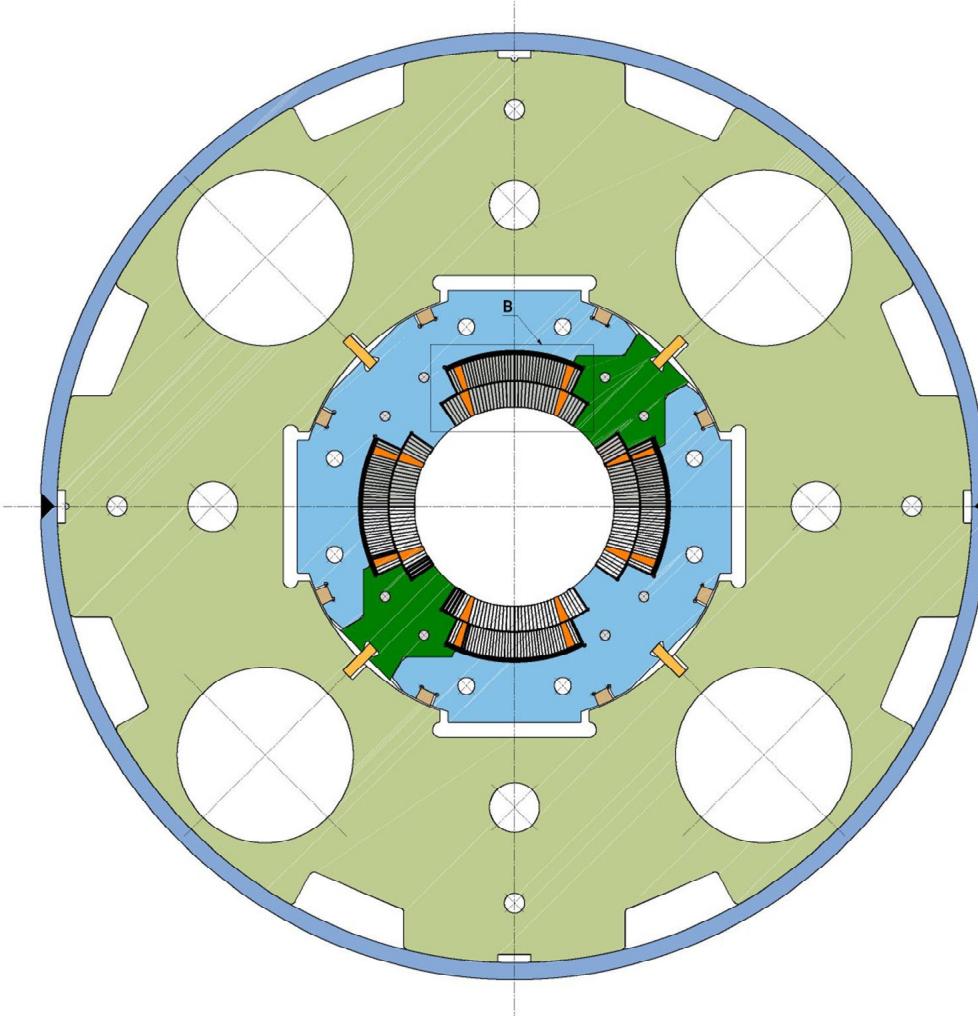
Baseline-Design (105 mm Heat-Exchanger at Mid-Plane)



Saturation effects
from off-centered
cryostat



Low- β Quadrupole MQXC

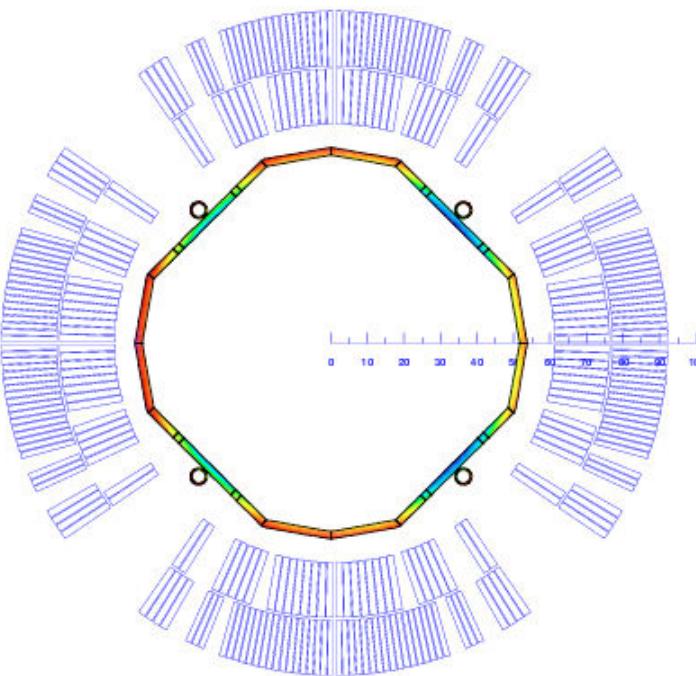
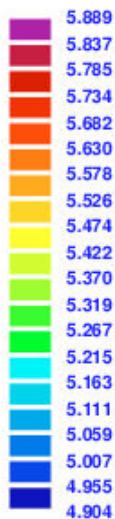


- ➔ Coil aperture 120 mm
- ➔ Gradient 127 T/m
- ➔ Operating temp 1.9 K
- ➔ Current 13.8 kA
- ➔ WP on load-line 85%
- ➔ Inductance 5.2 mH/m
- ➔ Yoke ID 260 mm
- ➔ Yoke OD 550 mm
- ➔ Magnetic length 9160 mm (Q1,Q3)
7760 mm (Q2)

- ➔ LHC cables 01 and 02
- ➔ Porous cable polyimide insulation
- ➔ Yoke OD identical to MB
- ➔ Self-supporting collars
- ➔ Single piece yoke
- ➔ Welded-shell cold mass

Beam Screen Type 1 (Field Quality for Eccentricity of 1 mm)

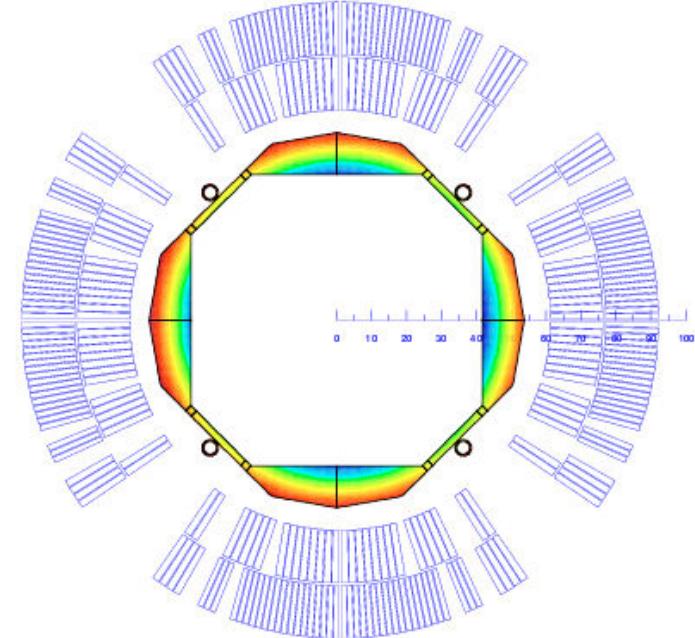
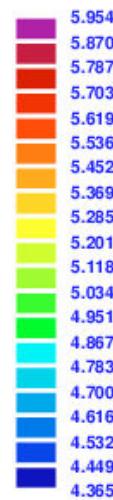
$|B_{tot}|$ (T)



NORMAL RELATIVE MULTipoles (1.D-4):

b 1:	0.00316	b 2:	10000.00000	b 3:	-0.00486
b 4:	-0.00338	b 5:	-0.02279	b 6:	-0.19069
b 7:	0.00512	b 8:	0.00497	b 9:	0.02075
b10:	0.09316	b11:	-0.00266	b12:	-0.00394
b13:	-0.01022	b14:	0.11445	b15:	0.00133

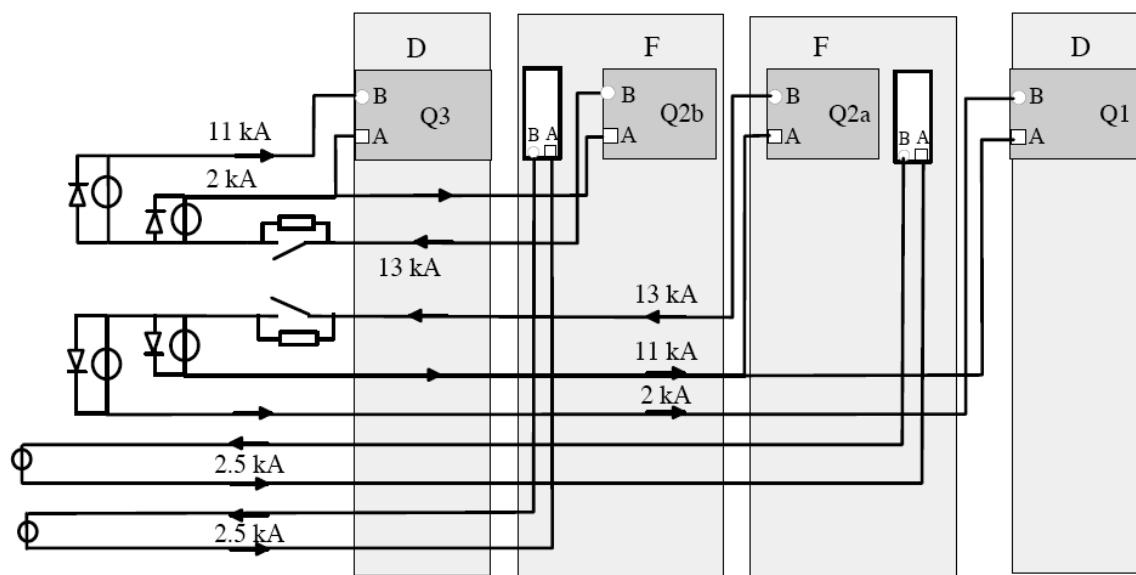
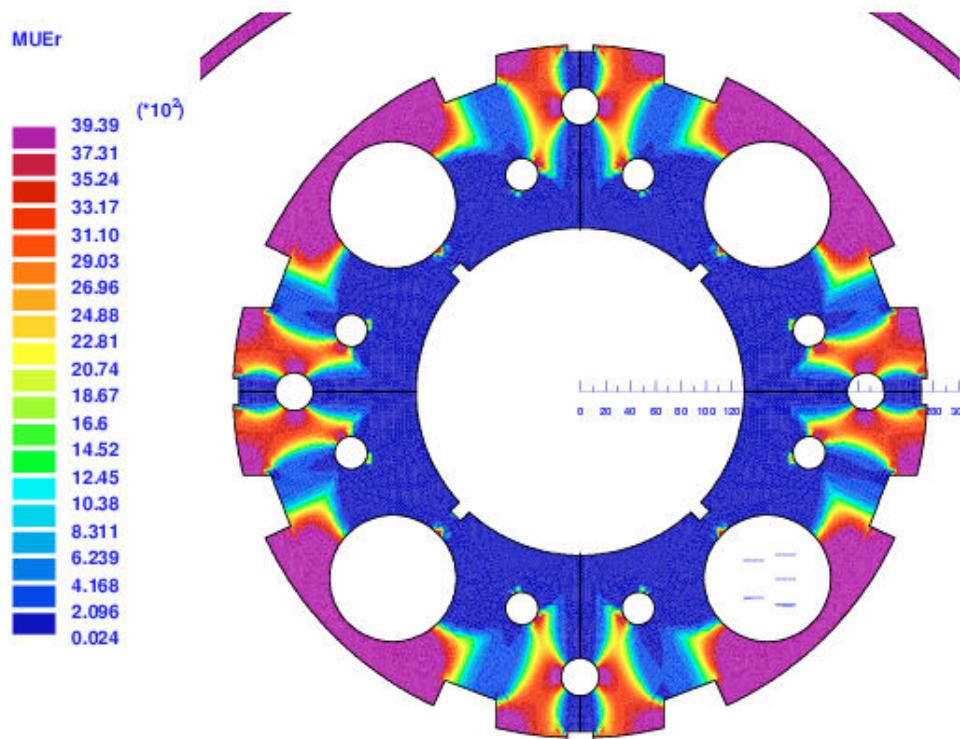
$|B_{tot}|$ (T)



NORMAL RELATIVE MULTipoles (1.D-4):

b 1:	-0.06983	b 2:	10000.00000	b 3:	0.07682
b 4:	-0.00505	b 5:	-0.04988	b 6:	-0.41232
b 7:	0.01509	b 8:	0.01626	b 9:	0.12523
b10:	0.55097	b11:	-0.01056	b12:	-0.00870
b13:	-0.04982	b14:	-0.01027	b15:	0.00306

Cartridge Solution

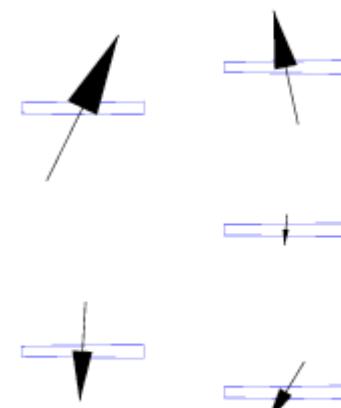


NORMAL RELATIVE MULTipoles (1. D-4):

b 1:	3.38036	b 2:	10000.00000	b 3:	0.43334
b 4:	0.63923	b 5:	-0.03264	b 6:	1.34425
b 7:	0.00177	b 8:	0.00644	b 9:	-0.00034
b10:	-0.00065	b11:	0.00001	b12:	0.00002
b13:	0.00000	b14:	0.06372	b15:	0.00000
b16:	0.00000	b17:	0.00000	b18:	0.12829
b19:	0.00000	b20:	0.00000	b	

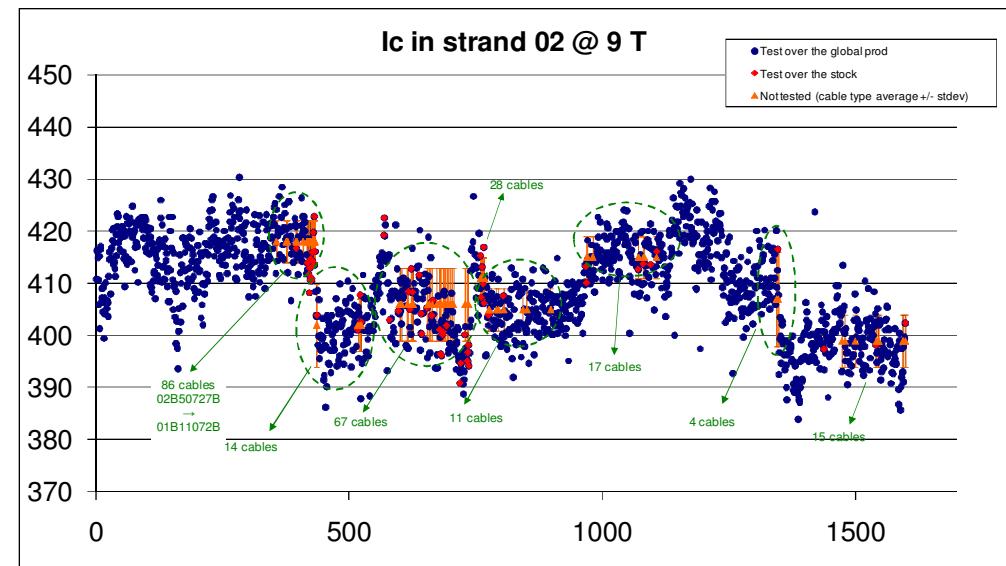
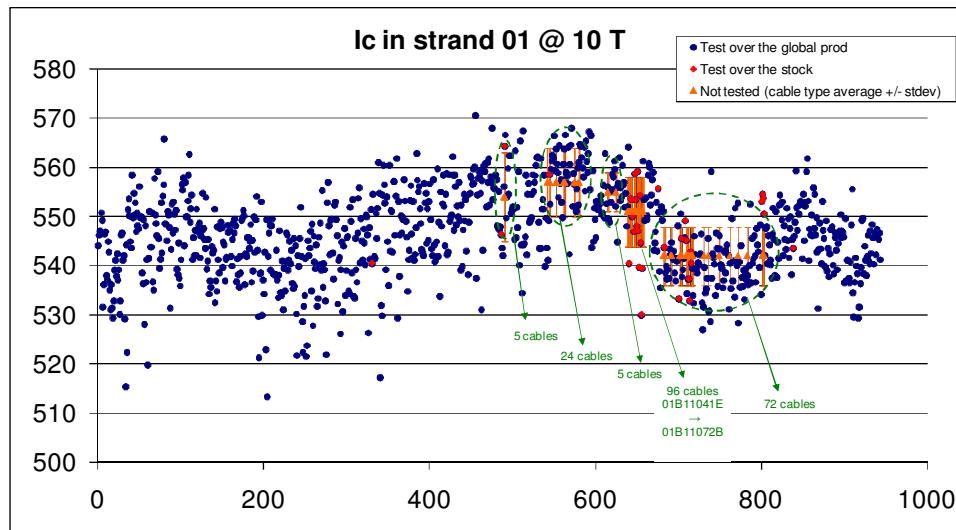
SKEW RELATIVE MULTipoles (1. D-4):

a 1:	-2.75975	a 2:	0.35356	a 3:	0.64007
a 4:	0.21998	a 5:	0.01367	a 6:	-0.00172
a 7:	0.00222	a 8:	0.00133	a 9:	0.00013
a10:	-0.00004	a11:	0.00000	a12:	0.00000
a13:	0.00000	a14:	0.00000	a15:	0.00000
a16:	0.00000	a17:	0.00000	a18:	0.00000
a19:	0.00000	a20:	0.00000	a	



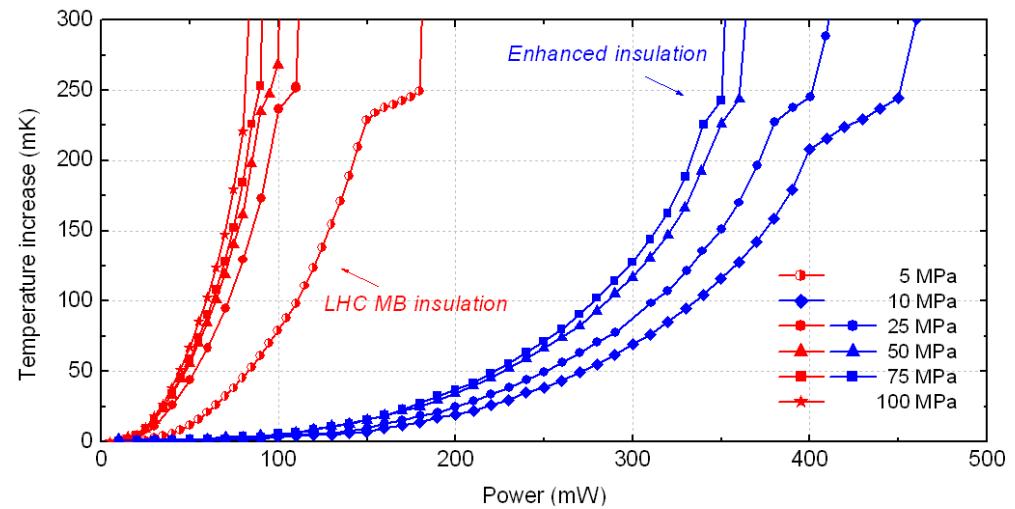
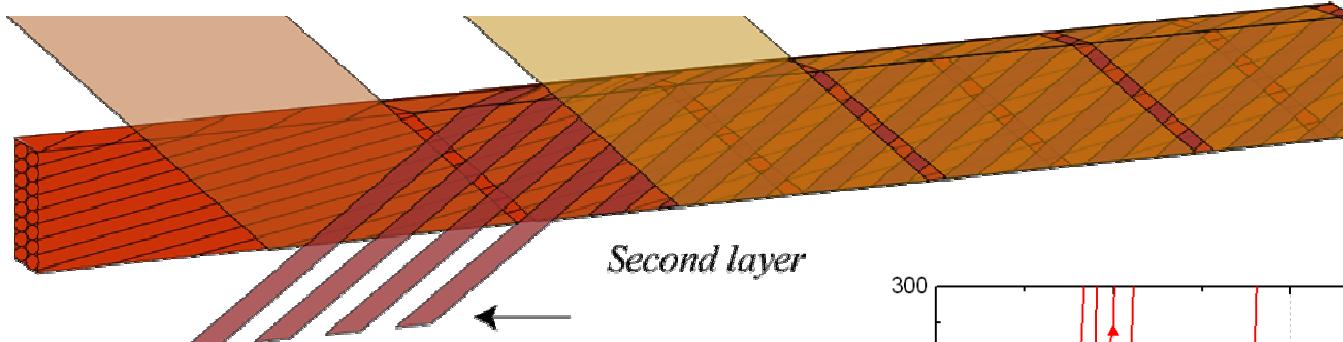
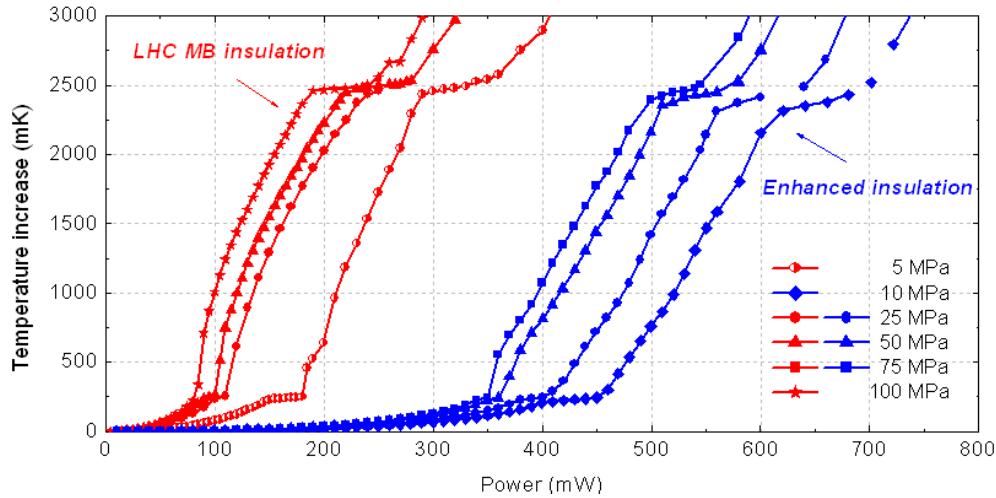
BLOCK	FORCE -X- (N/m)	FORCE -Y- (N/m)
7	-0.1617E+03	-0.2908E+04
8	0.2113E+04	0.4293E+04
9	-0.1105E+04	-0.1804E+04
10	-0.6970E+02	-0.8870E+03
11	-0.7191E+03	0.3349E+04
SUMM:	0.5749E+02	0.2043E+04

Selection of Cables

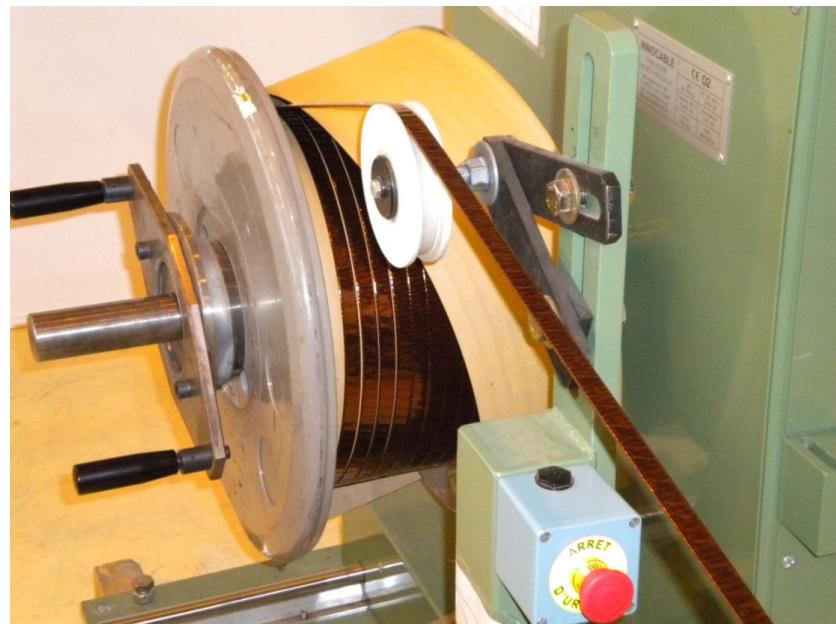
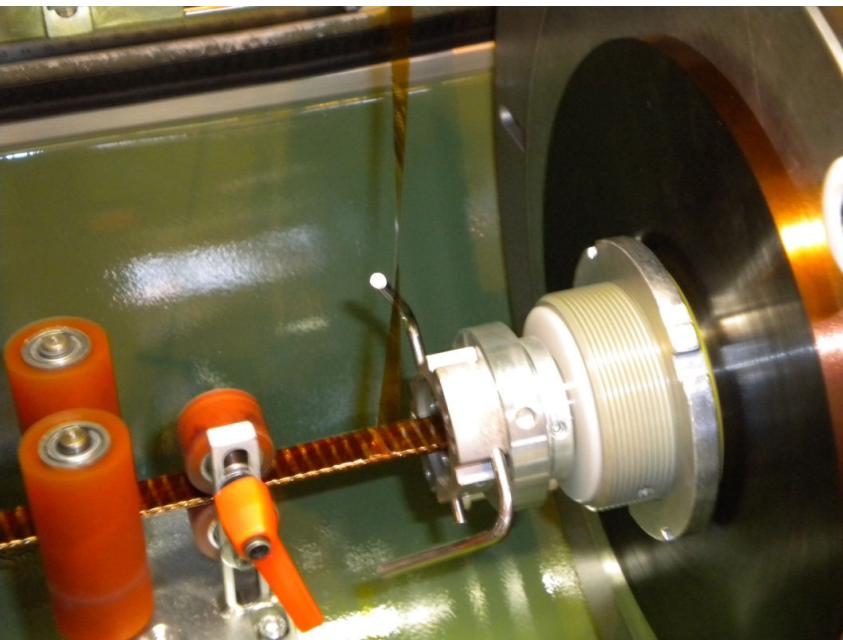
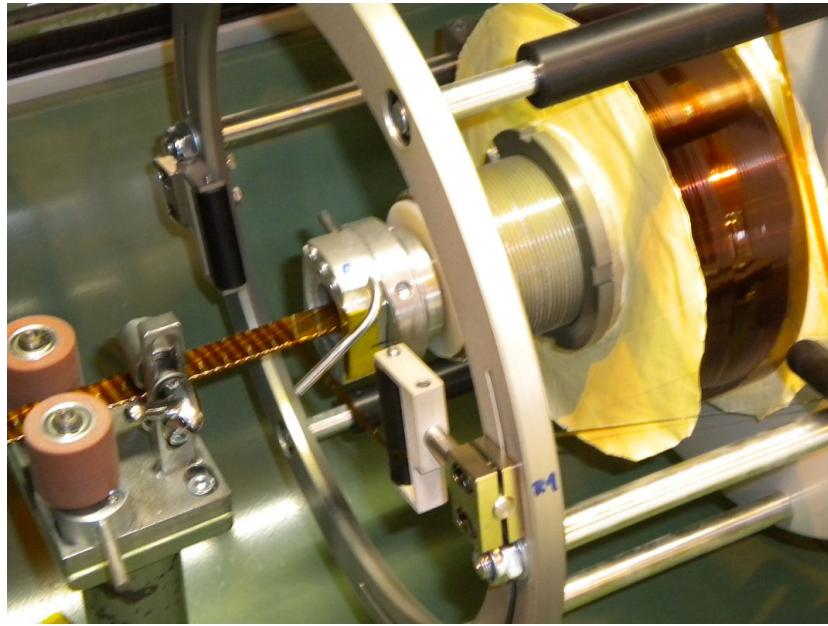
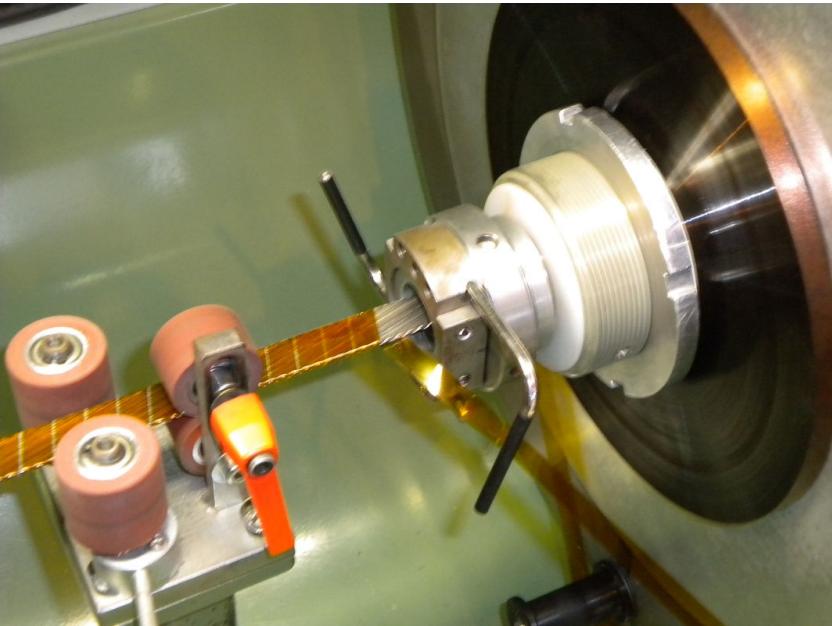


Aperture diameter [mm]	Magnetic length [m]	Inner layer turns	Outer layer turns	Total cable inner layer [m]	Inner layer unit length [m]	Total Outer layer [m]	Outer layer unit length [m]
110	9	15	19	320	448	400	740
120	10.3	18	19	420	448	445	740
130	11.5	18	24	445	448	590	740

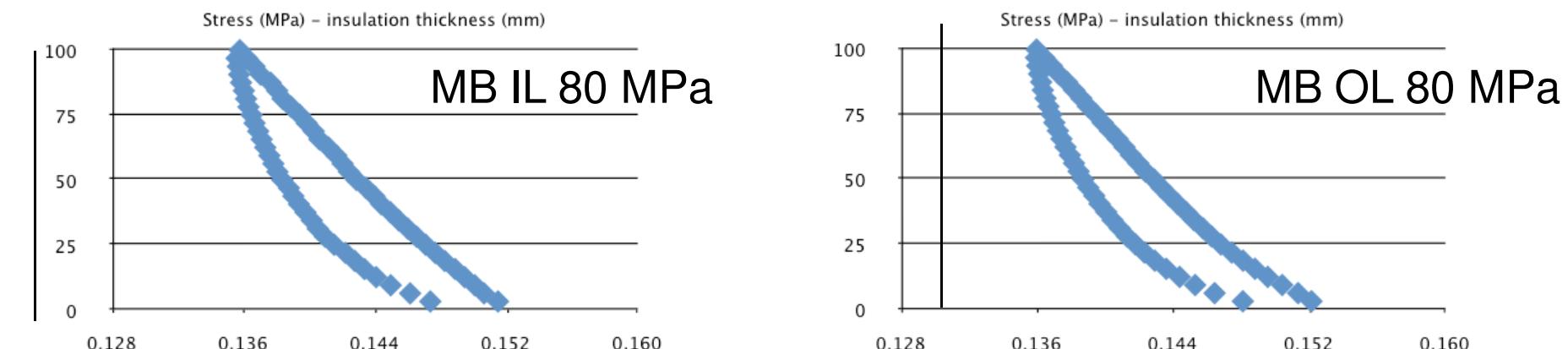
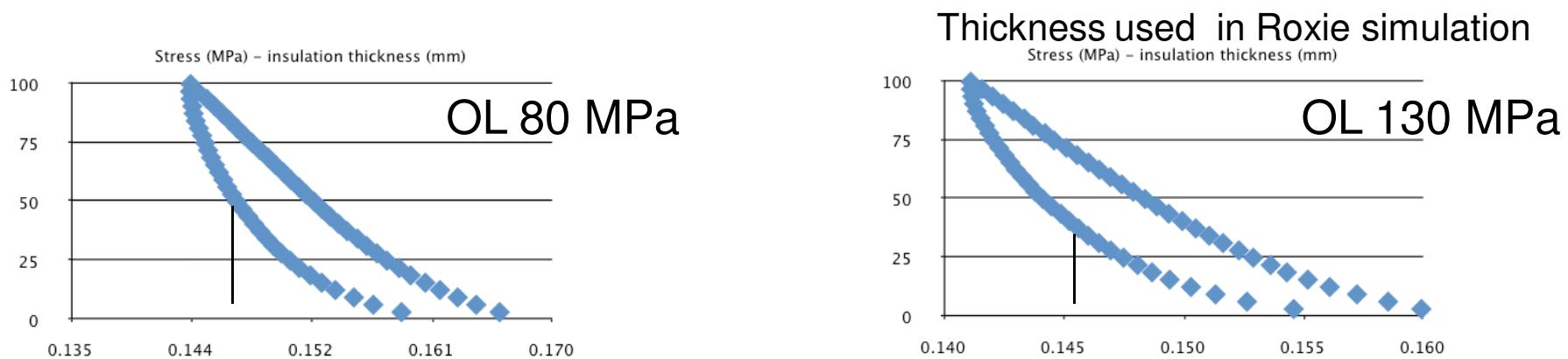
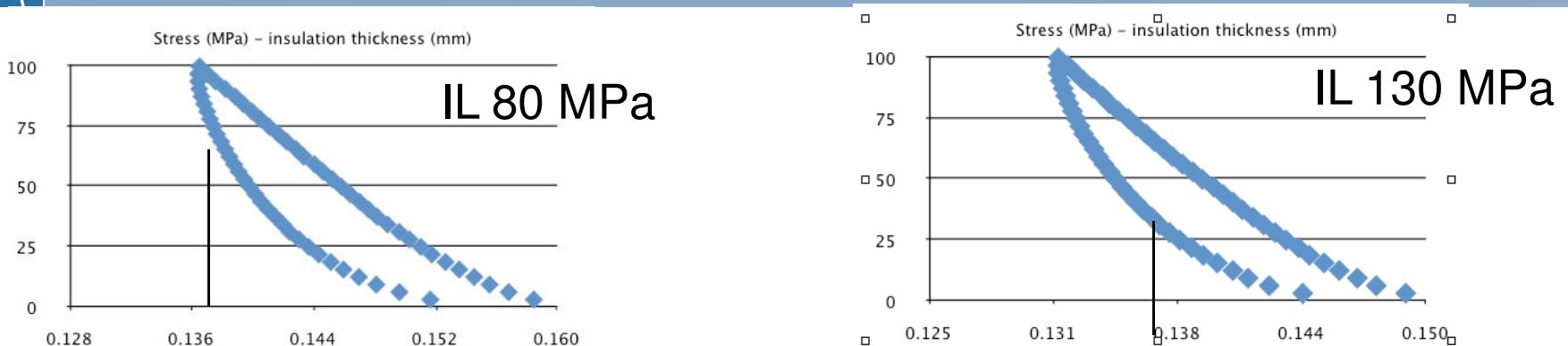
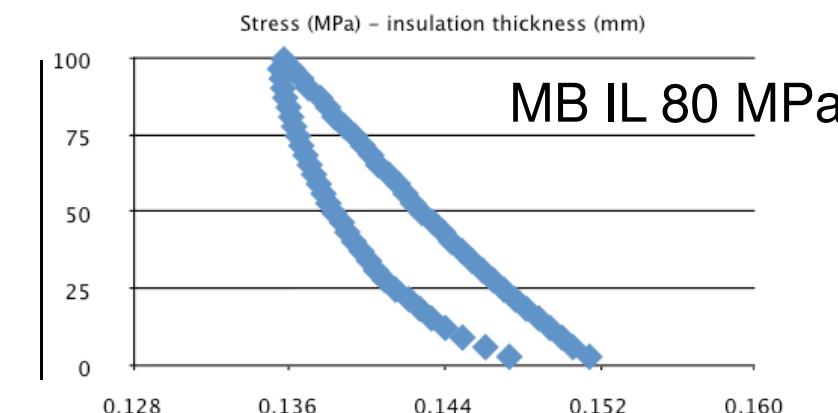
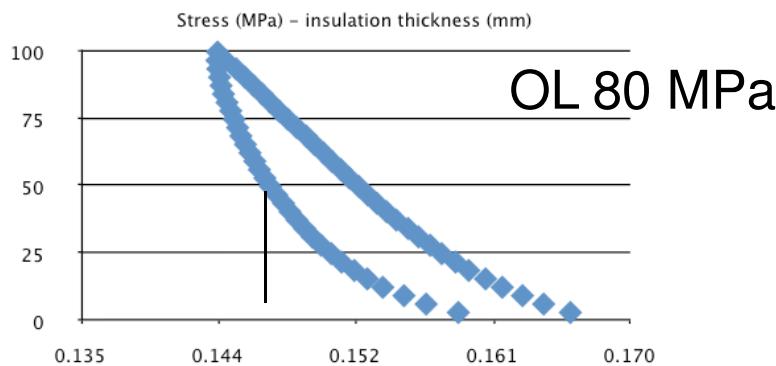
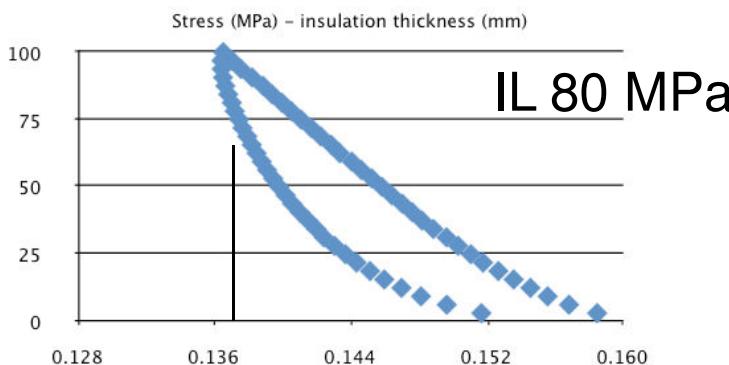
Heat Transfer up to $T \lambda$ and up to 3 K



Wrapping Machine fully Commissioned



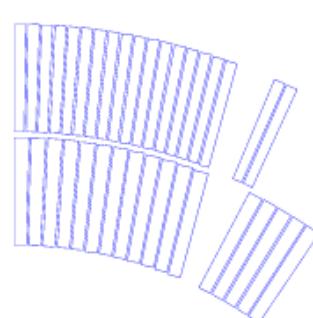
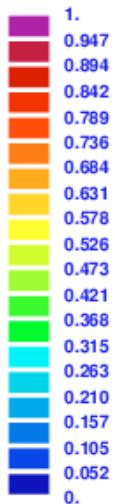
Insulation Thickness



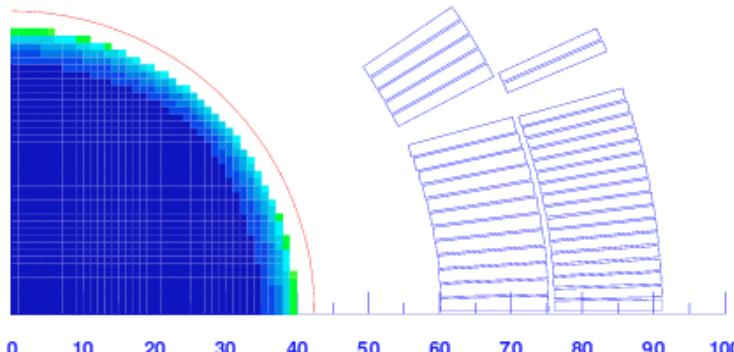
Instrumented collar pack needed for final verification

Coil Layouts

Rel. field errors (units 10^{-4})

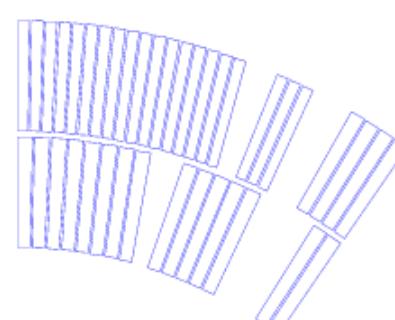
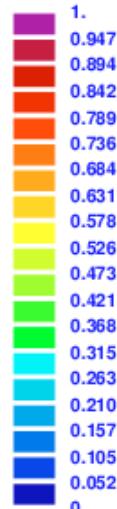


4-block

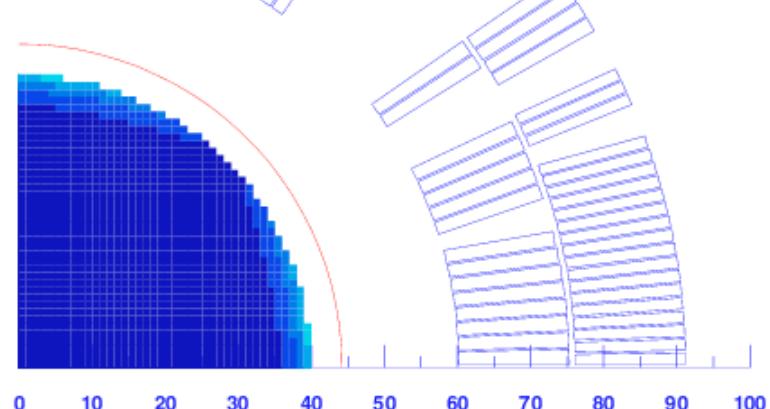


BEMFEM * ROXIE_{10.1}

Rel. field errors (units 10^{-4})



6-block



BEMFEM * ROXIE_{10.1}

Geometric !

NORMAL RELATIVE MULTipoles (1.D-4) :

b 1:	0.00000	b 2:	10000.00000	b 3:	0.00000
b 4:	0.00000	b 5:	0.00000	b 6:	-0.00015
b 7:	0.00000	b 8:	0.00000	b 9:	0.00000
b10:	0.00015	b11:	0.00000	b12:	0.00000
b13:	0.00000	b14:	-0.05686	b15:	0.00000

NORMAL RELATIVE MULTipoles (1.D-4) :

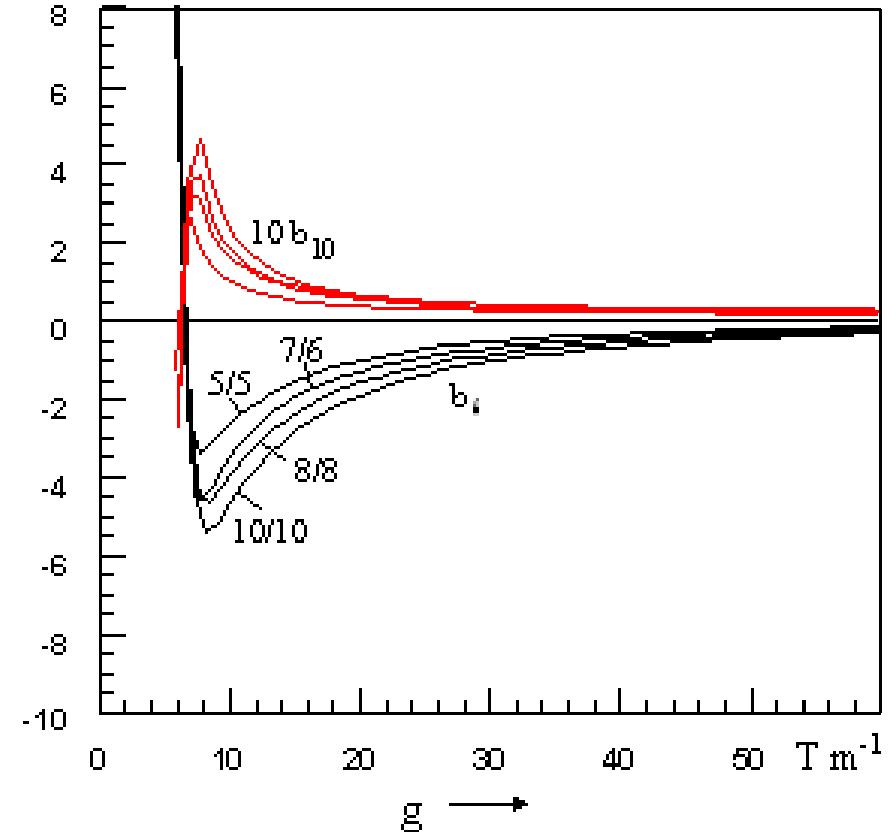
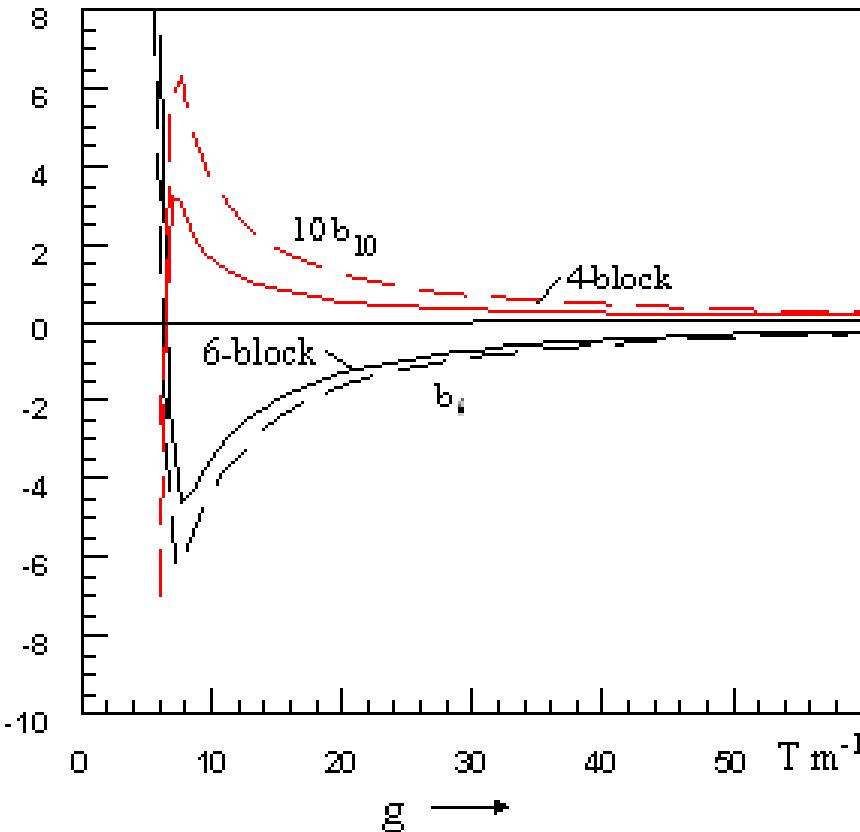
b 1:	0.00000	b 2:	10000.00000	b 3:	0.00000
b 4:	0.00000	b 5:	0.00000	b 6:	-0.00031
b 7:	0.00000	b 8:	0.00000	b 9:	0.00000
b10:	-0.00001	b11:	0.00000	b12:	0.00000
b13:	0.00000	b14:	0.13018	b15:	0.00000

12804 A, 79.6% on load-line

NL – calc.

12683 A, 78.45% on load-line

Persistent Current Multipoles



Sensitivity of Multipole Field Errors

Separate powering

	4-block	6-block
Only outer layer: b_6	128.9	0.803
Only outer layer: b_{10}	-4.99	0.202
Only inner layer: b_6	-115.7	-0.905
Only inner layer: b_{10}	4.48	-0.227

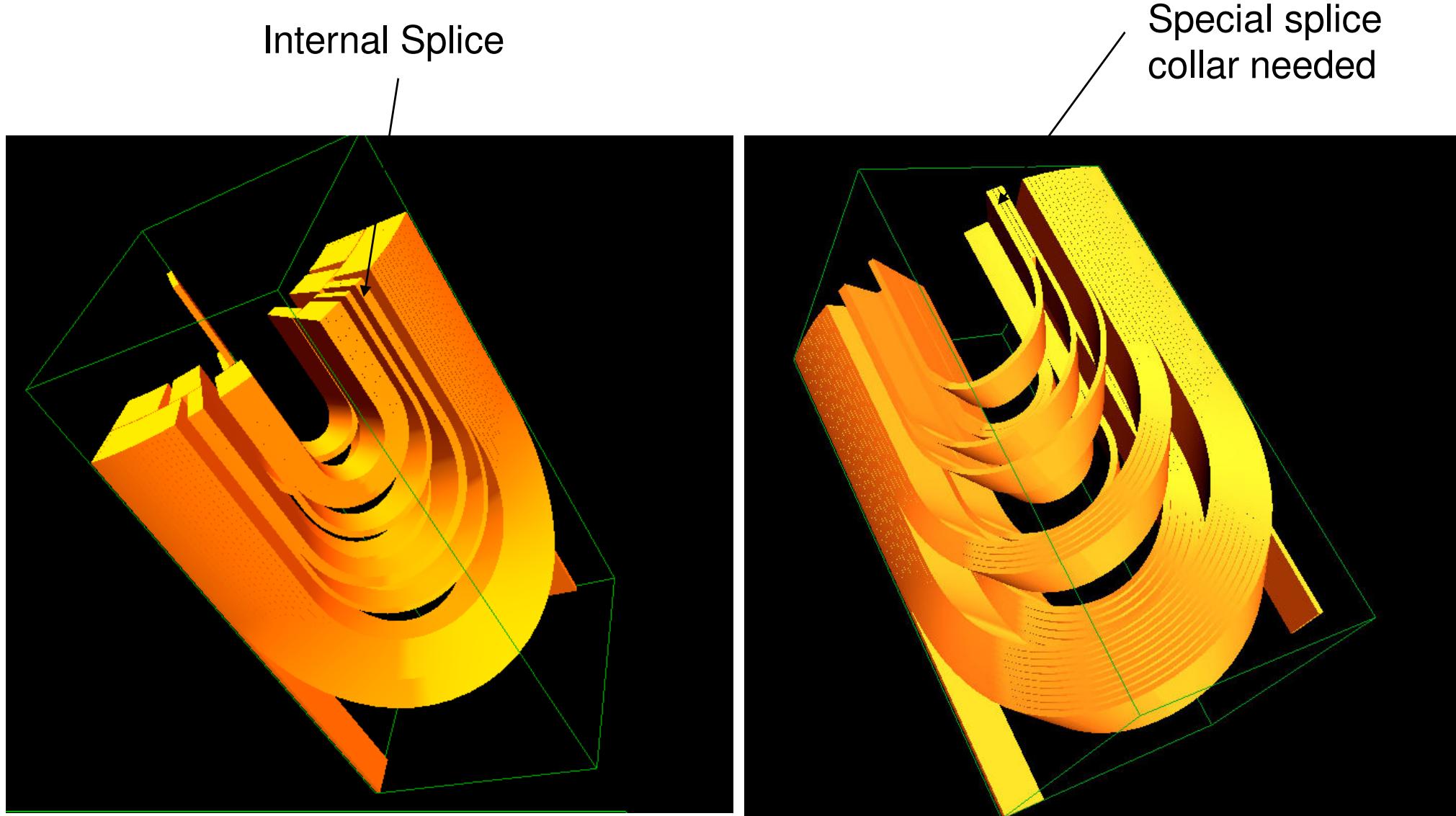
	4-block	6-block
b_1	0.767	0.684
b_3	0.623	0.534
b_4	0.446	0.398
b_5	0.330	0.258
b_6	0.218	0.188
b_7	0.137	0.119
b_8	0.093	0.086
b_9	0.056	0.054
b_{10}	0.034	0.037

Coil size effect

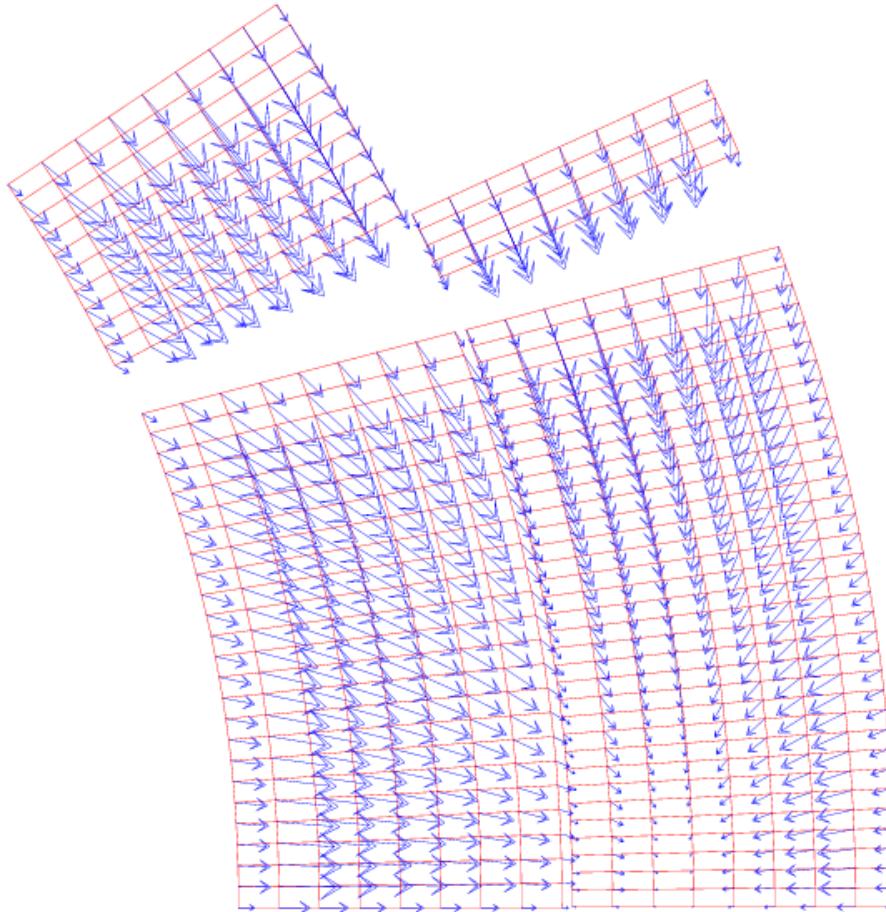
	4-block	6-block
Nominal: b_6	-0.0335	0.
Nominal: b_{10}	0.0005	0.
Inner + 0.34, Outer + 0.34: b_6	-7.75	-6.49
Inner + 0.34, Outer + 0.34 b_{10}	0.699	0.344
Inner + 0.34, Outer - 0.34: b_6	-4.06	-2.46
Inner + 0.34, Outer - 0.34: b_{10}	0.828	0.255

Random errors

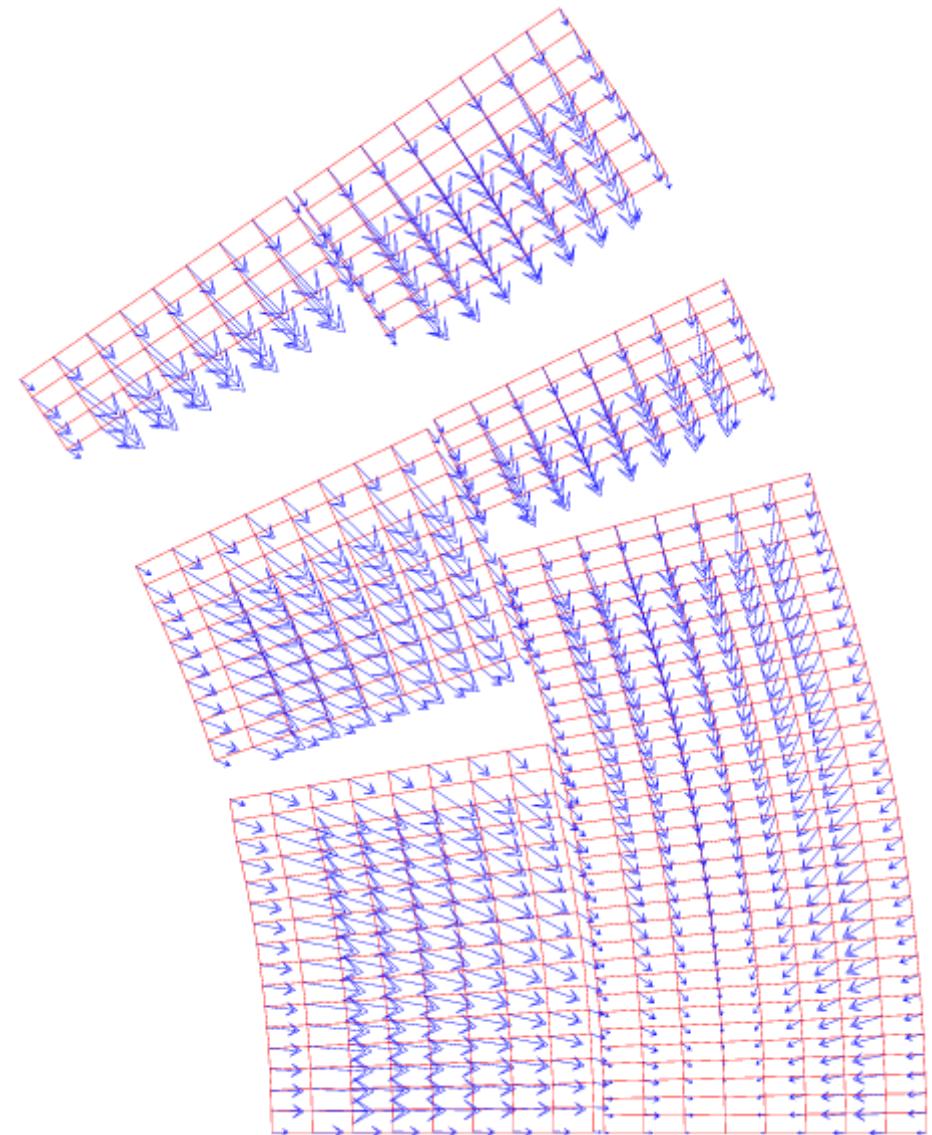
Coil Layouts (4-block / 6-block)



Magnetic Forces

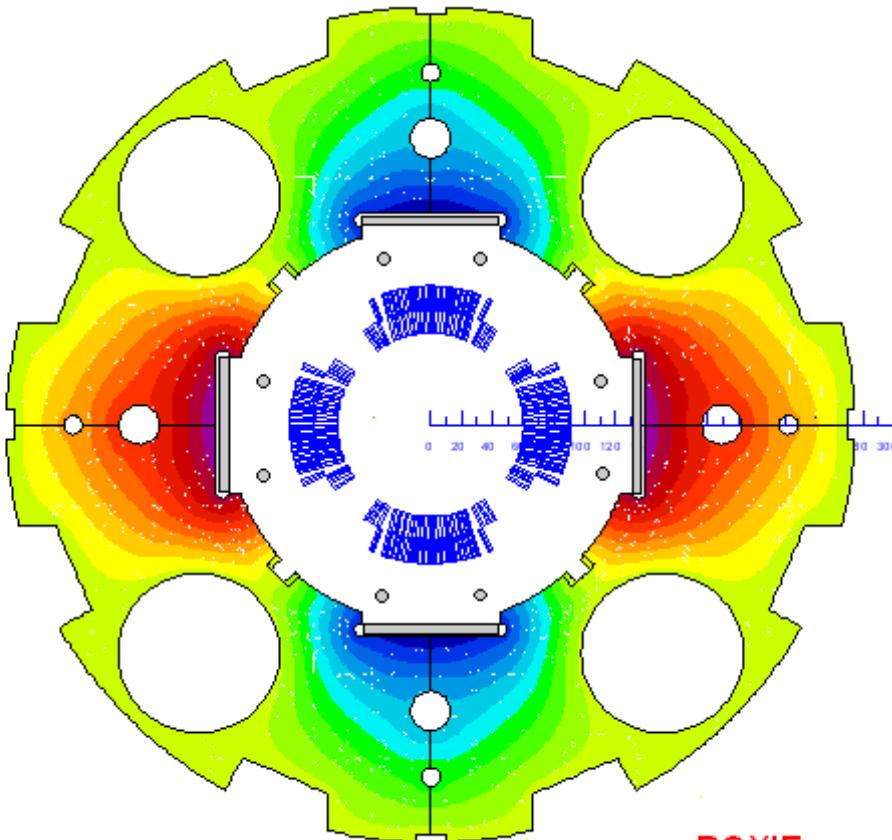


4-block model
($F = 1.6 \text{ MN/m}$)

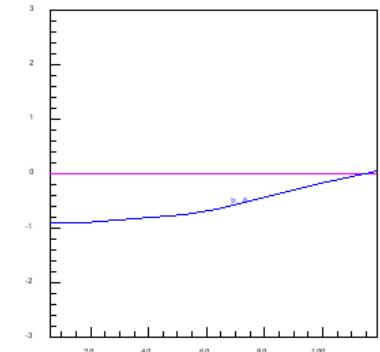
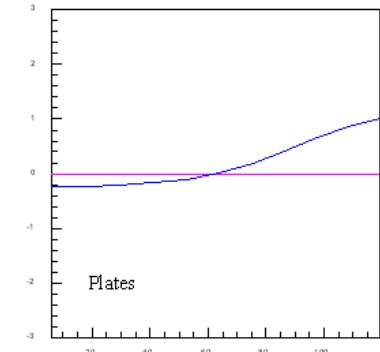
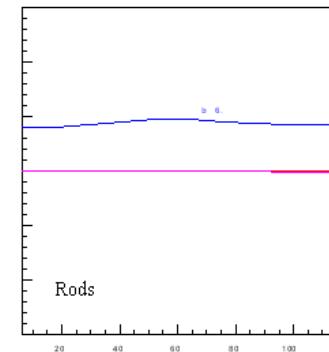
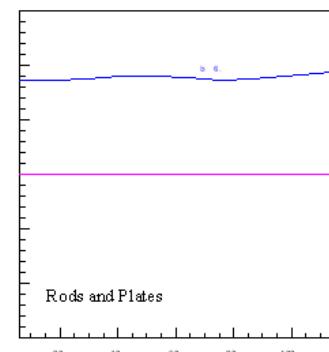


6-block model
($F = 1.8 \text{ MN/m}$)

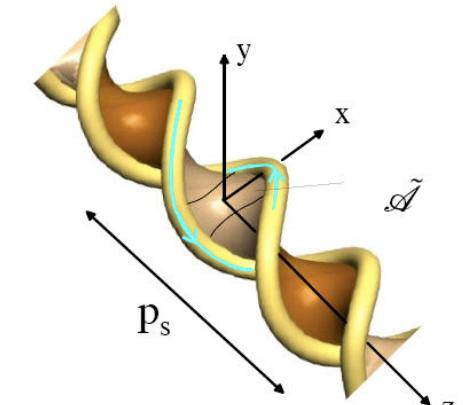
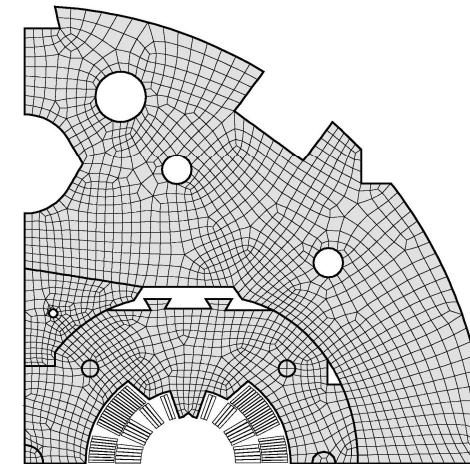
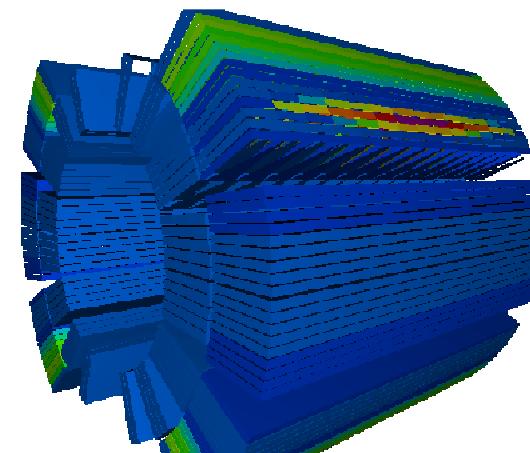
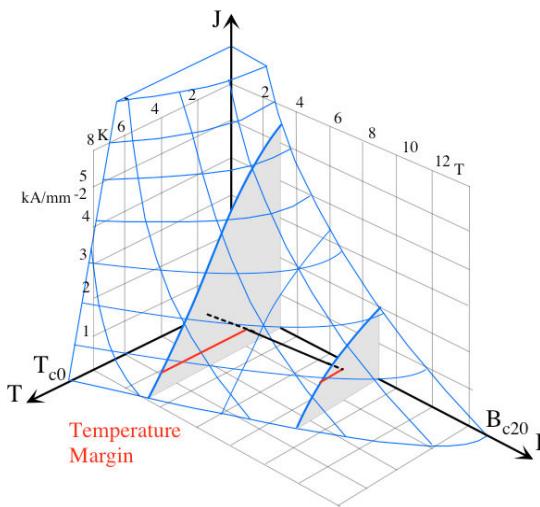
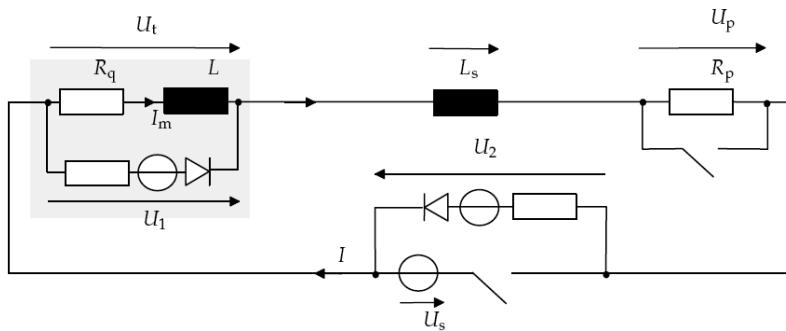
Ferromagnetic Tuning Shims (Rods and Plates)



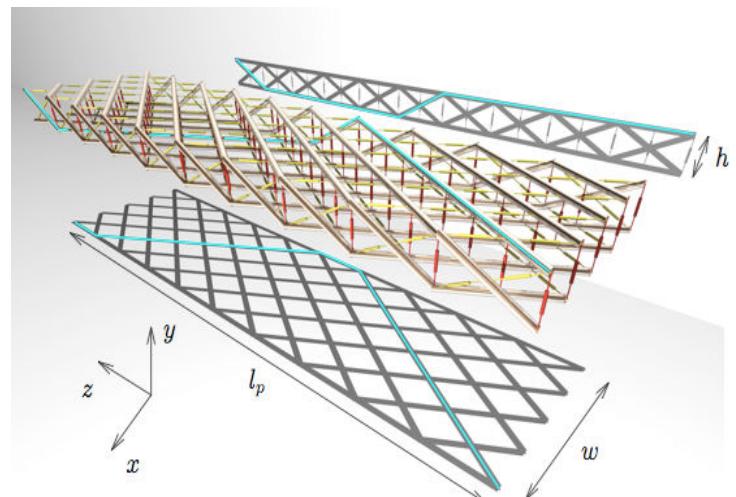
ROXIE 10.1



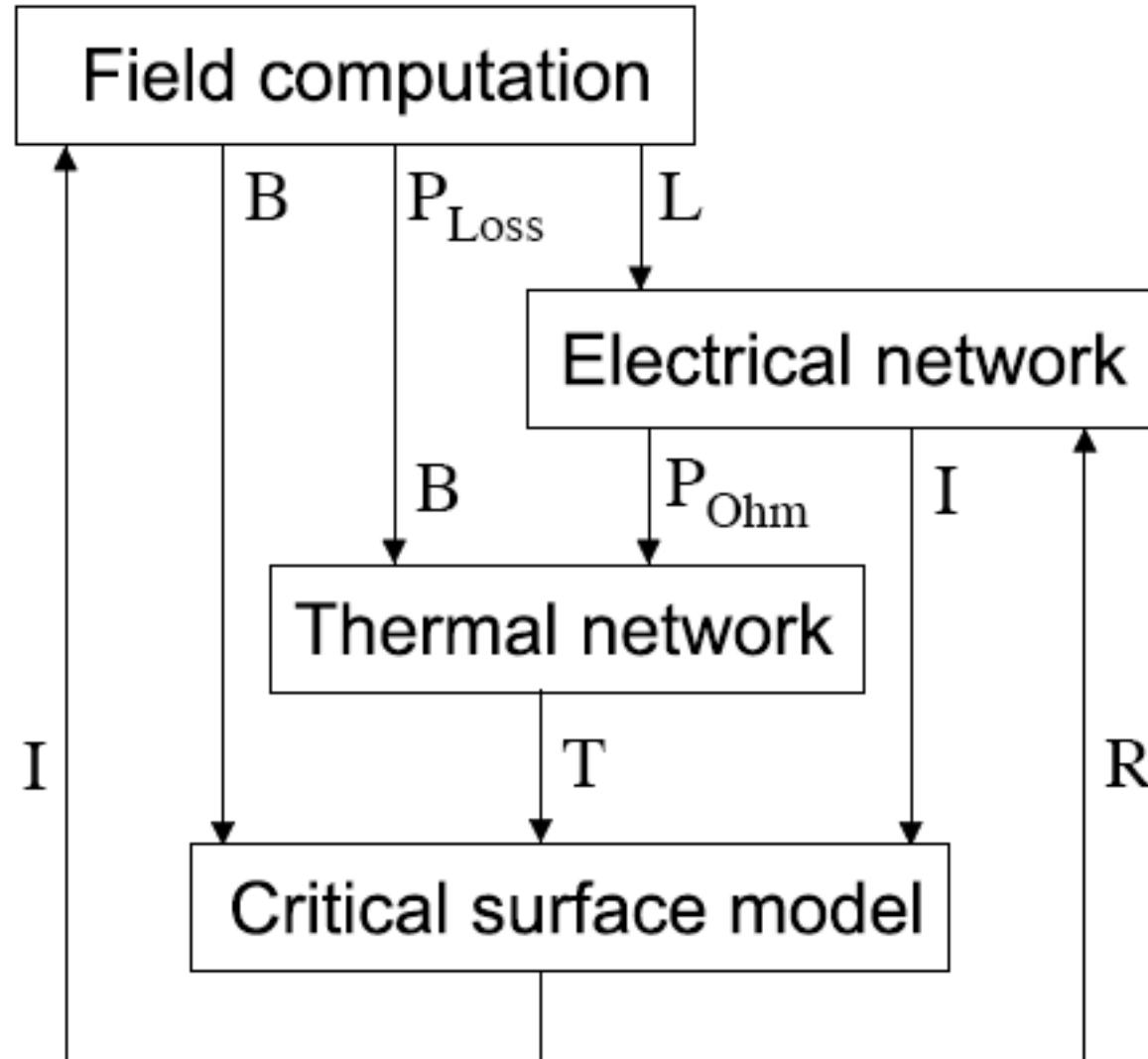
Quench Simulation (Multi-physics, Multi-scale)



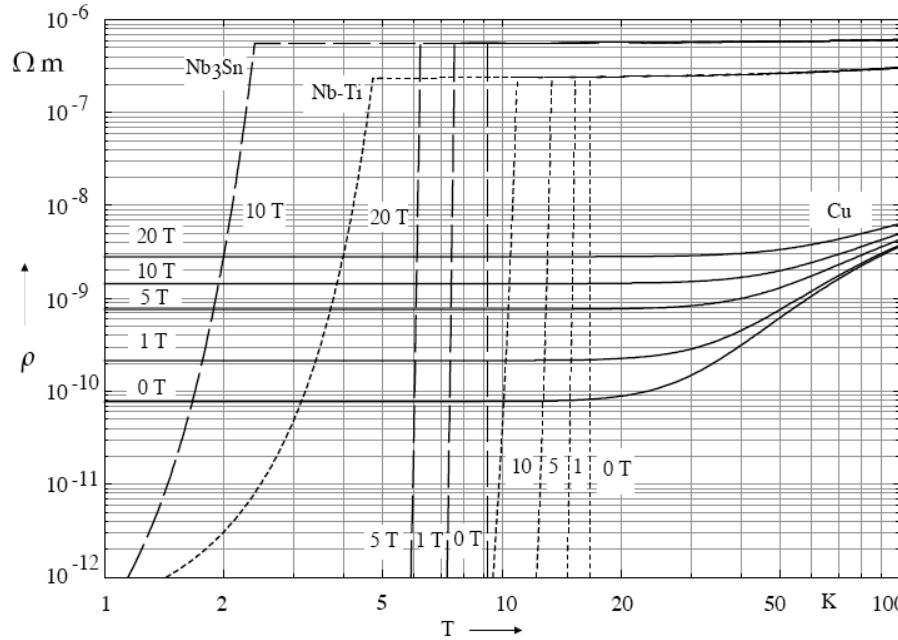
Quench Simulation in ROXIE



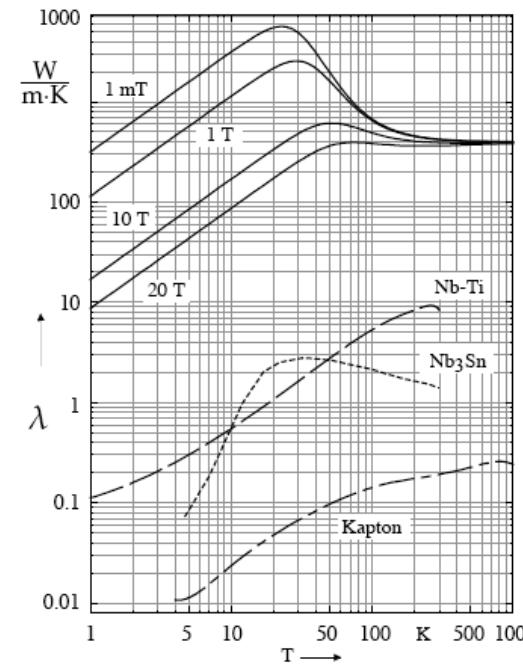
The Quench Algorithm



Material Parameters

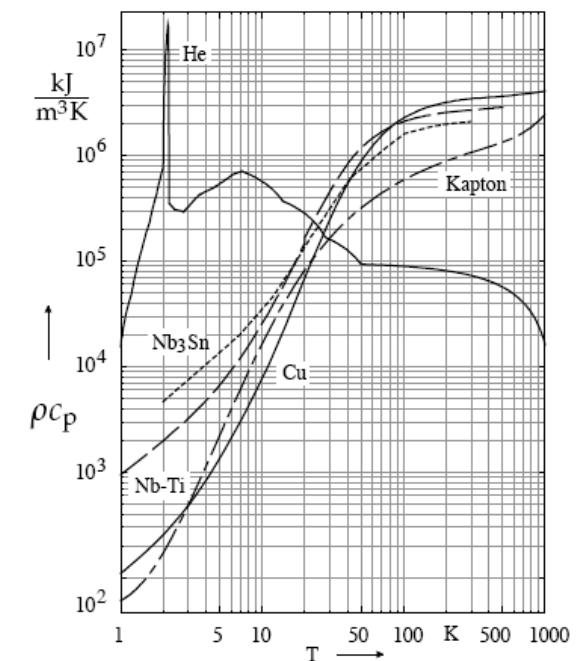


Electrical resistivity

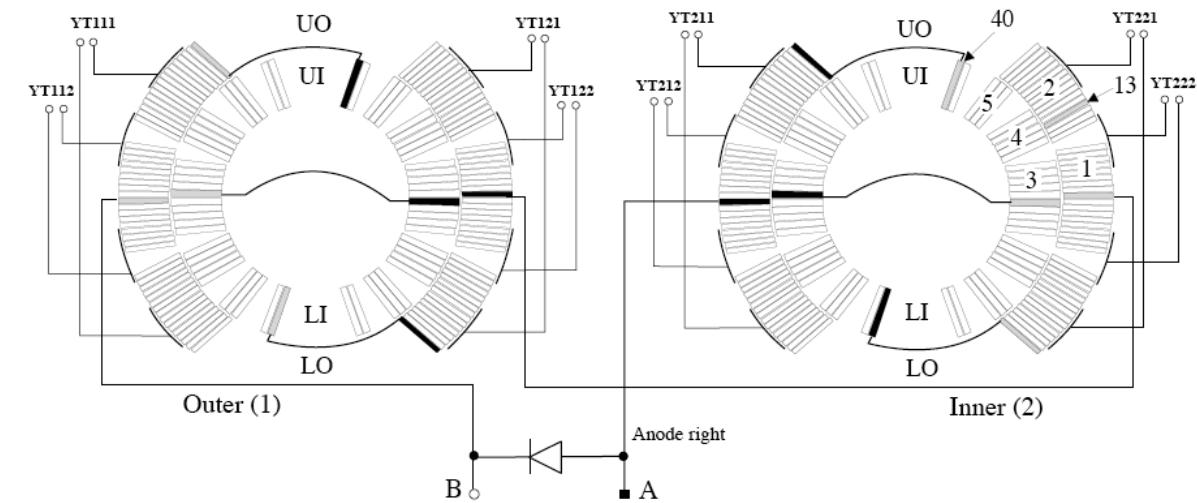
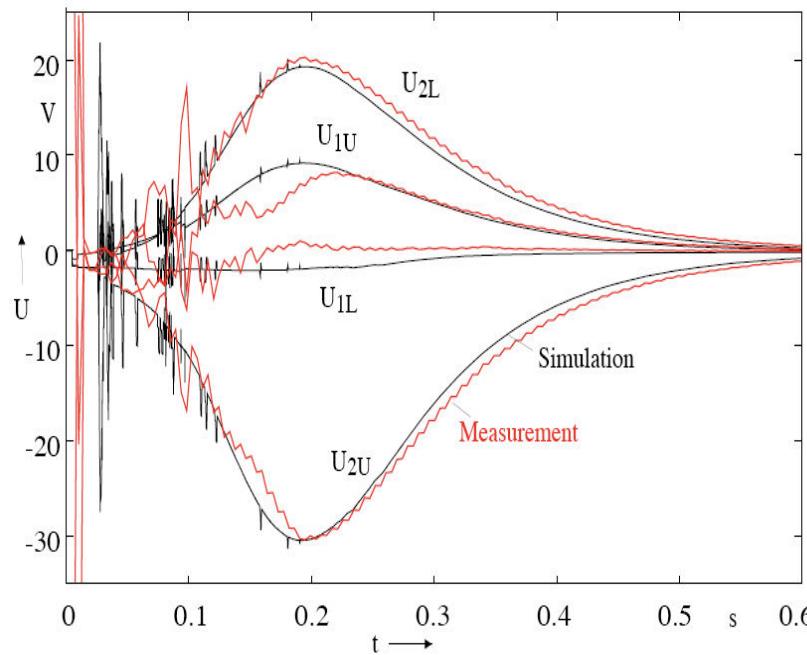
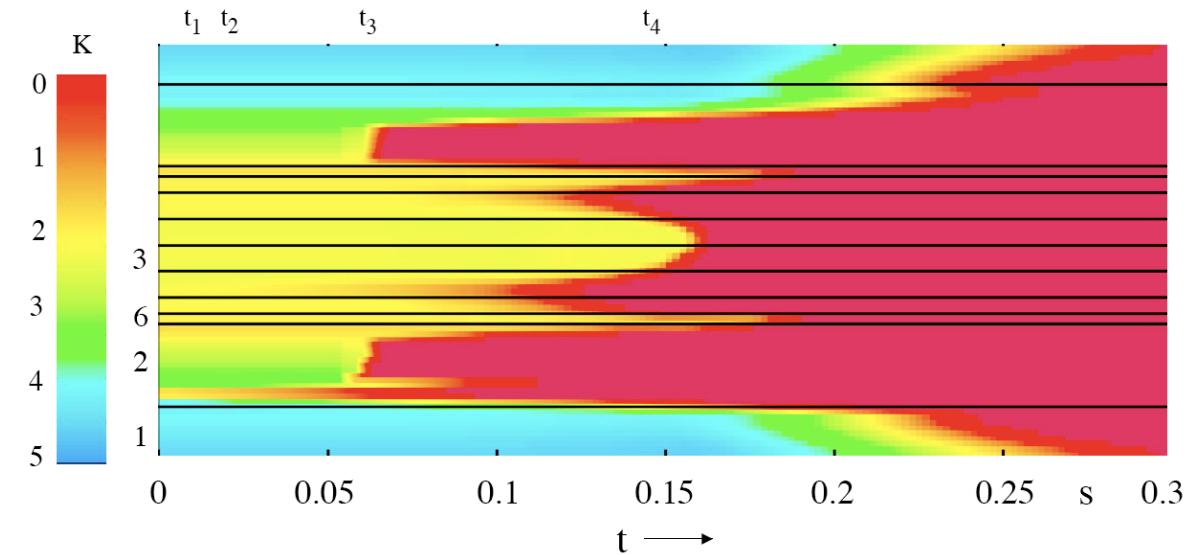
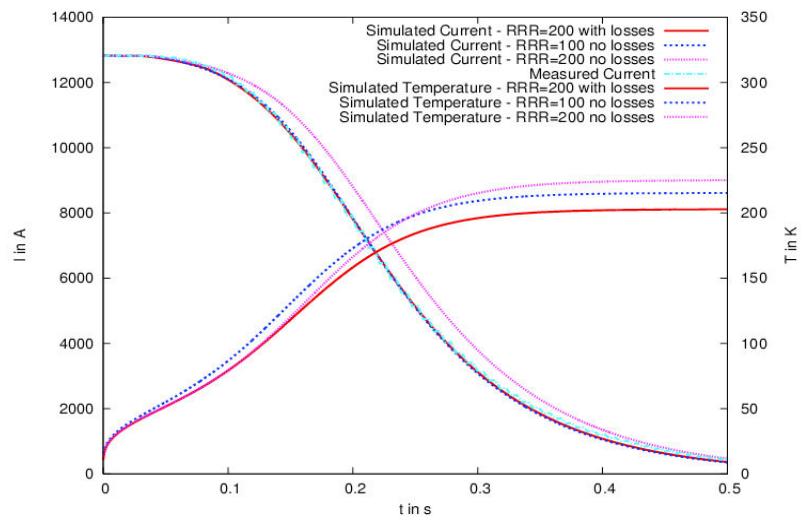


Thermal conductivity

Volumetric heat capacity

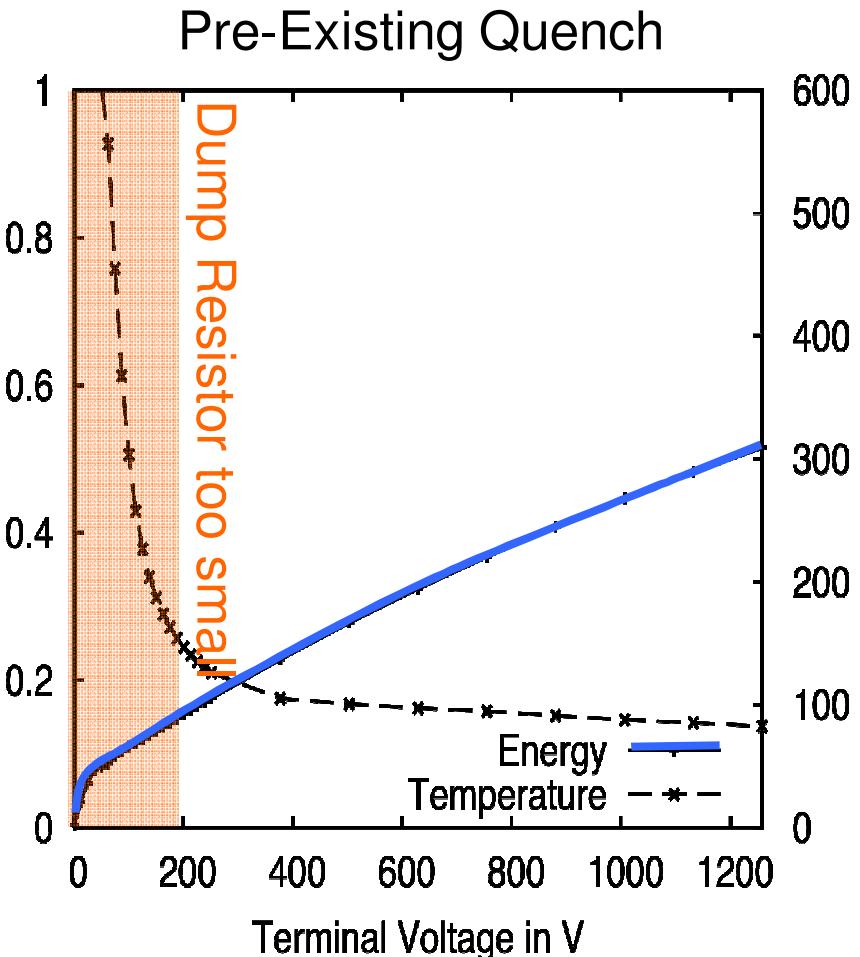


Quench Simulation (LHC MB)

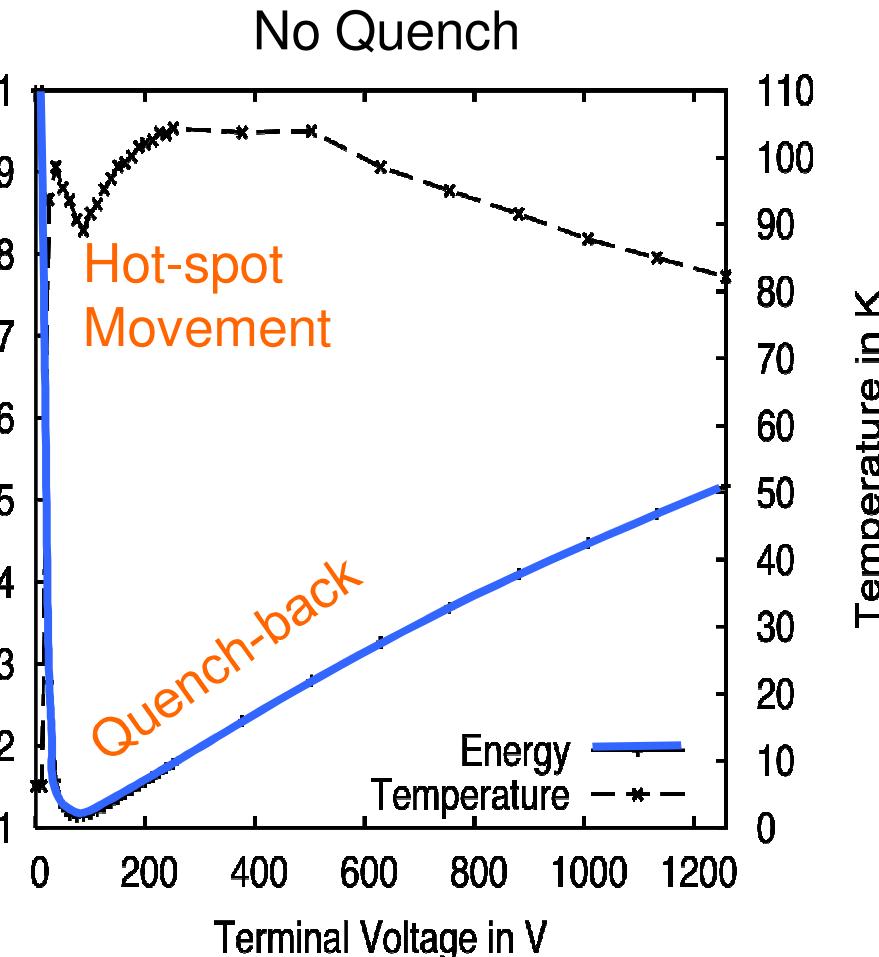


Energy Extraction Study

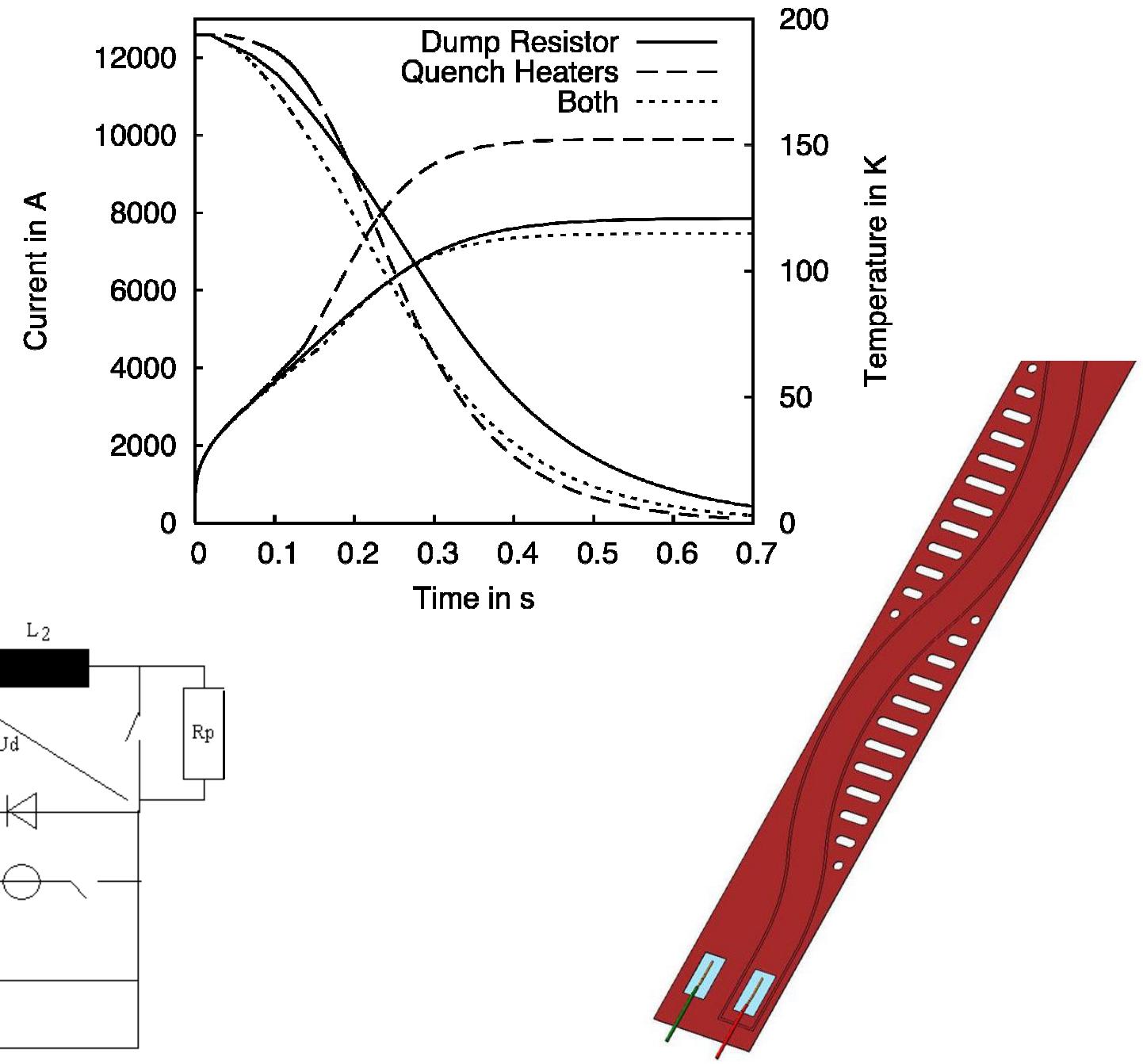
Extracted Energy versus Total Energy



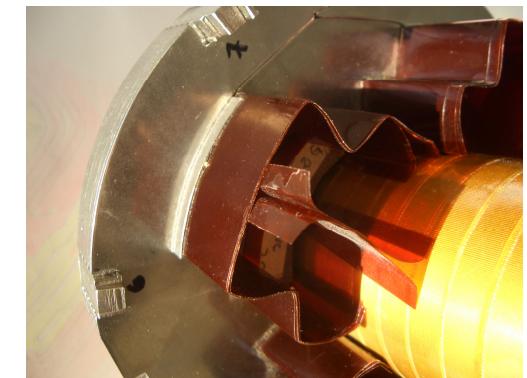
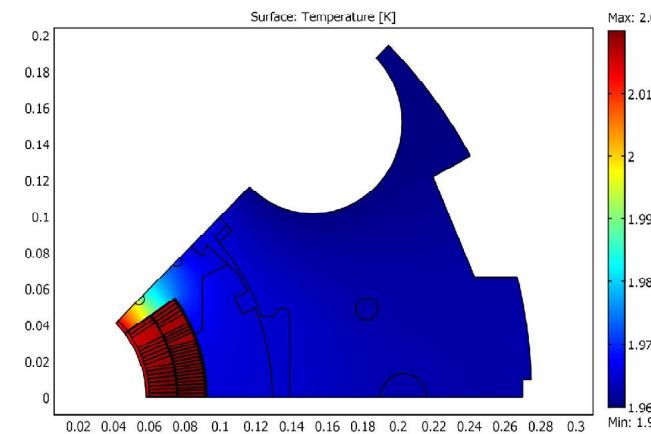
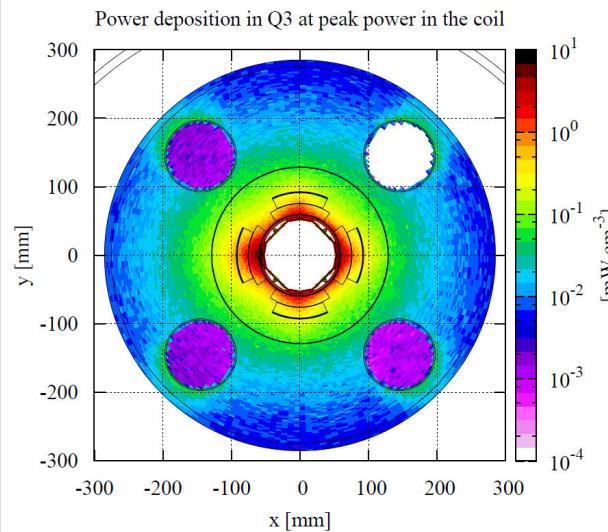
Extracted Energy versus Total Energy



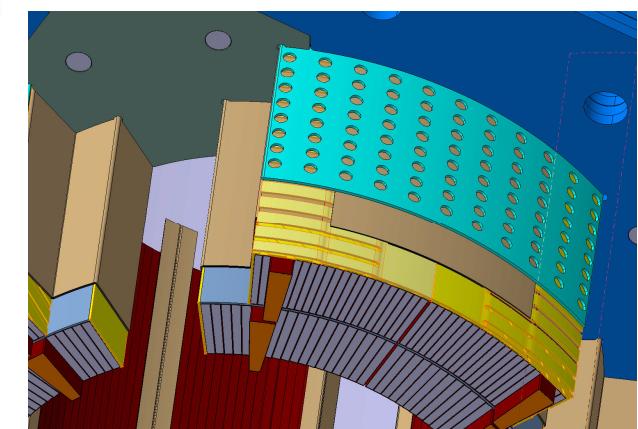
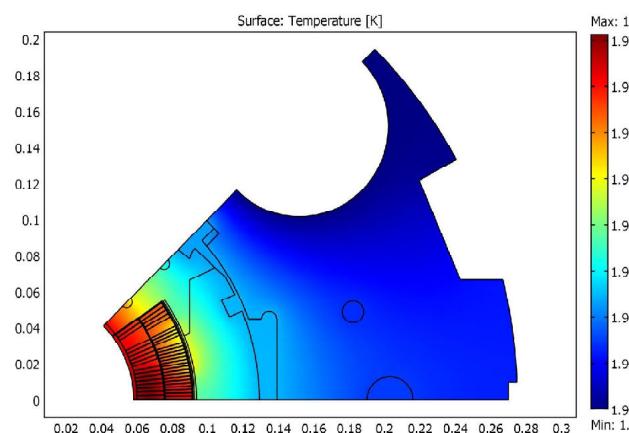
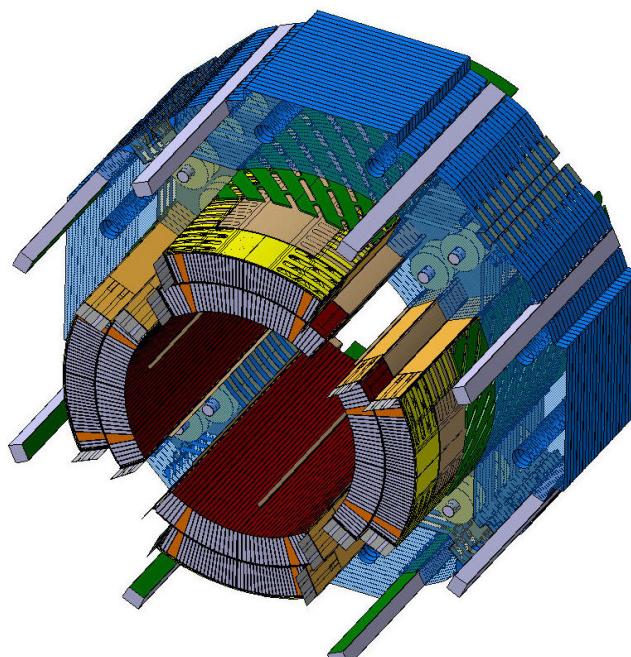
Magnet Protection Study (Dump Resistor and Heaters)



Extraction of the Steady-State Heat-Load 1 (Porous Ground-Plane Insulation)

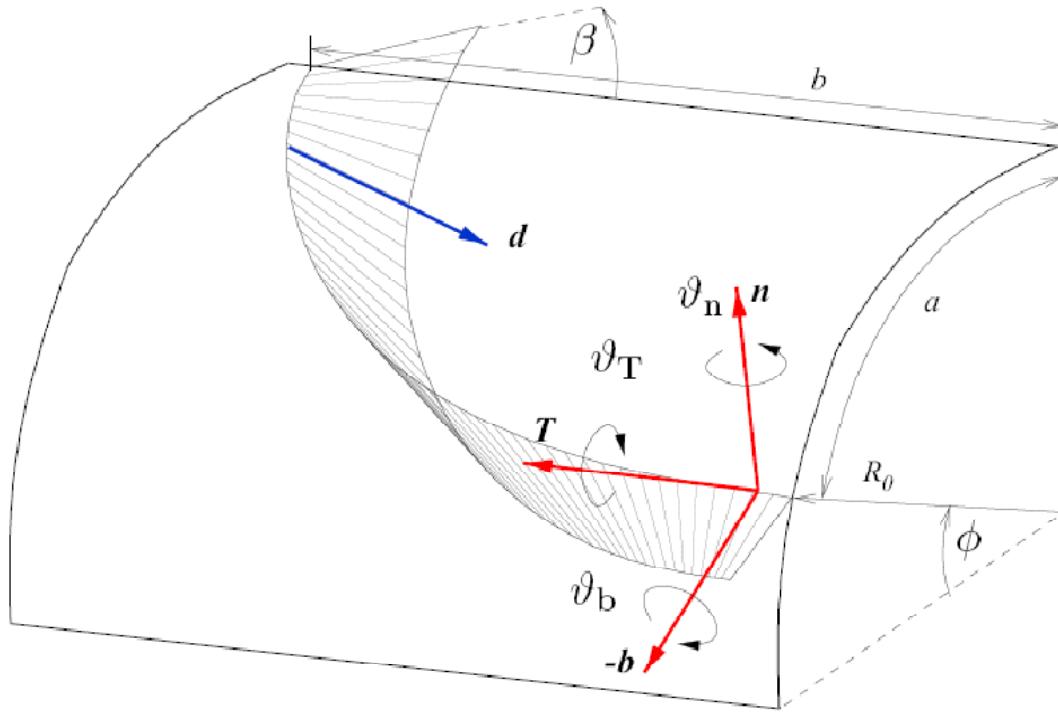


Conventional ground insulation



Open KCS ground insulation

Envelope of Planes



$$\begin{pmatrix} \mathbf{T}' \\ \mathbf{n}' \\ \mathbf{b}' \end{pmatrix} = \begin{pmatrix} 0 & \kappa_n & -\kappa_g \\ -\kappa_n & 0 & \tau \\ \kappa_g & -\tau & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T} \\ \mathbf{n} \\ \mathbf{b} \end{pmatrix}$$

Frenet Frame for strips

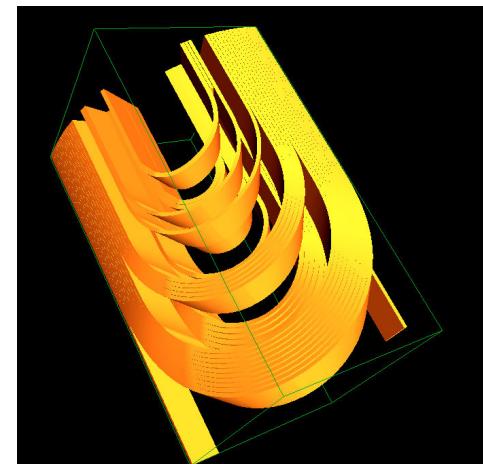
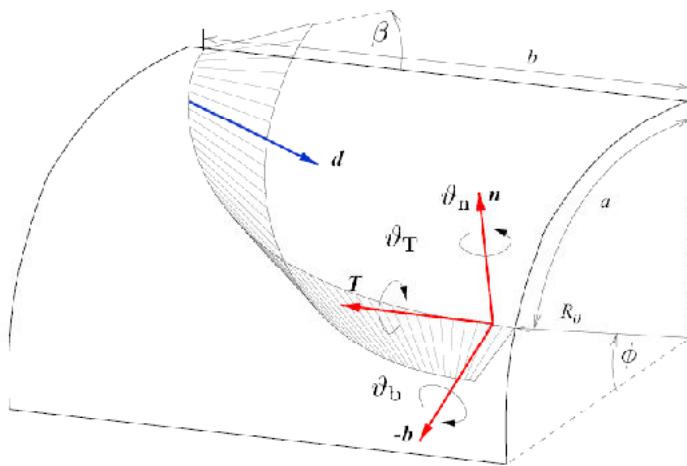
$$\begin{aligned} \tau &= \mathbf{b} \cdot \mathbf{n}' = \vartheta_{\mathbf{T}'} \\ \kappa_g &= \mathbf{T} \cdot \mathbf{b}' = \vartheta_{\mathbf{n}'} \\ \kappa_n &= \mathbf{n} \cdot \mathbf{T}' = \vartheta_{\mathbf{b}'} \end{aligned}$$

$$\begin{pmatrix} \mathbf{T}' \\ \mathbf{N}' \\ \mathbf{B}' \end{pmatrix} = \begin{pmatrix} 0 & \kappa & 0 \\ -\kappa & 0 & \tau \\ 0 & -\tau & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T} \\ \mathbf{N} \\ \mathbf{B} \end{pmatrix}$$

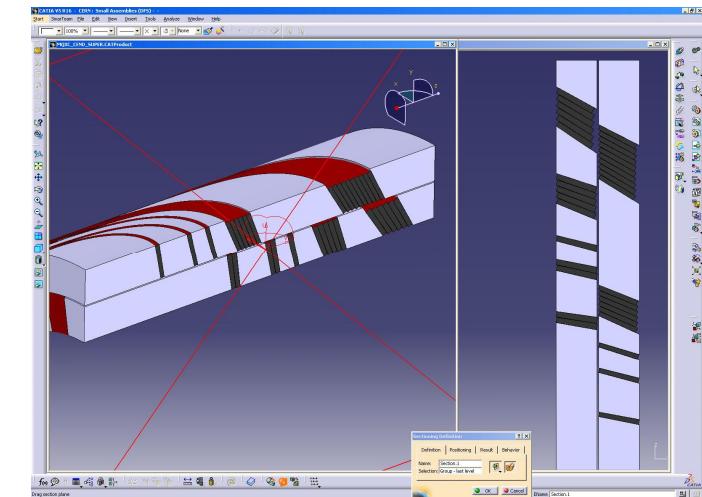
Frenet Frame for space curves

Endspacer Design and Manufacture

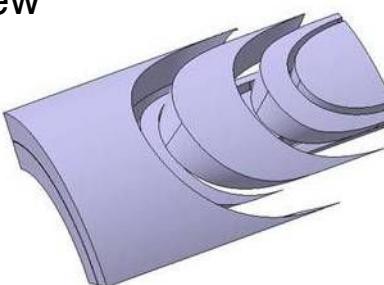
Differential Geometry Model



Virtual Reality Preview



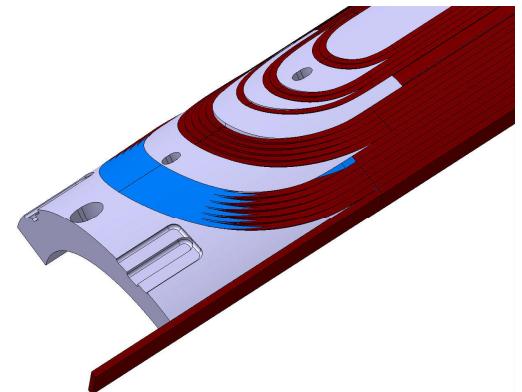
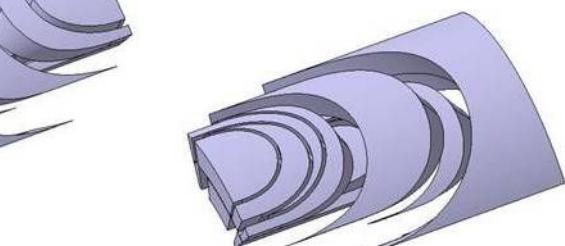
Roxie-Catia Interface



CNC-Machining



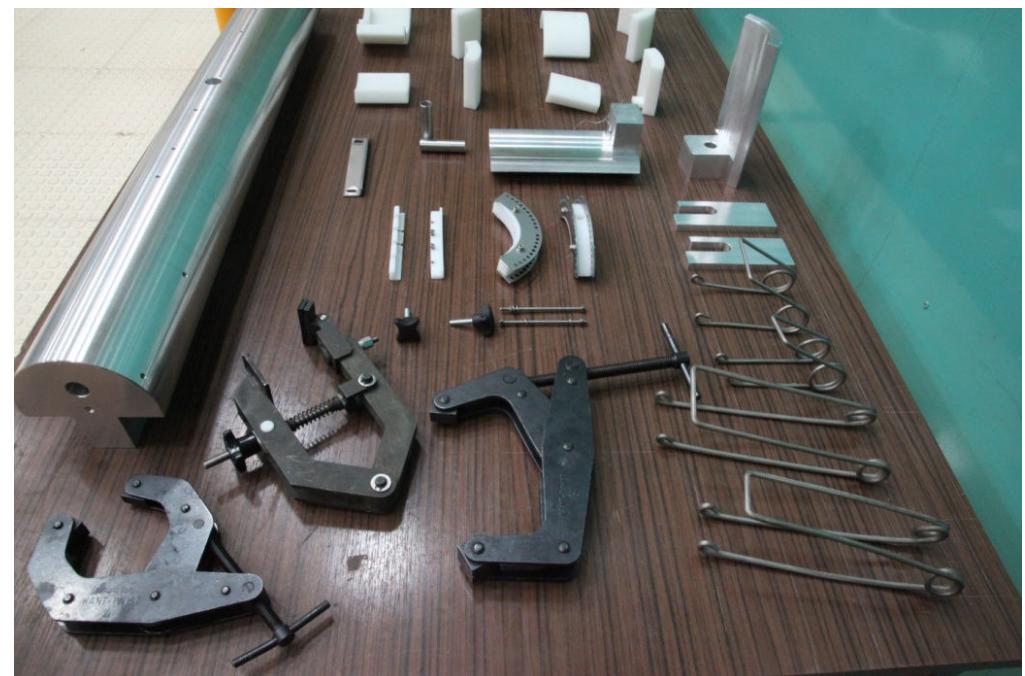
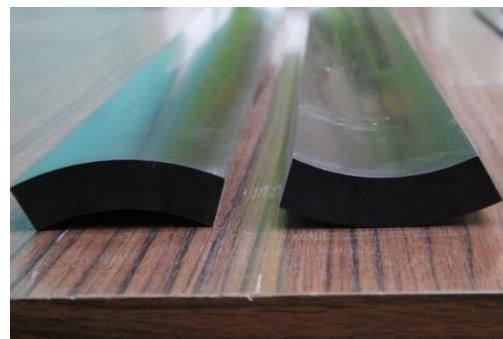
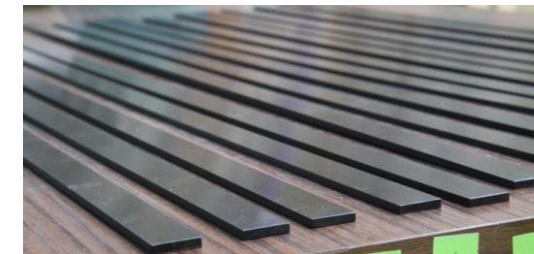
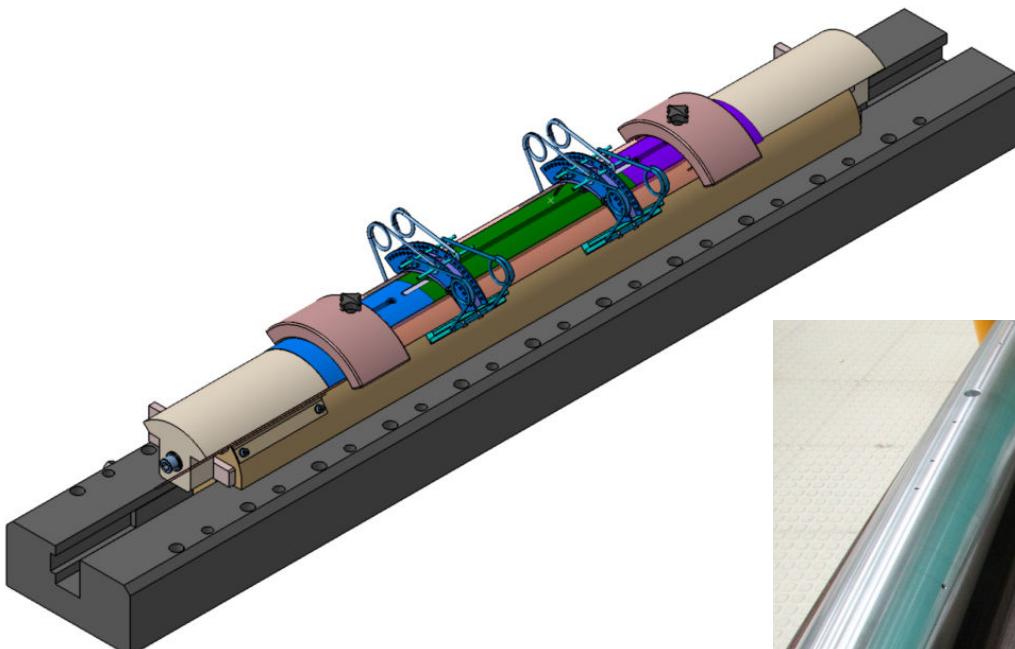
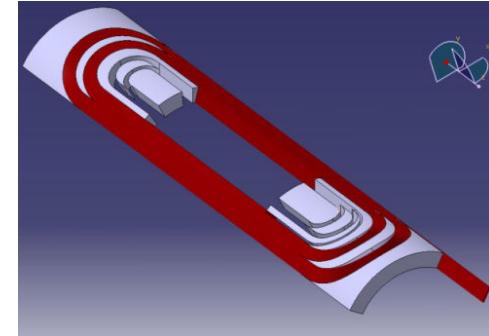
Rapid Prototyping



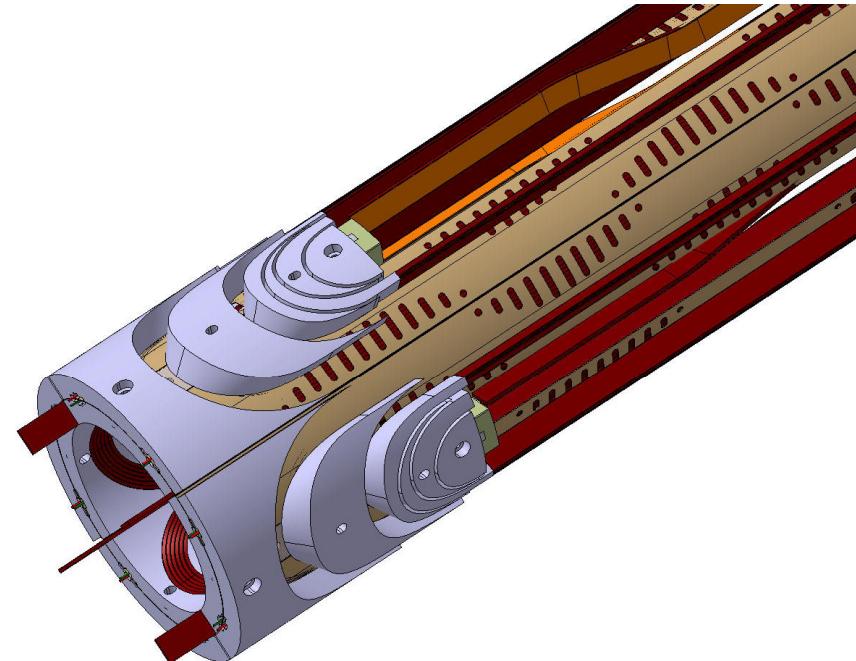
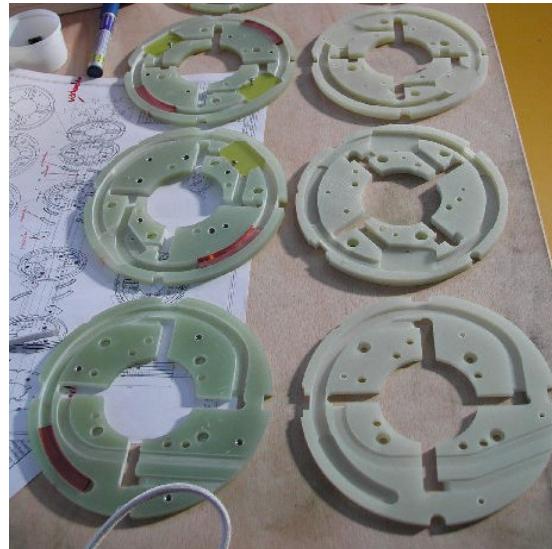
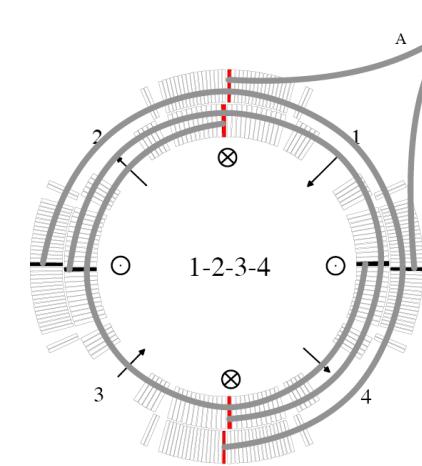
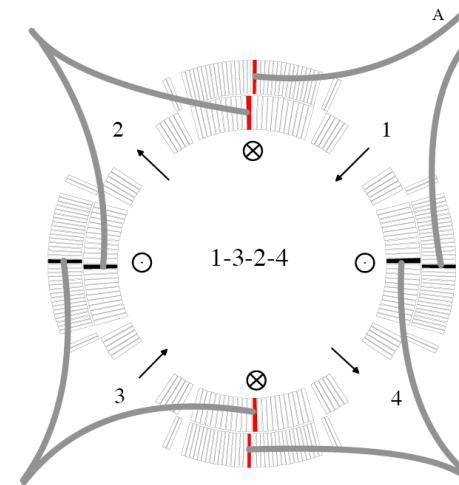
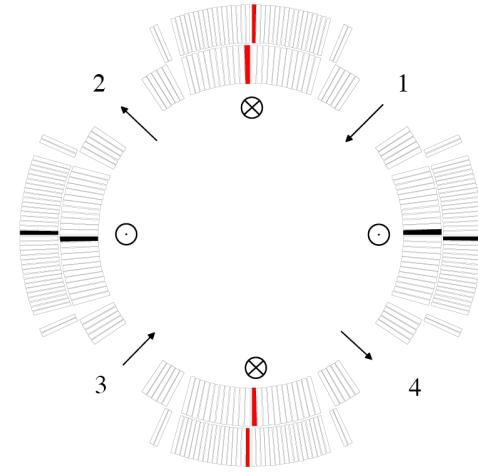
Actual status – Winding and curing trial

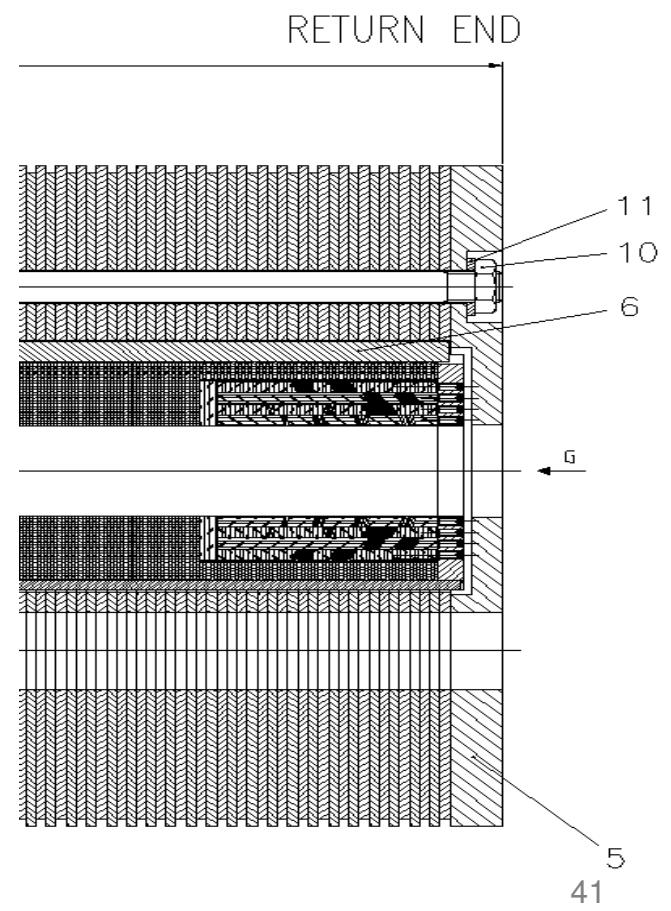
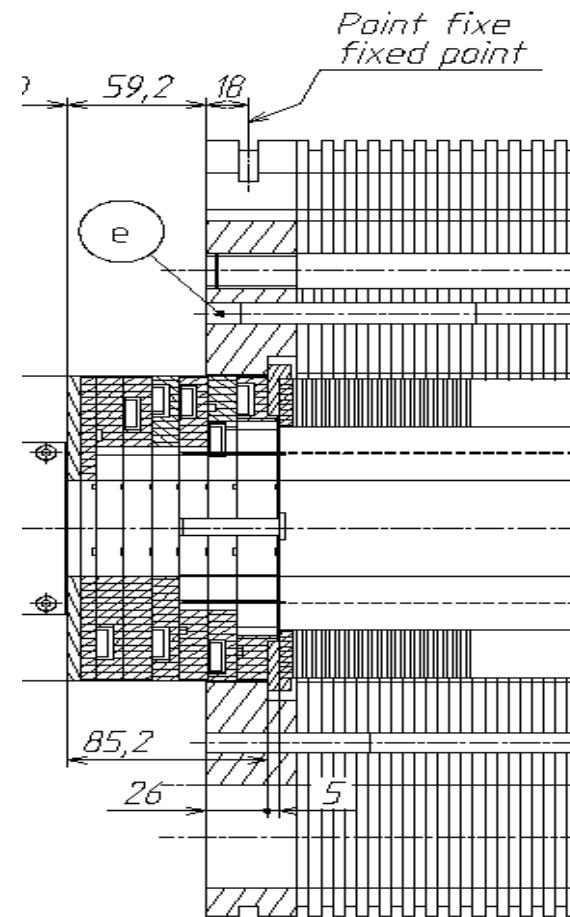
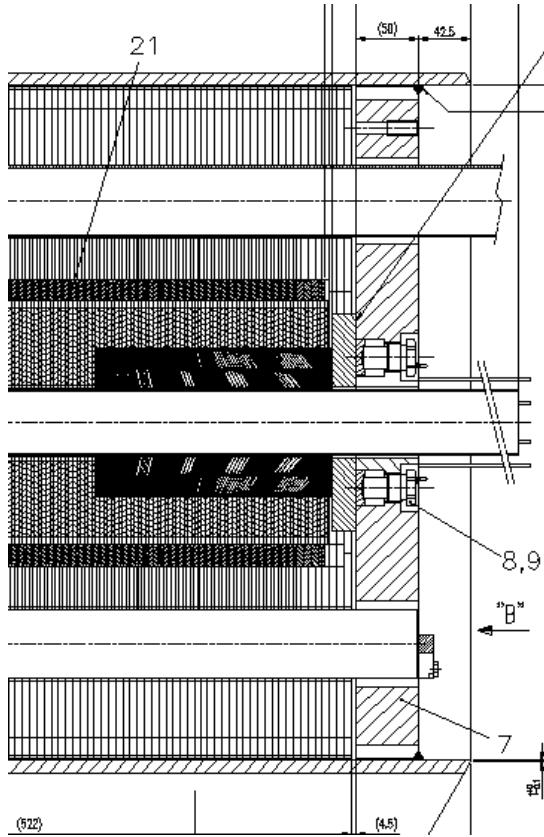
Trial design has been fixed beginning November 2009

Winding tooling has been designed and procured

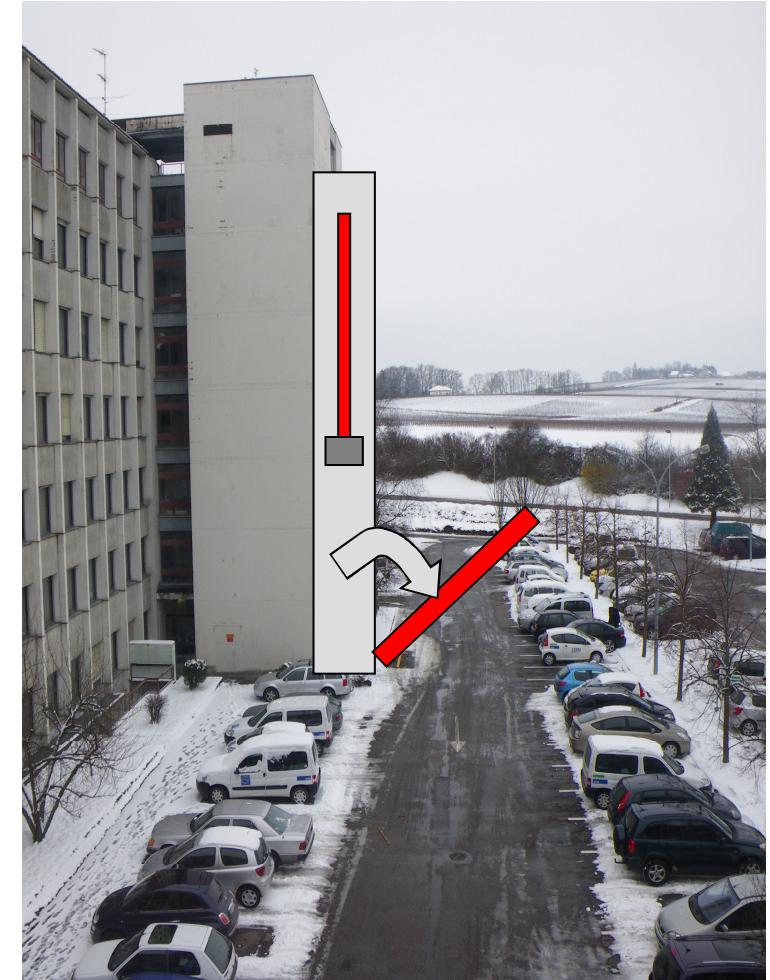


Electrical Connection Scheme



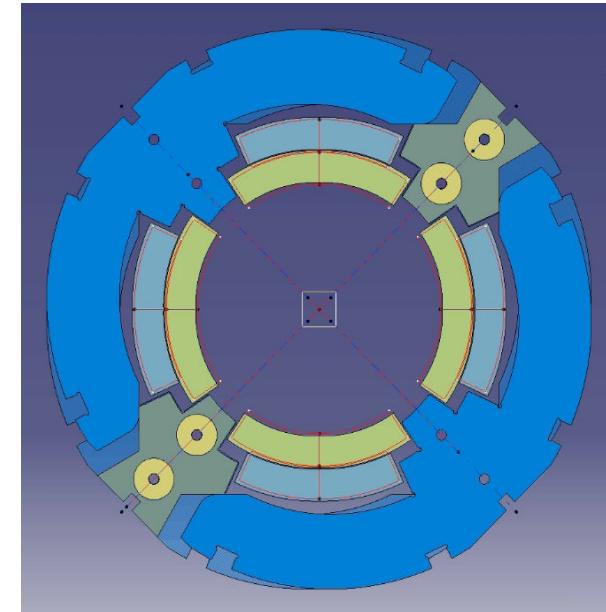
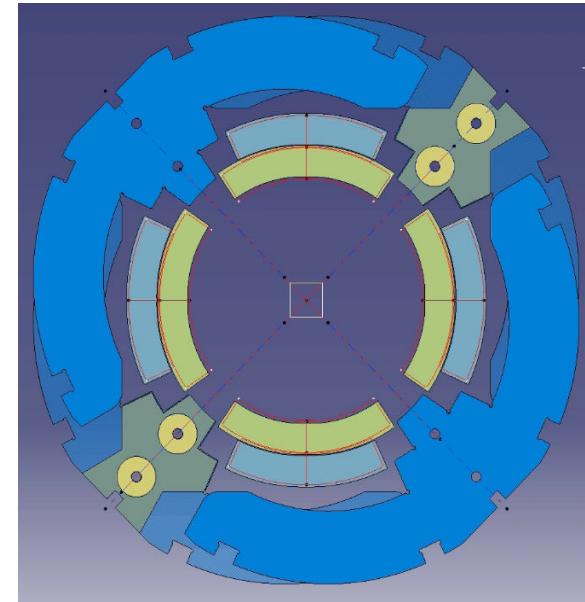


Vertical Collaring (Hardly Possible for 10-m-long Magnets)

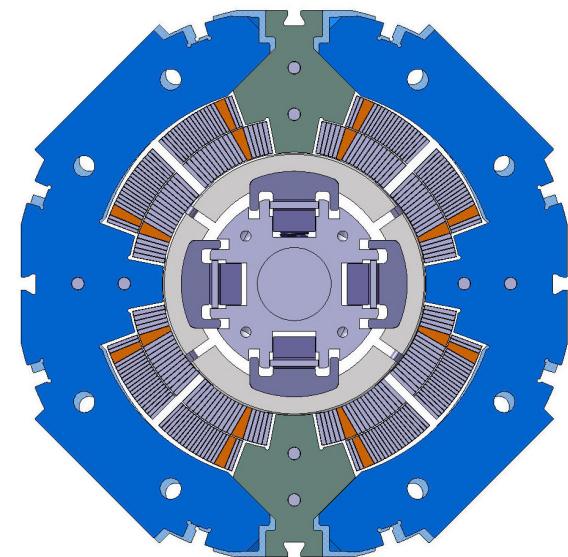
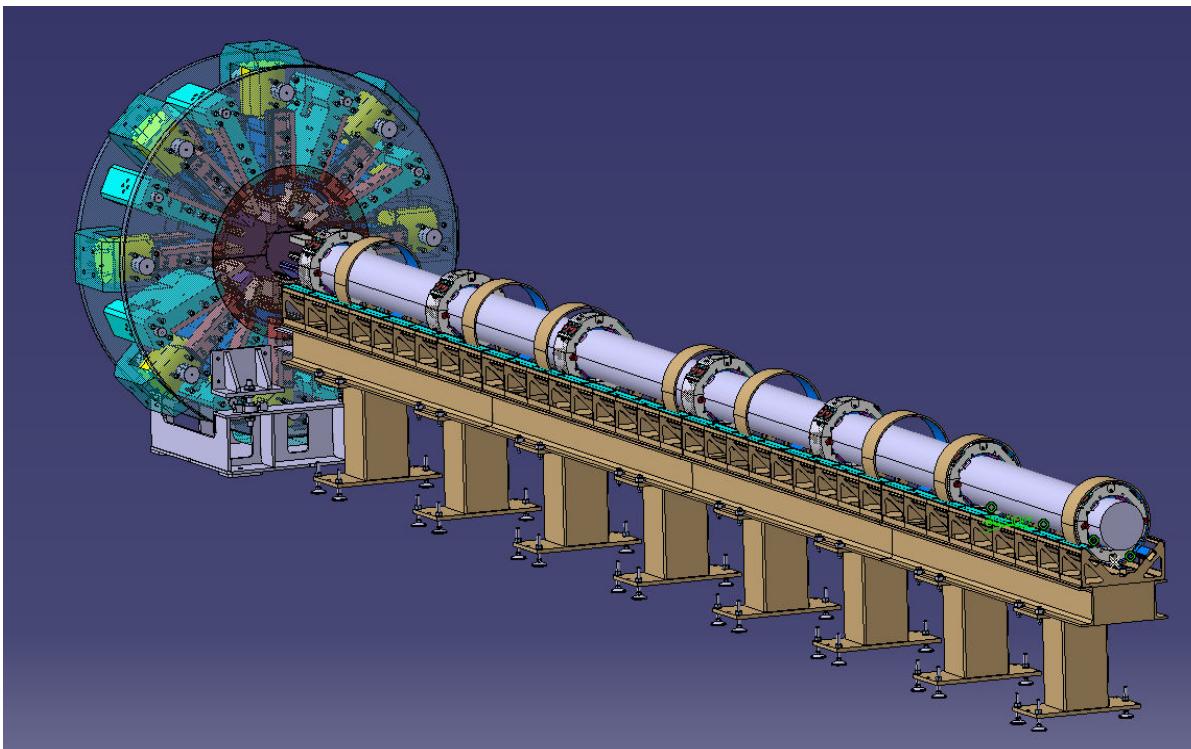


Horizontal Collaring

Self-locking collars

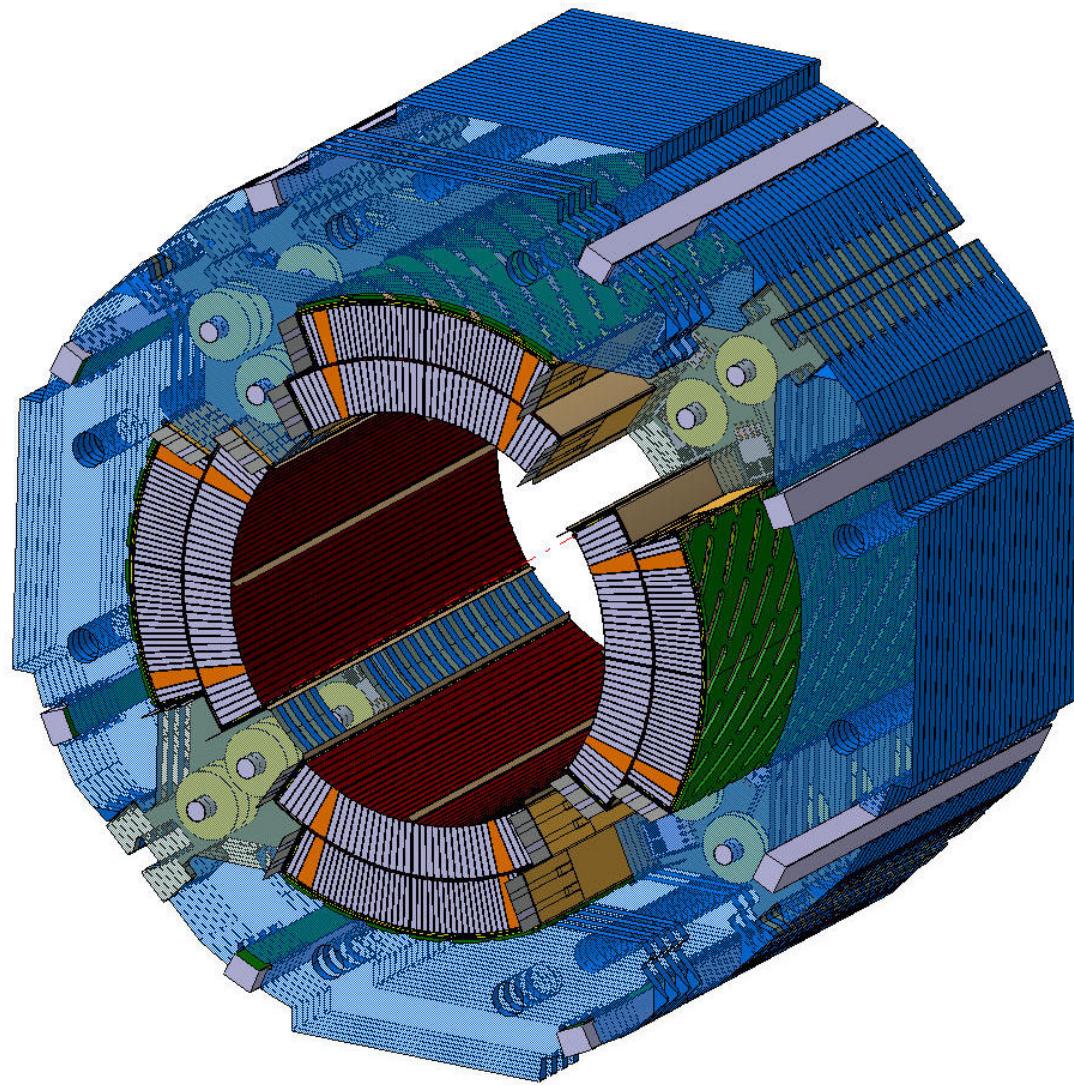


Collaring Press



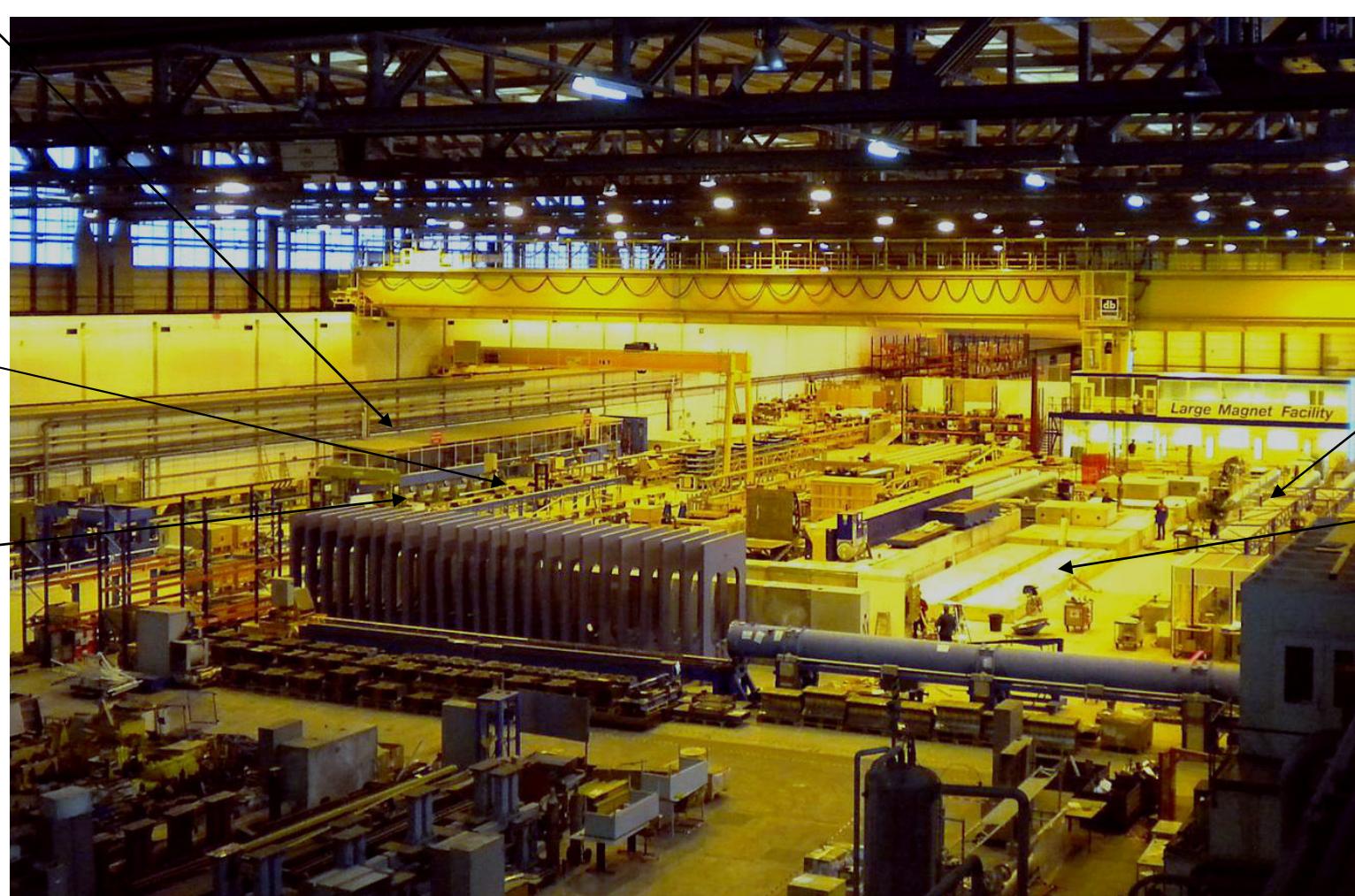
Assembly mandrel

Intermediate Milestone (The Short Model)



Large Magnet Facility (Building 180)

Cable insulation



Alignment
tables

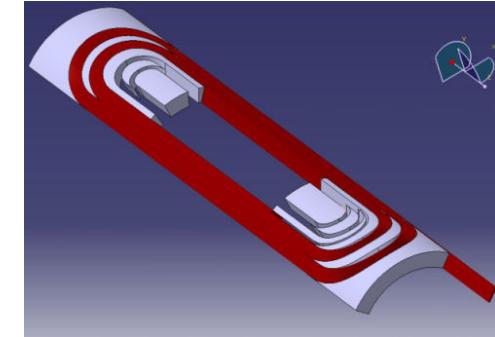
Ex-Ansaldo
winding
machine

Ex-Jeumont
winding
machine

Welding
press
area

Actual status – Winding and curing trial

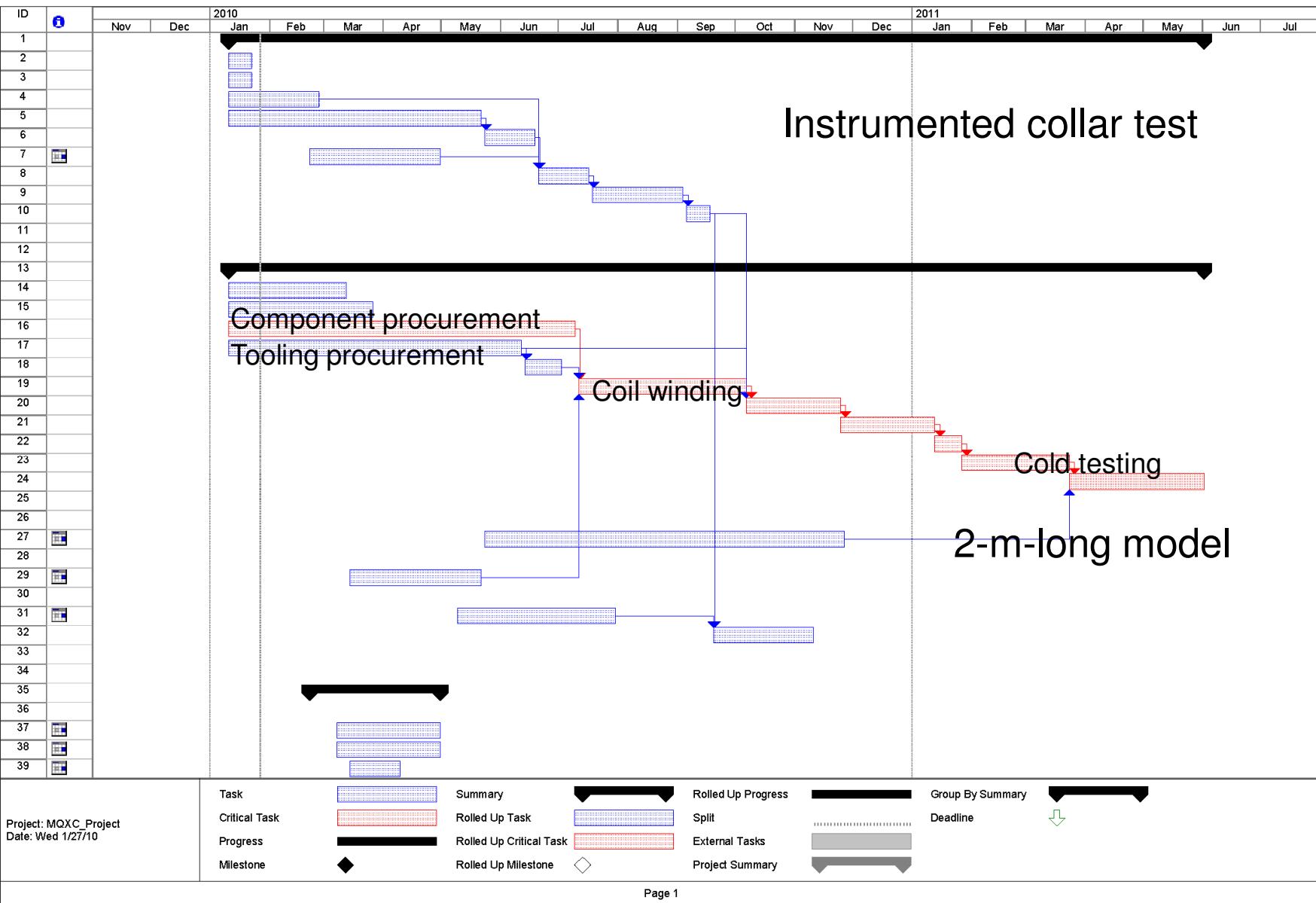
Winding machine is operative at CEA Saclay



Curing press is under installation
and repair → mid March 2010



Planning MQXC Model Magnet





Collaboration Website

LHC Upgrade Phase-I Quadrupole (MQXC) and Cryostat

https://espace.cern.ch/MQXC/

Google

MMM Services

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LHC Upgrade Phase-I Quadrupole (MQXC) and Cryostat

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Welcome

This collaboration site aims at facilitated communication between the different teams and engineers involved in the design, manufacture, and testing of the MQXC magnet for the LHC upgrade phase 1.

How to use this homepage

To request full access to this site, send your username to Stephan.Russenschuck@cern.ch. Outside-CERN collaborators are required to create a CERN External Account [here](#). You can subscribe to email alerts by clicking "Actions" in any of the following lists:

- **Logbook:** Keep track of relevant information grouped by subproject, component, and activity.
- **Meetings:** Repository of meeting summaries and minutes.
- **Document library:** Project planning, specifications, project notes, and other documents.

Announcements

There are currently no new announcement, c

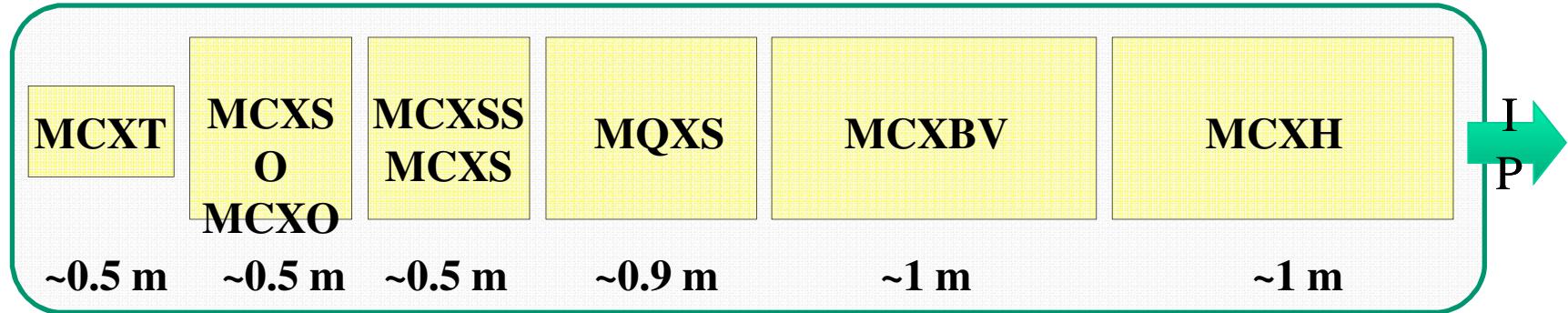
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Calendar

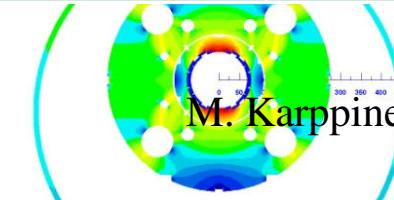
22/07/2009 09:00 AM

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Corrector Package (CP)

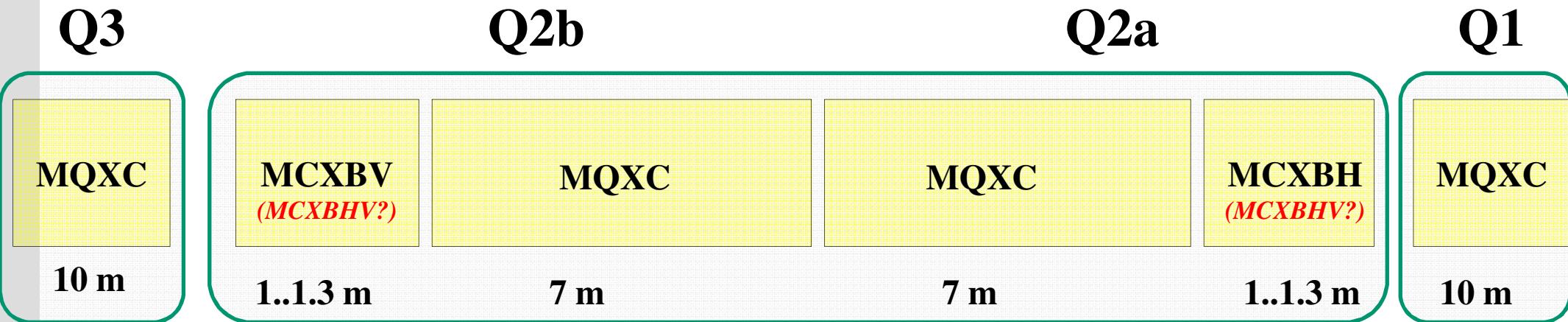


	Current	Integrated strength (field)	Aperture
MCXB (B_1/A_1)	+/- 2.4 kA	1.5 Tm	140 mm
MQXS (A_2)	+/- 2.4 kA	0.65 Tm @40 mm	140 mm
MCXT (B_6)	+/- 120A	0.075 Tm @ 40 mm	140 mm
MCXO (B_4)	+/- 120A	0.035 Tm @ 40 mm	140 mm
MCXSO (A_4)	+/- 120A	0.035 Tm @ 40 mm	140 mm
MCXSS (A_3)	+/- 120A	0.055 Tm @ 40 mm	140 mm
MCXS (B_3)	+/- 120A	0.055 Tm @ 40 mm	140 mm



M. Karppinen TE-MSC-ML

Correctors in Q2

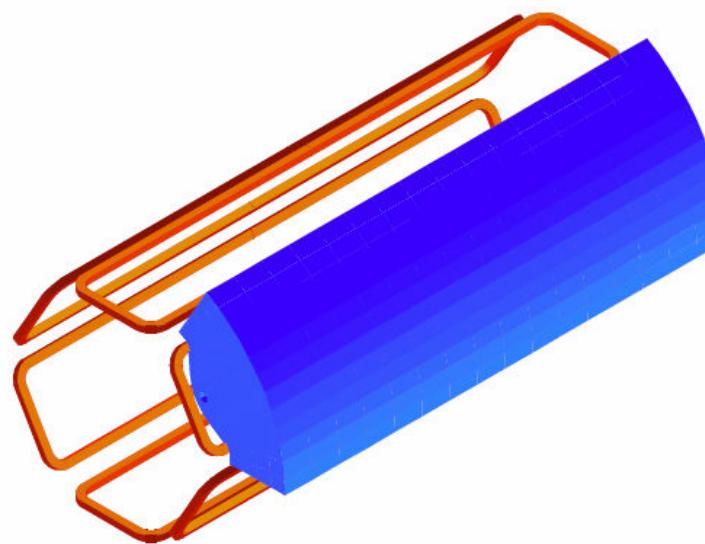


- Base-line (HV and VH) orbit corrector scheme allows controlling the orbit to a level 3 times larger than then BPM resolution.
- To reach the same level as the effective BPM resolution :
 - Provide 1.5 Tm (1.8 Tm) in H&V-plane in BOTH locations.
 - Feasibility study underway on combined H/V-corrector that meets the reliability requirements (Report by Mid-2010 + Model work..)
- An extra H/V pair means:
 - Magnet R&D, material R&D, design, component & tooling procurement
 - Additional powering and protections circuits

REF: S. Fartoukh, R. Tomas, J. Miles: "Specification of the Closed Orbit Corrector magnets for the NEW Inner Triplets", sLHC Project Report 030

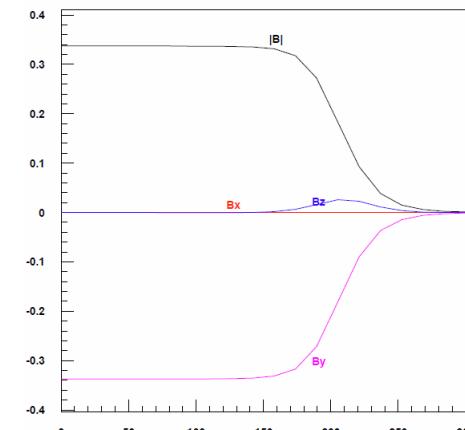
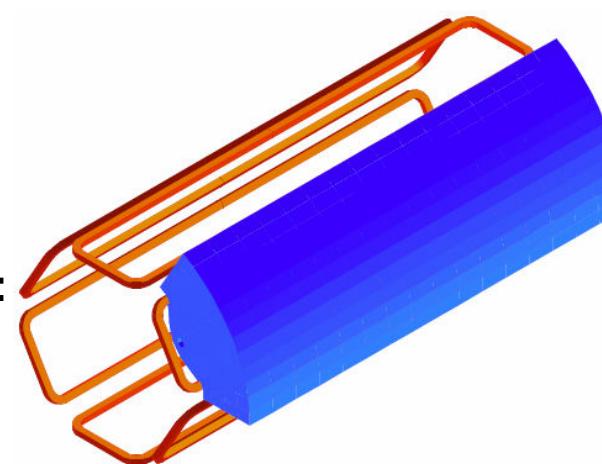
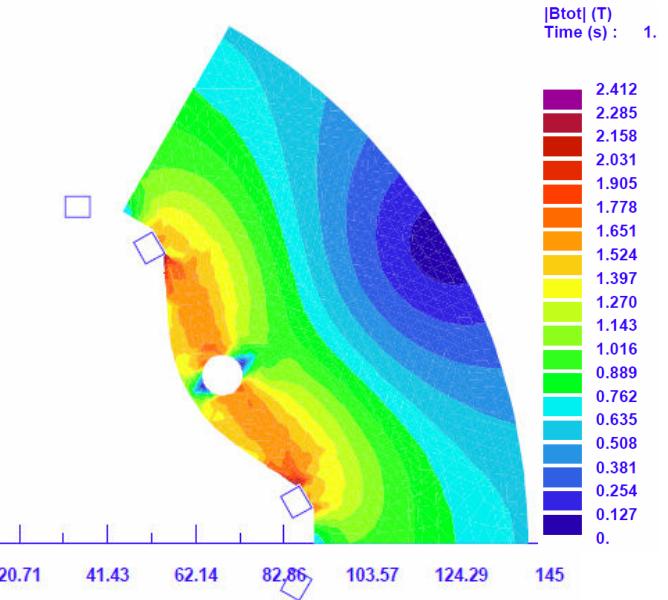
- Original specifications

Magnitude	Value	Units
Pole tip radius	70	mm
Reference radius	40	mm
Integrated strength	0.138	Tm
Max. overall length	0.5	m
Current	100 or 600	A

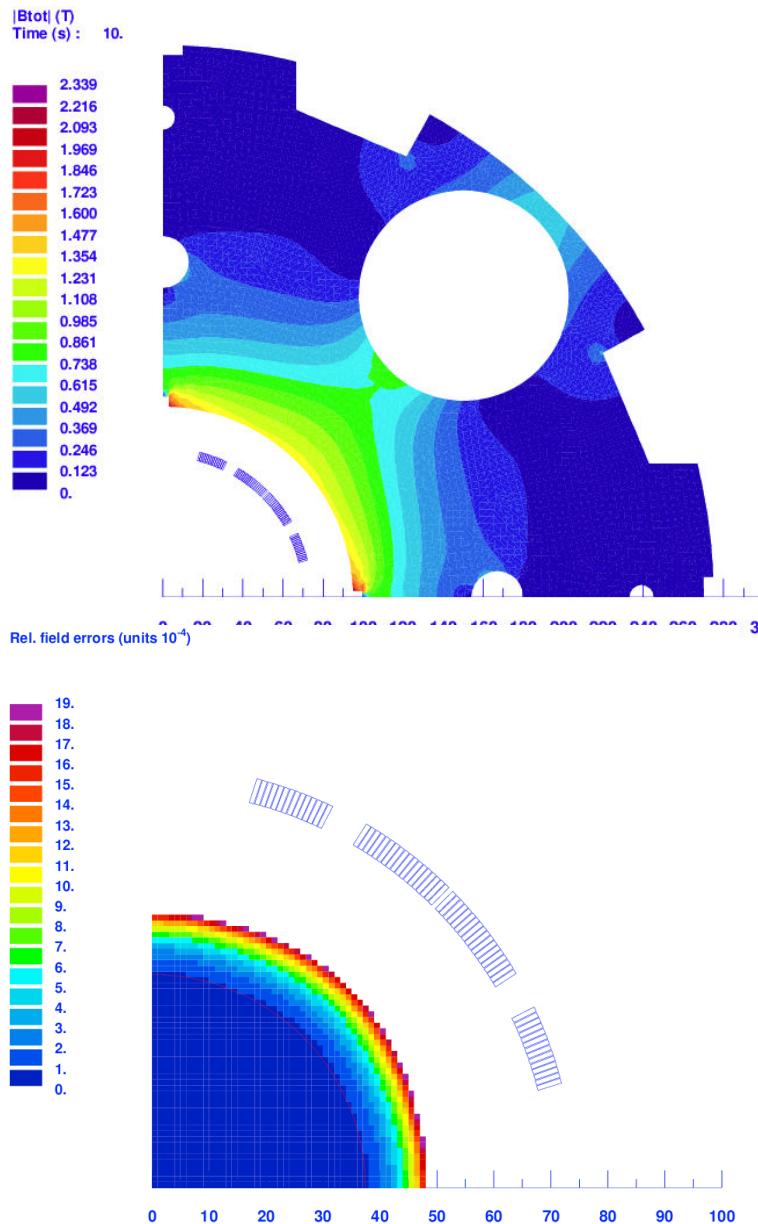


Calculation results

- **600 Amps**, 32 turns, 19200 A-turn.
- 5.84x5 mm coil, 0.73x1.25mm NbTi wire (1.6 Cu/Sc)
- 210.7 T/m², 0.337 T @ 40 mm. WP=54.3 % @ 1.9K
- **Inductance: 0.028 H/m, 5.15 KJ/m** stored energy
- Non-linearity in the load line: **0.2 %**
- 2D field quality (10⁻⁴ units):
 - b9: -0.0075
 - b15: -0.066
 - b21: -0.003
- Integrated strength: **0.1387 Tm**
- Effective length: **0.41 m**
- Peak field (3D): **2.19 T**
- Iron length: **392 mm**
- Iron weight: **126 kg**
- 3D field quality (10⁻⁴ units):
 - b9: 0.172
 - b15: -0.059
 - b21: -0.001

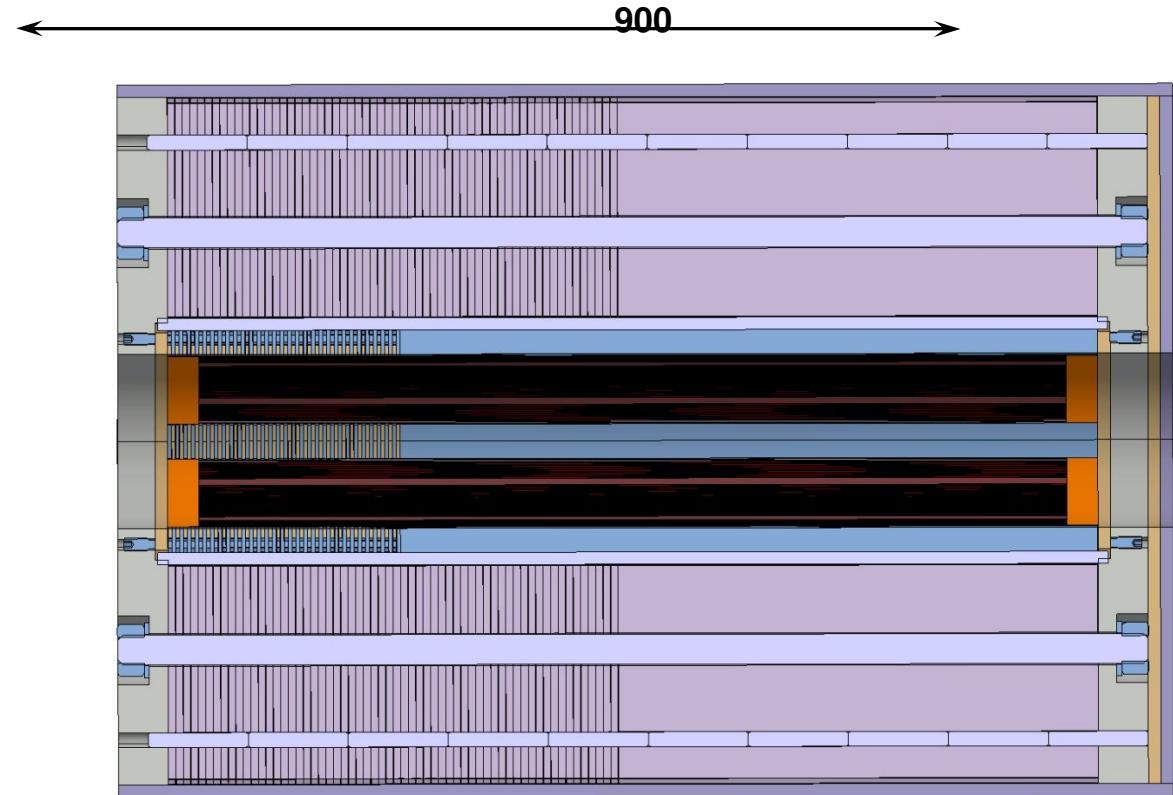
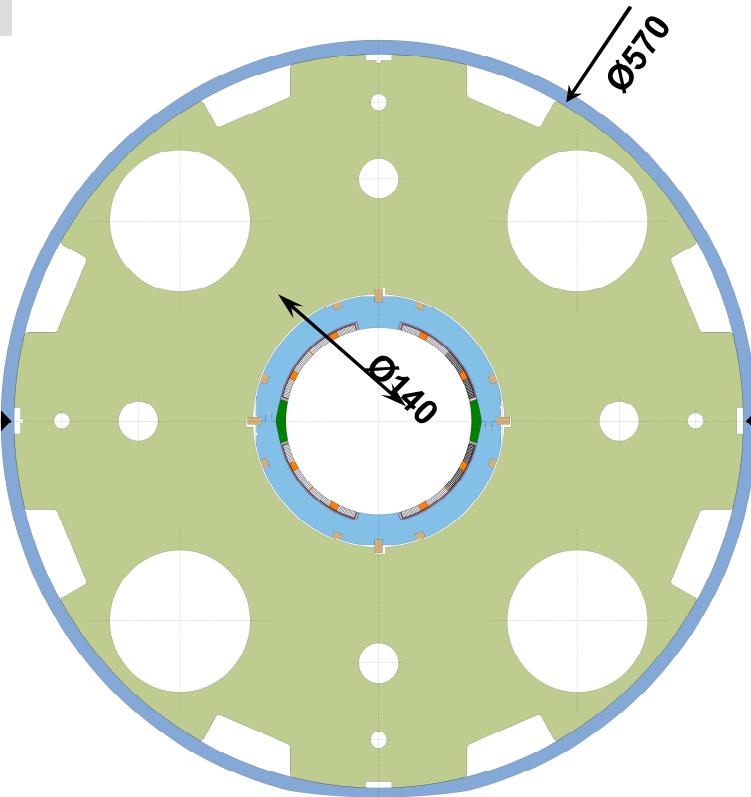


MQSX Single-Layer Base-Line Design

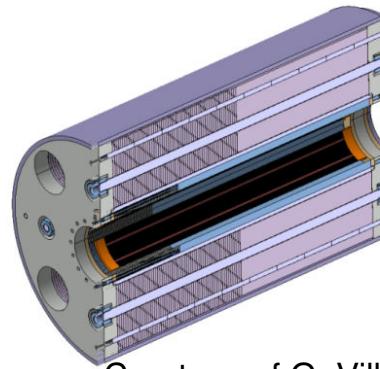


	Unit	
Nominal gradient	T/m	21
Mag. length	m	0.64
Nominal current	A	2400
Stored energy	kJ	8.8
Self inductance	mH	3.0
Working point		44 %
Cable width/mid-height	mm	4.37 / 0.845
Cu/Sc		1.2
Total length	m	~0.9
Aperture	mm	Ø140
Total mass	kg	~500

MQXS Assembly



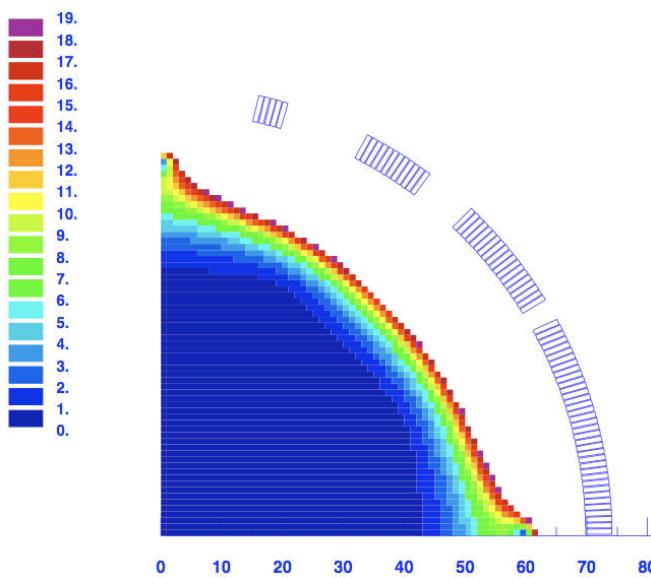
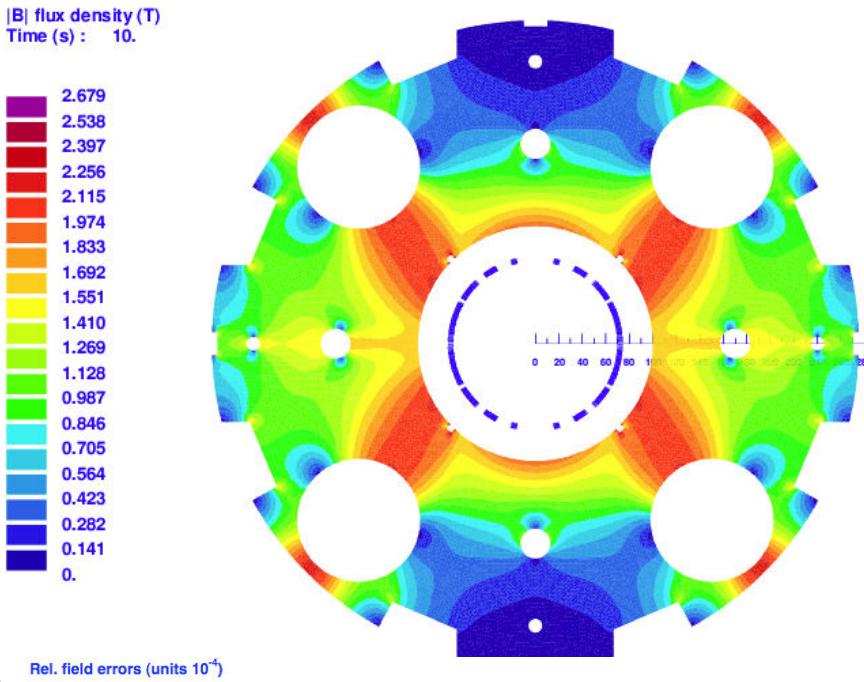
New 4.37 mm cable & Polyimide insulation
Single layer coils
Self-supporting collars
Single piece yoke



Courtesy of G. Villiger

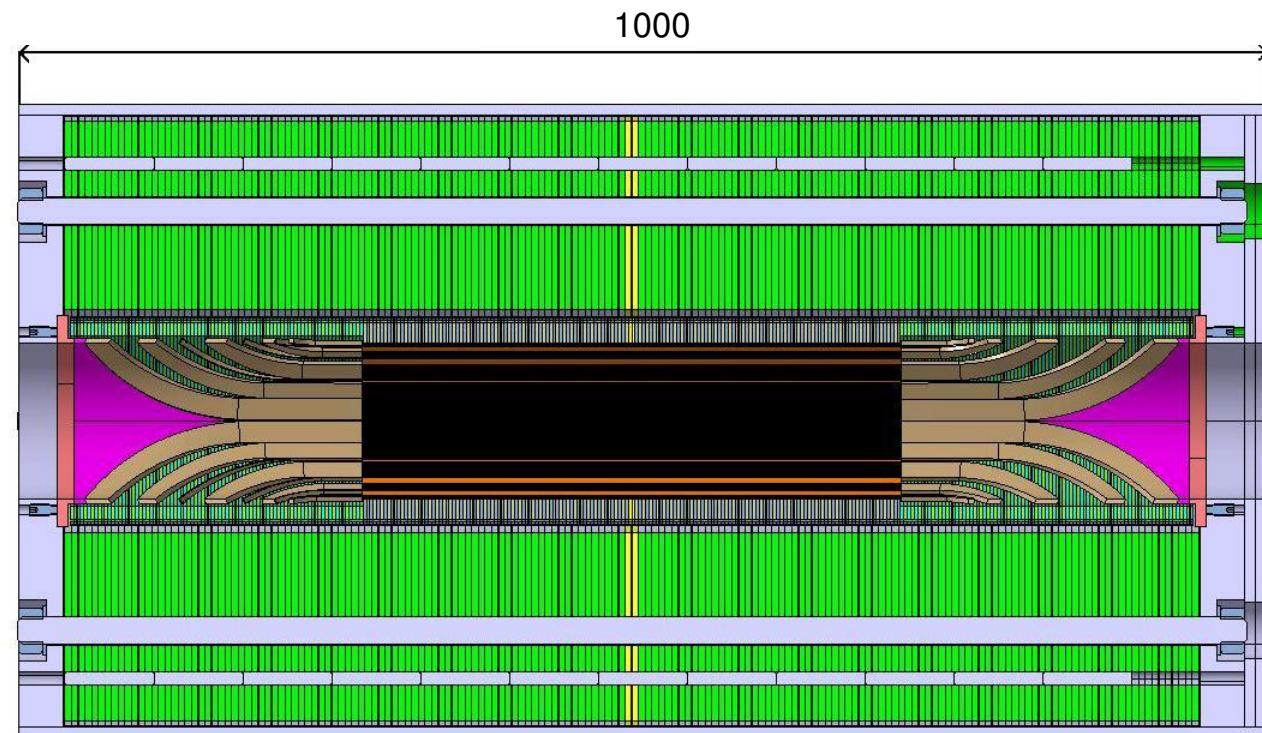
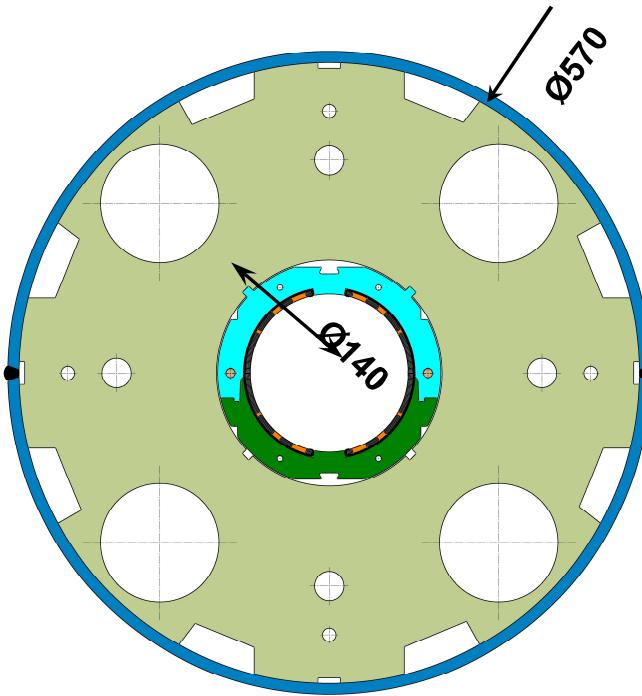
Field strength	0.65 Tm
Gradient	25.5 T/m
Operating temp	1.9 K
Current	2.4 kA
Inductance	3.3 mH

MCXB Single-Layer Design

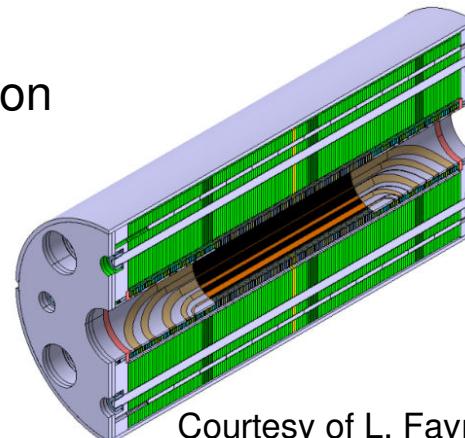


	Unit	
Integrated field	Tm	1.5
Nominal field	T	2.3
Mag. length	m	0.65
Nominal current	A	2400
Stored energy	kJ	28
Self inductance	mH	10
Working point		50%
Cable width/mid-height	mm	4.37 / 0.845
Total length	m	~1
Aperture	mm	Ø140
Total mass	kg	~2000

MCXB 4-Block Design



New 4.37 mm cable & Polyimide insulation
Self-supporting collars
Single piece yoke



Courtesy of L. Favre

Field strength	1.5 Tm
Operating temp	1.9 K
Current	2.4 kA
Inductance	10 mH

18-Strand Cable

Strand parameters		
Cu:Sc	1.75	
Strand diameter	0.48	mm
Metal section	0.181	mm ²
No of filaments	2300	
Filament diam.	6.0	µm
I(5T,4.2K)	203*	A
j _c	3085*	A/mm ²

*) extracted strand March -09

Cable Parameters		
No of strands	18	
Metal area	3.257	mm ²
Cable thickness	0.845	mm
Cable width	4.370	mm
Cable area	3.692	mm ²
Metal fraction	0.882	
Key-stone angle	0.67	degrees
Inner Thickness	0.819	mm
Outer Thickness	0.870	mm

**Polyimide Insulation: 2 x 25µm + 55 µm
 Trial cabling length (~100 m) done!
 Insulation trials & characterization in progress..**

Milestones... (MCXB & MQXS)

→ Parameter list	Oct-09..Jan-10
→ Magnetic and mechanical design	Nov-09
→ Fabrication drawings	May-10
→ Trial coils	Jul-10
→ Mechanical model	May-10 & Jul -10
→ Model magnets completed	Dec-10
→ Technical specifications	Mar-11
→ Industrial contracts	Jul-11
→ Pre-series magnets	Jul-12
→ Series production	Sep-12 .. Dec-13