



Modification of the shielded beam screen design & misalignment analysis

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Outline

- Concept
- Behaviour during quench
- Main modifications of the beam screens due to CLIQ
- Misalignment effects of the beam screen in the cold bore
- Conclusions

Concept

Beam screen tube (BS) at 60-75 K:

- Perforated tube (~2%) in High Mn High N stainless steel (1740 l/s/m (H2 at 50K))
- Internal copper layer (75 μm) for impedance
- a-C coating (as a baseline) for e- cloud mitigation
- Laser treatments under investigation

Thermal links:

- In copper
- Connected to the absorbers and the cooling tubes or beam screen tube

Cold bore (CB) at 1.9 K:
4 mm thick tube in 316LN

Cooling tube:

- Outer Diameter: 10 or 16 mm
- Laser welded on the beam screen tube

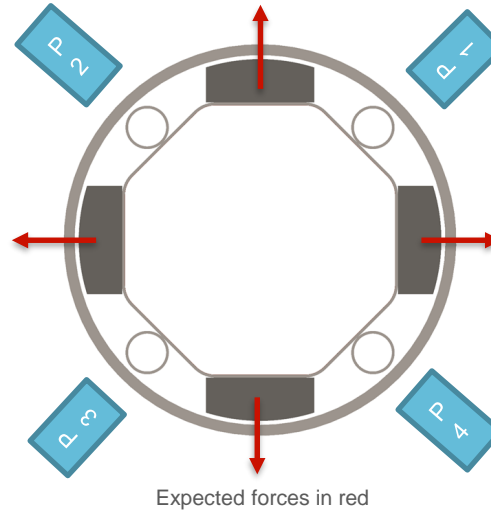
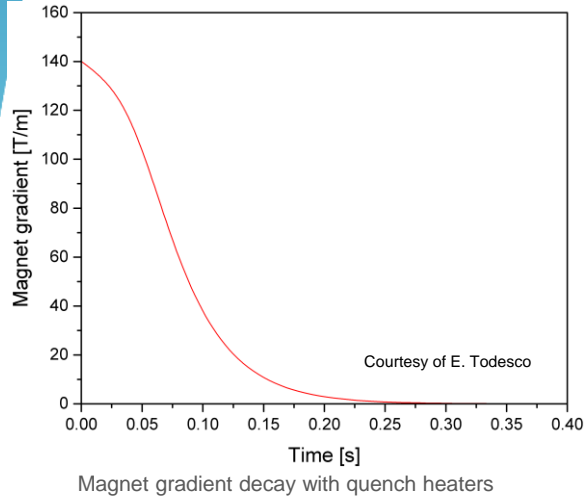
Elastic supporting system:
Low heat leak to the cold bore tube at 1.9K. Ceramic ball with titanium spring

Tungsten alloy blocks:

- Chemical composition: 95% W, ~3.5% Ni, ~1.5% Cu
- Mechanically connected to the beam screen tube: positioned with pins and titanium elastic rings
- Heat load: 15-25 W/m
- 40 cm long

Behaviour during a magnet quench

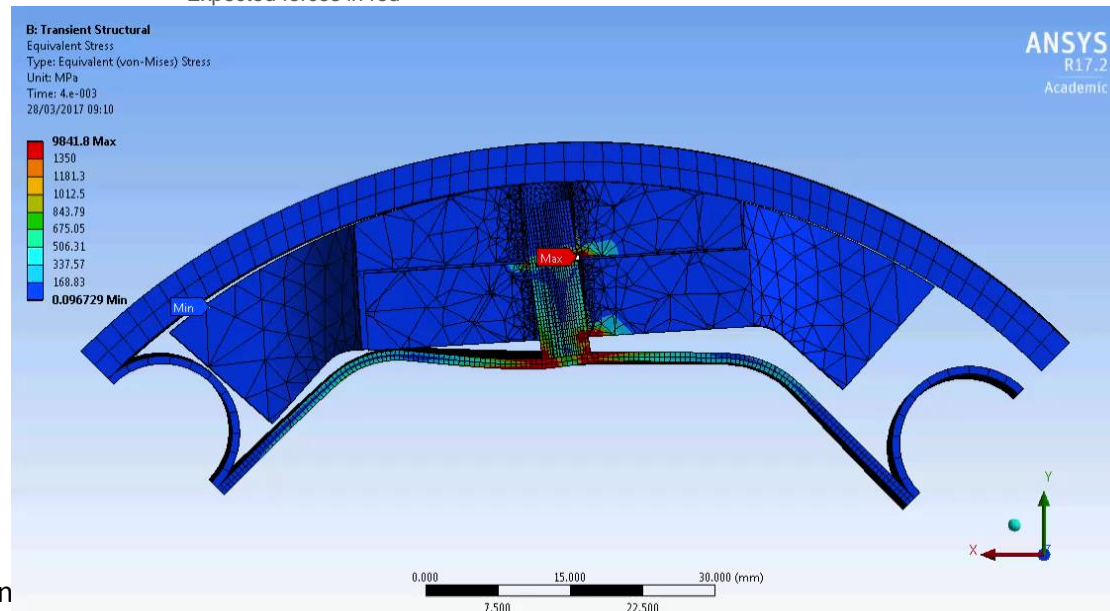
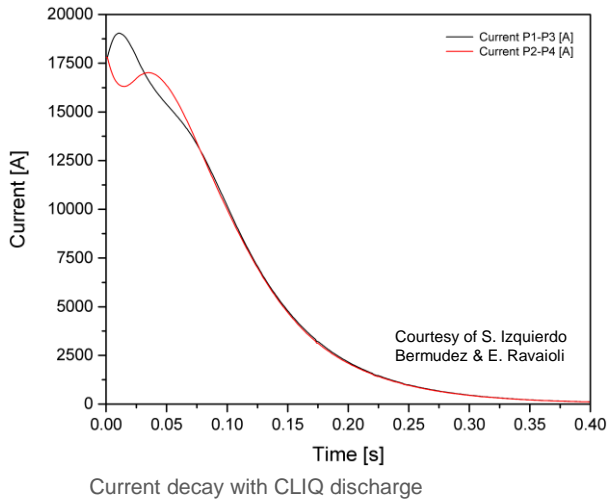
Quench heaters vs CLIQ



Specific Lorentz forces reads:

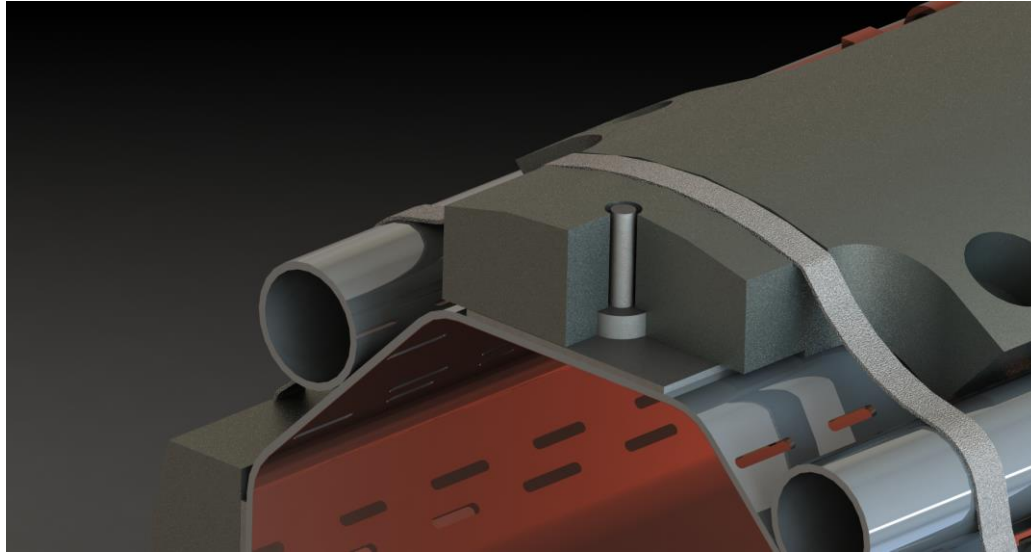
$$f \propto \frac{G\dot{G}}{\rho} r^3$$

- Lorentz forces driven by GG' product
- Lorentz forces acting on the beam screen are pointing toward the cold bore
- Lorentz forces are maximum after 50 ÷ 60 ms.



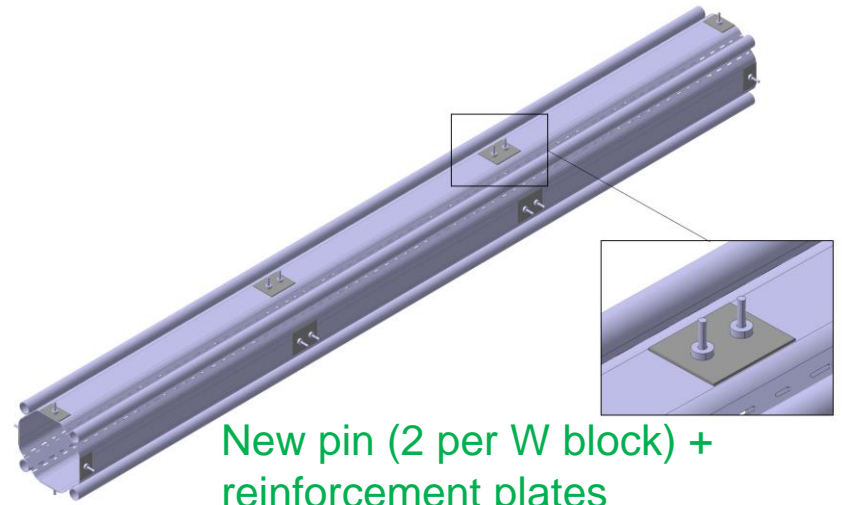
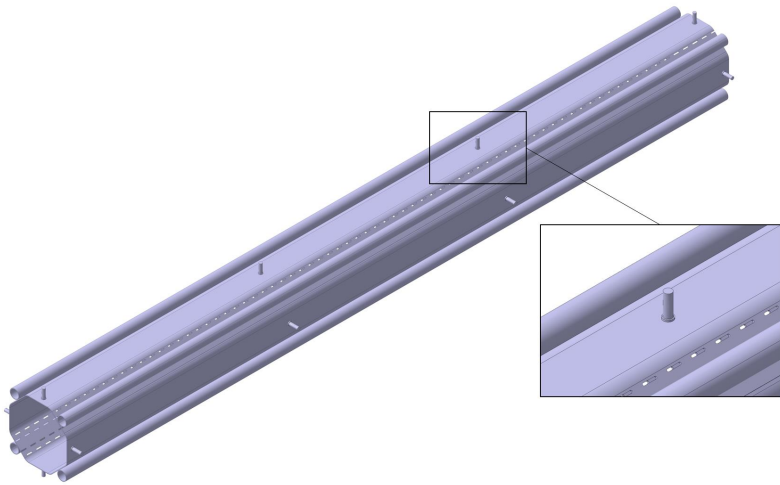
The study has been presented at the HL-LHC Project meeting (https://indico.cern.ch/event/655550/).

Main modifications of the Q1 beam screen



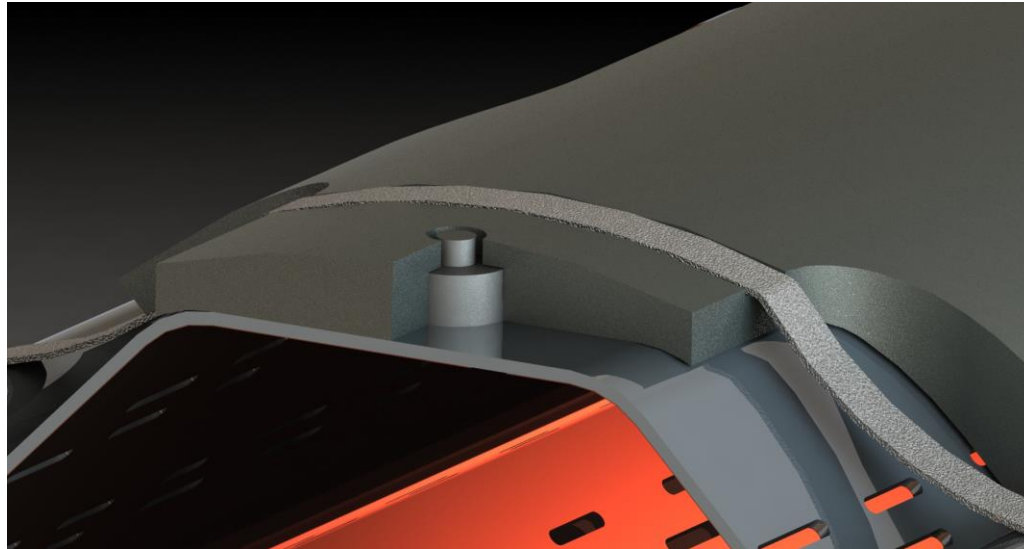
Old design

New design



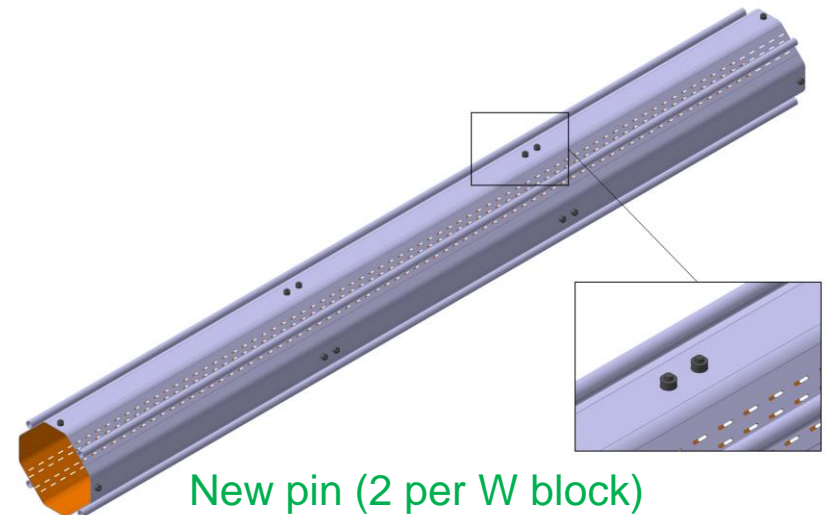
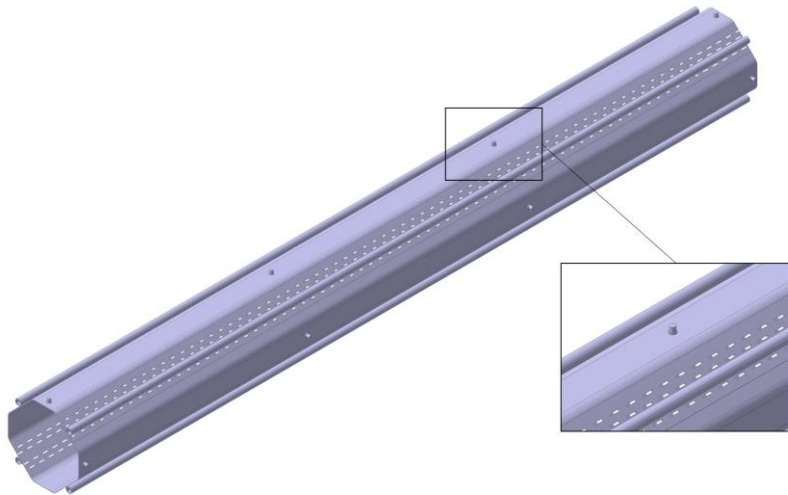
New pin (2 per W block) + reinforcement plates

Main modifications of the Q2x-Q3-D1 beam screens



Old design

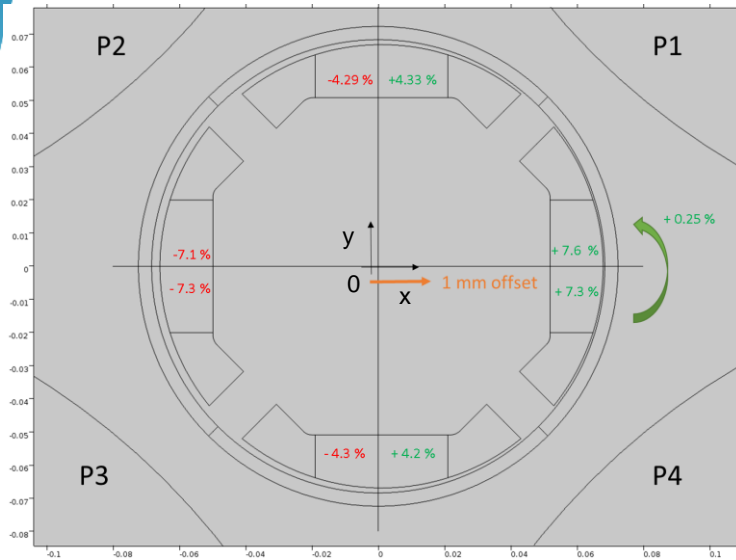
New design



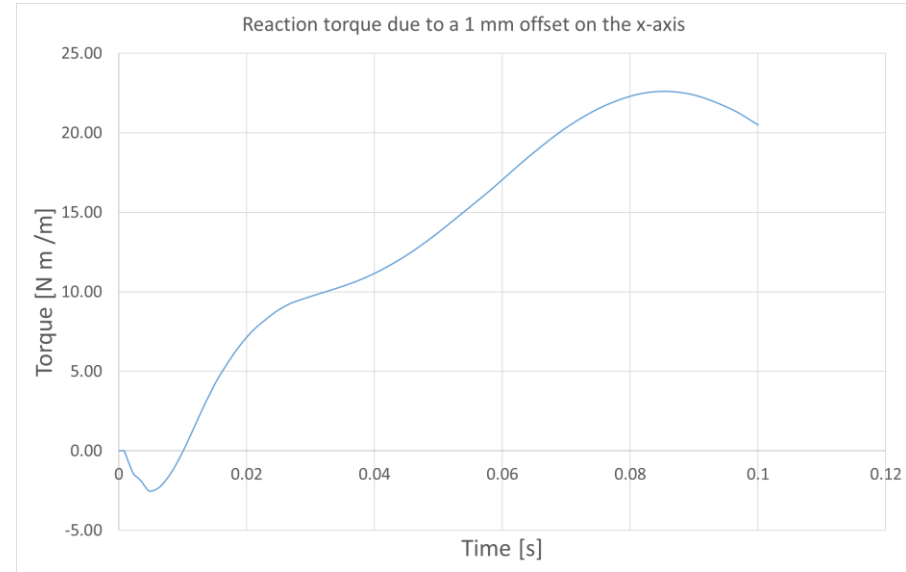
New pin (2 per W block)

Misalignment effects of the beam screen in the cold bore

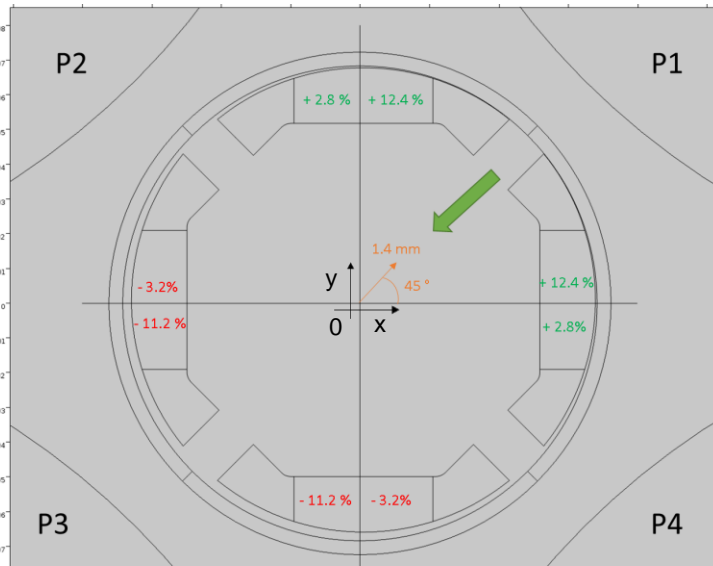
@ 5 ms



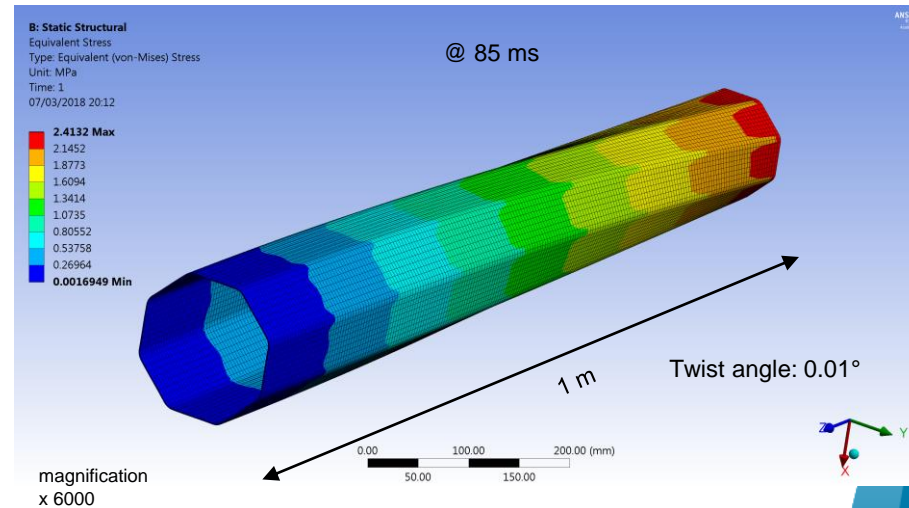
Variation of the forces in the W blocks due to 1 mm offset on the x-axis of the BS in comparison with the nominal case at 5 ms.



Reaction torque of the BS fixed at one end during the CLIQ discharge



Variation of the forces in the W blocks due to 1.4 mm offset at 45° of the BS in comparison with the nominal case at 5 ms.



Maximum V.M. stress on the fixed end of the BS due to the 1 mm offset .

The misalignment effects are negligible at the fixed point of the beam screen. M. Morrone, C. Garion

Conclusions

- The cost estimate for the beam screen modification is 250 kCHF, which includes:
 - raw material;
 - machining and assembly of additional pins;
 - reinforcement plates;
 - elastic rings;
 - drawing updates.
- No impact neither on schedule nor on the performance is expected:
 - no impact on aperture;
 - no impact on field quality;
 - non significant impact on shielding efficiency.
- No impact on the beam screen fixed point due to a misalignment of the beam screen in the cold bore.



EDMS NO. 1893675	REV. 0.1	VALIDITY DRAFT
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REFERENCE : LHC-VSM-EC-0001

HL – LHC Engineering Change Request Modification of the shielded beam screen design

ECR DESCRIPTION

WP Originator	WP12, PBS 12.1.1	Process	Engineering
Equipment	LHCVSM	Baseline affected	Cost
Drawing	N/A	Date of Issue	2018-01-07
Document	N/A	CI responsible	C. Garion
WPs Affected	WP12	Reference Document	TDR Version 0.1

Detailed Description

New beam screens with tungsten based alloy shielding will be installed in the HL-LHC triplet areas. The design of these beam screens is based on an octagonal perforated tube made of 1 mm stainless steel with a 75 µm copper layer on the inner side. Absorbers, 16 mm and 6 mm thick for the Q1 and Q2a to D1, respectively, are 40 cm blocks positioned on the beam tube thanks to stainless steel pins. To minimize the amount of pins, an overlap of two consecutive blocks is applied. The heat deposited on the tungsten absorbers is transferred to the cryogenic cooling tubes by copper thermal links (Fig. 1).



Fig. 1 HL-LHC shielded beam screen

The design of these beam screens shall be compatible with magnet quenches (EDMS 1361079). During fast magnetic field decay, eddy currents and consequently Lorentz forces are induced in the conductive parts of the beam screen in particular in the copper layer and the tungsten absorbers. In case of monotonic field decay, as produced by quench heaters, Lorentz forces acting on the beam screen are pointing toward the cold bore. For example, for the Q1 quadrupole, forces per quadrant of 37 N/m and 230 N/m are expected in the copper layer and tungsten absorbers. During the quench, the beam screen is elastically deformed, the tungsten blocks leans on the cold bore and most of the Lorentz forces induced in the tungsten absorbers is transferred to the 4 mm thick stainless steel tube.

Reasons for change

A new quench protection system, called CLIQ [1], has been proposed for the triplet quadrupoles. It is based on a fast transient alternative current unbalanced between the different coils of the magnet. This fast alternative current induces dissipation and temperature increase in the superconductor and then leads to the resistive transition. The fact that the current evolution is not anymore monotonic leads to an inversion of the Lorentz force direction (forces pointing toward the aperture center for a current increase). In addition, during this transient, the current evolution is different in two adjacent coils: one is subjected to a current decay leading to forces pointing to the cold bore whereas a current increase occurs in the other one leading to forces toward the aperture center. For the beam screen and in particular for the tungsten blocks, this leads to torques of 700 N.m and 580 N.m, per beam screen meter, for the absorbers and beam screen tube, respectively (Fig. 2). In case of magnet quench with the CLIQ protection system, the pins are not anymore only positioning elements but are structural components subjected to mechanical forces and torques. The design of the beam screen with positioning pins is not compatible with the CLIQ discharge (high stresses and plastic deformation in the pin areas).

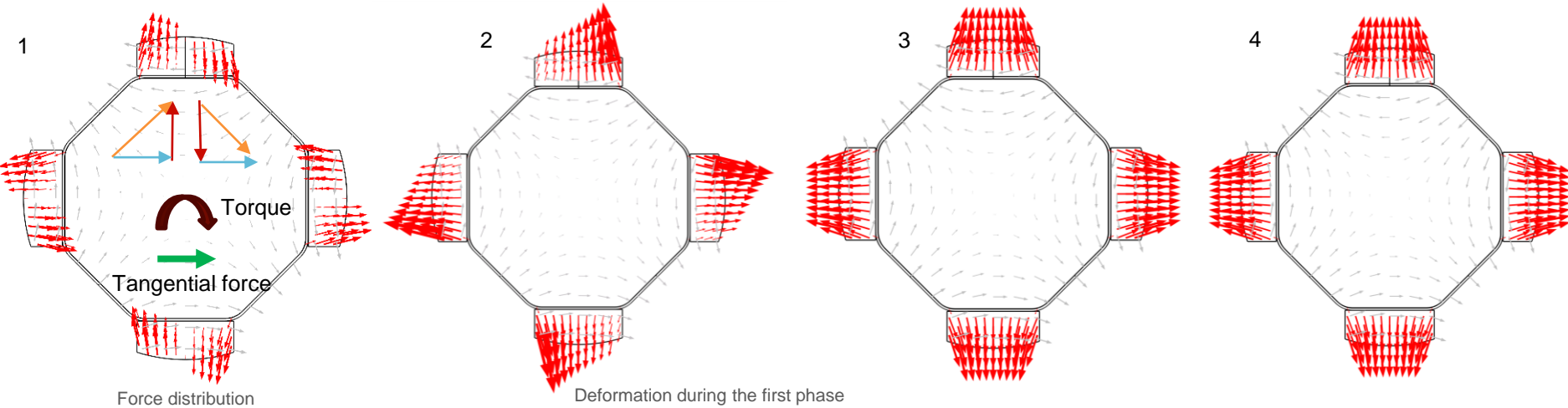
Thank you for your attention



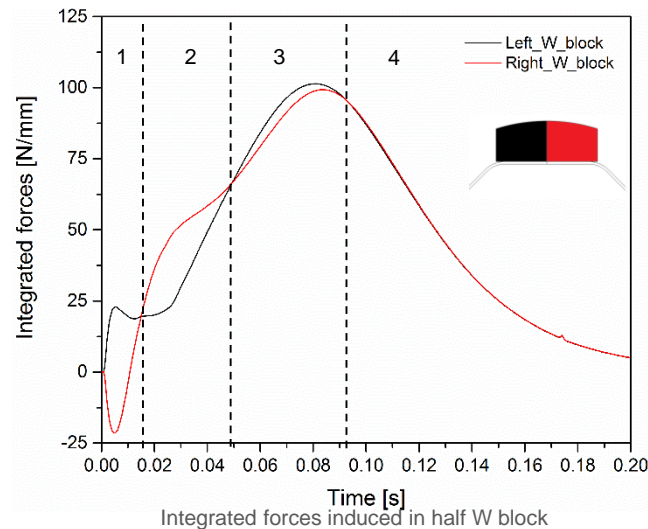
Backup slides

Behaviour during a magnet quench

Impact of CLIQ



Phase 1: Most critical!!



component	Q1		Q2	
	Torque [N m/W block]	Tangential force [N/W block]	Torque [N m/W block]	Tangential force [N/ W block]
Cold bore	250	3400	250	3400
Heat absorber	280	4200	150	2200
Octagonal pipe	80	1600	230	3800

Phase 2: Less severe than phase 1

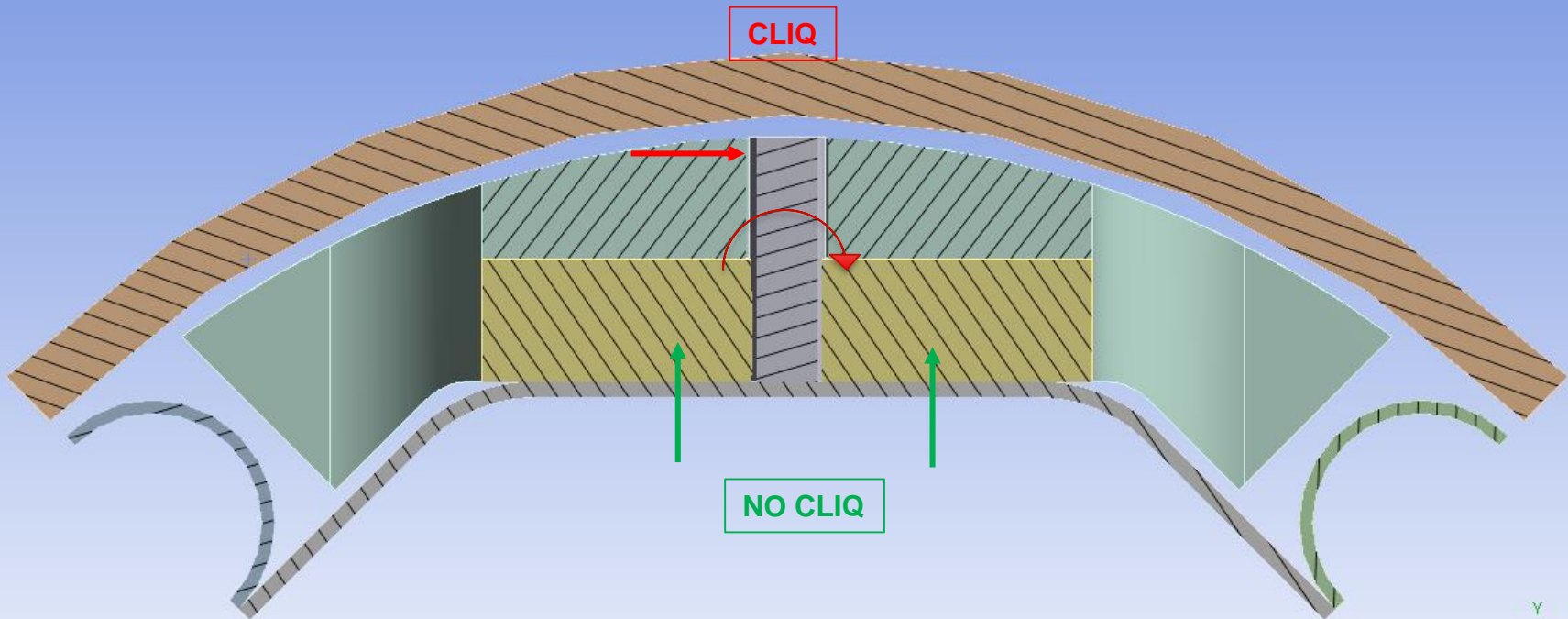
Phase 4: Less severe than without CLIQ

E.g. F_y for the tungsten block: $Q1_{NO\ CLIQ} \sim 230$ [N/mm] > $Q1_{CLIQ} \sim 200$ [N/mm]

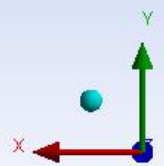
Impact of CLIQ

Geometry
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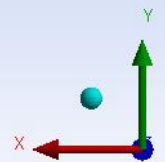
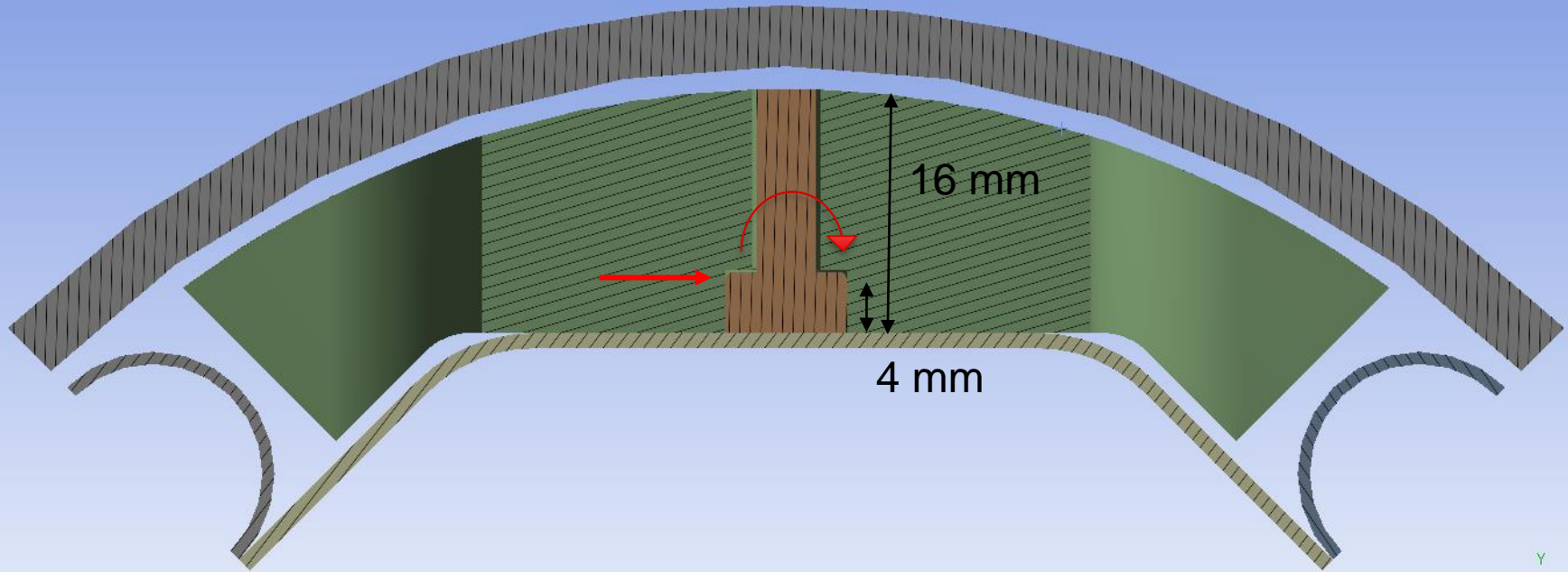
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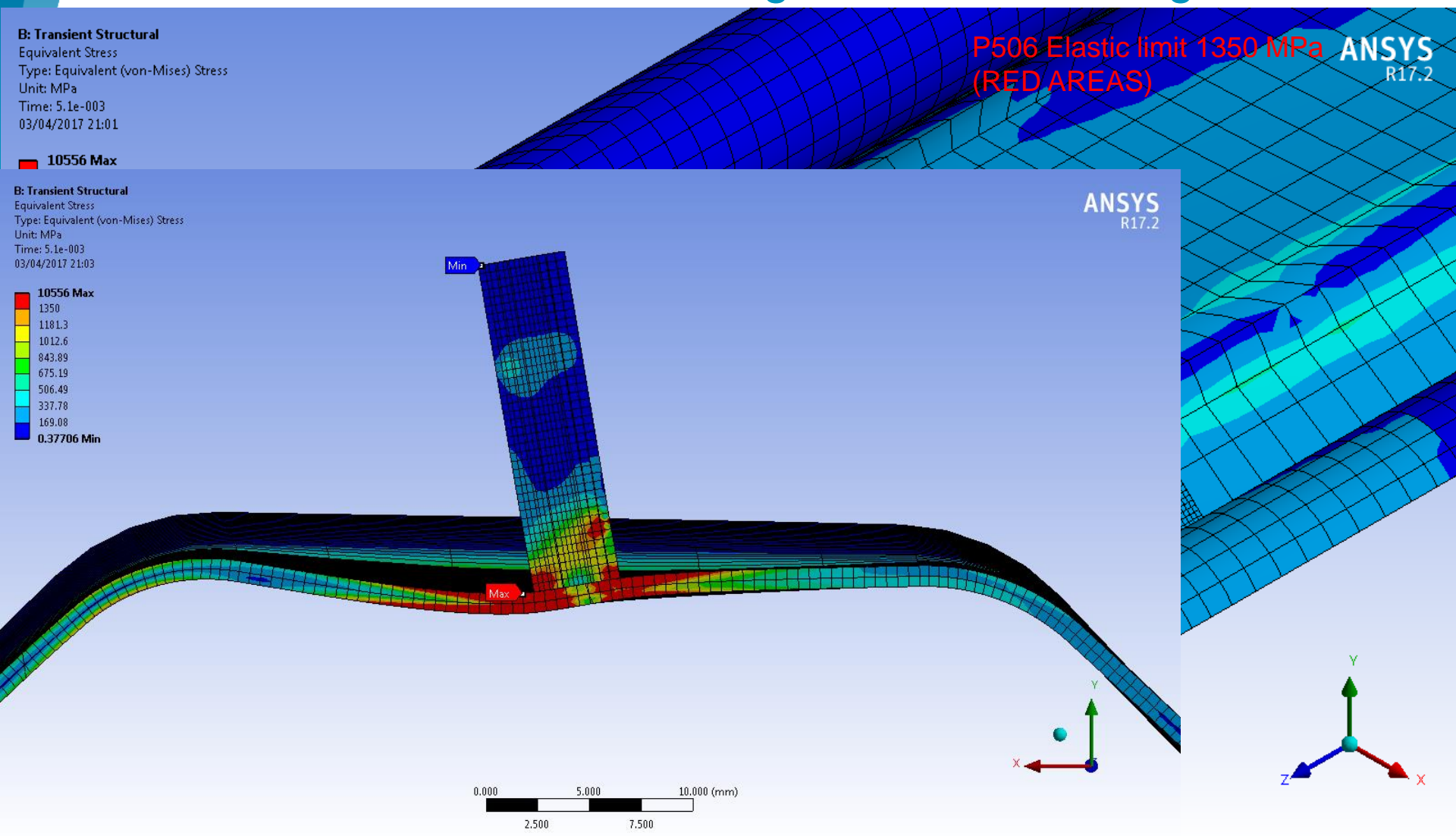
The pin becomes a structural component!
→ New solution needs to be found!



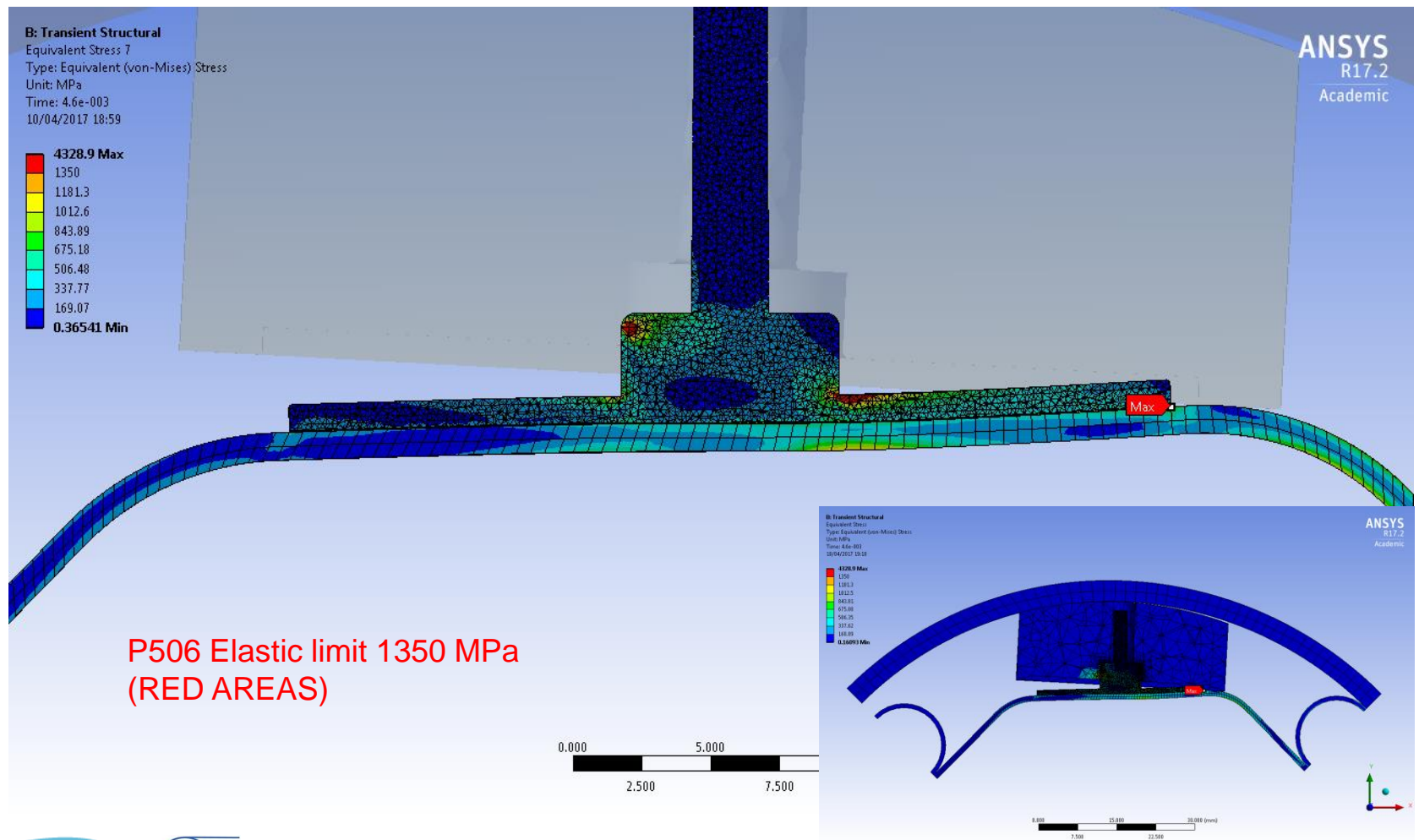
Proposed solution



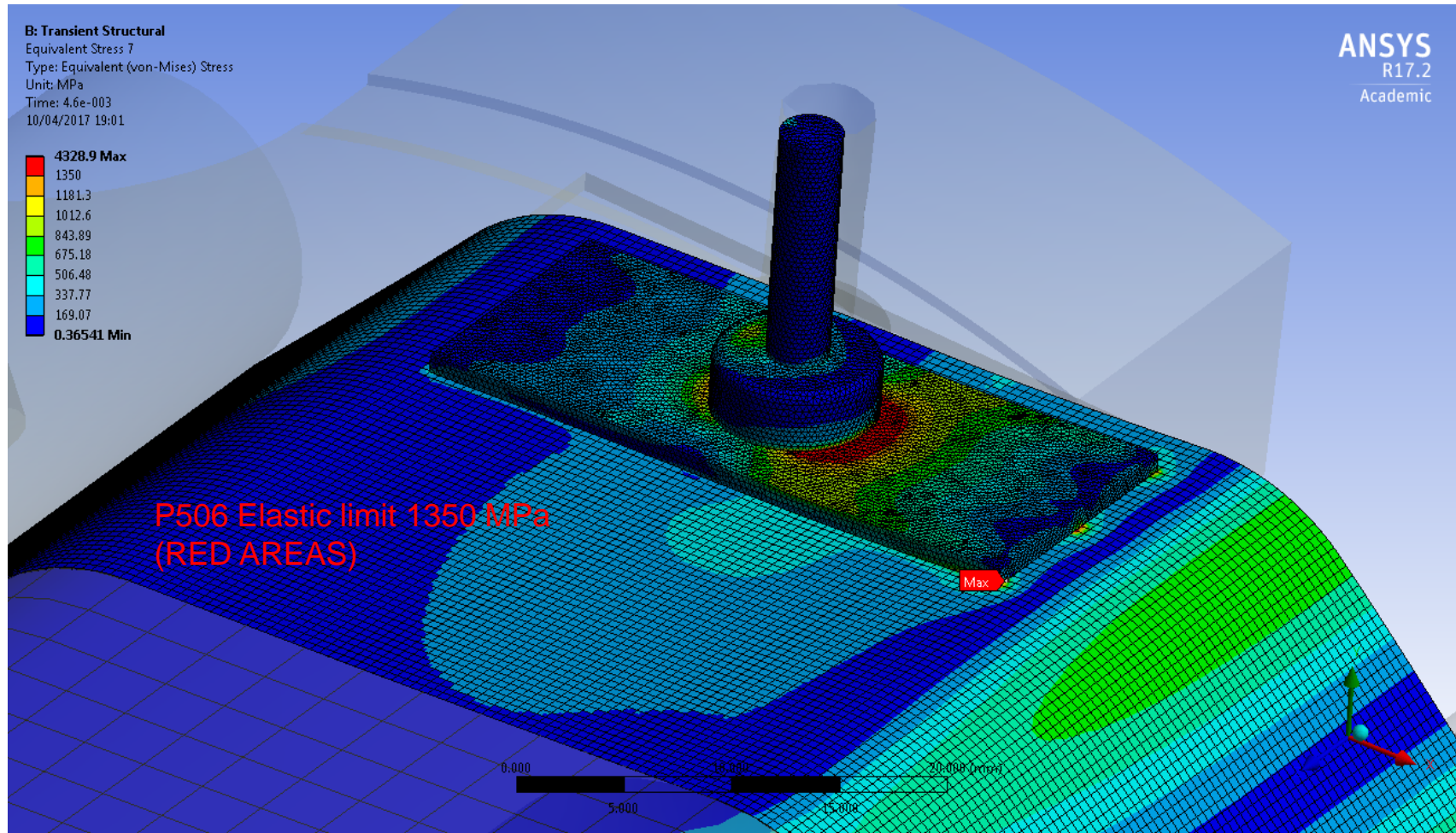
Q1 beam screen during the CLIQ discharge



Proposed Q1 beam screen during the CLIQ discharge_v2



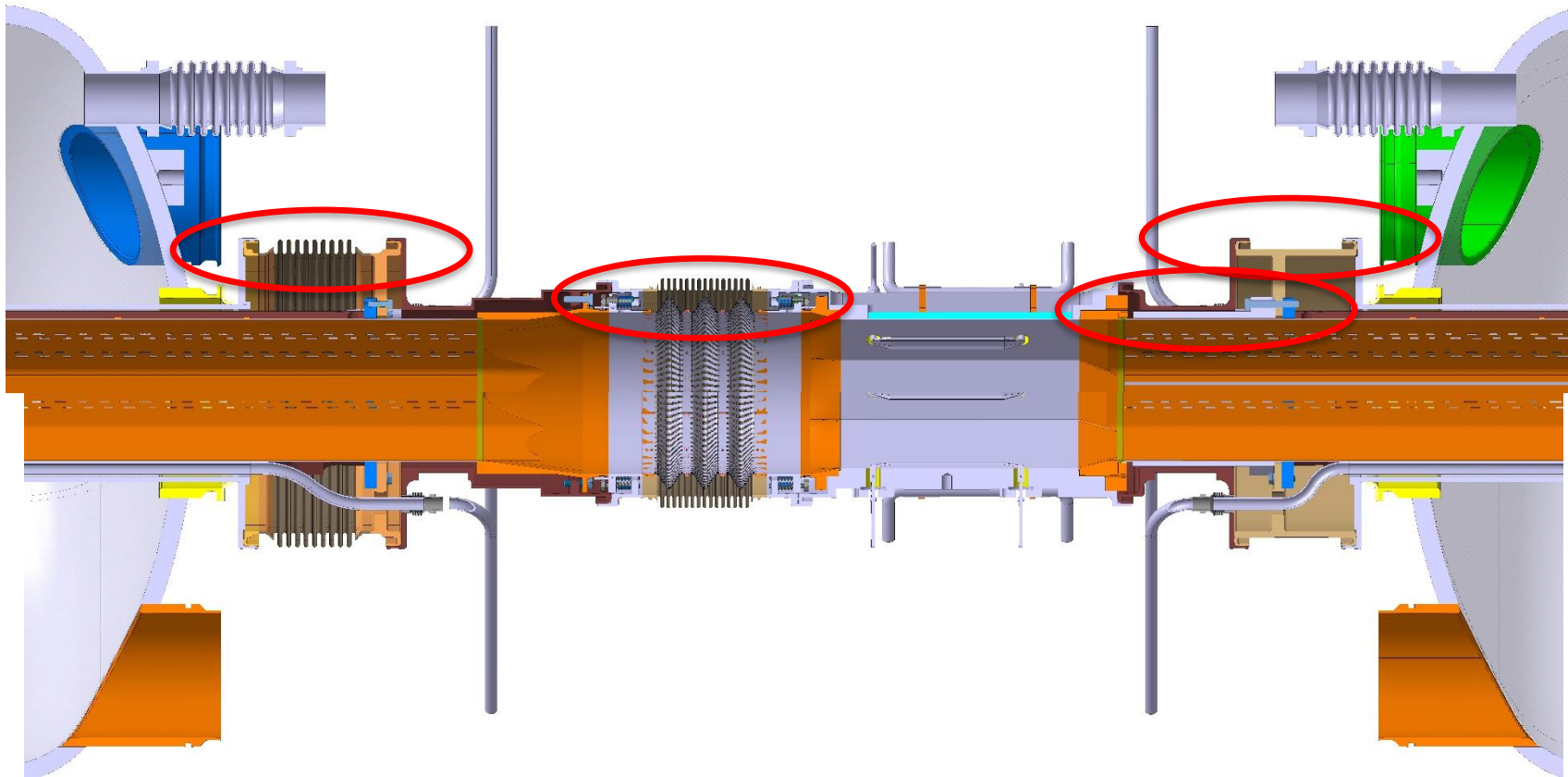
Proposed Q1 beam screen during the CLIQ discharge_v2



Beam screen extremities and interconnections

Layout

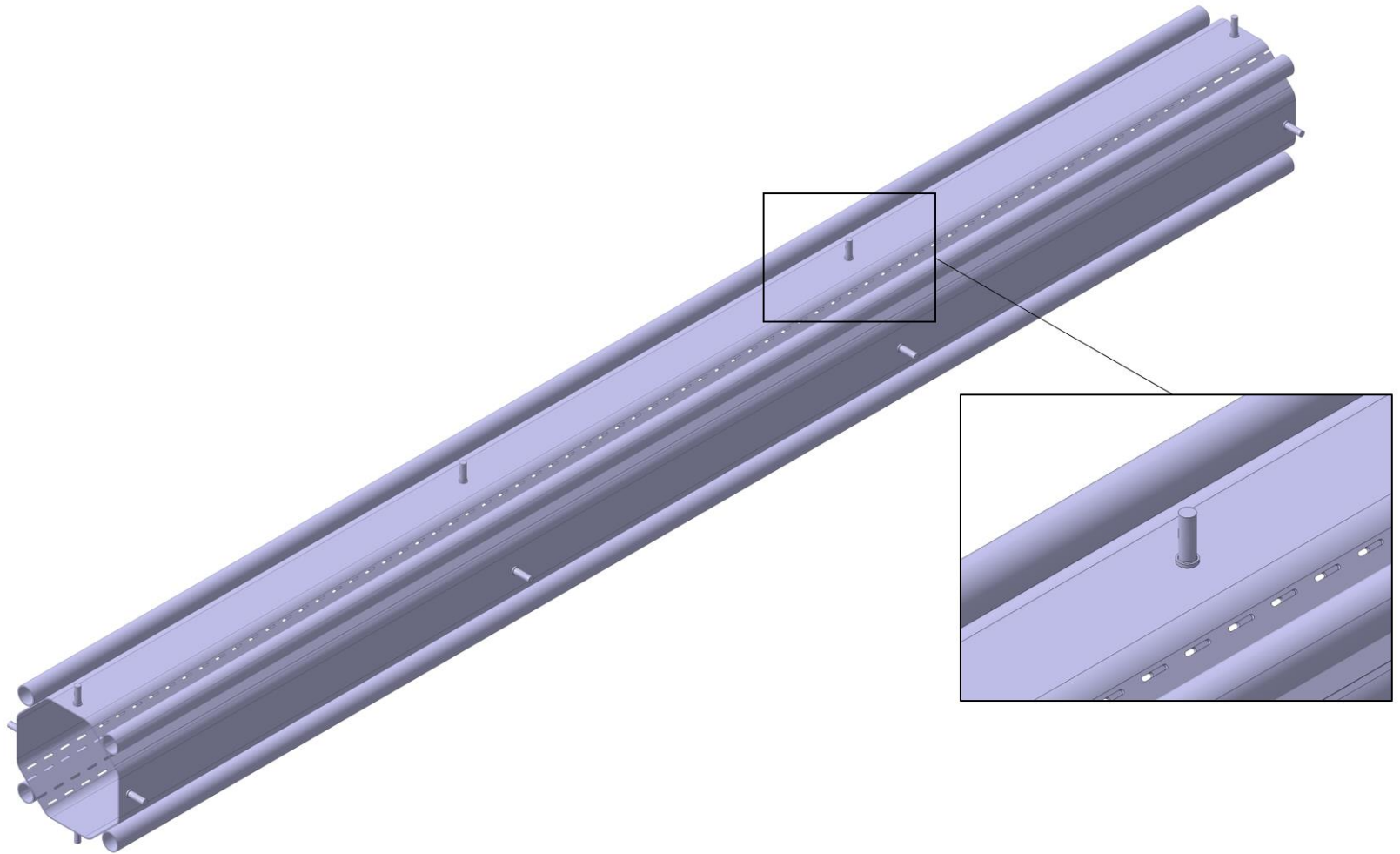
0/90° cut



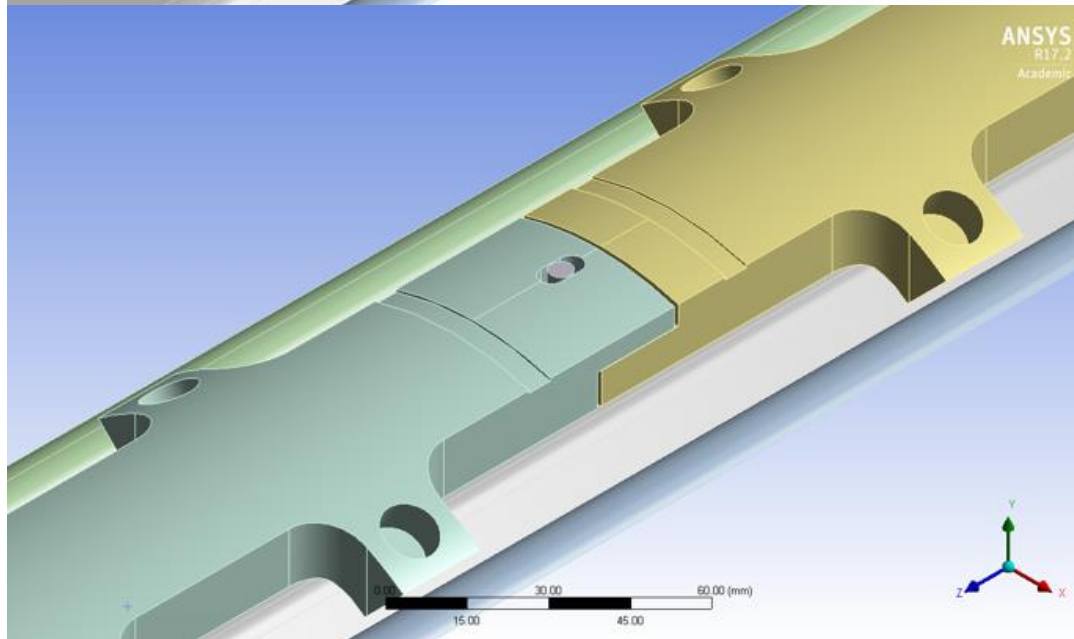
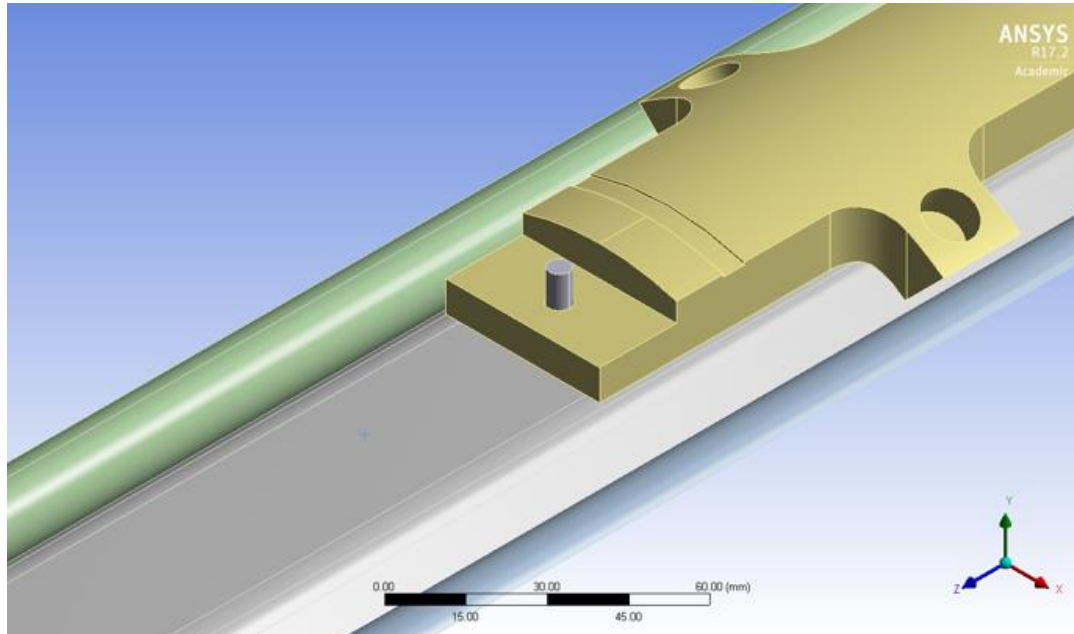
+/-45° cut

- More compact components (transversally)
- Longer absorber at the beam screen extremities
- Update of the interconnection module design

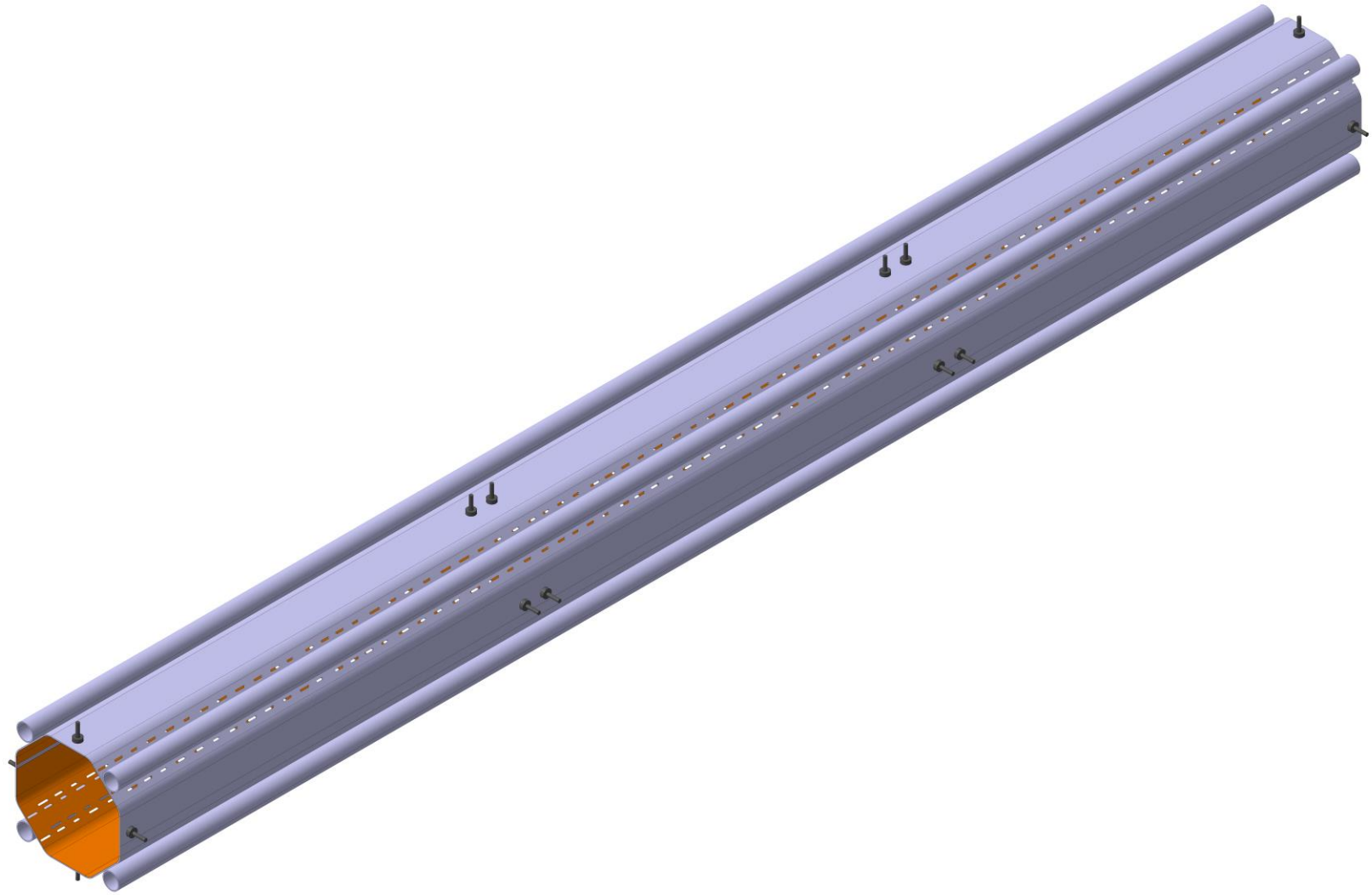
Old pins



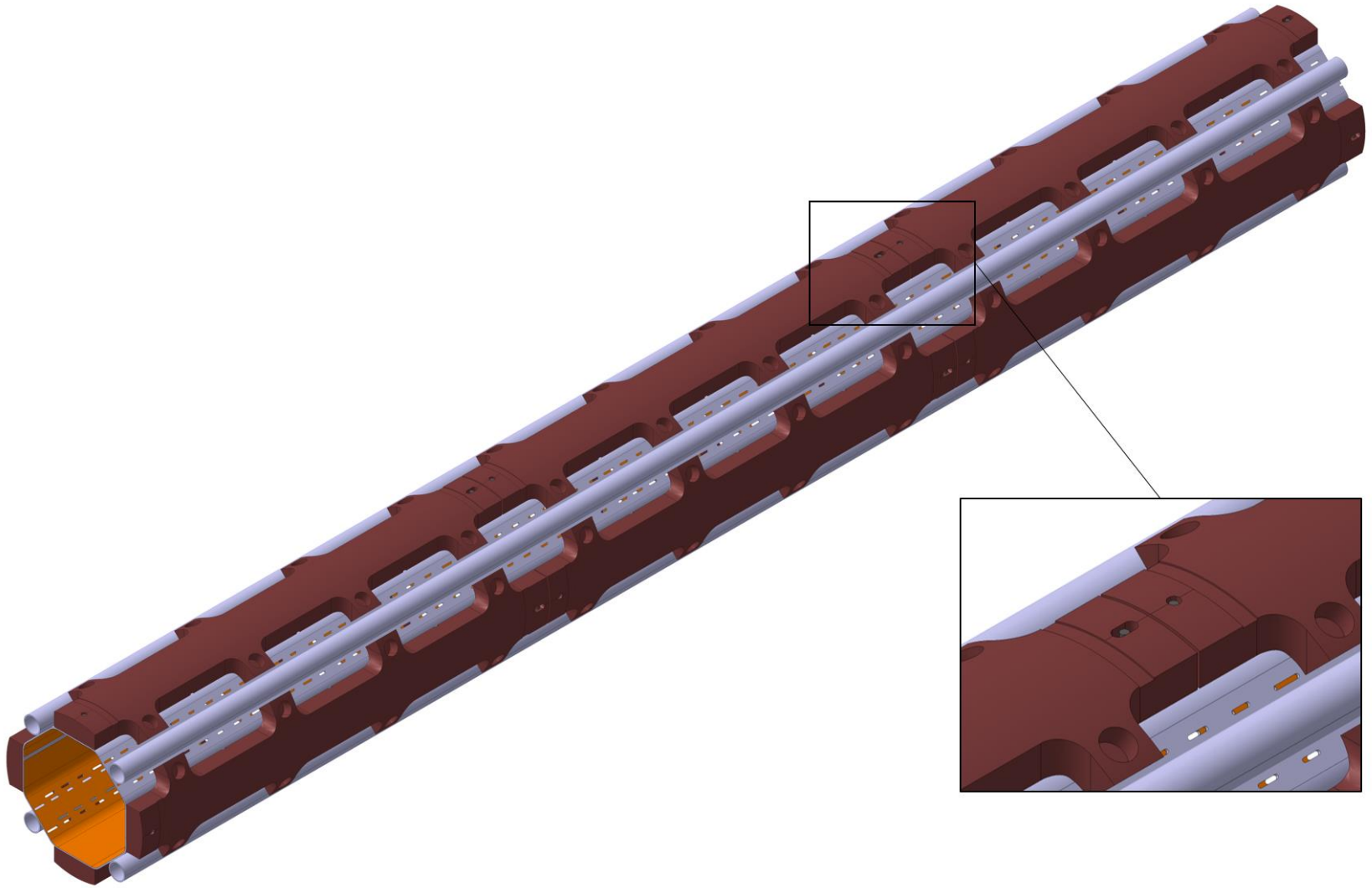
Old W blocks



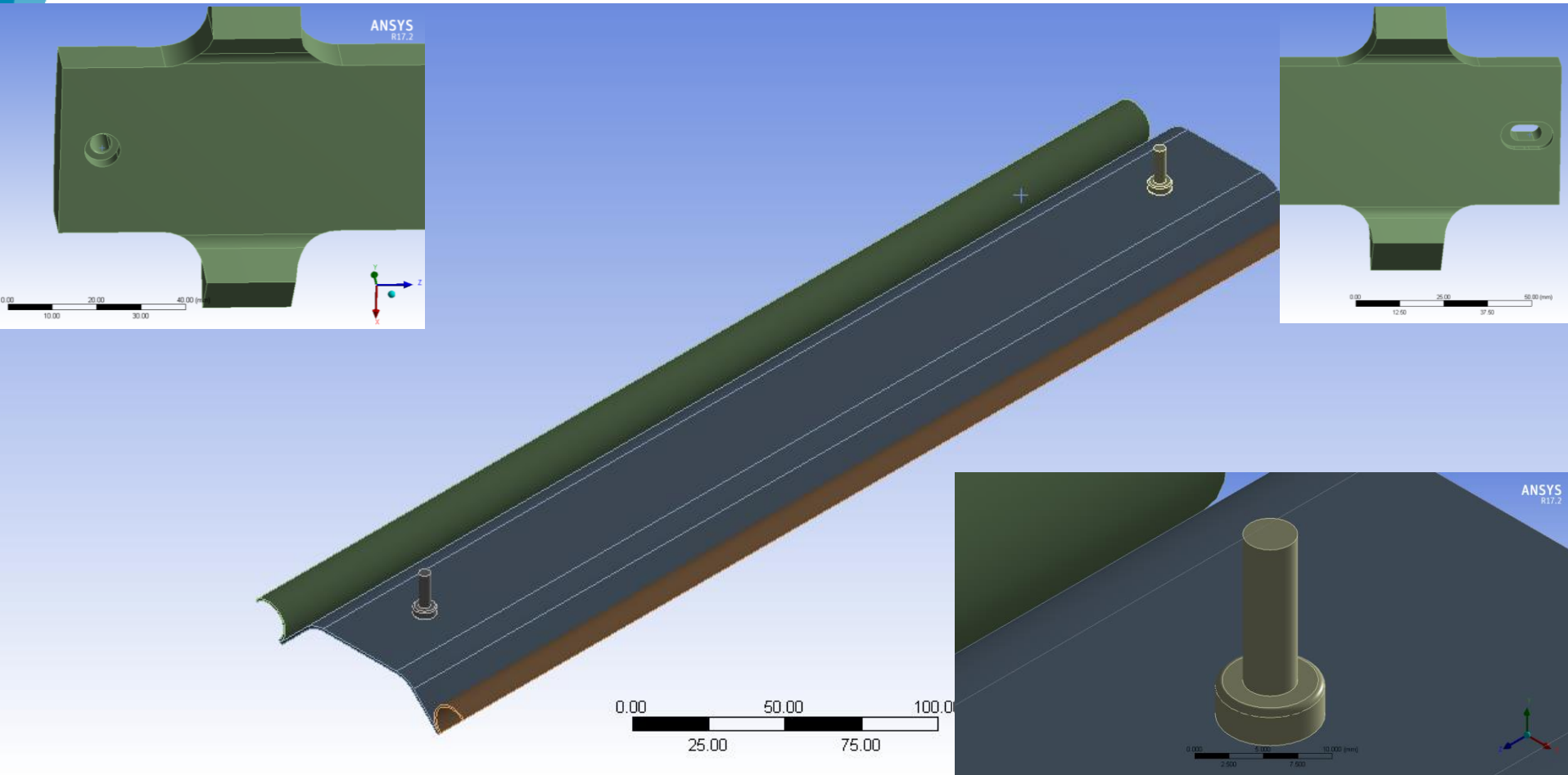
New pins



New W blocks



Details of the proposed beam screen design



Supporting system

