



Wrocław University  
of Science and Technology

# HP side CFD simulations

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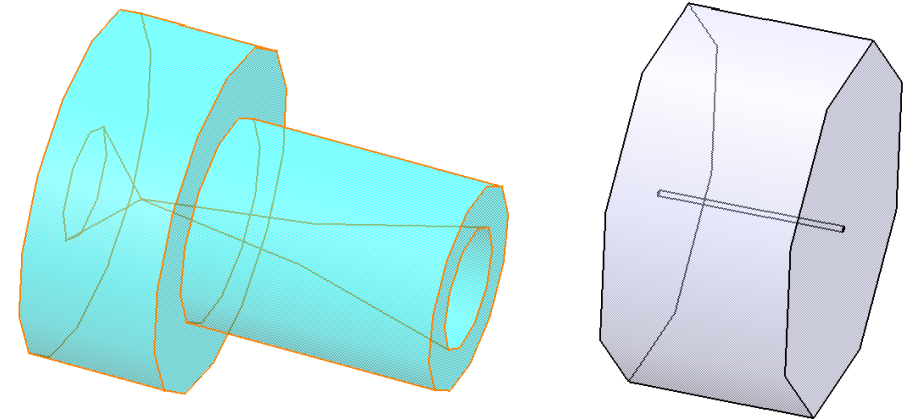
BGC Collaboration Meeting

Hotel Krone, Hirschberg

2018-03-19

# Agenda

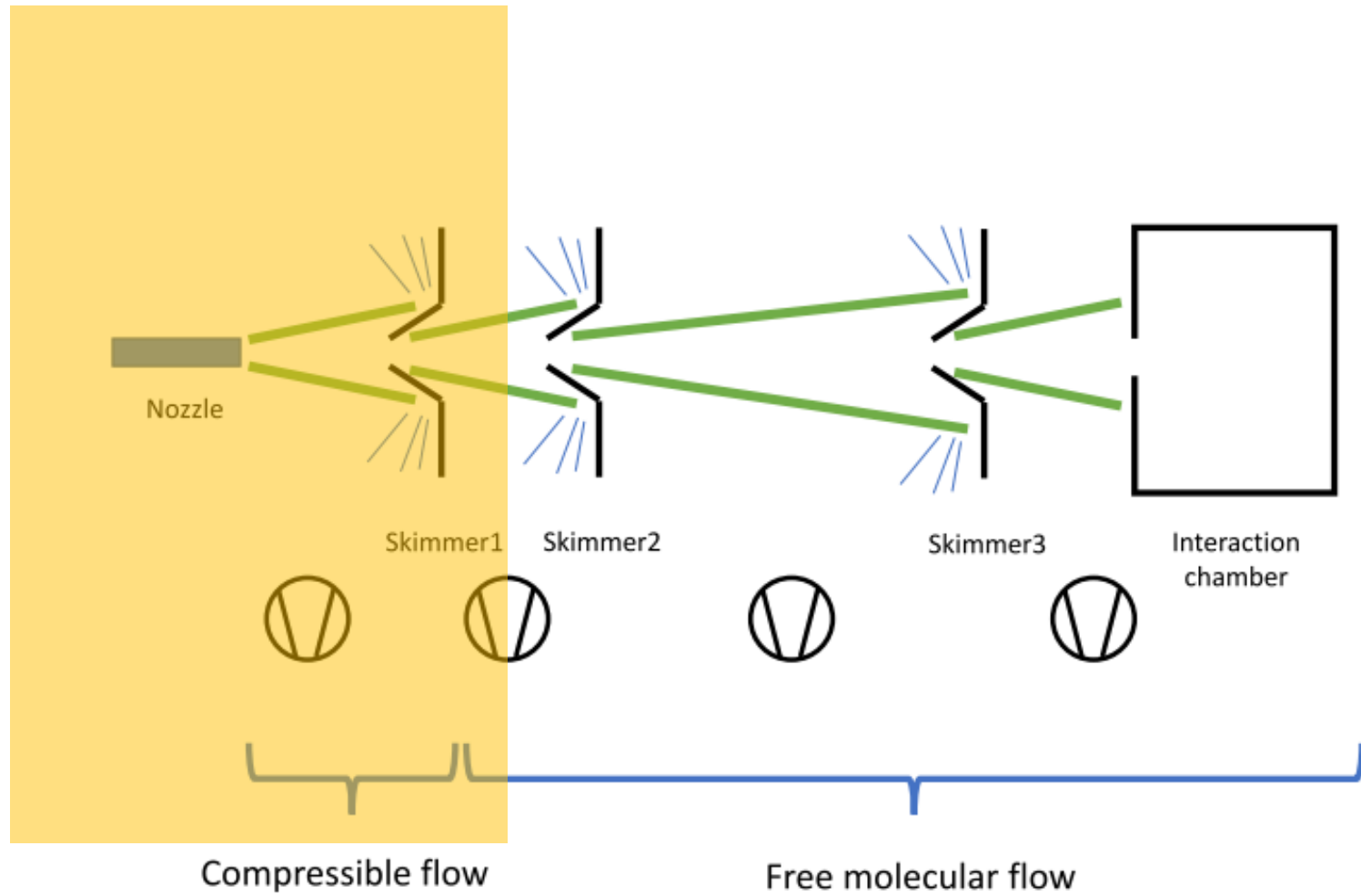
- Work done so far – a brief summary
- What we have learned from the CFD simulations
  - Nozzle parameters dependences
  - Gas temperature after expansion
  - Impact of the first skimmer
- Nozzle optimization
- Further development of the simulations



Abbreviations used in the presentation:

- Simple Geometry nozzle -> SG
- de Laval nozzle -> DL

# Gas jet formation



# Work done so far in CFD

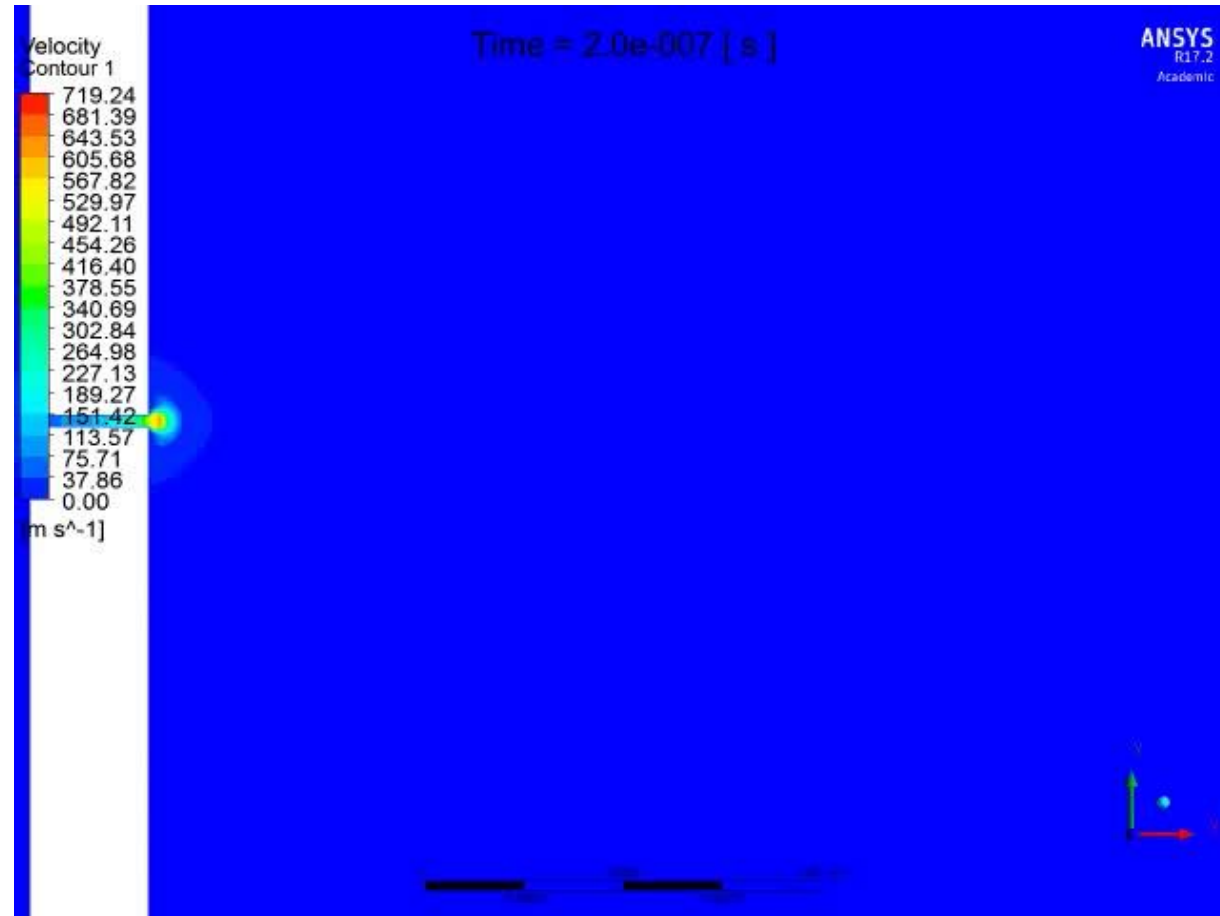
- Formation of the gas jet for SG in time – *without the skimmer*
- Comparison between SG and DL – *without the skimmer*
- Simulations with the 1<sup>st</sup> skimmer for SG and DL
- Comparison between different boundary conditions for DL

## Some statistics:

- Solved over 79 different simulations, from which approx. 80% were used as an initial value for single case: One case consist of 3 to 5 initial value simulations
- Time for single simulation ~ 6h
- Processor core used: from 8 to 16 per one simulation
- RMS error target  $10^{-7}$

# Forming of a jet – first $1 \cdot 10^{-5}$ s

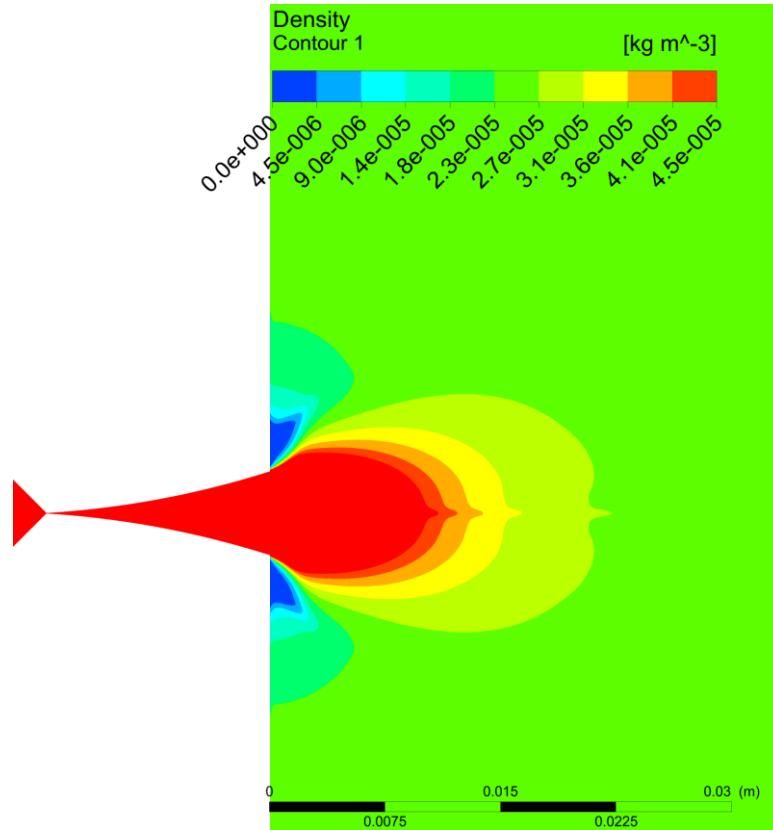
Jet formation into high vacuum needs **less than  $1e-5$  s** to fully developed a stable stream



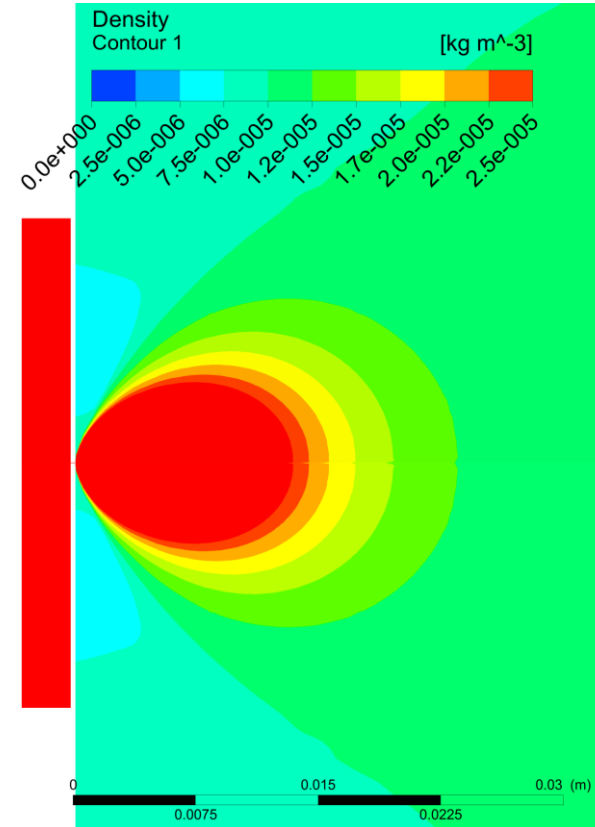
# Density Profile – comparison of the nozzle design

nozzle throat 30  $\mu\text{m}$

De Laval



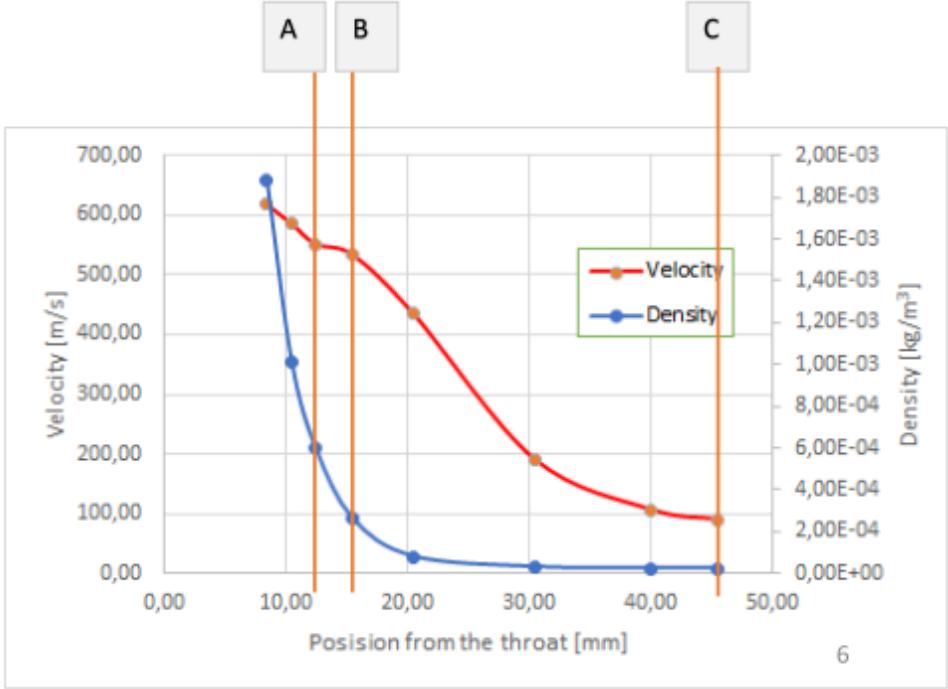
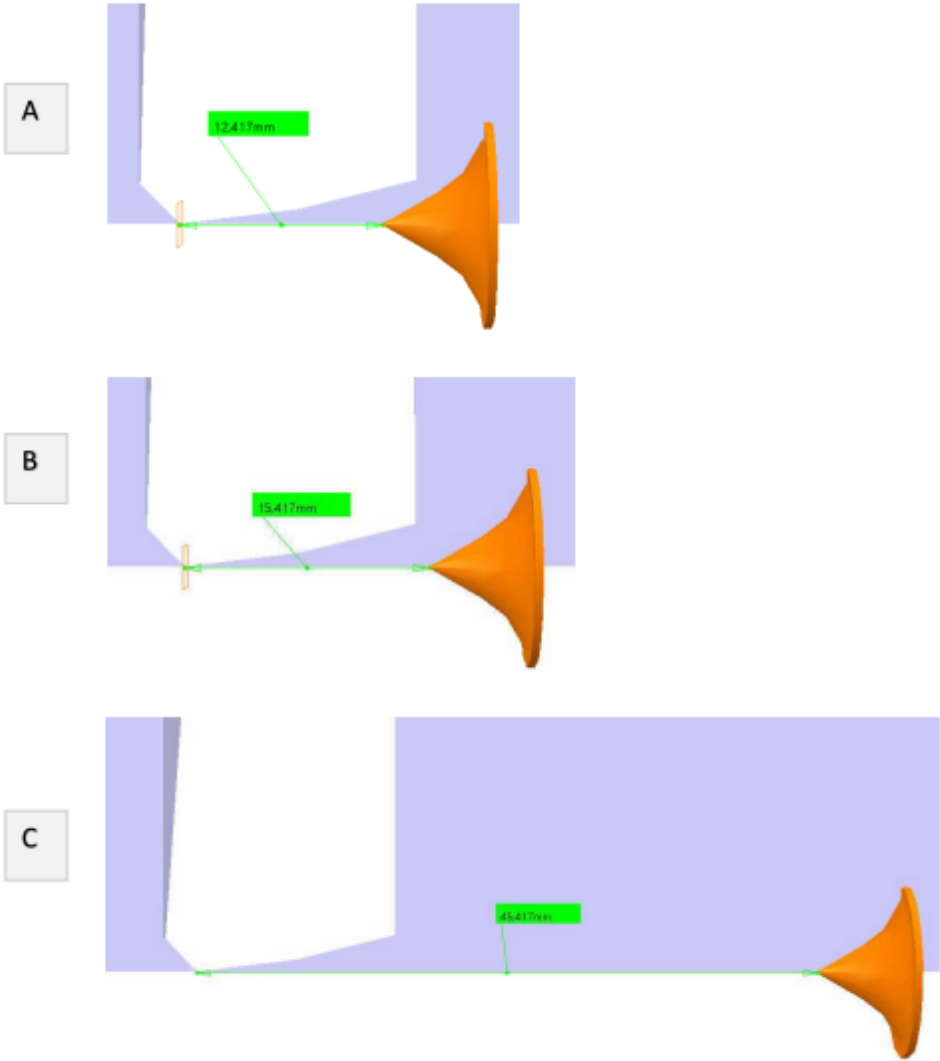
Simple Geometry



Taking into consideration the same boundary conditions, the de Laval (convergent-divergent) nozzle shows higher density profile, which is around **2 times higher** in comparison to simple geometry nozzle.

# Influence of the distance to the throat cross-section

Free parameters, high pressure part



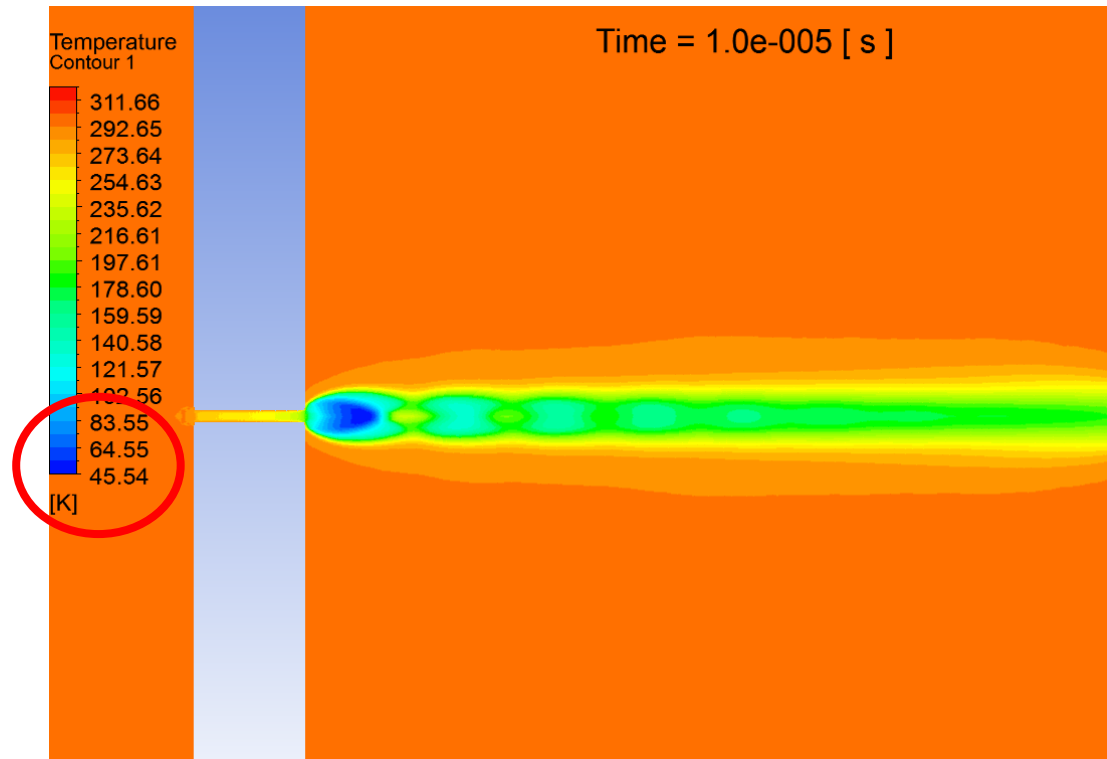
# Gas temperature after expansion

SG

$T_{in} = 20^{\circ}\text{C}$

$P_{in} = 10 \text{ bar}$

$P_{out} = 1.0 \text{ mbar}$

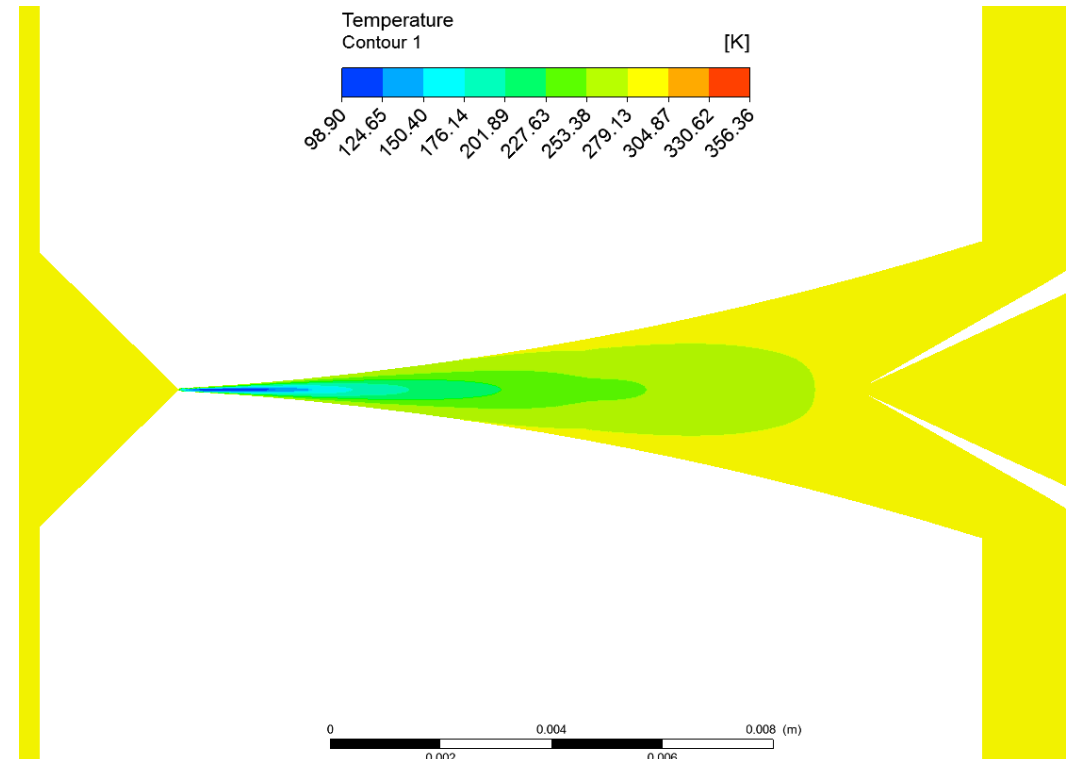


DL

$T_{in} = 20^{\circ}\text{C}$

$P_{in} = 3 \text{ bar}$

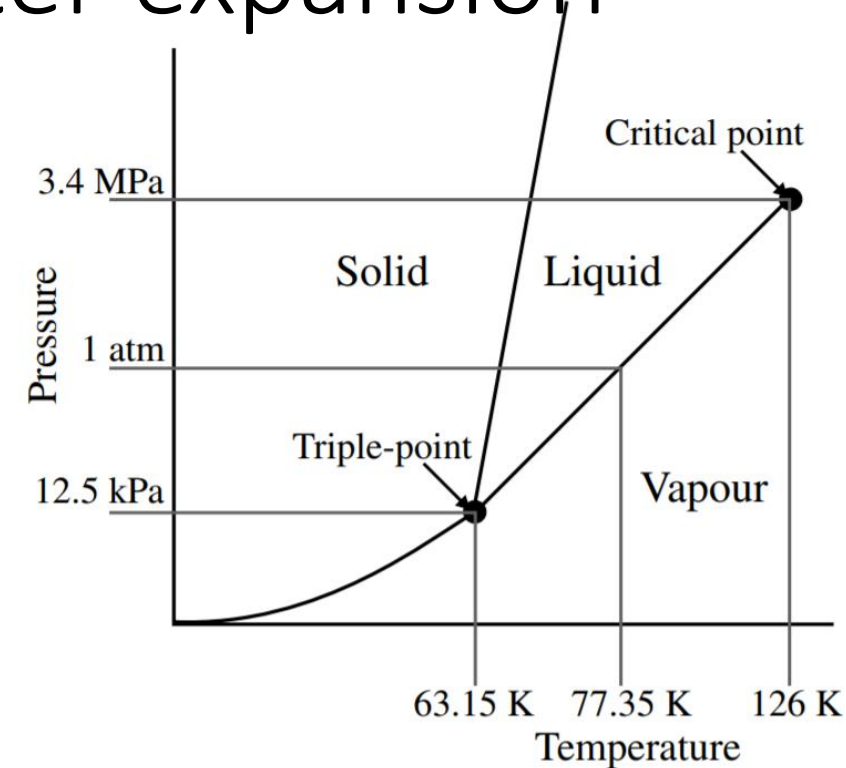
$P_{out} = 0 \text{ Pa}$





# Gas temperature and pressure after expansion

- After expansion of a gas is possible to reach the cryogenic temperature of the medium
- It could be dangerous in order to:
  - reach a liquid or solid state at the end of expansion
  - simulation results obtained for a single phase medium will be wrong



	$T_{\text{liquid @ 1bar}}$	$T @ \text{triple-point}$	$p @ \text{triple-point}$
Nitrogen	77.35 K	63.15 K	12.50 kPa
Argon	87.30 K	83.81 K	68.89 kPa
Neon	27.10 K	24.56 K	43.37 kPa

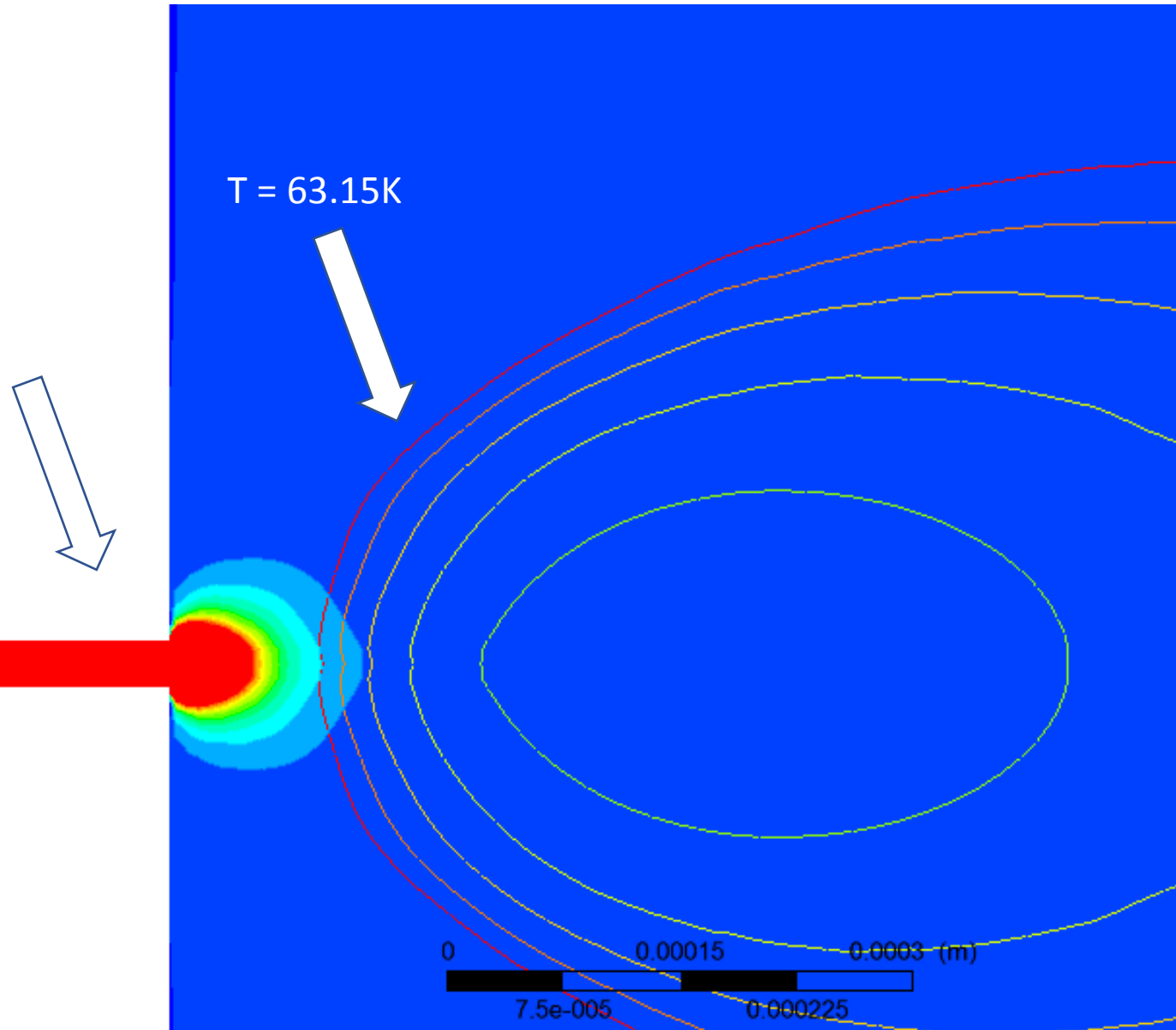
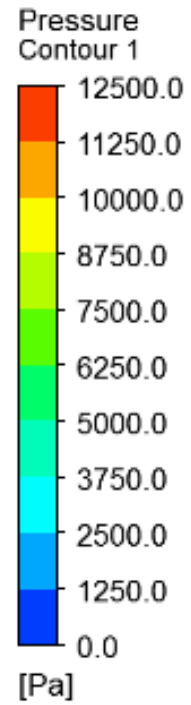
SG

$T_{in} = 20^{\circ}\text{C}$

$P_{in} = 10 \text{ bar}$

$P_{out} = 1.0 \text{ mbar}$

Steady-state simulation



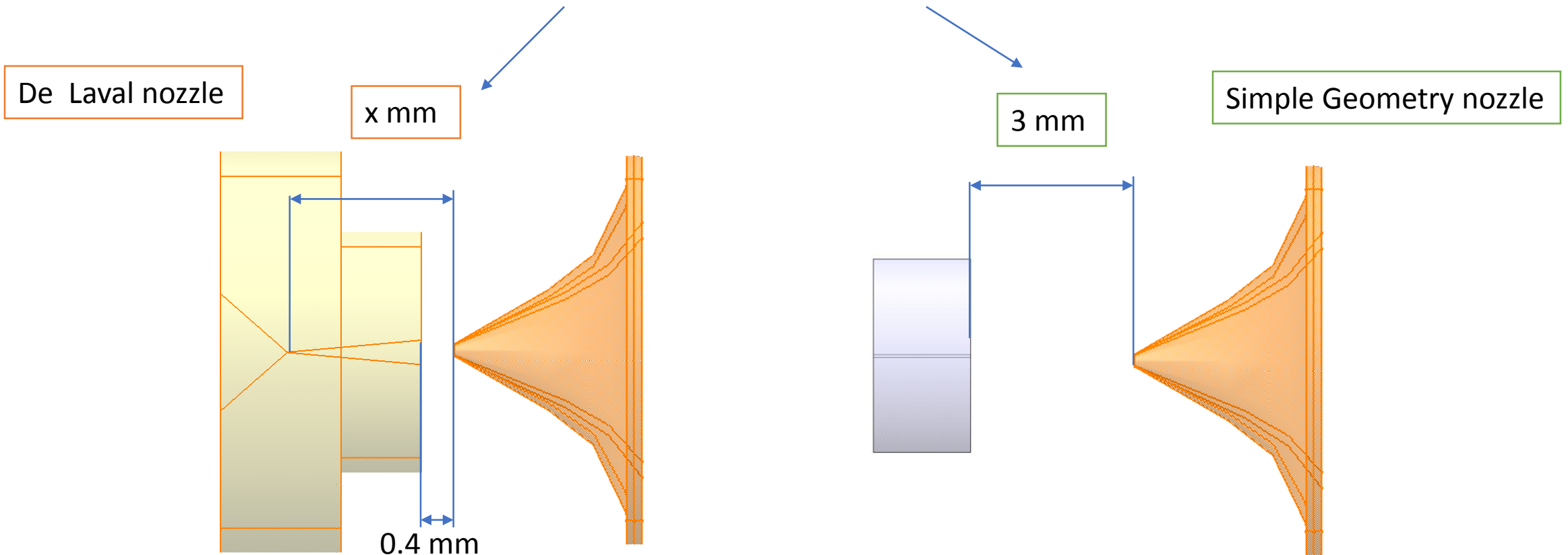
Gas: Nitrogen

Nozzle throat  $30\mu\text{m}$

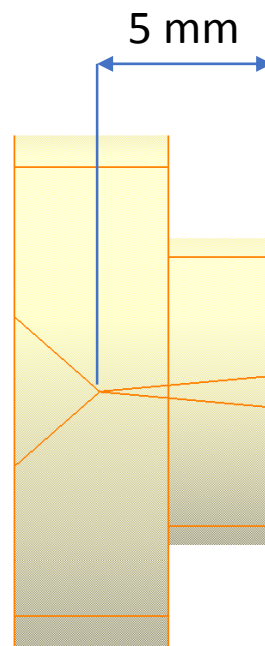
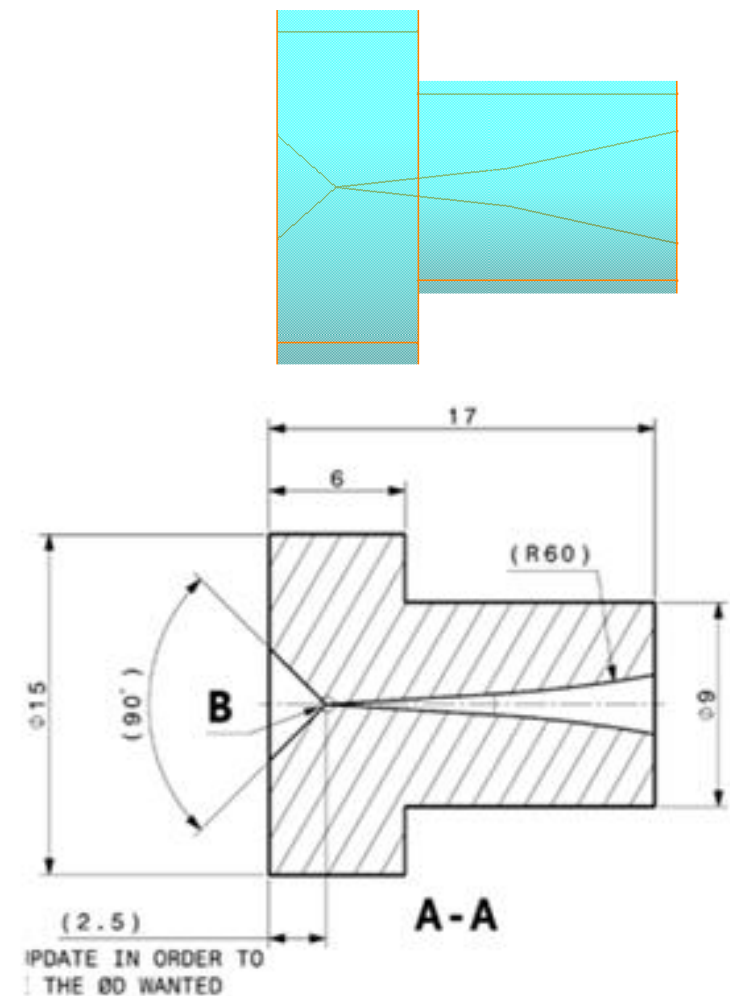
# Nozzle optimization

## Comparison criteria

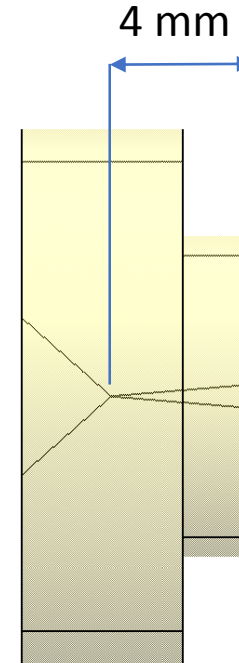
- For the comparison of the both nozzle constructions was chosen the distance between critical nozzle diameter and 1st skimmer inlet



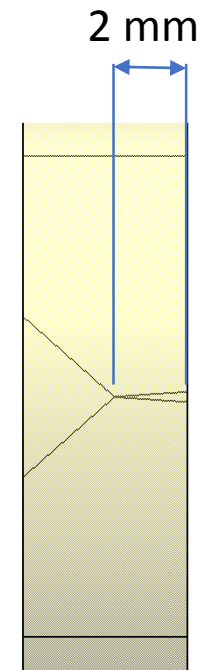
# Modification of the nozzle shape – divergent part of the nozzle



L5mm



L4mm

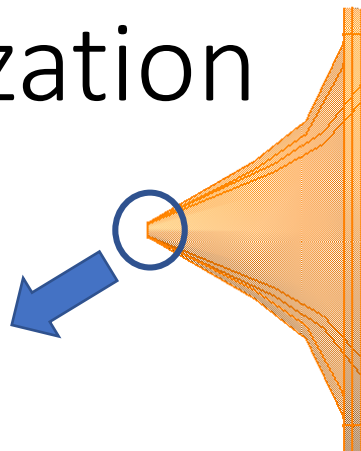


L2mm

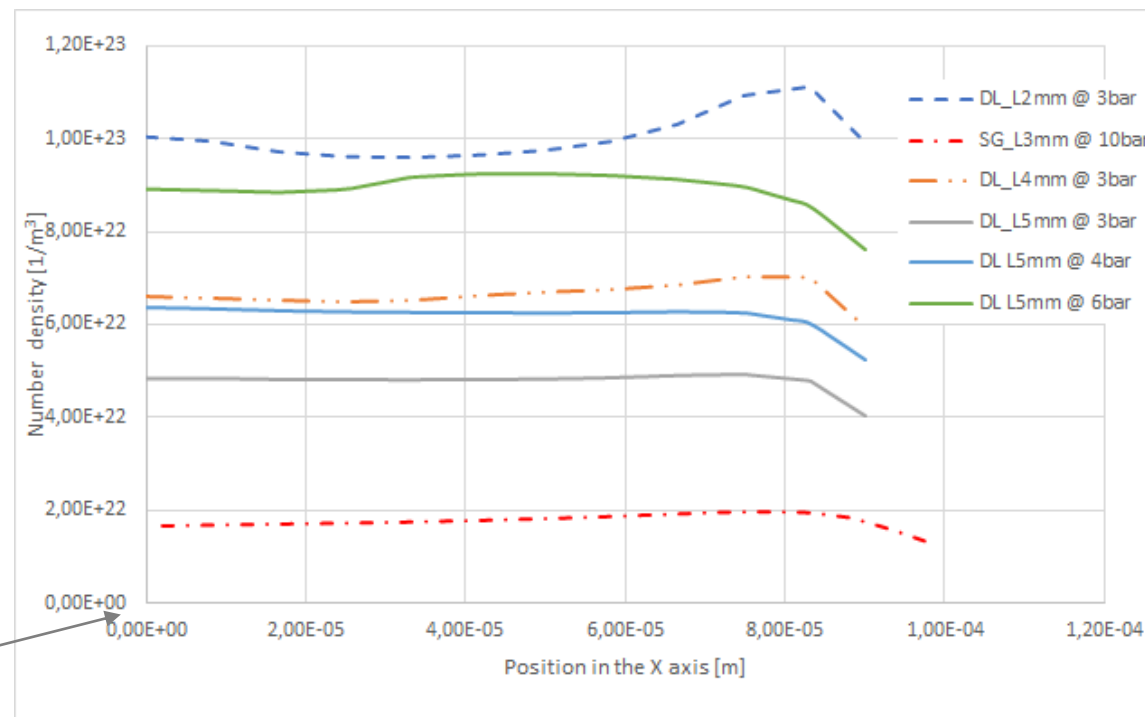
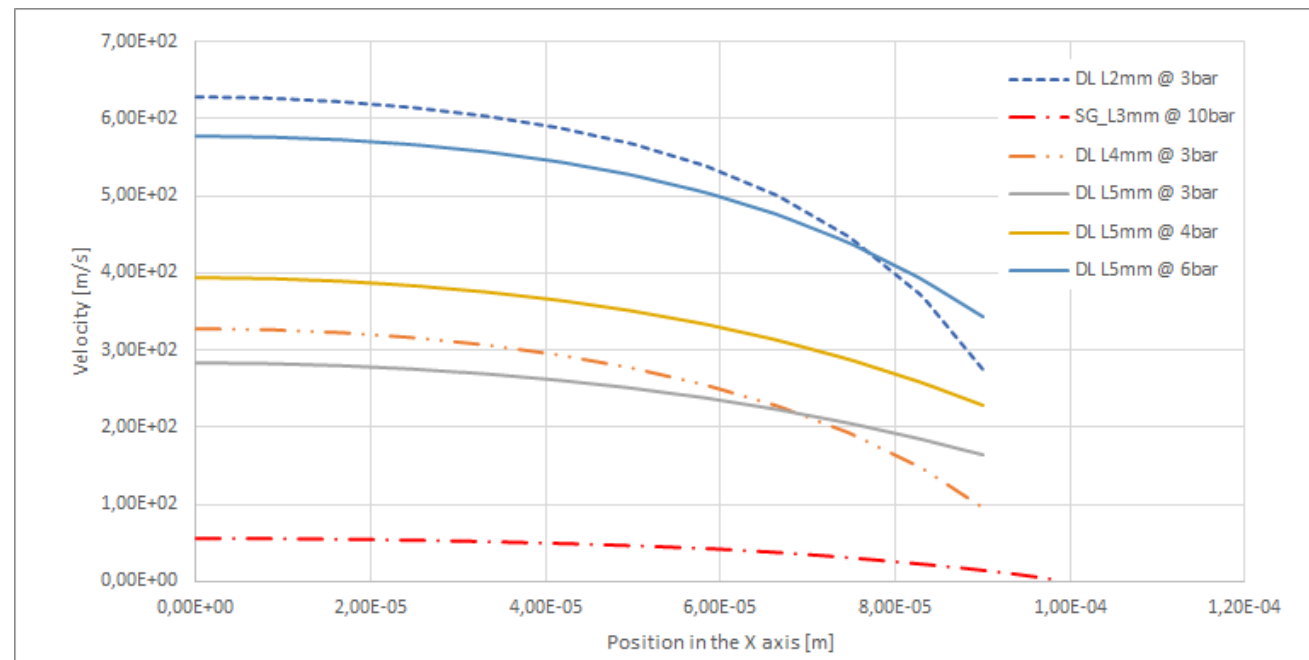
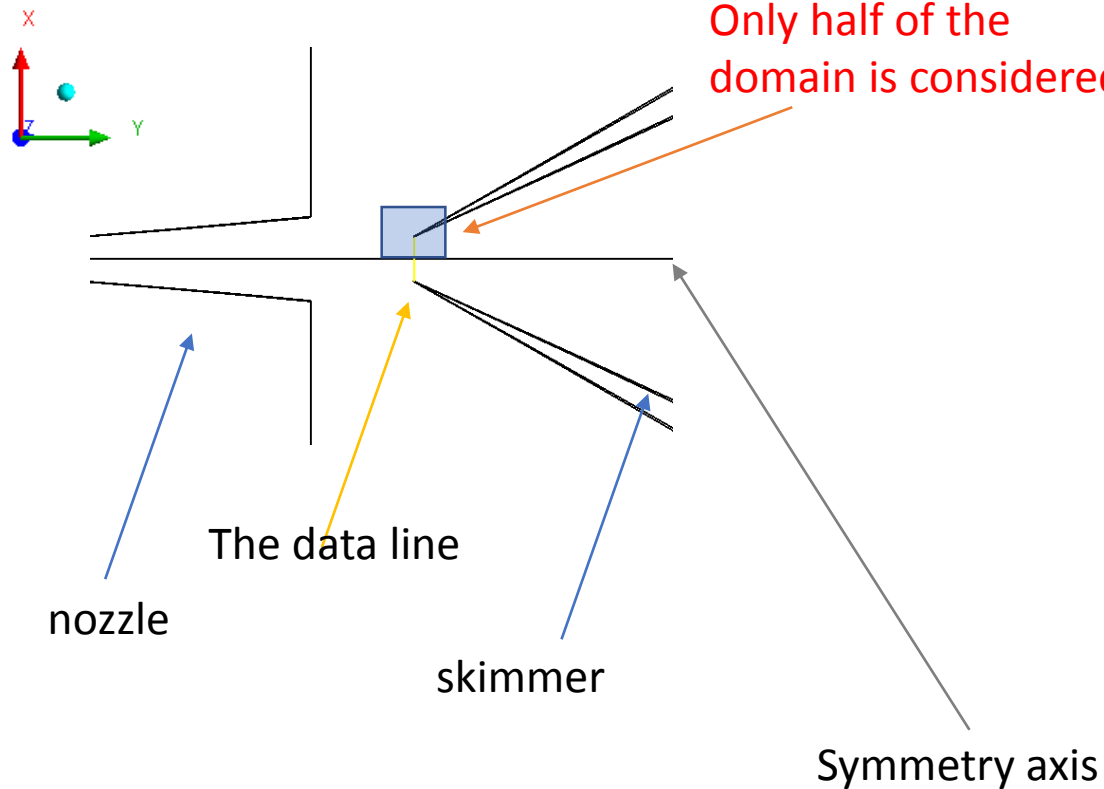
# Nozzle optimization

Gas: Nitrogen

Nozzle throat  $30\mu\text{m}$



Only half of the domain is considered

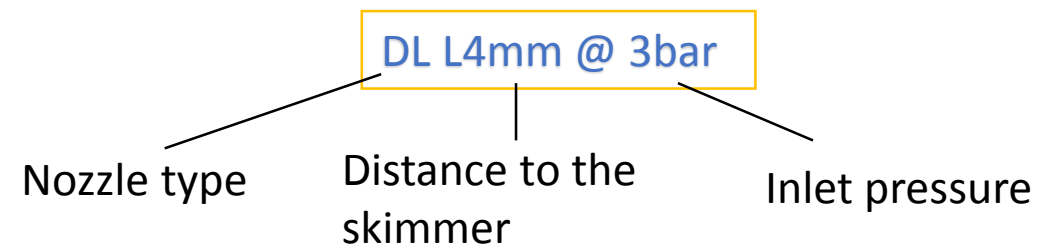
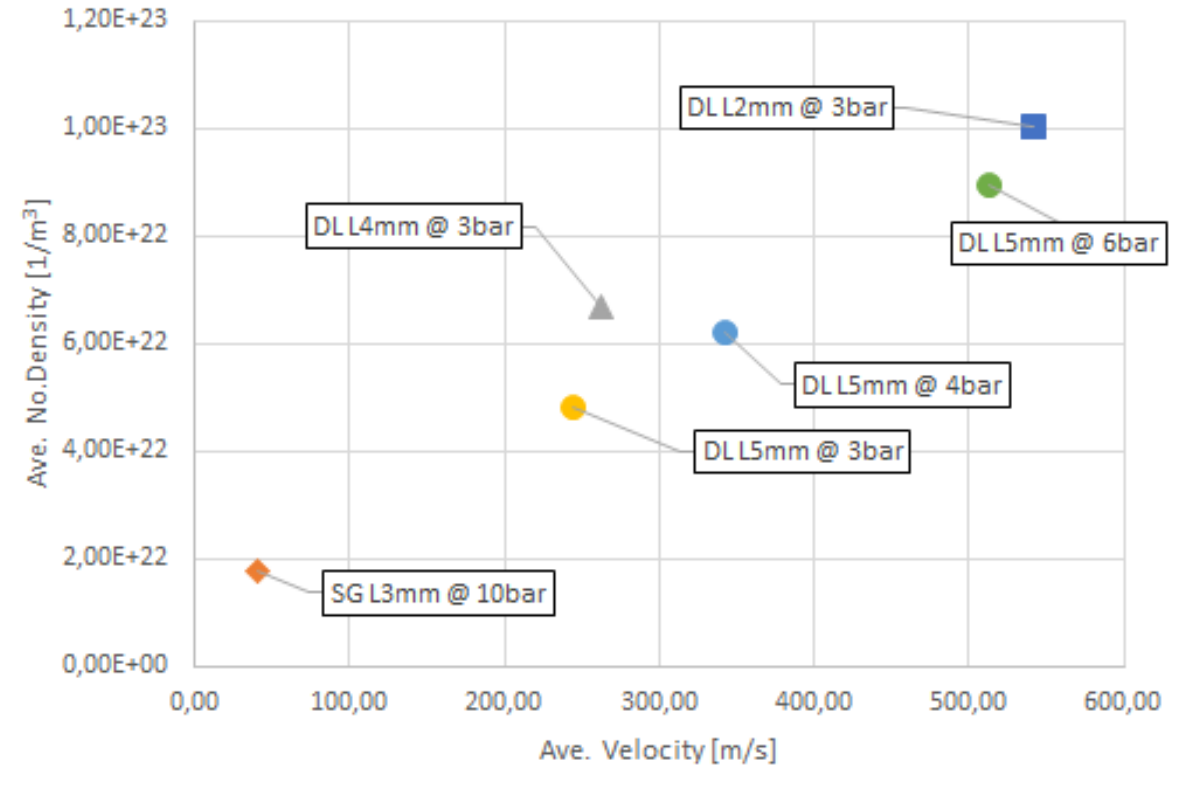


# Nozzle optimization

- By extending the numerical simulation procedure it is possible to obtain an optimal solution for given requirements
- To perform the next step of the simulation, the boundary conditions need to be set up (minimal/maximal density level at skimmer inlet or velocity value)

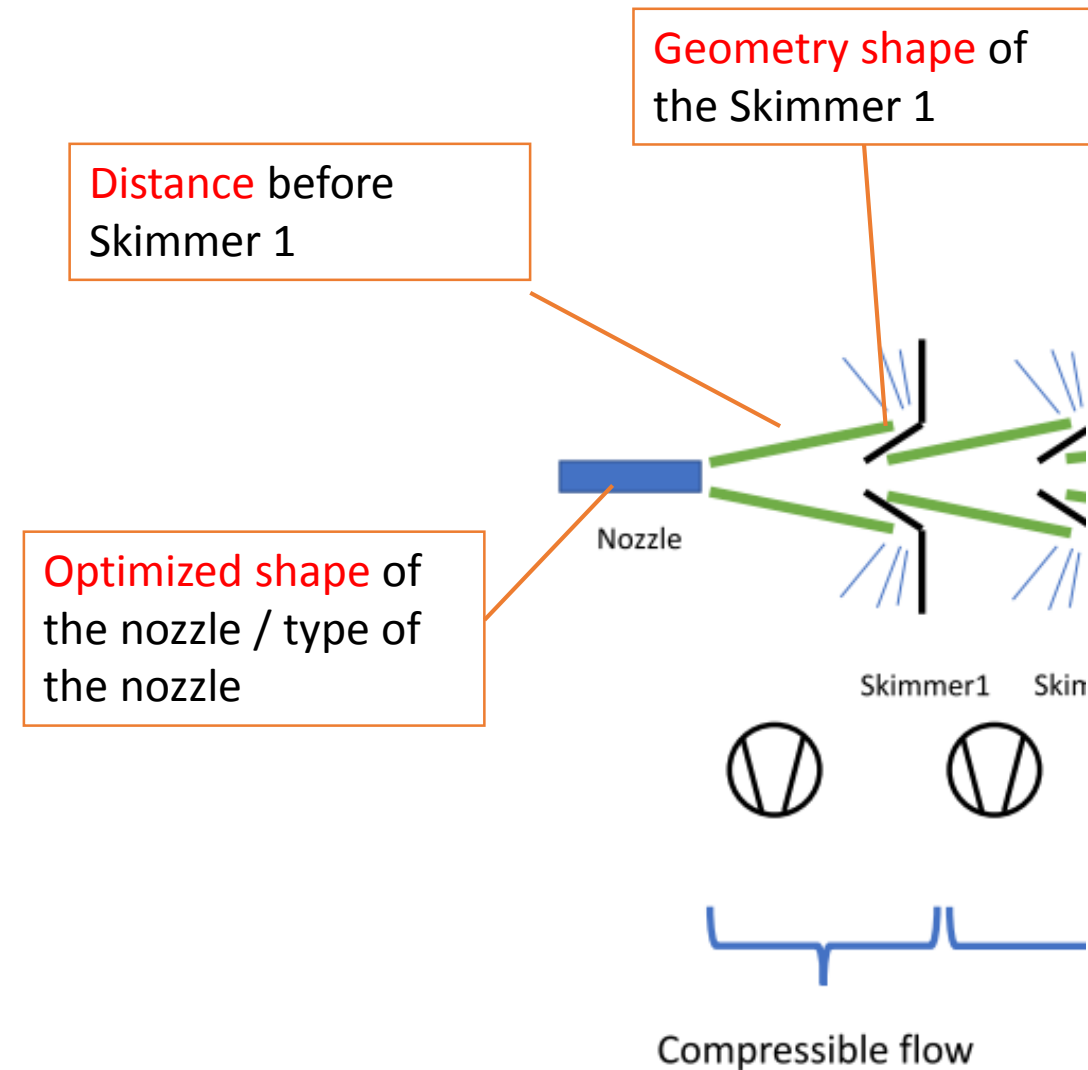
Gas: Nitrogen

Nozzle throat 30 $\mu$ m



# Next steps

- Influence of the Skimmer wall thickness on overall nozzle performance.
- Shape modification in order to increase the density of the gas at the Skimmer inlet.
- Simulations for different gas mediums (Argon, Neon...)
- Optimization of major dimensions in order to get high speed, uniform, dense gas jet at the Skimmer together with reduction of mass stream at the nozzle outlet
- Reduction of the mass stream to meet the requirements of the project -> pulsating gas stream formation ?



# Concluions

- Numerical simulations for HP side show that higher densities and velocities at the first skimmer inlet are possible to obtain by convergent-divergent, de Laval nozzle
- Optimization of the high pressure side could be performed in various options in case of using DL
- Parameters at a nozzle have to be controlled in order to avoid liquefaction or solidification of the jet medium



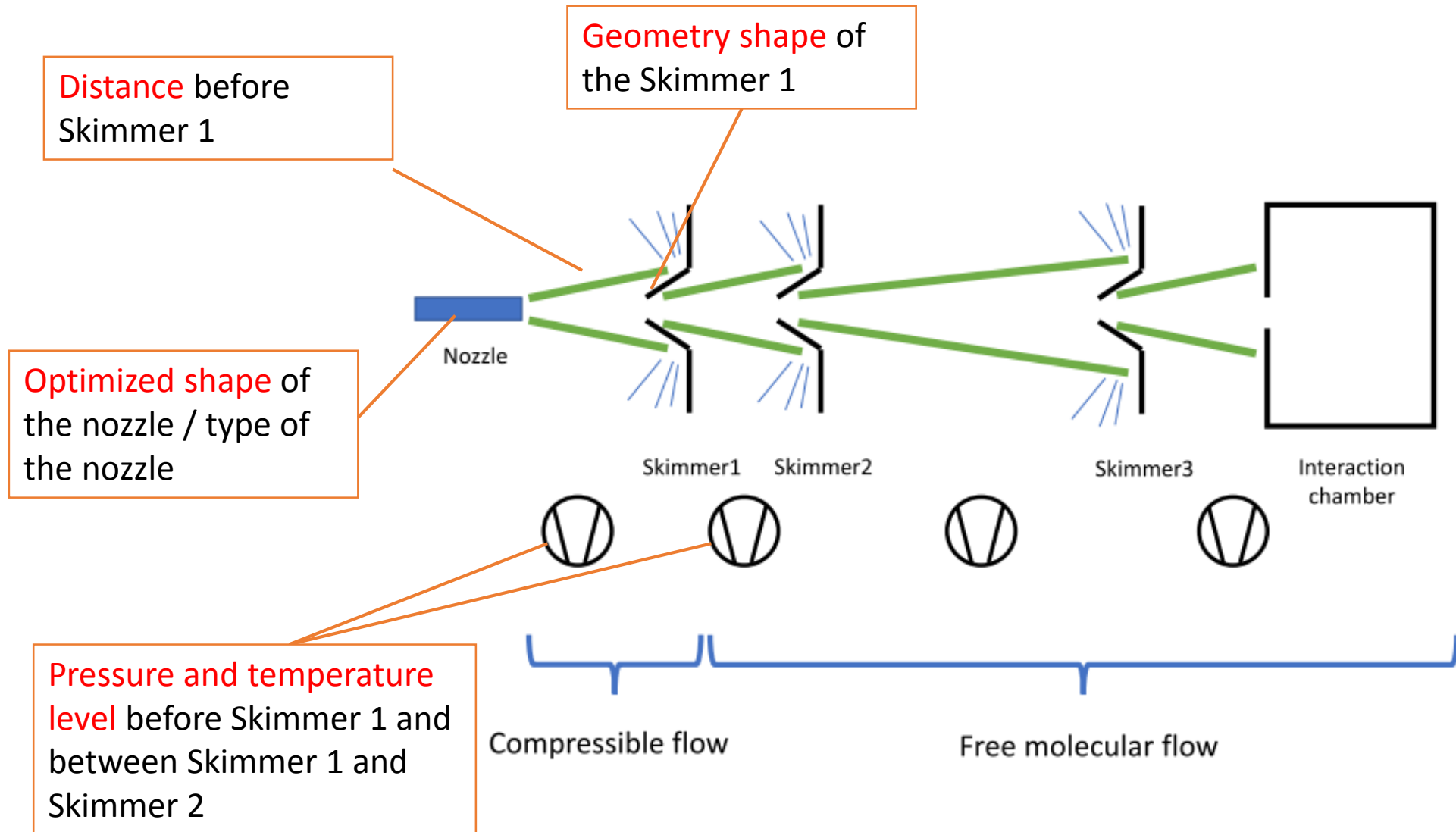


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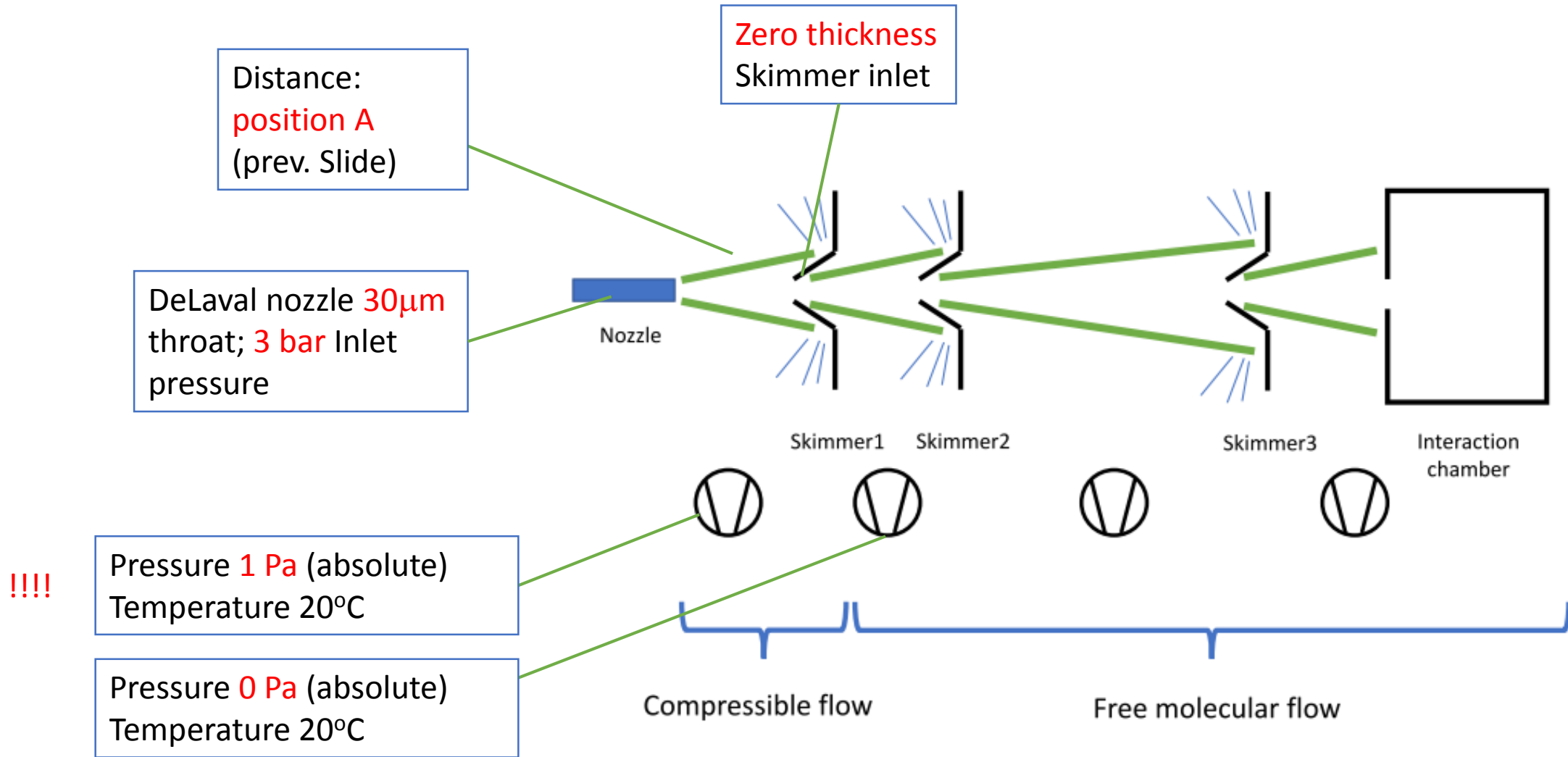
Thank you for your attention

# Still to consider in HP side ...



# Bounadry conditions

Gas: Nitrogen



# T-s diagram for nitrogen

