



Proton EDM hardware challenges

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with valuable input from M. Atanasov, M. Barnes, C. Carli, L. Jorat, M. Lamont, A. Prost, V. Senaj, N. Voumard

Outline

- Baseline lattice
- Bends
- Quadrupoles
- Injection devices, septa and fast deflectors
- Conclusion

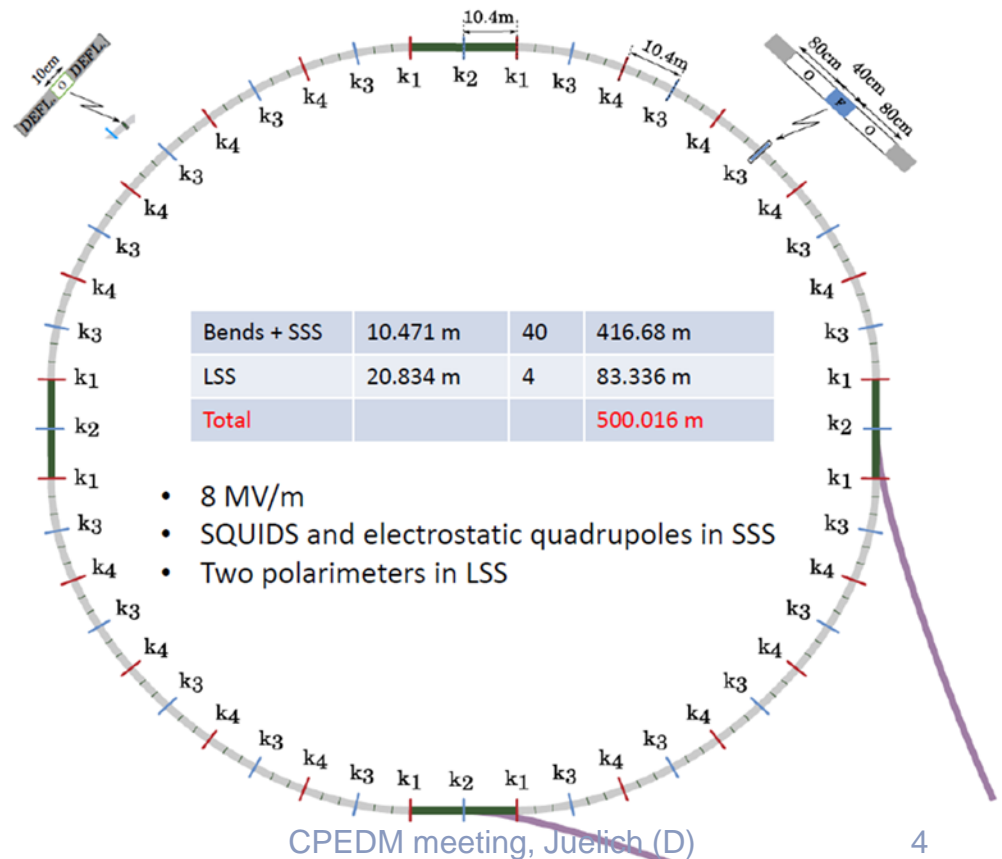
Baseline lattice

Arc cell

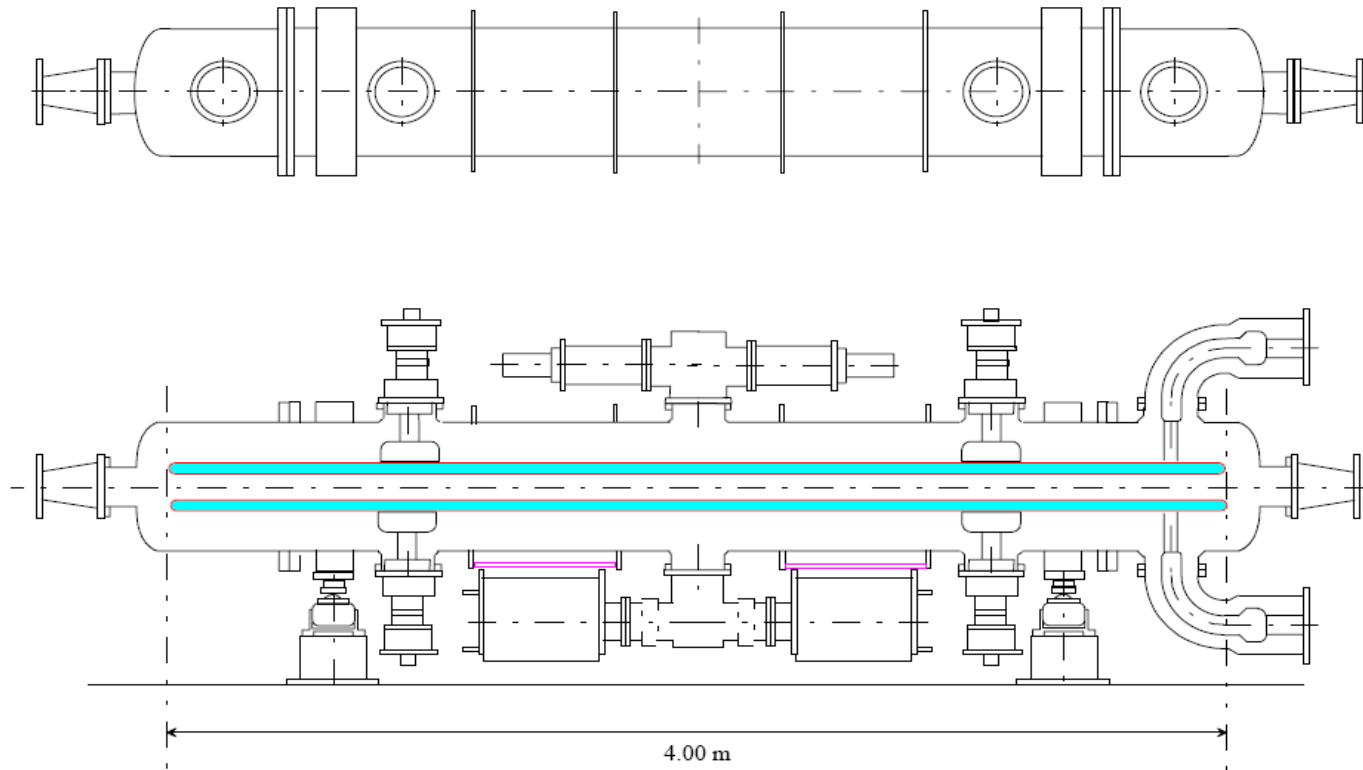
- Drifts before and after bend 0.8 m (used for experiments and/or correctors/skew quad/sextupole/BPM)
- 2 bends of 4.16 m
- Drift between bends 0.1 m
- Quad 0.4 m
- Total cell length: 10.417 m

Beam

- Protons
- 700.74 MeV/c
- 232.8 MeV



Physical length vs Effective length

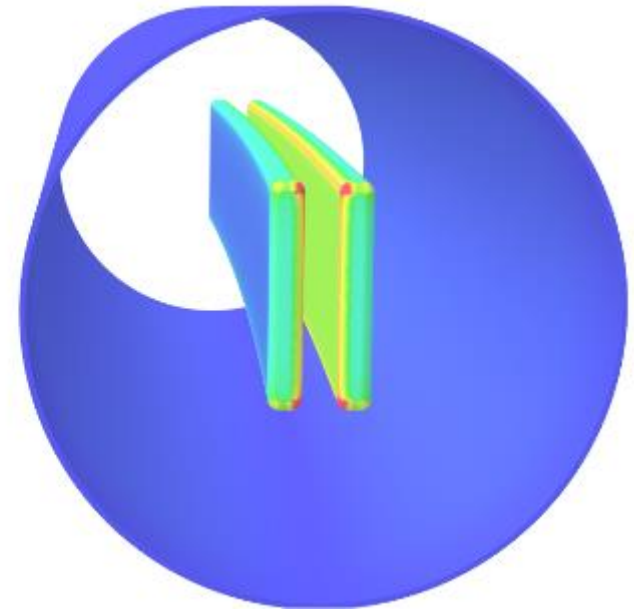
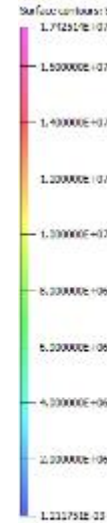


- SPS ZS septa: 3000 mm active length and 3378 mm device length; spacing > 870 mm
- LEP ZL: 4000 mm active length; 4500 mm device length; spacing > 650 mm

Note: Additional space would be needed for vacuum valves in case plug-in systems would be adopted to reduce down time in case of exchange due to failure

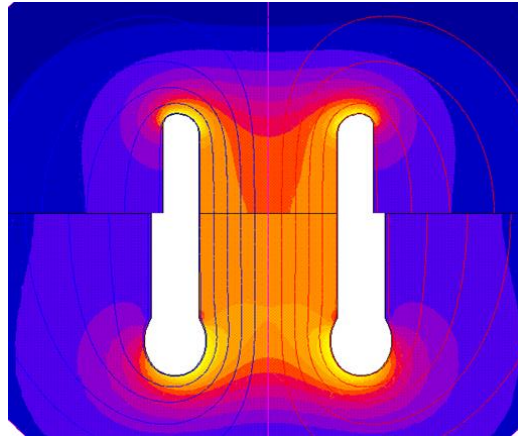
Bend requirements

- Total number of bends: 80
- L_{physical} : 4.1585 m
- L_{eff} : 3.7985 m
- Gap width: 30 mm
- Deflection angle: 78.54 mrad
- E_{gap} : 8.655 MV/m
- $V_{\text{per polarity}}$: ± 130 kV
- Electrode height: 200 mm [1]
- Cylindrical electrodes [1]
- Vacuum: 10^{-11} mbar [1]
- Field homogeneity: 1 ppm on $\text{Ø}20$ mm [2]
- Power supply stability $< 1 \cdot 10^{-4}$ [2]
- Magnetic leak field: $< 10^{-11}$ T [3]



Bend challenges

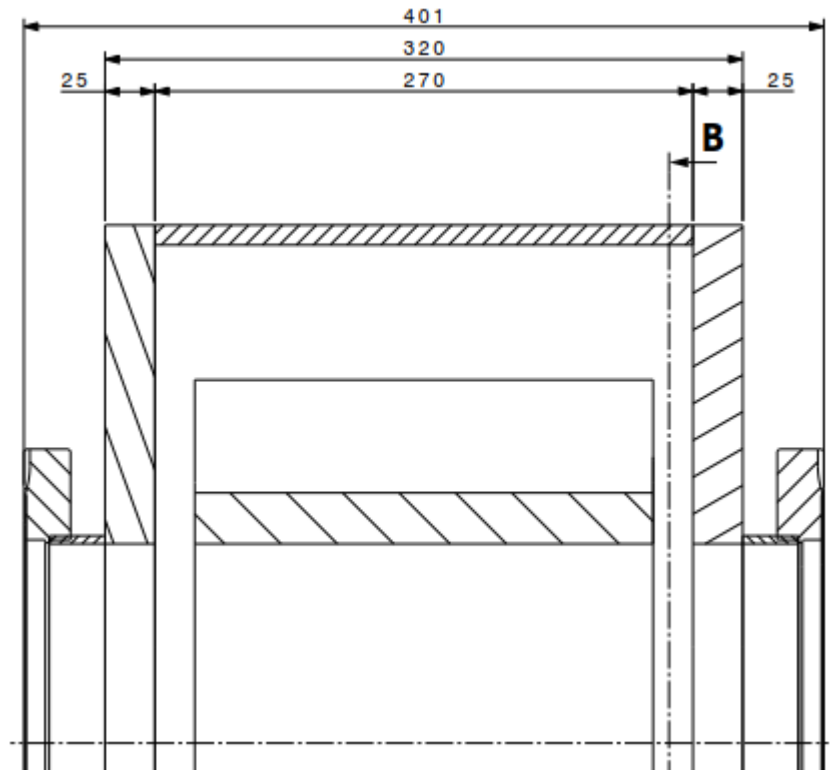
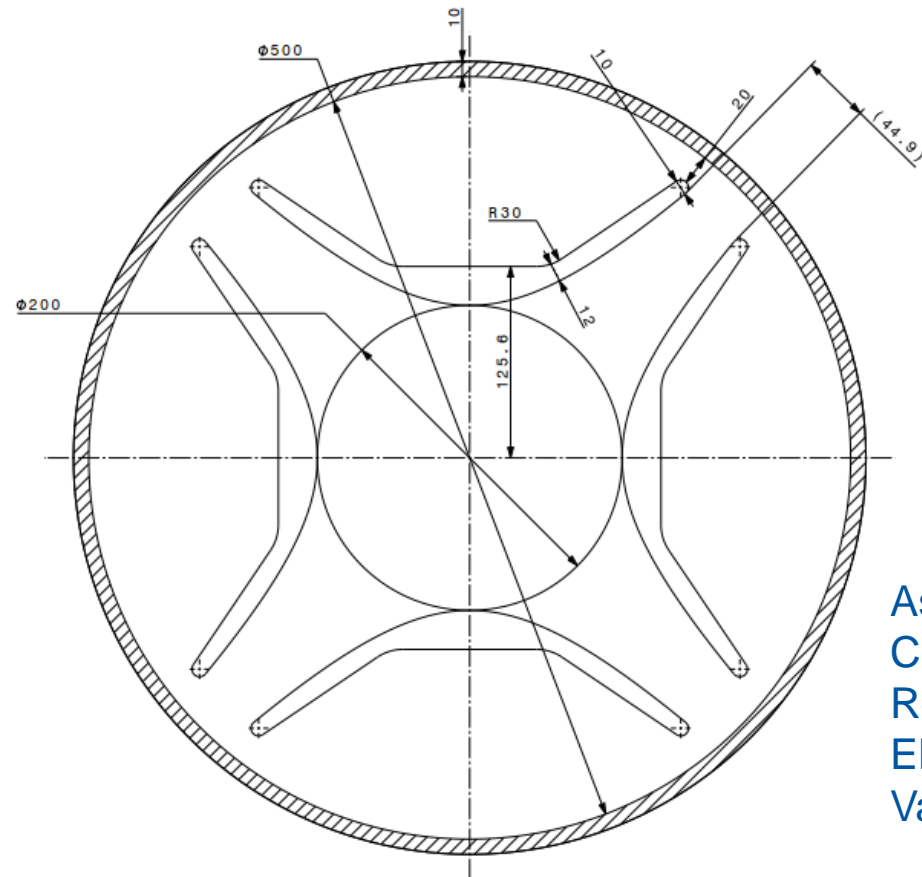
- Feasibility of 1 ppm field homogeneity tbc.
- Electrode profile needed to achieve required homogeneity causes higher fields on electrodes → need to reduce the average field assumed for the beam.
- E field high for use of Ti. Alternatives (TiN coated Al)?



Bend challenges

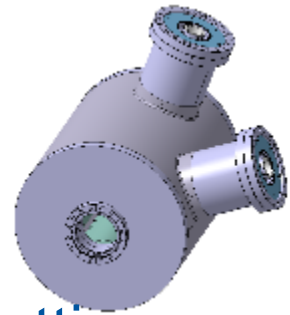
- Non // plates induce skew quadrupolar effect → need to estimate achievable **electrode precision** to estimate requirements for skew quads in lattice.
- Does magnetic leak field requirement exclude **use of stainless steel**?
- To study if Al or Ti qualify as alternative construction materials.
- Assume bends at room temperature: **bake out** needed to obtain required vacuum.
- Assume all bends powered in // to reduce systematics, **HV conditioning** prior to operation needs to be studied.

0.4 m Quad



Assuming purely hyperbolic electrodes $x^2 - y^2 = \pm R$
Central radius $R = 100\text{mm}$
Rounded edges with $r = 5\text{mm}$
Electrode length $l = 230\text{mm}$, flange-to flange 401mm
Vacuum tank $ID = 500\text{mm}$

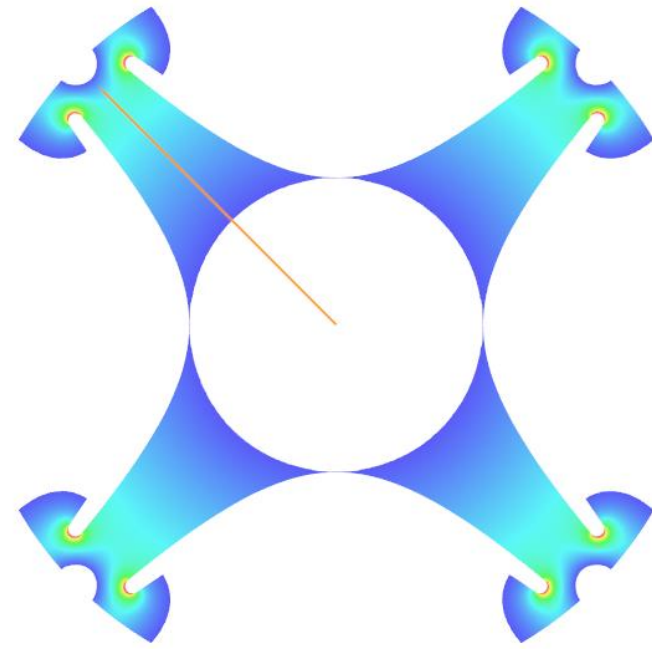
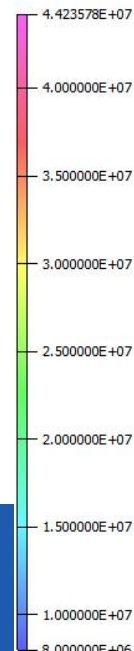
Quadrupoles



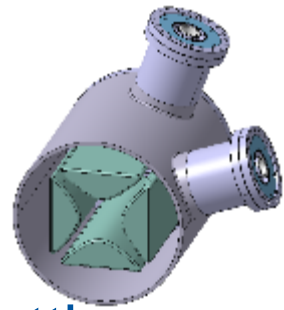
Field strength depends on strong or weak focussing lattice.

- Aperture (w x h): 30 x 200 mm²
- $k = 50 \text{ MV/m}^2$ (strong focussing), assuming $L_{\text{eff}} = 0.4 \text{ m}$
- $L_{\text{ph}} = 400 \text{ mm} \rightarrow \underline{L_{\text{eff}} = 246 \text{ mm}} \rightarrow k = 81 \text{ MV/m}^2$
- Knowing that $U = \pm \frac{1}{2} k R^2 \rightarrow \underline{U = \pm 404 \text{ kV}}$
- $E_{\text{pole-tip}}: 8.1 \text{ MV/m}$
- $E_{\text{pole-wings}}: >20 \text{ MV/m}$

Surface contours: E



Quadrupoles



Field strength depends on strong or weak focussing lattice.

- Aperture (w x h): 30 x 200 mm²
 - $k = 50 \text{ MV/m}^2$ (strong focussing), assuming $L_{\text{eff}} = 0.4 \text{ m}$
 - $L_{\text{ph}} = 400 \text{ mm} \rightarrow \underline{L_{\text{eff}} = 246 \text{ mm}} \rightarrow k = 81 \text{ MV/m}^2$
 - Knowing that $U = \pm \frac{1}{2} k R^2 \rightarrow U = \pm 405 \text{ kV}$
- a. $\underline{U \leq \pm 100 \text{ kV} + R = 0.1 \text{ m}} \rightarrow k < 20 \text{ MV/m}^2$, $E_{\text{pole}} = 2 \text{ MV/m}$
- b. $\underline{L_{\text{ph}} = 0.8 \text{ m}} \rightarrow L_{\text{eff}} = 646 \text{ mm} \rightarrow k = 30.8 \text{ MV/m}^2$, $E_{\text{pole}} = 3.1 \text{ MV/m}$,
 $U = \pm 154 \text{ kV}$
- c. $\underline{U = 100 \text{ kV}, k = 81 \text{ MV/m}^2, L_{\text{ph}} = 0.4 \text{ m}} \rightarrow R = 50 \text{ mm}$, $E_{\text{pole}} = 4.1 \text{ MV/m}$

Quad challenges

- **Field homogeneity** dominated by end fields. Could be mitigated to some extent [4]. Need to determine minimum quad length that can achieve requirements
- **HV feedthrough integration** challenging for short quads.
- **Alignment precision** tbd, but assumed to be critical.
- Cryo quad makes alignment/**positioning** more complex, but **industrial solutions** may exist [5], using flexure guides and piezo actuators.
- Main quads to be powered in **4 families**; conditioning to be studied.

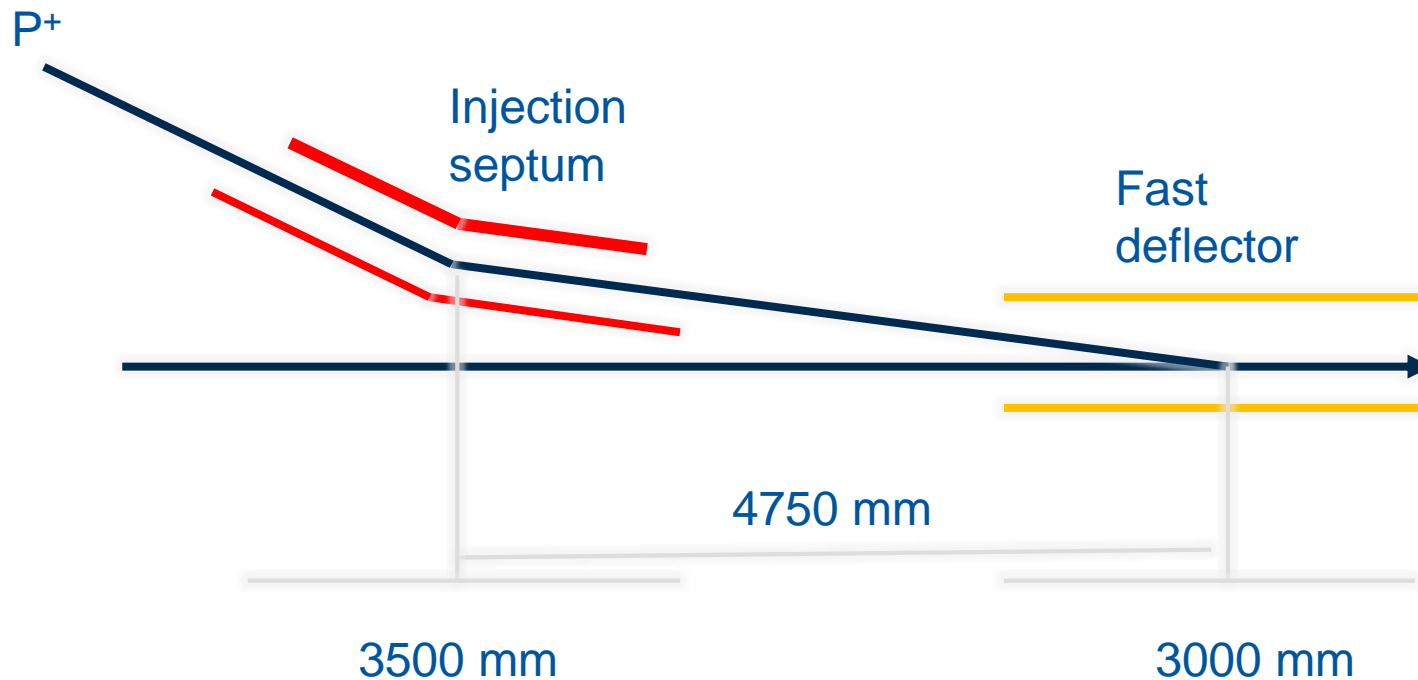


Courtesy WWW.JPE.NL



Injection straights

- Uses most of LSS



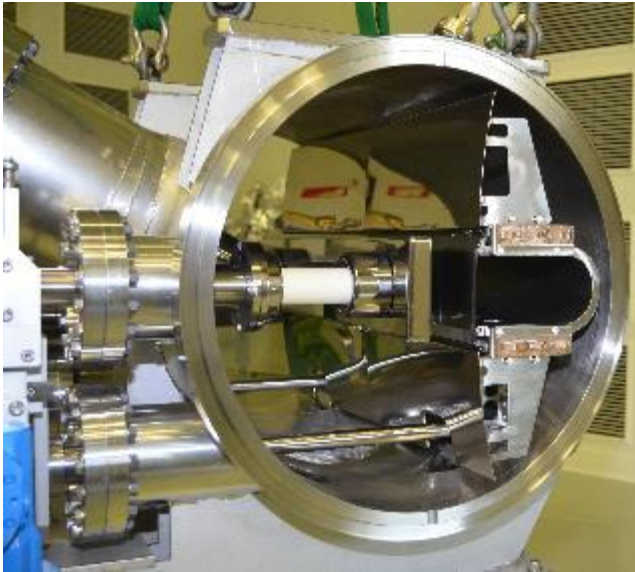
Injection devices

	Injection septum	Fast deflector
L_{physical} [m]	3.5	3.0
Active length [m]	3.0	2.5
Deflection angle [mrad]	57.34	10
Gap width [mm]	30*	42.5**
Field [MV/m]	8.0	1.674
Radius of curvature electrodes [m]	52.32	-
Nominal electrode voltage [kV]	- 240	± 35.6
T_{rise} and T_{fall} (2‰ - 998‰) [μs]	DC	1.0
Capacitance per electrode (to gnd) [pF]	~ 660	< 500

* Assuming curved or segmented septum and electrode

** Assuming parallel electrodes

Segmented septum, fast deflector examples



Segmented septum MedAustron



Fast deflector at CERN in ELENA

Open issues injection devices

Segmented foil septum v.s. curved wire septum

Feasibility of Fast Deflector pulse generator:

- rise and fall time feasibility to be validated
- voltage switch: not easily done using off the shelf switches (for example Behlke refreshes their switches at regular intervals even when switched off, and the electrodes wouldn't remain grounded).
- Switches need to be located close to fast deflectors (0.5 m). Feasibility and reliability in the radiation to be studied.
- HV feedthroughs need development, not commercially available.

Alternative: stripline kicker(s)

- replacing fast deflector would reduce voltages to 30 kV (-20%) on plates, but at cost of added complexity.
- replacing the septum with a stripline kicker is not feasible.

Conclusion

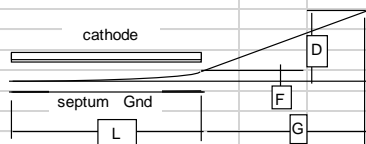
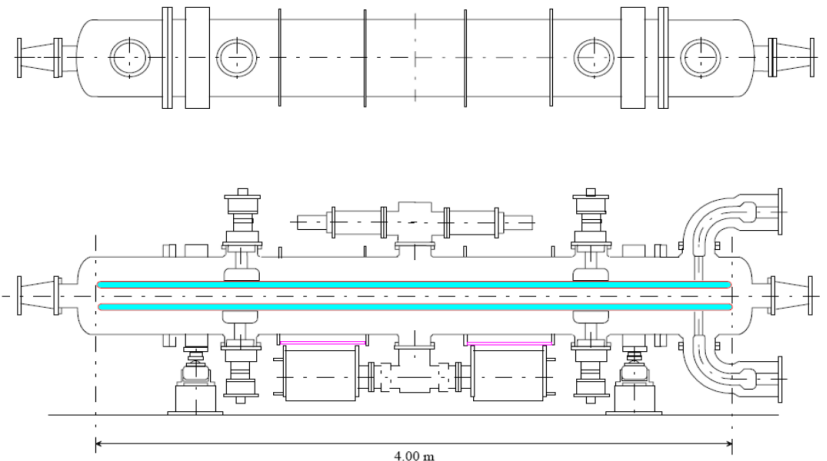
- ✓ Electrode material will determine max. field strength, hence size of elements.
- ✓ Quad field strength to be quantified and feasibility of precision requirement to be determined.
- ✓ Lattice needs updating with:
 - Longer quads
 - Skew quads
 - Trim quads
 - Sextupoles
 - Vertical correctors
 - Present circumference seems optimistic
- ✓ Conditioning strategy for quads and bends to be studied.
- ✓ Injection equipment feasible in principle.
 - Fast deflector rise and fall time requirement to be validated.
- ✓ Use of stainless steel for construction desirable, but compatibility with magnetic leak field requirements tbc.

References

1. M. Lamont, “EDM storage ring – siting at CERN”, CERN EDM WG meeting, 1 June 2017
2. Y. Semertzidis, “All-electric versus combined field storage ring”, EDM kick-off meeting, CERN, 13-14 March 2017
3. Reference to leak field level
4. R. Baartman, “Quadrupole shapes”, Phys. Rev. ST – Accel. Beams 15, 074002 (2012)
5. www.janssenprecisionengineering.com

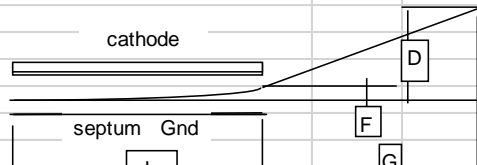
Back-up slides

Bend

EDM Bend			ZL active length 4000 mm; device length 4500 mm.		
particularités					
DONNEES			RESULTATS		PROTONS
particules			Masse au repos	mi	0.93826 GeV/c ²
type: electrons: e protons: p ions: i			Energie cinétique	0.2328	GeV
quant.mouv: MV Energie cin: EC			Quantité de mouvement	0.7007	GeV/c
Rigidité fais. BR			charge	1.00000	e
Quantité de mouvement p =			beta	0.5984	
	0.7007	GeV/c	gamma	1.2481	
			beta*gamma	0.7469	
Déflexion requise			Brho	2.3374	T m
	78.54	mrad	Champ Electrique	8.670	MV/m
Gap entre électrodes			Tension entre électrodes	260.1	kV
longueur active du seperateur			Voltage per polarity	130.0	kV
Espace de glissement			Déplacement à la sortie du septum	149.17	mm
	0	mm	Déplac.après espace de glissement	149.17	mm
			E. dl	32.933	MV
			radius of curvatur electrodes	48.36	m
			longueur septum L	3798.5	mm
			Espace de glissement G	0	mm
			Déflexion sortie septum F	149.1667462	mm
			Déflexion après espace de glissement D	149.1667462	mm
					

Fast deflector

EDM Fast deflector						
particularités						
DONNEES			RESULTATS		PROTONS	
particules			Masse au repos	mi	0.93826	GeV/c ²
type: electrons: e protons: p ions: i		p	Energie cinétique		0.2328	GeV
quant.mouv: MV Energie cin: EC		mv	Quantité de mouvement		0.7007	GeV/c
Rigidité fais. BR			charge		1.00000	e
Quantité de mouvement p =	0.7007	GeV/c	beta		0.5984	
			gamma		1.2481	
			beta*gamma		0.7469	
Déflexion requise	10	mrاد	Brho		2.3374	T m
Gap entre électrodes	42.5	mm	Champ Electrique		1.677	MV/m
longueur active du seperateur	2500	mm	Tension entre électrodes		71.3	kV
Espace de glissement	0	mm	Voltage per polarity		35.6	kV
T _{rise} and T _{fall} (2‰ - 998‰)	1.0	µs	Déplacement à la sortie du septum	12.5	mm	<i>angle defl * long / 2</i>
eletrode height	100	mm	Déplac.après espace de glissement	12.5	mm	<i>angle defl * (long / 2 + gliss)</i>
			E.dI	4.193	MV	
			Capacitance per electrode	5.56E-10	F	
			longueur septum L	2500	mm	
			Espace de glissement G	0	mm	
			Déflexion sortie septum F	12.5	mm	
			Déflexion après espace de glissement D	12.5	mm	



Electrostatic injection septum

EDM Injection Septum						
Curved/segmented septum and electrode						
particularités						
DONNEES		RESULTATS		PROTONS		
particules				Masse au repos m_i	0.93826	GeV/c ²
type: electrons: e protons: p ions: i	p	Energie cinétique		0.2328	GeV	
quant.mouv: MV Energie cin: EC	mv	Quantité de mouvement		0.7007	GeV/c	
Rigidité fais. BR		charge		1.00000	e	
Quantité de mouvement $p =$	0.7007	beta		0.5984		
		gamma		1.2481		
		beta*gamma		0.7469		
Déflexion requise	57.34	mrad	Brho	2.3374	T m	
Gap entre électrodes	30	mm	Champ Electrique	8.014	MV/m	
longueur active du septum	3000	mm	Tension entre électrodes	240.4	kV	
Espace de glissement	0	mm	Déplacement à la sortie du septum	86.01	mm	
electrode height	100	mm	Déplac.après espace de glissement	86.01	mm	
			E.dl	24.043	MV	
			radius of curvature electrodes	52.32	m	
			Capacitance per electrode	6.655E-10	F	
			longueur septum L	3000	mm	
			Espace de glissement G	0	mm	
			Déflexion sortie septum F	86.01	mm	
			Déflexion après espace de glissement D	86.01	mm	

