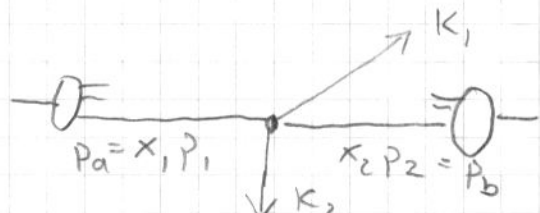


Collision Kinematics



Prob. system:

$$p_a = x_1 E(1, v, v, 1)$$

$$p_b = x_2 E(1, v, v, -1)$$

(beam along z-axis)

$$P_{cm} = p_a + p_b = E(x_1 + x_2, v, v, x_1 - x_2)$$

is boosted along z-axis by rapidity  $\gamma_{cm}$

$$\begin{aligned} \begin{pmatrix} E \\ P_z \end{pmatrix}_{cm} &= \begin{pmatrix} \gamma & \gamma\beta \\ \gamma\beta & \gamma \end{pmatrix} \begin{pmatrix} \sqrt{s}/2 \\ 0 \end{pmatrix} \\ &= \begin{pmatrix} \cosh \gamma_{cm} & \sinh \gamma_{cm} \\ \sinh \gamma_{cm} & \cosh \gamma_{cm} \end{pmatrix} \begin{pmatrix} \sqrt{s}/2 \\ 0 \end{pmatrix} \\ &= \exp \left\{ \begin{pmatrix} v & 1 \\ 1 & v \end{pmatrix} \gamma_{cm} \right\} \end{aligned}$$

↑ boost generator
↑ rapidity

$$\left[ \frac{E + P_z}{E - P_z} = \frac{\cosh + \sinh}{\cosh - \sinh} = \frac{e^{\gamma}}{e^{-\gamma}} \right]$$

$$\Rightarrow \gamma_{cm} = \frac{1}{2} \ln \left( \frac{E + P_z}{E - P_z} \right) = \frac{1}{2} \ln \frac{x_1}{x_2}$$

along z axis

Product of boosts: add rapidities!

Rapidity of general 4 vector  $k^\mu$

$$\gamma = \frac{1}{2} \ln \frac{k^0 + k_z}{k^0 - k_z}$$

Boost along z axis leaves transverse momentum invariant

$$k_z = 0: \quad K_0^M = (E_T, P_T \cos \varphi, P_T \sin \varphi, 0) \quad (3.2)$$

$$E_T = \sqrt{m^2 + P_T^2}$$

general  $k_z$ :

$$K^M = (E_T \cosh \eta, P_T \cos \varphi, P_T \sin \varphi, E_T \sinh \eta)$$

$$= E (1, \beta \sin \theta \cos \varphi, \beta \sin \theta \sin \varphi, \beta \cos \theta)$$

rapidity

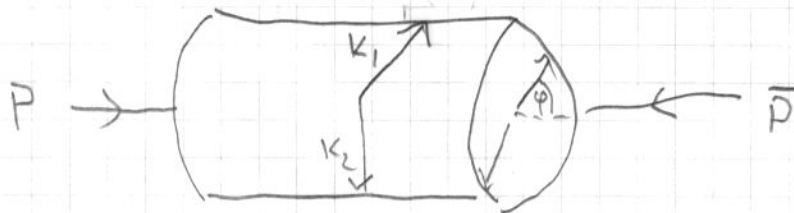
$$\eta \equiv \frac{1}{2} \ln \frac{1 + \cos \theta}{1 - \cos \theta}$$

massless case

$$\eta = \frac{1}{2} \ln \frac{k^+ + k_z}{k^+ - k_z} = \frac{1}{2} \ln \frac{E + E \cos \theta}{E - E \cos \theta} = \eta$$

- collider coordinates  $E_T$  (or  $P_T$ ),  $\varphi$  (or  $\eta$ ),  $\varphi$
- rapidity differences are boost invariant (boosts along z-axis)

Application: dijet production (massless jets)



$$P_a + P_b = K_1 + K_2$$

in lab:  $K_1^M = P_T (\cosh \eta_1, \cos \varphi, \sin \varphi, \sinh \eta_1)$

$$K_2^M = P_T (\cosh \eta_2, -\cos \varphi, -\sin \varphi, \sinh \eta_2)$$

cm frame

$$\eta_i \rightarrow \bar{\eta}_i \quad \eta_1 = \eta_{cm} + \bar{\eta}_1$$

$$\eta_2 = \eta_{cm} - \bar{\eta}_1$$

$$x_{1/2} = \frac{2P_T}{\sqrt{S}} \cosh \frac{\eta_1 - \eta_2}{2} e^{\pm \frac{1}{2}(\eta_1 + \eta_2)}$$

$$= \frac{P_T}{\sqrt{S}} \left( e^{\frac{\eta_1 - \eta_2}{2}} + e^{-\frac{\eta_1 + \eta_2}{2}} \right) e^{\pm \frac{\eta_1 + \eta_2}{2}}$$

$$\Rightarrow x_1 = \frac{P_T}{\sqrt{S}} \left( e^{\eta_1} + e^{\eta_2} \right)$$

$$x_2 = \frac{P_T}{\sqrt{S}} \left( e^{-\eta_2} + e^{-\eta_1} \right)$$

$$\Rightarrow \gamma_{cm} = \frac{1}{2} (\eta_1 + \eta_2)$$

$$\bar{\eta}_1 = \frac{1}{2} (\eta_1 - \eta_2) = \frac{1}{2} \ln \frac{1 + \cos \theta_{cm}}{1 - \cos \theta_{cm}}$$

→ c.m scattering angle

in c.m frame :  $\bar{k}_1^0 = \frac{\sqrt{s}}{2} = p_T \cosh \bar{\eta}_1$

$$\Rightarrow \hat{s} = 4 p_T^2 \cosh^2 \frac{\eta_1 - \eta_2}{2} = \underbrace{x_1 x_2}_z s$$

$$\gamma_{cm} = \frac{1}{2} \ln \frac{x_1}{x_2}$$

$x_1 = \sqrt{\tau} e^{\gamma_{cm}}$	$= \frac{p_T}{\sqrt{s}} (e^{\eta_1} + e^{\eta_2})$
$x_2 = \sqrt{\tau} e^{-\gamma_{cm}}$	$= \frac{p_T}{\sqrt{s}} (e^{-\eta_1} + e^{-\eta_2})$

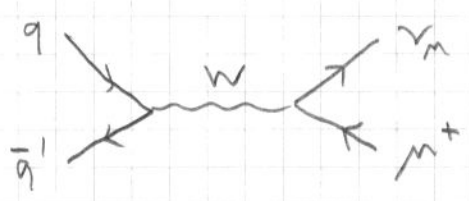
Note: in cross section formula integrate over  $x_1, x_2$

$$dx_1 dx_2 = \underbrace{\begin{vmatrix} \frac{\partial x_1}{\partial \tau} & \frac{\partial x_2}{\partial \tau} \\ \frac{\partial x_1}{\partial \gamma_{cm}} & \frac{\partial x_2}{\partial \gamma_{cm}} \end{vmatrix}}_{\begin{vmatrix} \frac{1}{2\sqrt{\tau}} e^{\gamma} & \frac{1}{2\sqrt{\tau}} e^{-\gamma} \\ \sqrt{\tau} e^{\gamma} & -\sqrt{\tau} e^{-\gamma} \end{vmatrix}} d\tau d\gamma_{cm} = d\tau d\gamma_{cm}$$

- determine  $x_1, x_2$  from final state
- determine  $f_{a/p}(x_1) f_{b/p}(x_2)$  from measured rate

W production

Consider  $w^+ \rightarrow \mu^+ \nu_\mu$  signal



$q\bar{q}' = u\bar{d}, u\bar{s}, c\bar{d}, c\bar{s}$

$\frac{d\hat{\sigma}}{d\cos\theta} \sim \sum |m|^2 \sim |V_{q\bar{q}'}|^2 \frac{1}{(\hat{s} - m_w^2)^2 + (m_w \Gamma_w)^2} (1 + \cos\theta)^2$

$V_{q\bar{q}'}$  : CKM matrix

$$V_{q\bar{q}'} \approx \begin{pmatrix} \cos\theta_c & \sin\theta_c & 0 \\ -\sin\theta_c & \cos\theta_c & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{matrix} u \\ c \\ t \end{matrix}$$

$\sin^2\theta_c = |V_{us}|^2 \approx 0.05$

$u\bar{b} \rightarrow W$  or  $c\bar{b} \rightarrow W$  negligible because

$|V_{ub}|^2 \ll |V_{cb}|^2 \approx 0.0017$

and small b pdf

$\Rightarrow$  CKM mixing effect small compared to NLO QCD corrections

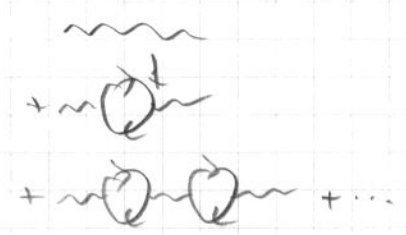
Corrections are proportional to

$\sin^2\theta_c (u(x_1) - c(x_1))(d(x_2) - s(x_2))$

suppressed at small x, i.e. LHC

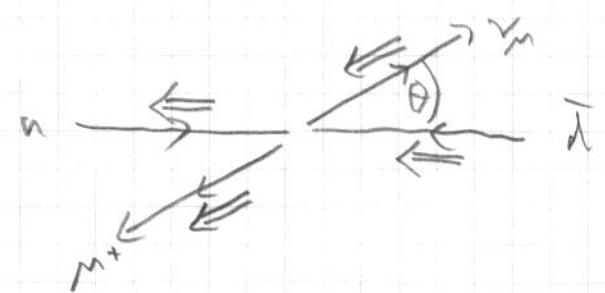
Breit-Wigner propagator

$m \sim \frac{1}{\hat{s} - m_w^2 + i m_w \Gamma_w}$  : resum  
 $\uparrow$   
 $i \text{Im} \Pi_{ww}(\hat{s})$



→ first order perturbation theory does not work: need to resum unstable particle propagators

A<sub>FB</sub>: W couples to LPA handed fermions



angular momentum not conserved at  $\theta = \pi$   
 $\Rightarrow \sigma \sim 1 + \cos\theta$

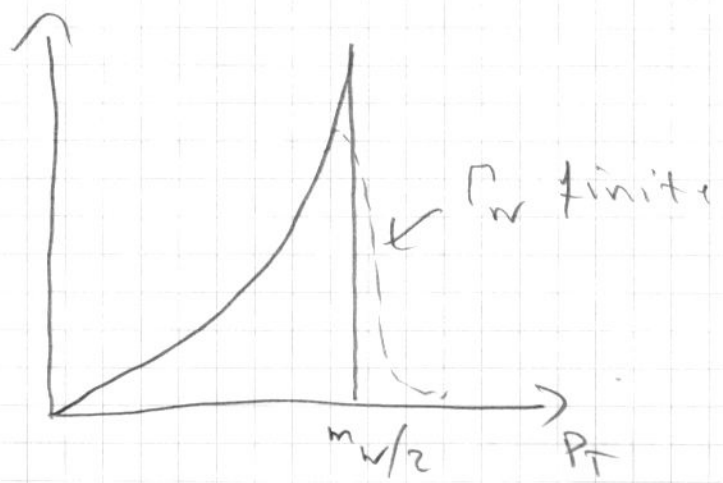
Problem  $\nu$  not observed  $\Rightarrow \cos\theta$  cannot be measured: only  $p_T$  and  $z_{\nu}$  available  
 but

$$\frac{d\sigma}{dp_T} = \frac{d\sigma}{d\cos\theta} \left| \frac{d\cos\theta}{dp_T} \right| = \frac{d\sigma}{d\cos\theta} \frac{4p_T}{\hat{s}} \frac{1}{\sqrt{1 - 4p_T^2/\hat{s}}}$$

with  $p_T = \frac{\sqrt{\hat{s}}}{2} \sin\theta \Rightarrow \cos\theta = \sqrt{1 - \frac{4p_T^2}{\hat{s}}}$

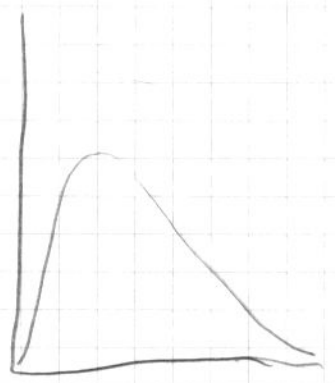
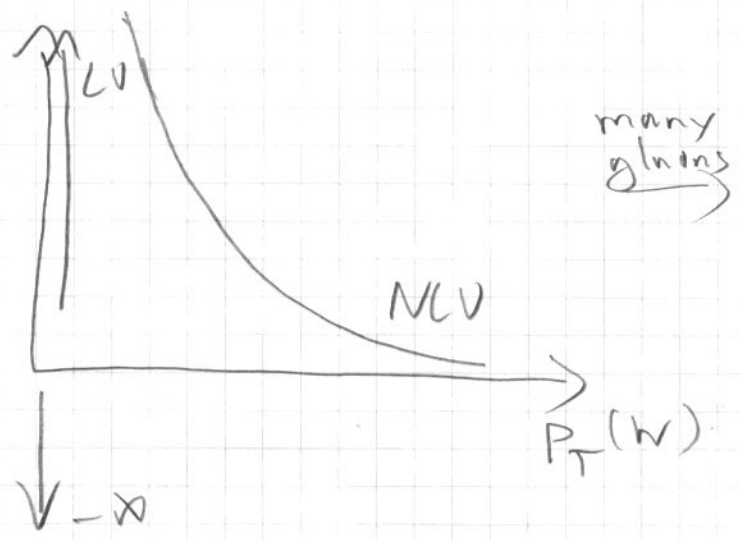
Jacobian factor, A diverges at

$$p_{Tmax} = \frac{\sqrt{\hat{s}}}{2} = \frac{m_W}{2} \text{ in narrow width approx}$$





$w$  produced at finite  $p_T$  at NLO



Absorb  $p_T$  kick by using transverse mass instead

$$m_T^2 \equiv (E_{Te} + E_{Tv})^2 - (\vec{p}_{Te} + \vec{p}_{Tv})^2$$

$$= 2(E_{Te} E_{Tv} - \vec{p}_{Te} \cdot \vec{p}_{Tv}) \leq m_w^2$$