

# Requirements for longitudinal HOM damping in FCC-hh

Ivan Karpov and Elena Shaposhnikova

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Rama Calaga, Erk Jensen, and James A. Mitchell

# Why damping of HOM is needed?

The FCC-hh is high-current machine with 10400 circulating bunches

→ Interaction of beam with high-order modes (HOM) can result in longitudinal coupled-bunch instability (CBI)

Unlike electron synchrotrons with strong synchrotron radiation, in FCC-hh we have to rely on Landau damping

How to evaluate the threshold? It can be obtained

→ from particle tracking simulations (very difficult for FCC-hh)

→ using semi analytical methods

# Method of threshold diagrams

Dispersion relation obtained from Vlasov equation with assumptions (A. N. Lebedev 1968):

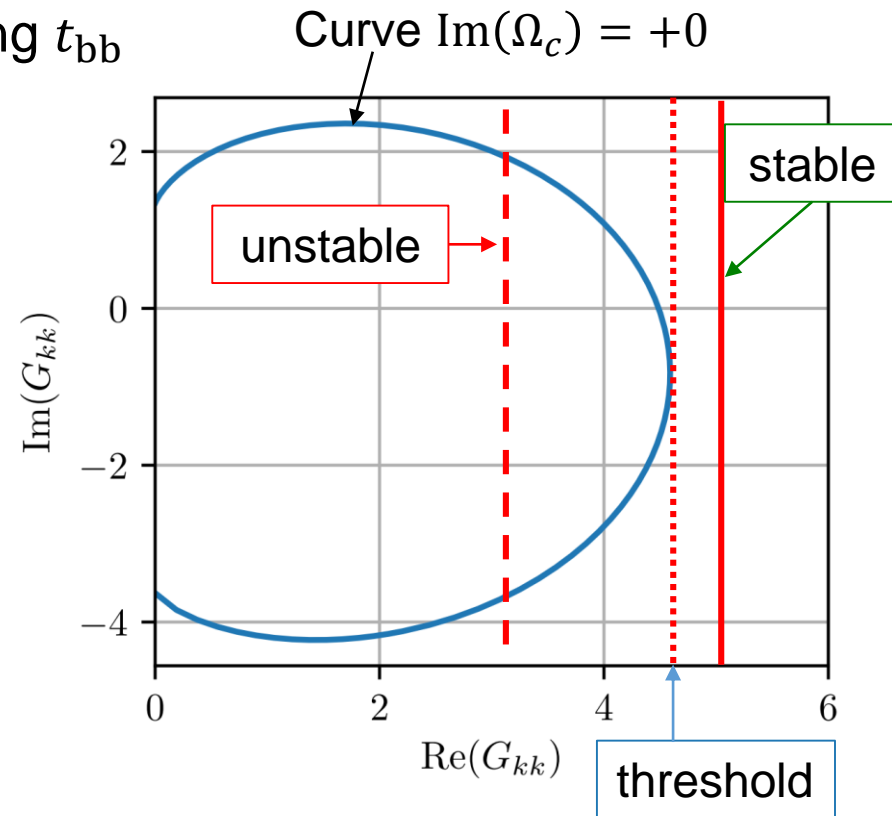
- Uniformly filled machine with spacing  $t_{bb}$
- $\Delta f_r = \frac{f_r}{2Q} \ll \frac{1}{t_{bb}}$ , and  $\Delta f_r \ll \left| f_r - \frac{l}{2t_{bb}} \right|$

$$\frac{1}{Z_k(\Omega_c)} = G_{kk}(\Omega_c)$$

HOM impedance:

$$\frac{1}{Z_k(\Omega_c)} = \frac{1}{R_{sh}} \left( 1 - iQ \frac{\omega^2 - \omega_r^2}{\omega \omega_r} \right)$$

$$\omega = k\omega_0 + \Omega_c, \quad k \approx \omega_r/\omega_0$$



- There is a unique diagram for given resonant frequency  $f_r$
- In practice, it is difficult to use diagrams for threshold evaluation

# Approximate threshold

Additional assumptions:

- Single RF system
- Short bunches with binomial distribution



Phase of synchronous particle

Synchrotron frequency spread  $\frac{\Delta\omega_s}{\omega_{s0}} = \frac{\omega_{\text{RF}}^2}{64} \left( 1 + \frac{5}{3} \tan^2 \phi_{s0} \right) \tau_b^2$

Line density  $\lambda(\tau) \propto \left[ 1 - \left( \frac{2\tau}{\tau_b} \right)^2 \right]^{\mu+1/2}$

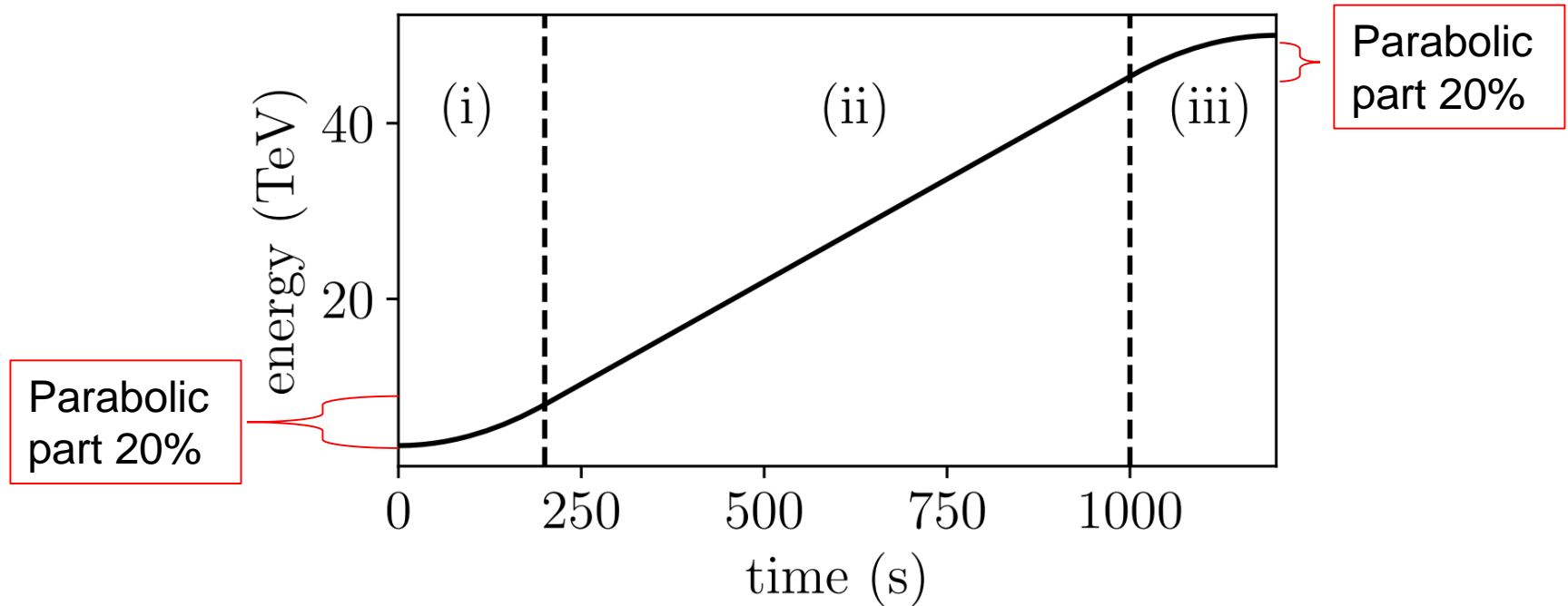
$\tau_{\text{FWHM}} = \tau_b \sqrt{1 - 2^{\frac{2}{2\mu+1}}}$

**Threshold shunt impedance**  $R_{\text{sh}} < \frac{t_{\text{bb}} \omega_{\text{RF}} \tau_b V_{\text{RF}} |\cos \phi_{s0}|}{4eN_p} \frac{\Delta\omega_s}{\omega_{s0}} G_\mu(f_r \tau_b)$

$$G_\mu(x) = \frac{x}{\mu(\mu+1)} \min_{y \in [0,1]} [(1-y^2)^{\mu-1} J_1^2(\pi xy)]^{-1}$$

→  $R_{\text{sh}}$  depends on RF voltage, bunch length, and synchronous phase for constant intensity

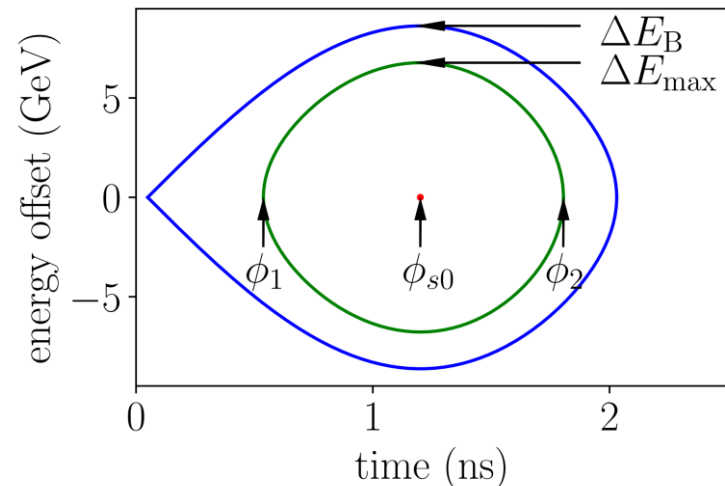
# Acceleration cycle



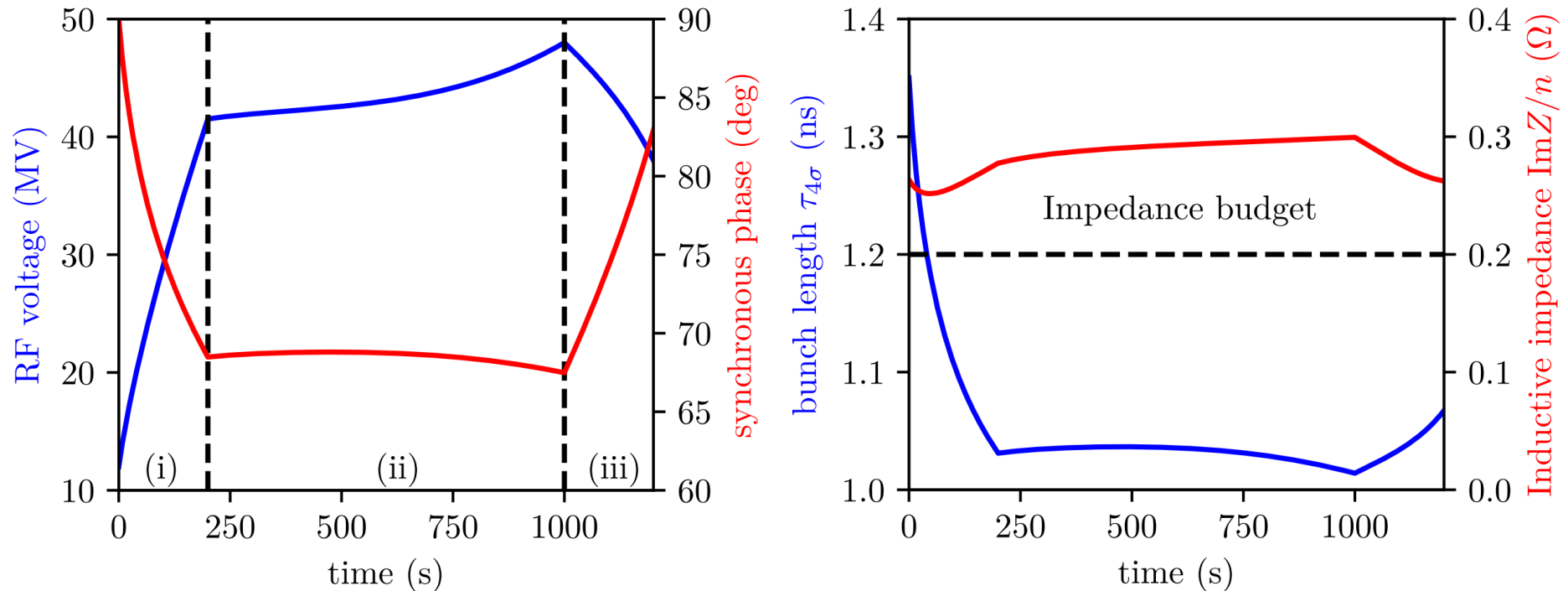
## Considerations:

- controlled emittance blow-up  $\epsilon \propto \sqrt{E}$  for longitudinal single-bunch stability
- Maximum energy filling factor

$$q_p = \frac{\Delta E_B}{\Delta E_{max}} = 0.941 \text{ to avoid losses}$$

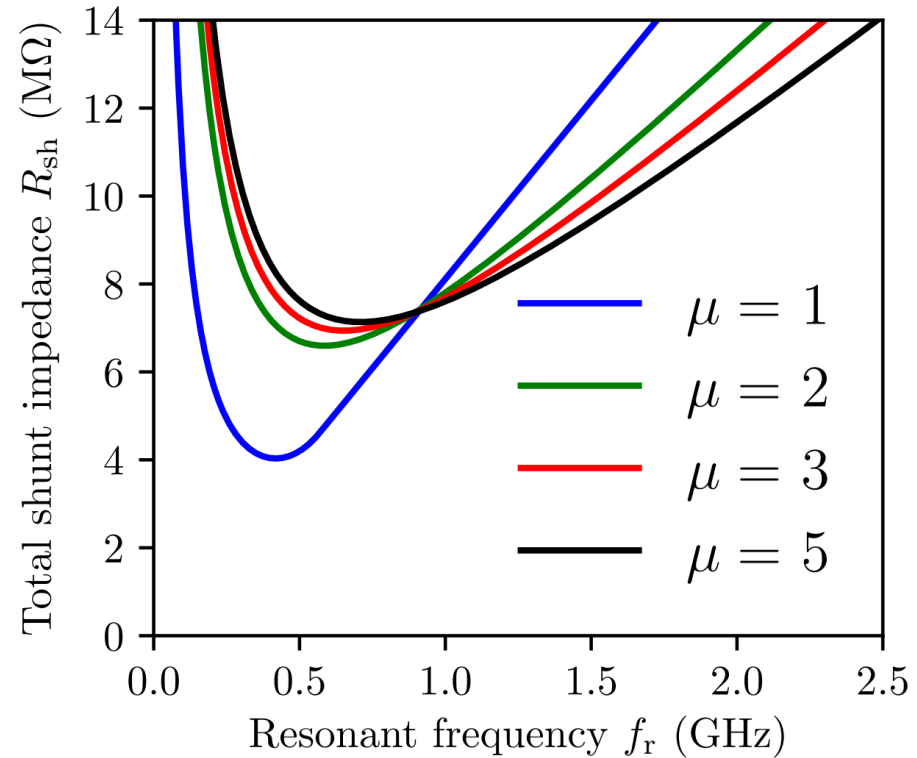
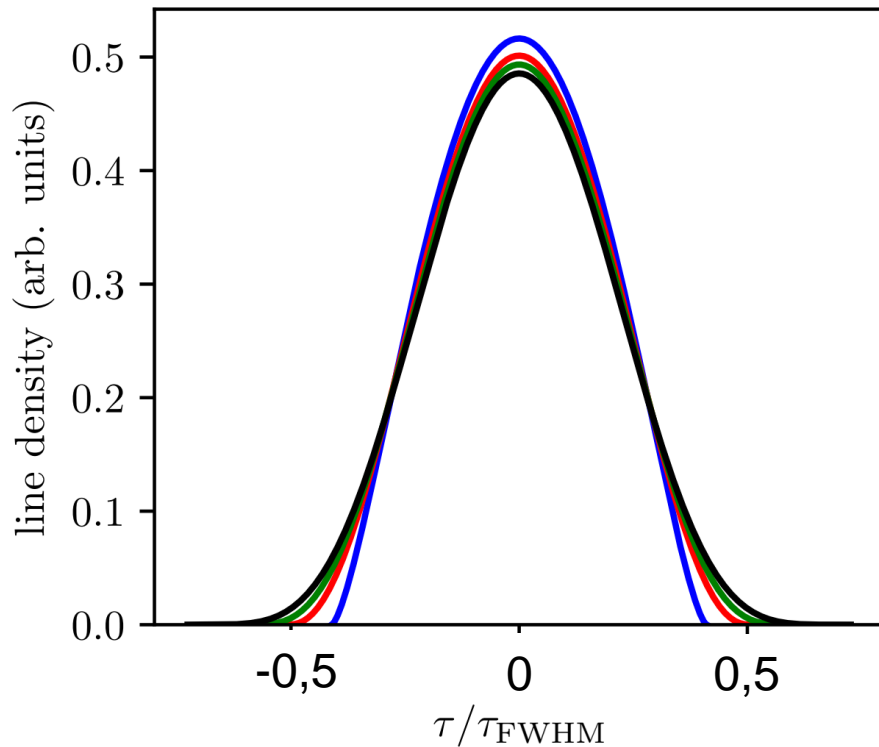


# Parameters during cycle



- Threshold of the loss of Landau damping is higher than longitudinal impedance budget
- Obtained parameters are used for longitudinal CBI threshold calculations

# Results at 50 TeV

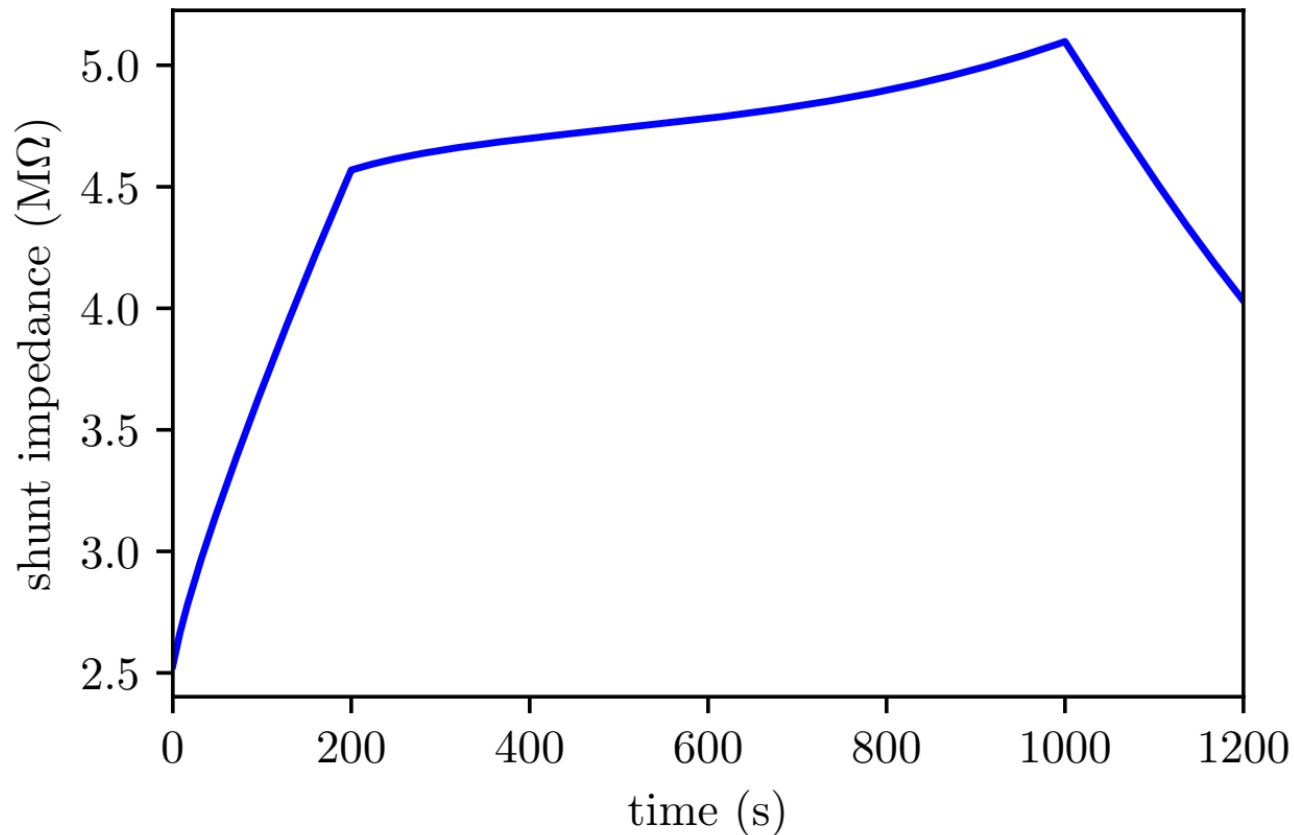


For the same  $\tau_{FWHM}$ :

- The lowest  $R_{sh}$  is for  $\mu = 1$
- Thresholds are similar for  $\mu > 1$

# Threshold during cycle

Obtained from  $\tau_{FWHM}$  bunch length for  $\mu = 1$

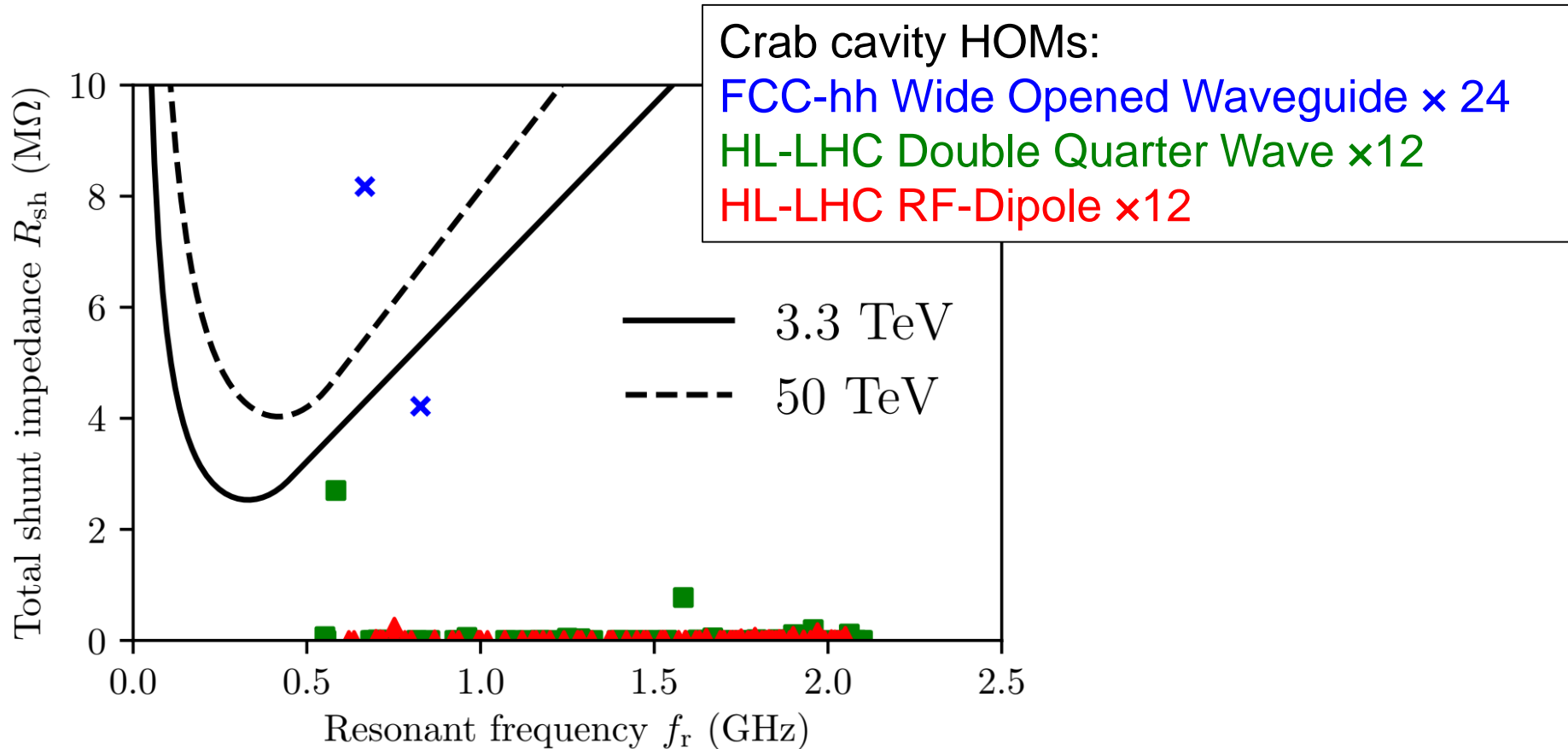


→ The lowest value at flat bottom



# HOMs in FCC-hh impedance model

Worst case scenario:  $f_r$  is the same in all cavities

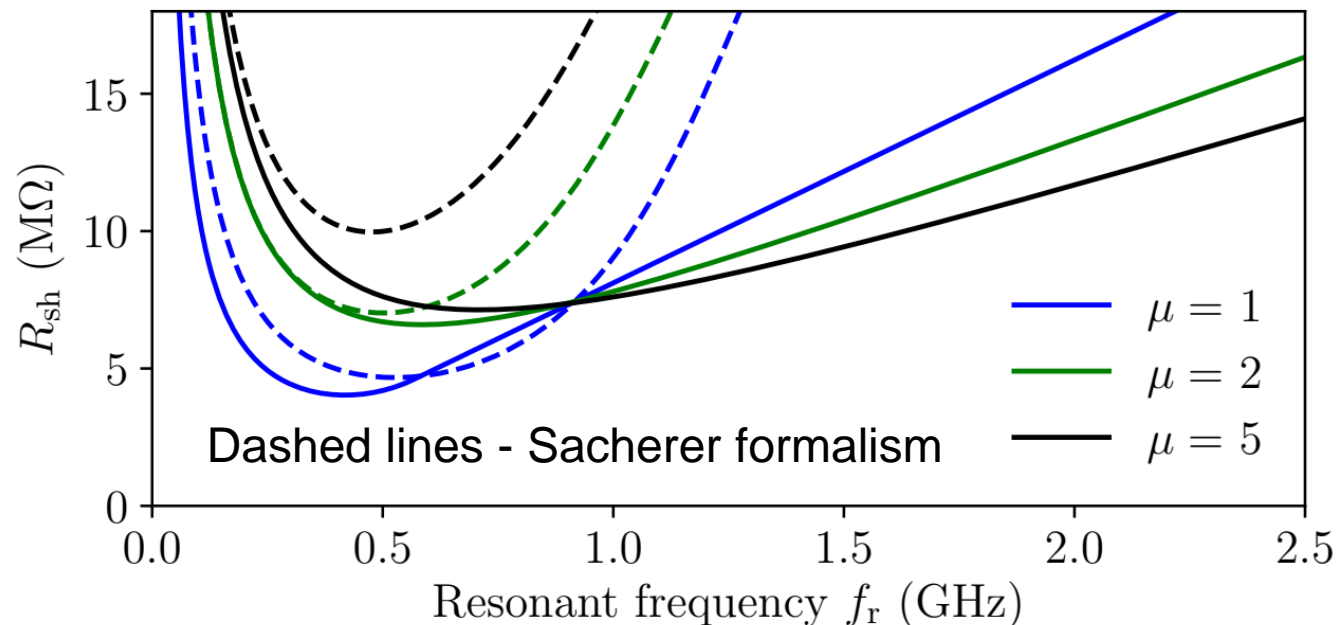


→ Damping of HOMs has to be revisited for Wide Opened Waveguide crab cavities

# Sacherer formalism

Solution of dispersion relation is split in two parts (Sacherer 1973):

- Calculation of complex coherent frequency shift neglecting synchrotron frequency spread
- Removing dependence on  $f_r$  from stability diagram using Taylor expansion



- Sacherer approach underestimates threshold at higher frequencies
- The minimum of thresholds are similar for small  $\mu$

# Summary

- The longitudinal coupled-bunch instability thresholds were evaluated for the FCC-hh cycle, which is optimised for longitudinal single-bunch stability.
- For the considered family of the binomial particle distributions, bunches with different  $\mu$  (except  $\mu = 1$ ) but the same FWHM bunch length have similar threshold shunt impedances.
- To prevent longitudinal CBI in FCC-hh due to HOMs of WOW crab cavities further damping is required.

**Thank you for your attention!**