

#### Shreyas Balachandran

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Acknowledgments:

This material is partly based upon work supported by the U.S. Department of Energy, Office of Science, Office of High Energy Physics under Award Number DE-SC0012083, and cooperative agreement No KN2713 from CERN. A portion of the work was performed at the National High Magnetic Field Laboratory, which is supported by National Science Foundation Cooperative Agreement No.-DMR-1644779 (2018-) and the State of Florida. Thanks to Jeff Parrell, Bruker OST for providing the Nb-4Ta precursor alloy used in this fabrication.







### Key points of this talk: 1

### **Background:**

- In 2018 we compared 1Hf and 1Zr alloyed Nb4at%Ta with and without an O source, finding that O-free Nb-4Ta-1Hf suffered no degradation of H<sub>irr</sub> (4.2 K)~23 T and the highest layer J<sub>c</sub>(16 T, 4.2 K) of ~5000 A/mm<sup>2</sup> (RRP non-Cu J<sub>c</sub> of 0.6 J<sub>clayer</sub>) which exceeds FCC specification
  - Our study showed that internal oxidation is not the only route to fine grain A15, perhaps opening an avenue to simplify the manufacture of FCC magnet conductors

### What have we done?

- Full range (30 T) VSM measurements on our own monofilaments and the first multi-filament Nb-Ta-Hf conductor (PIT made by HyperTech Research Inc (HTRI).
- Compared drawability of Nb-Ta-Hf and the well known Nb-Ta.
- Performed a recrystallization study of Nb-Ta-Hf, and Nb-Ta composite



### Key points of this talk: 2

### What did we find?

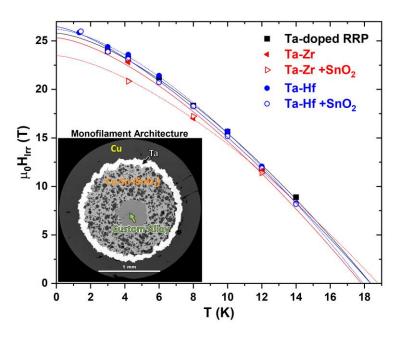
- Verified shift in  $H_{max}$ (4.2 K) above 5 T without suppression of  $H_{irr}$  (4.2 K) ~23.5 T.
- Found that **Nb-Ta-Hf work hardens** similarly to Nb-Ta alloy.
- Found that BOTH ASC/NHMFL and HTRI-sourced Nb-4Ta-1Hf prevent recrystallization of worked Nb-Ta-Hf during Nb<sub>3</sub>Sn formation, setting up conditions for fine grain A15 phase formation.

### So what?

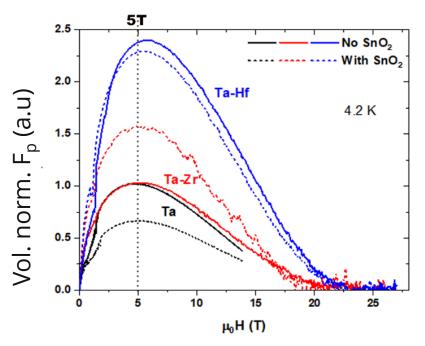
- Recrystallization during A15 formation is prevented in Nb-Ta-1Hf, greatly enhancing  $J_{c.}$
- Although, internal oxidation may offer additional benefits, we believe 50-75 nm grains start with inhibiting recrystallization of the starting alloy before A15 formation.
- Avoiding extra oxygen additions could greatly simplify application to existing Nb<sub>3</sub>Sn production wires.



**2018 Background**: Potential of Nb-4Ta-1Hf alloy for high  $J_c$  (>1500 A/mm<sup>2</sup>, 16 T, 4.2 K) Nb<sub>3</sub>Sn conductor was established with monofilament wires.



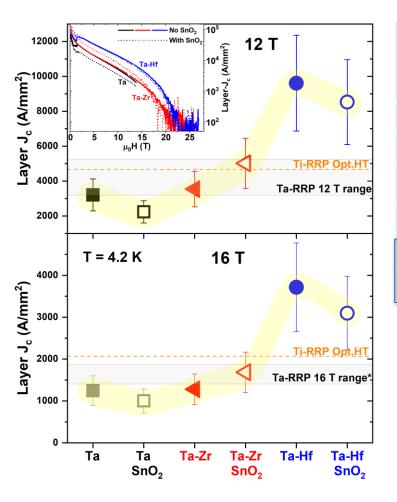
 Ta doped RRP, Ta-Hf, and Ta-Zr all have comparable H<sub>irr</sub> (4.2 K) ~23 T.



- *F*<sub>pmax</sub> is substantially higher in Nb-Ta-Hf than Nb-Ta-Zr or Nb-Ta.
- Position of  $F_{pmax}$  ( $H_{max}$ ) shifted to 5.8T in the case of Nb-Ta-Hf without SnO<sub>2</sub>.
- Enhanced  $F_{pmax}$  and  $H_{max}$  above Tadoped RRP occurs in all cases.

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## **Background:** 16 T Layer J<sub>c</sub> estimates of Nb-4Ta-1Hf conductor without SnO<sub>2</sub> exceed 3500 A/mm<sup>2</sup>



Alloy	SnO <sub>2</sub>	J <sub>clayer</sub> (A/mm²)		Eq. RRP non- Cu J <sub>c</sub>
		12 T	16 T	(A/mm²)
Nb-Ta	No	3209 ± 916	1245 ± 355	747 ± 213
Nb-Ta	Yes	2237 ± 639	1003 ± 286	602 ± 172
Nb-Ta-Zr	No	3545 ±1012	1281 ± 366	768 ± 219
Nb-Ta-Zr	Yes	5017 ±1433	1684 ± 481	1010 ± 289
Nb-Ta-Hf	No	9609 ±2744	3714 ±1061	2229 ± 636
Nb-Ta-Hf	Yes	8523 ±2434	3093 ± 883	1856 ± 530

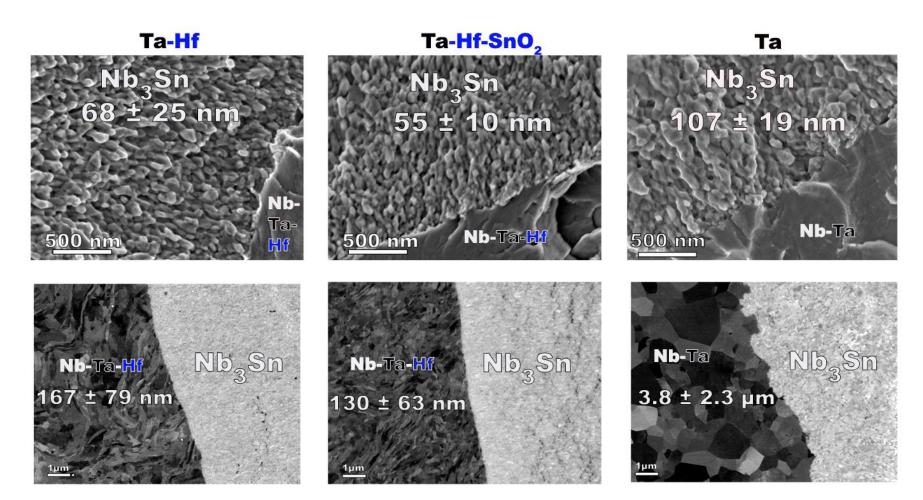
Ta-Hf doping without SnO<sub>2</sub> opens up existing conductor architecture options (**RRP**, **PIT and Distributed Tin**, **bronze-route**) without need to incorporate O source.

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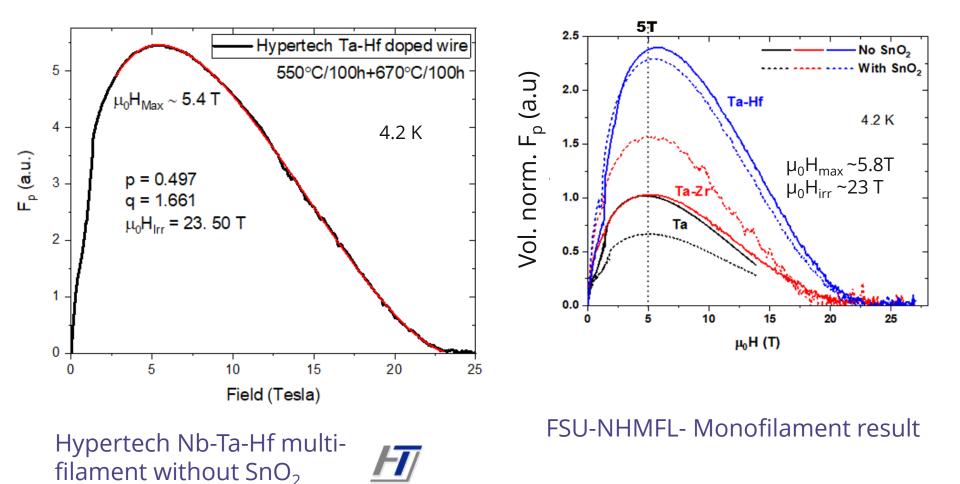
## Nb-4Ta-1Hf rod does not recrystallize during A15 formation, unlike Nb-4Ta (or pure Nb used in RRP wires)



- Fine grain alloy rod leads to halved Nb<sub>3</sub>Sn grain size.
- Hf appears to increase the recrystallization temperature of Nb-4Ta
- Sn penetrates Nb alloy by preferential grain boundary diffusion



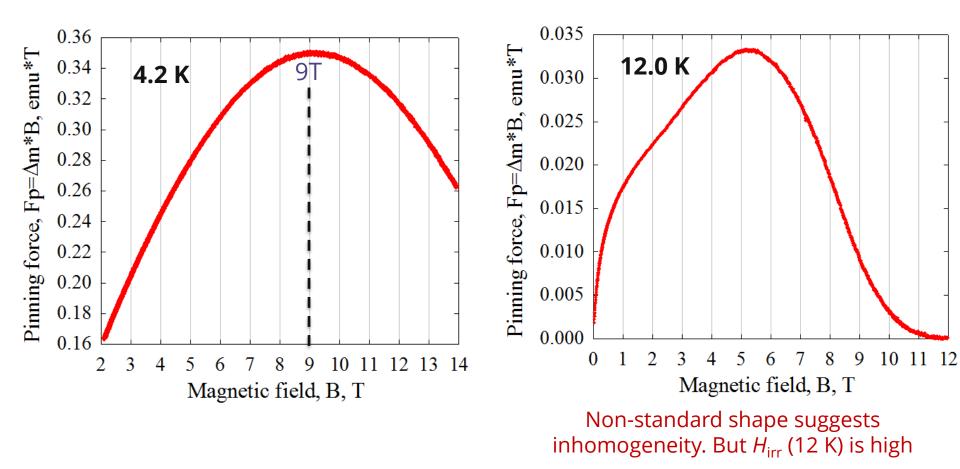
### Multi-filament conductor made by HTRI (without $SnO_2$ ) confirms the monofilament result of $H_{max}$ shift beyond 5 T, $H_{irr}$ (4.2 K) of 23.5 T.



#### The Hyper Tech Nb-4Ta-1Hf tubes were independently sourced



# Hyper Tech Hf conductor with $SnO_2 - H_{max}$ shift to 9 T, suggesting additional oxide pinning centers add to fine A15 grain pinning.



Thanks to Xingchen Xu (FNAL), and Xuan Peng (Hypertech)



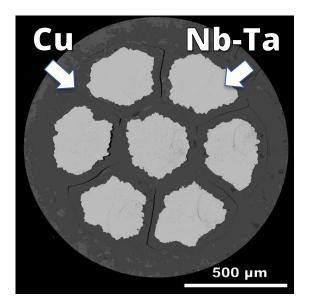
### Development of multi-filament conductors with Nb-Ta-Hf alloys

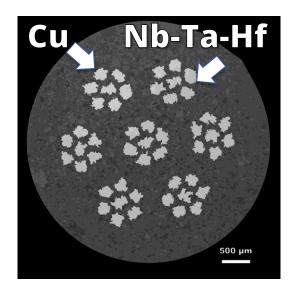
• Can Nb-4Ta-1Hf alloy be drawn to large strains?

 Does the worked multi-filament microstructure survive the Nb<sub>3</sub>Sn reaction heat treatment temperature?



## Cu/Nb-4Ta and Nb-4Ta-1Hf multifilament wires were drawn to large strains.

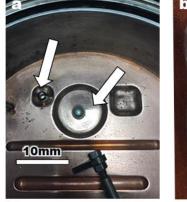




Nb-4Ta (avg. fil. *α* ~300 μm)

(avg. fil. ∅ ~250 µm)

Nb-4T-a1Hf



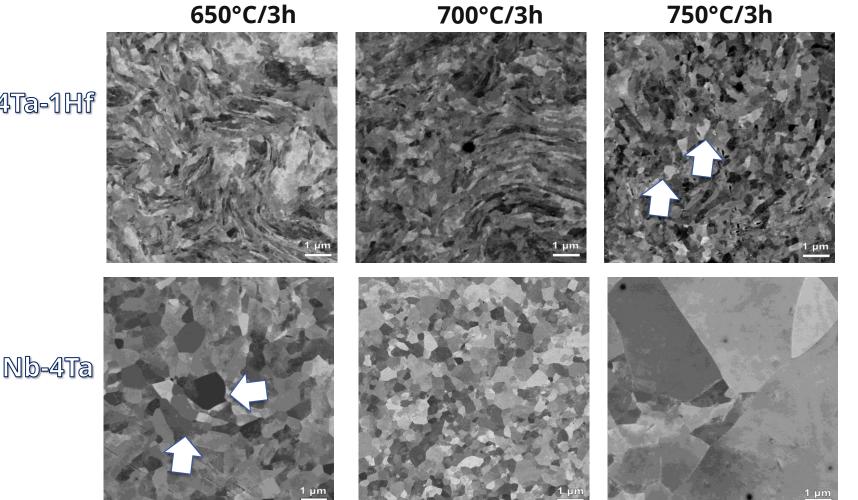
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- 30 g ingot arcmelted ingots.
- Ingots swaged to 3 mm diameter rod.
- Cu-sheathed, restacked and drawn to larger strains.

Note that these 30 g ingots could not be properly recrystallized and they did not deform uniformly at large strains

The total true strain  $\left(\ln\left(\frac{A_0}{A}\right)\right)$  is ~7

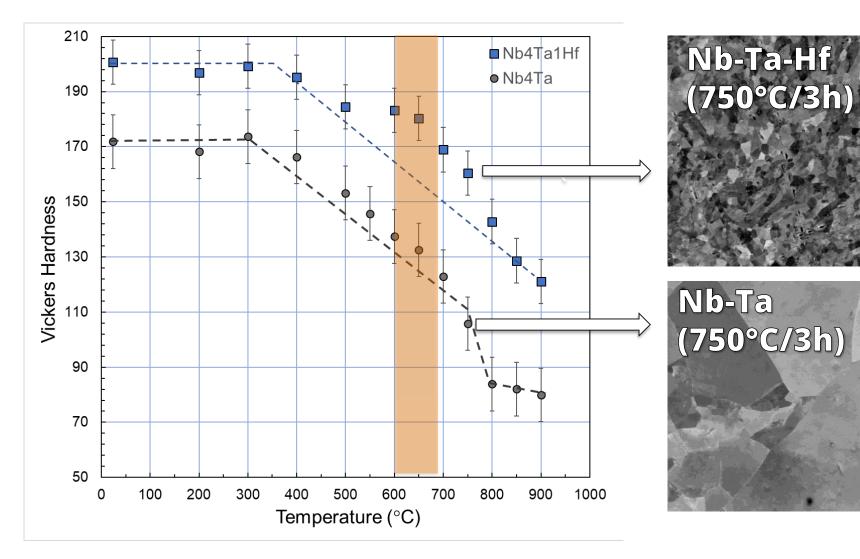
### Worked microstructure persists in Nb-Ta-Hf after 3 h at 650°C-700°C. Nb-Ta shows new grain growth already at 600°C.



Nb-4Ta-1Hf

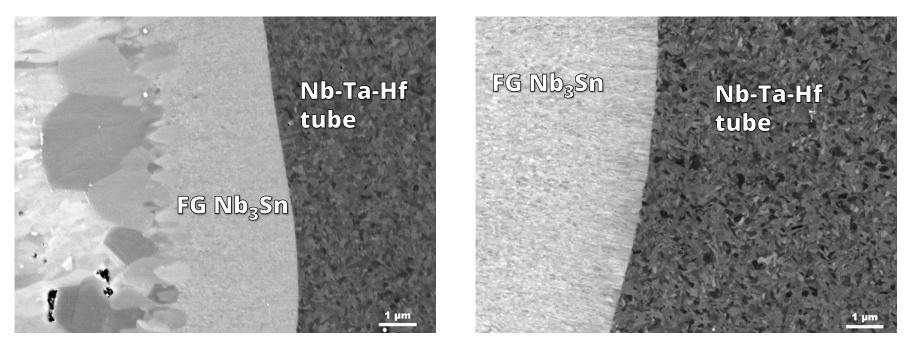
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### **Recrystallization of Nb4Ta is evident in hardness**



1 µm

## HyperTech tube confirms delayed recrystallization in Nb-Ta-Hf alloy during Nb<sub>3</sub>Sn reaction heat treatment.



### 625°C/740h

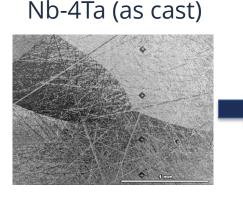
### 675°C/385h

Hf appears to raise Nb-4Ta recrystallization temperature significantly.

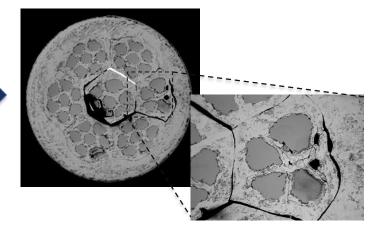
Thanks to Xuan Peng (Hyper Tech) and Xingchen Xu (FNAL) for wire sample.



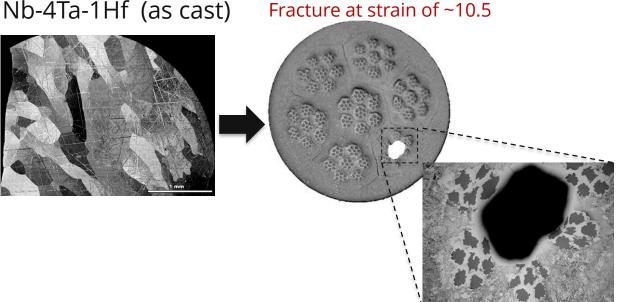
### Workability of Nb-4Ta, Nb-4Ta-1Hf IS limited by initial cast microstructure.



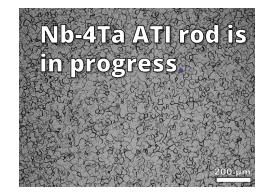
Fracture at strain of ~9



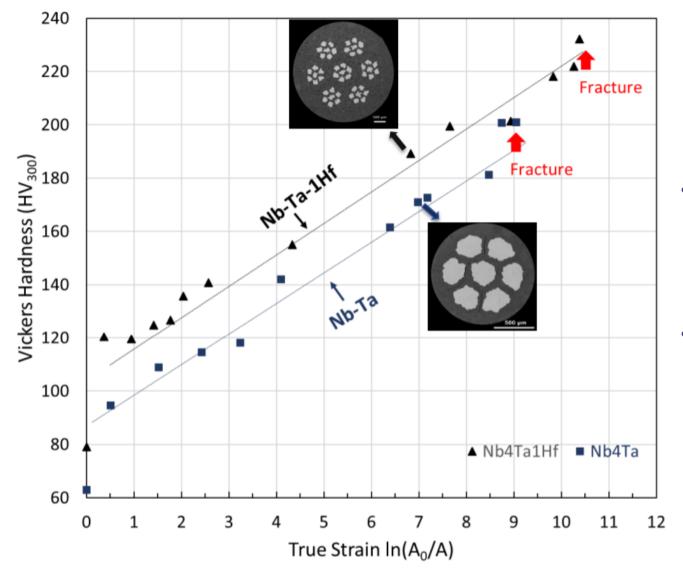
Fracture at strain of ~10.5



- Large mm size starting grains lead to non-uniform deformation of the alloy rod in a soft Cu sheath.
- Large scale industrial Nb-4Ta-1Hf alloy from **HC Starck Inc** expected in July with fine recrystallized grain structure



### Hardening behavior of Nb-4Ta-1Hf is similar to Nb-4Ta.

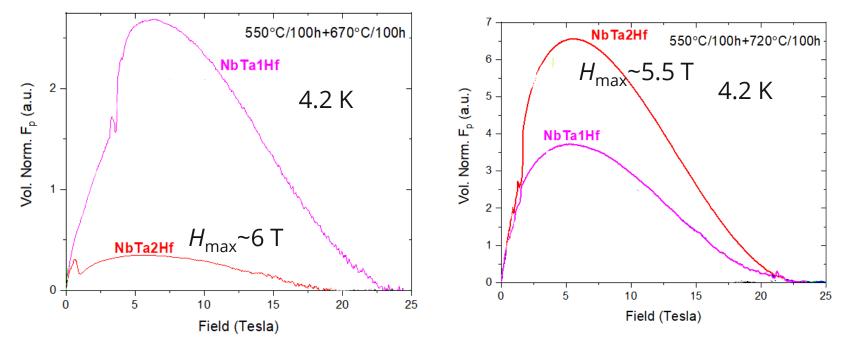


- Nb-Ta-Hf has a higher hardness compared to Nb-Ta.
- This does not limit the deformability of the conductor.

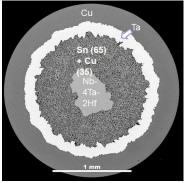
# Is 1at% Hf addition to a Nb-4Ta alloy optimum?



# Monofilament studies show benefit to pinning force by doubling the Hf content to 2 at%. $H_{max}$ (4.2 K) is higher without suppression of $H_{irr}$ (4.2 K).



- Consistent peak shift above 5 T in Nb-4Ta-2Hf conductor.
- Considering industrial alloy of Nb-4Ta-2Hf now.
- Increasing Hf content could provide a control knob for delaying recrystallization.



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### Conclusions

- Hf additions to Nb-4Ta provide <<100 nm Nb<sub>3</sub>Sn grain size due to additional GB diffusion paths provided by enhanced recrystallization temperature.
  - Demonstrated in both ASC monofilaments and Hypertech multifilament conductors for Nb<sub>3</sub>Sn reaction heat treatments at 625°C- 675°C.
  - Enhanced H<sub>max</sub> (4.2 K) and unsuppressed H<sub>irr</sub> (4.2 K) is verified by Hyper Tech multifilament conductor
  - Hyper Tech wires with Sn-oxide may provides interesting opportunities also.
- Multifilament Nb-4Ta-1Hf failed at a higher strain of 10.5 than the strain of 9 in Nb-4Ta. Cast grain structure was the cause in both cases.
  - Larger batches of alloy with controlled grain size from commercial vendors are expected imminently in progress.
  - Rod microstructure evolution during A15 heat treatment and its effect on fine grain Nb<sub>3</sub>Sn formation in Hf based alloys needs exploration.

#### • Nb-Ta-Hf conductors provide avenues in various architecture types.

- FG Nb<sub>3</sub>Sn by optimization of Hf doping provides a direct avenue to implement the new alloy in RRP, bronze route, and PIT configurations.
- Additions of oxygen as advanced by Ohio State-Hypertech-Fermilab seems to enhance H<sub>max</sub> and are being evaluated in PIT conductor form.

