



RF Characterisation of HTS-CC Tapes as Alternative Coating for the FCC-hh Beam Screen

Patrick Krkotic^{1,2}, Joan O'Callaghan², Montse Pont¹, Francis Perez¹
Artur Romanov³, Joffre Gutierrez³, Teresa Puig³

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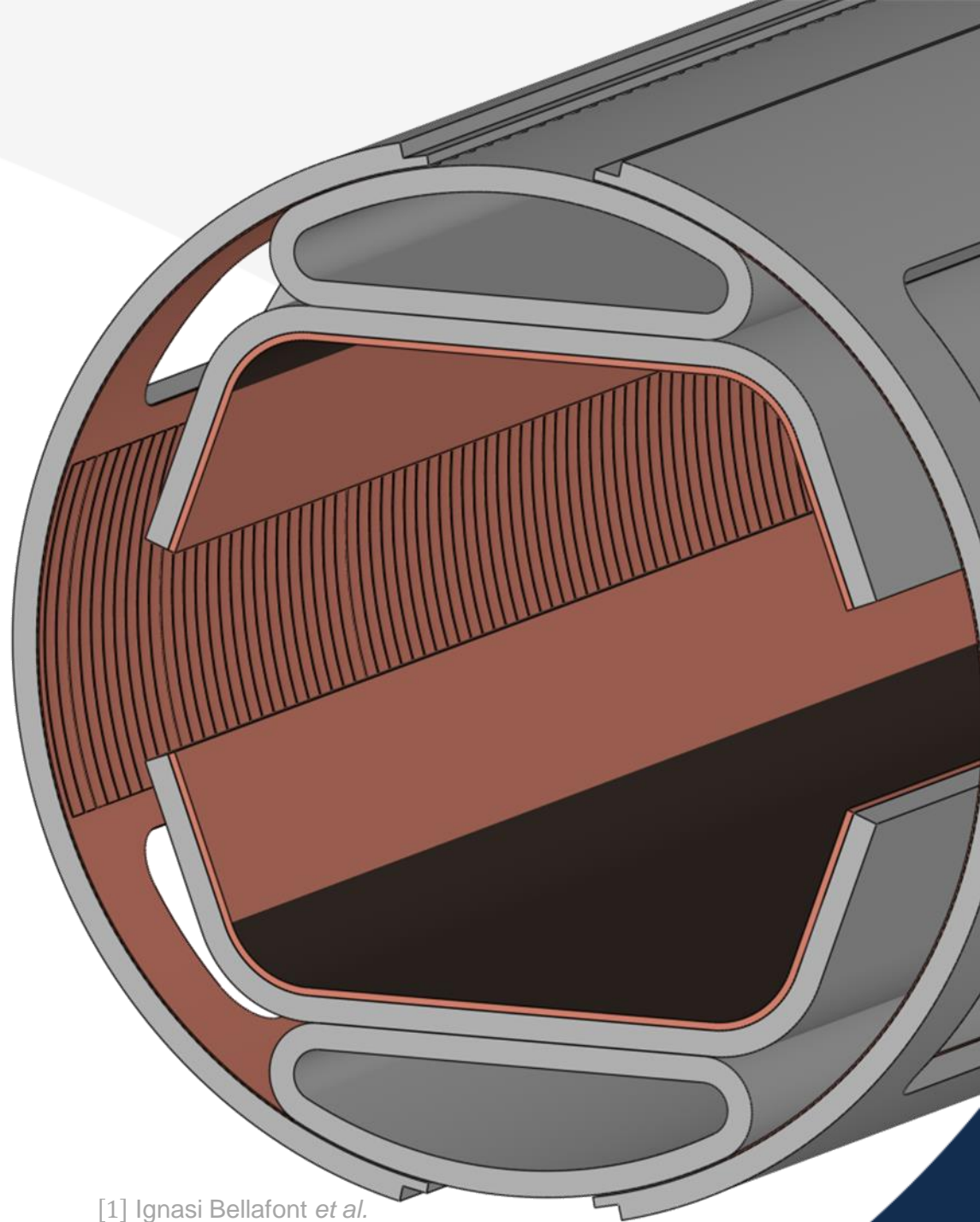
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Beam Screen Design FCC-hh

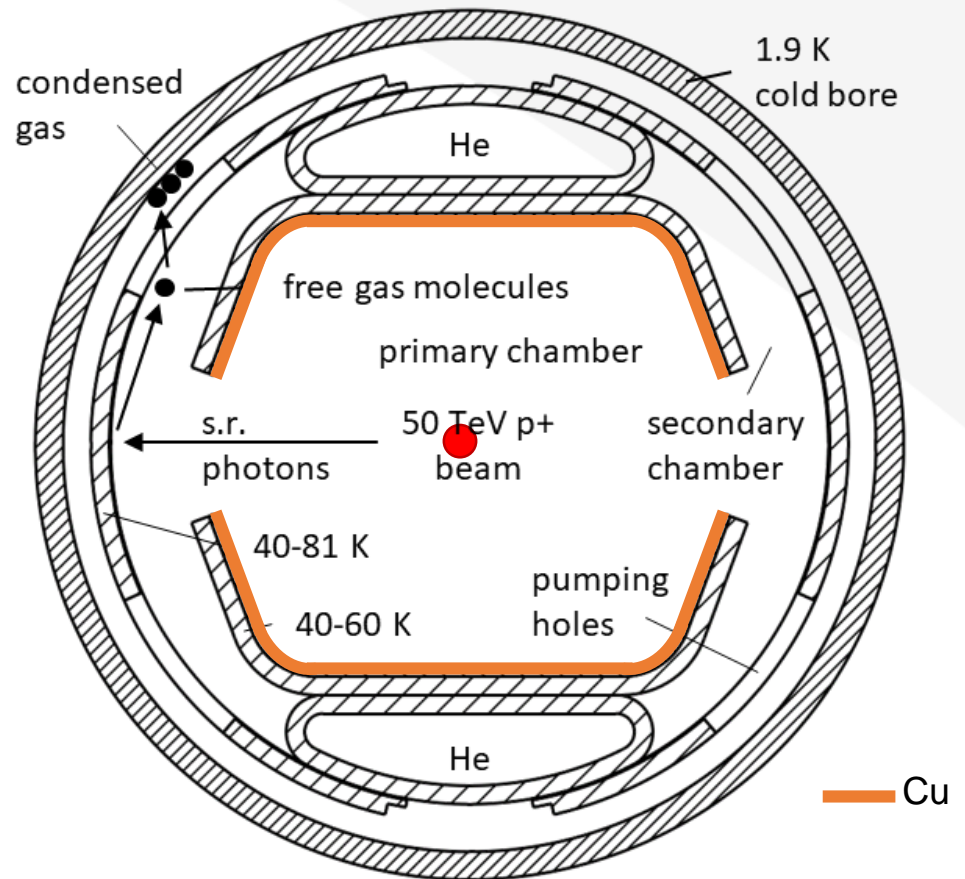
Coated Conductor Coating



Beam Screen Design

FCC-hh

- Nominal aperture:
 - H: 28.37 mm
 - V: 24.4 mm
- Slit height:
 - 7.5 mm
- Beam screen:
 - 1.0 mm steel
 - 0.3 mm copper
- Operating temperature
 - 50 ± 10 K

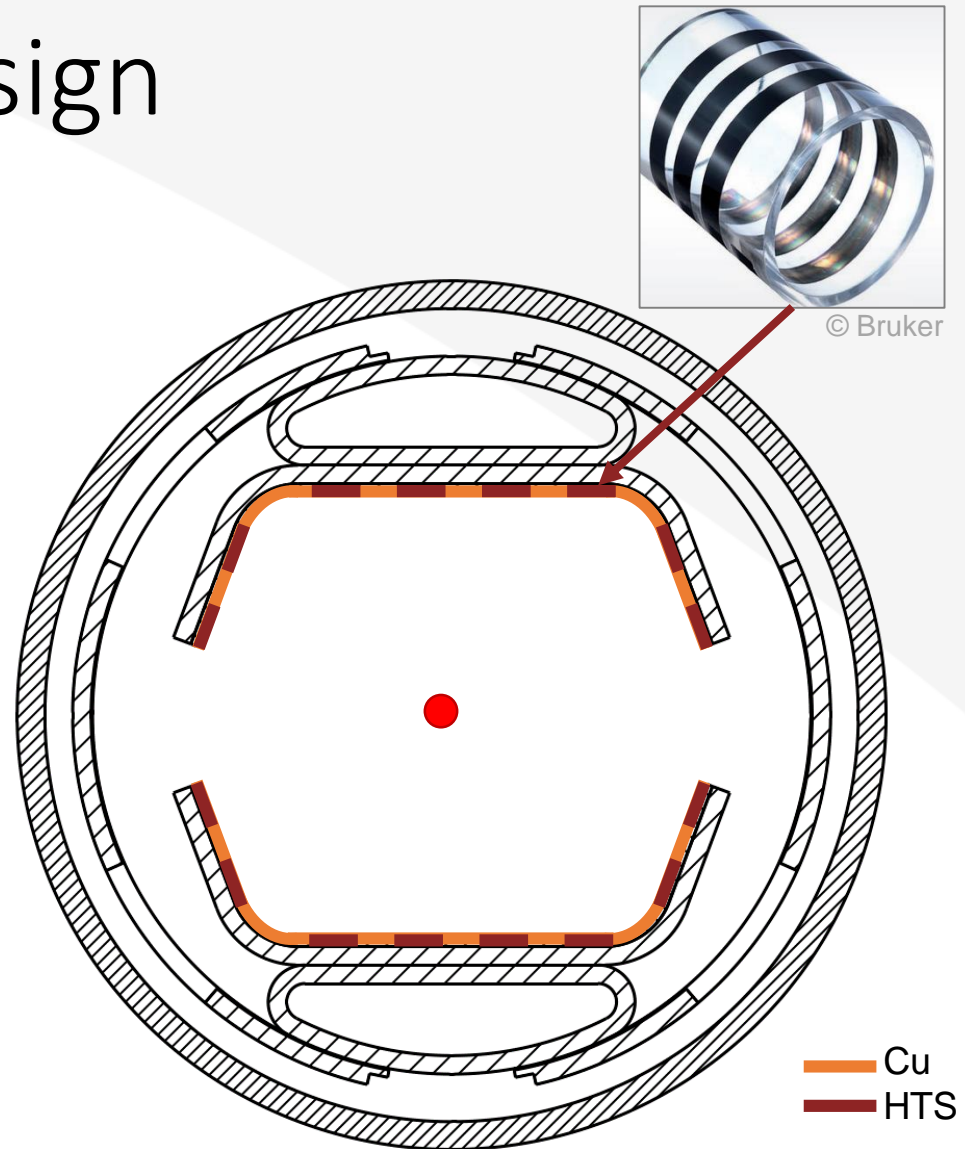


[1] Ignasi Bellafont *et al.*

Beam Screen Design

Coated Conductor Coating

- HTS coated conductor stripes
 - commercially available 2 – 12 mm
- Display on several chosen positions
 - e.g. alternating CC and Cu
 - lower ac losses
- Covered with amorphous Carbon to reduce SEY
- Reducing beam coupling impedance
 - low surface resistance

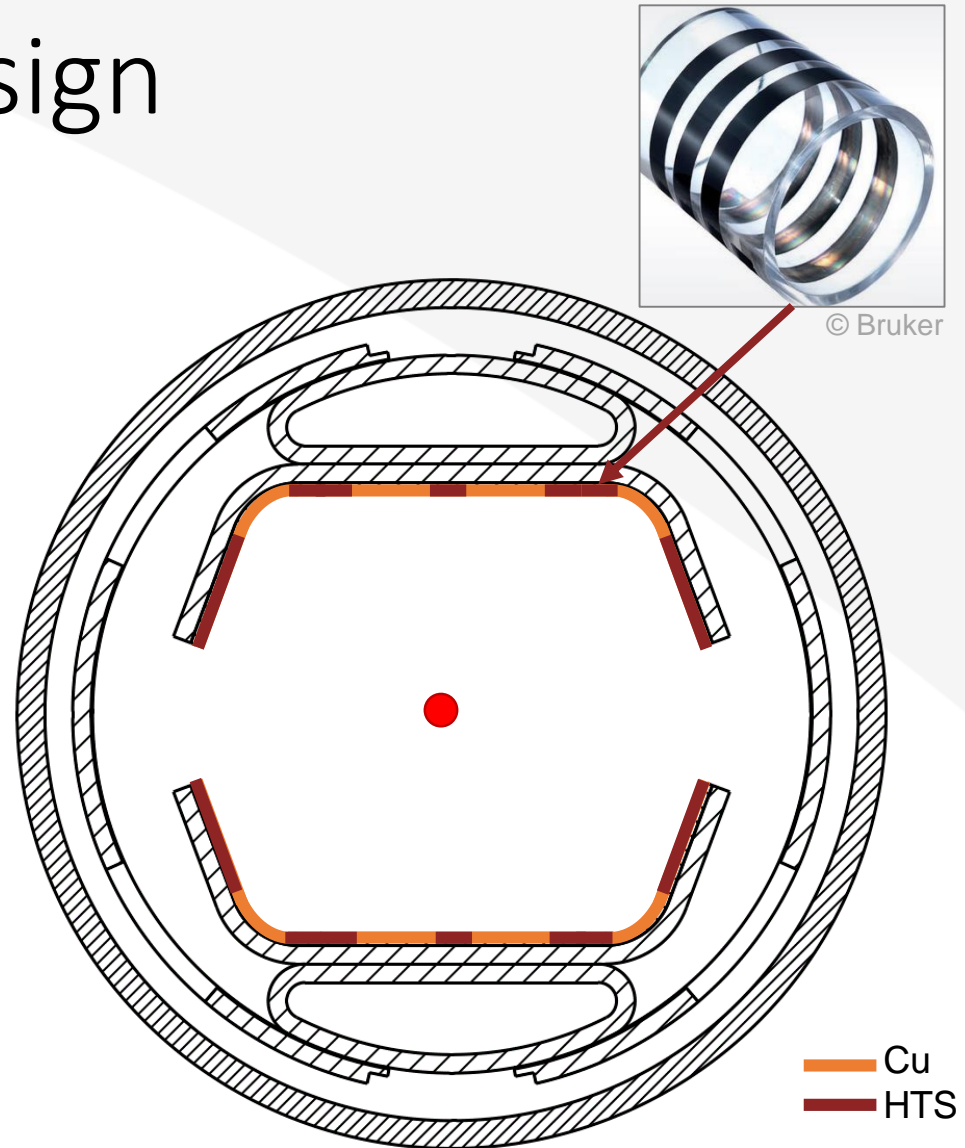


[1] Ignasi Bellafont *et al.*
[2] Patrick Krkotić *et al.*

Beam Screen Design

Coated Conductor Coating

- HTS coated conductor stripes
 - commercially available 2 – 12 mm
- Display on several chosen positions
 - e.g. gradually increasing tapes
 - lower ac losses
- Covered with amorphous Carbon to reduce SEY
- Reducing beam coupling impedance
 - low surface resistance

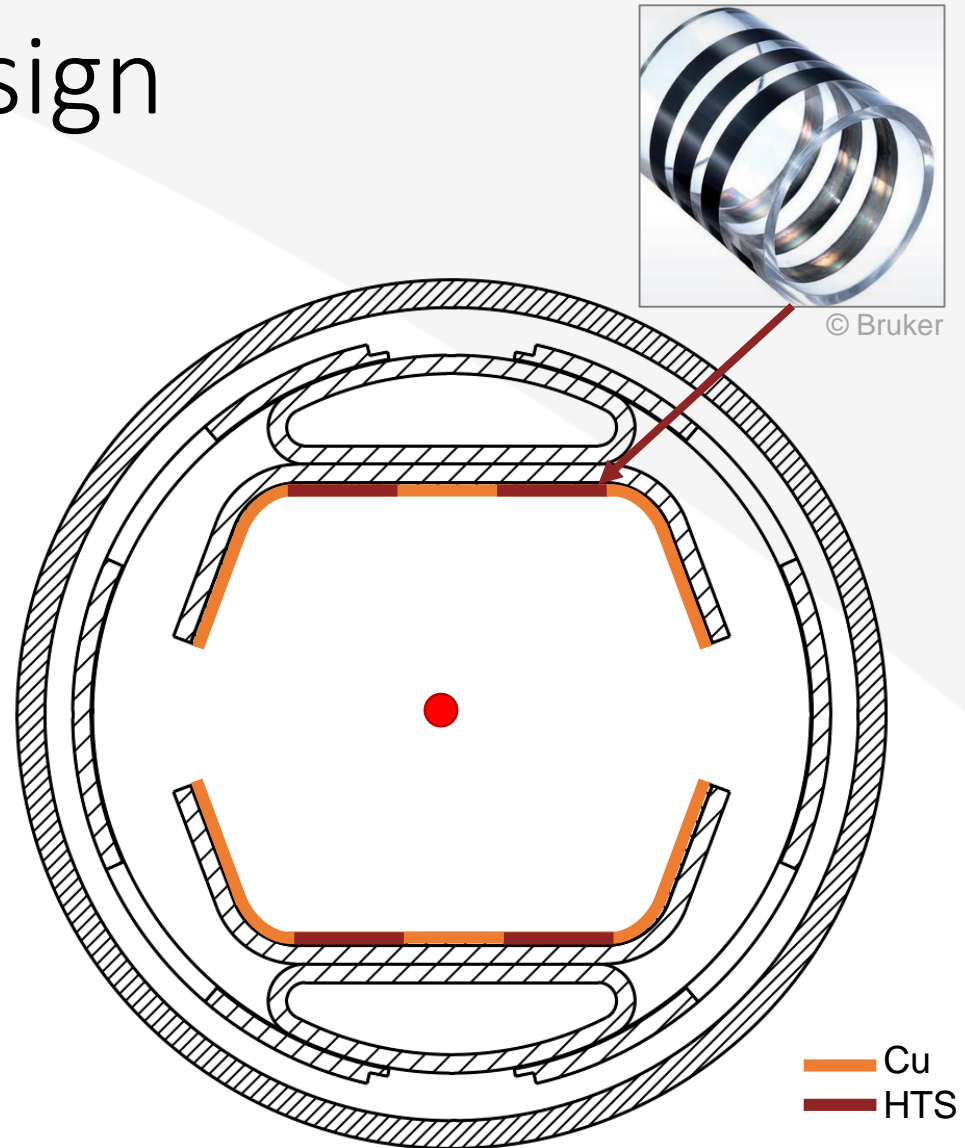


[1] Ignasi Bellafont *et al.*
[2] Patrick Krkotić *et al.*

Beam Screen Design

Coated Conductor Coating

- HTS coated conductor stripes
 - commercially available 2 – 12 mm
- Display on several chosen positions
 - e.g. double track
 - lower ac losses
- Covered with amorphous Carbon to reduce SEY
- Reducing beam coupling impedance
 - low surface resistance



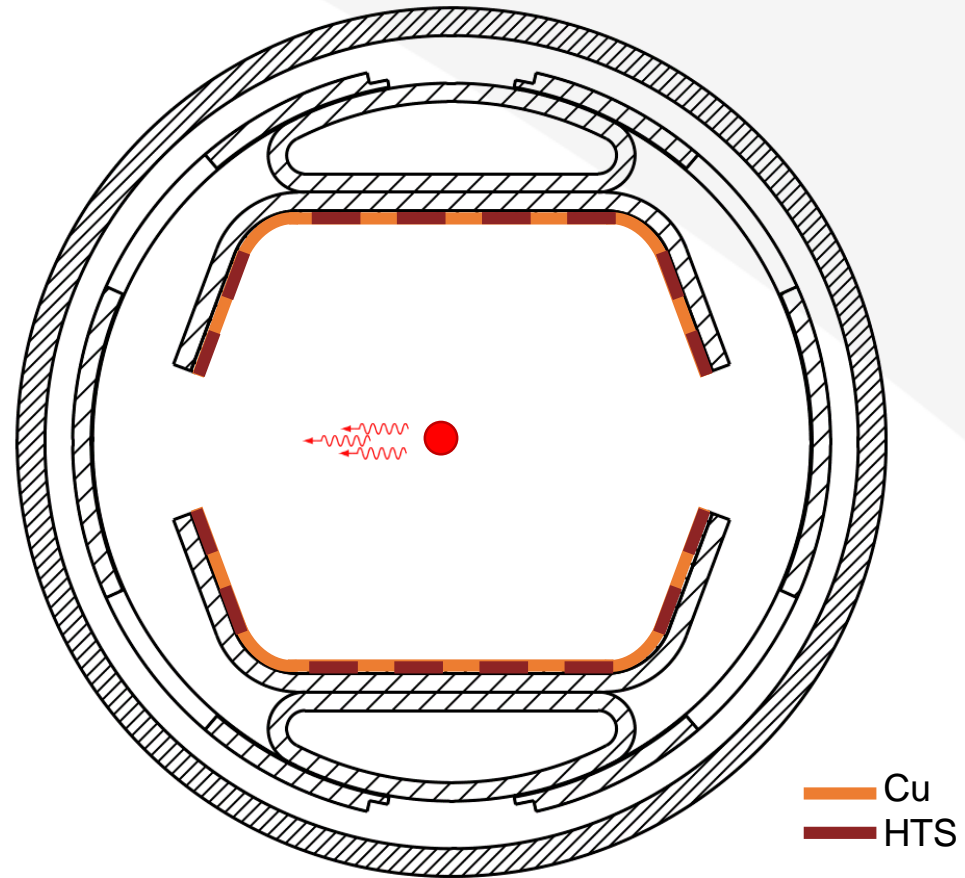
[1] Ignasi Bellafont *et al.*
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Beam Screen Design

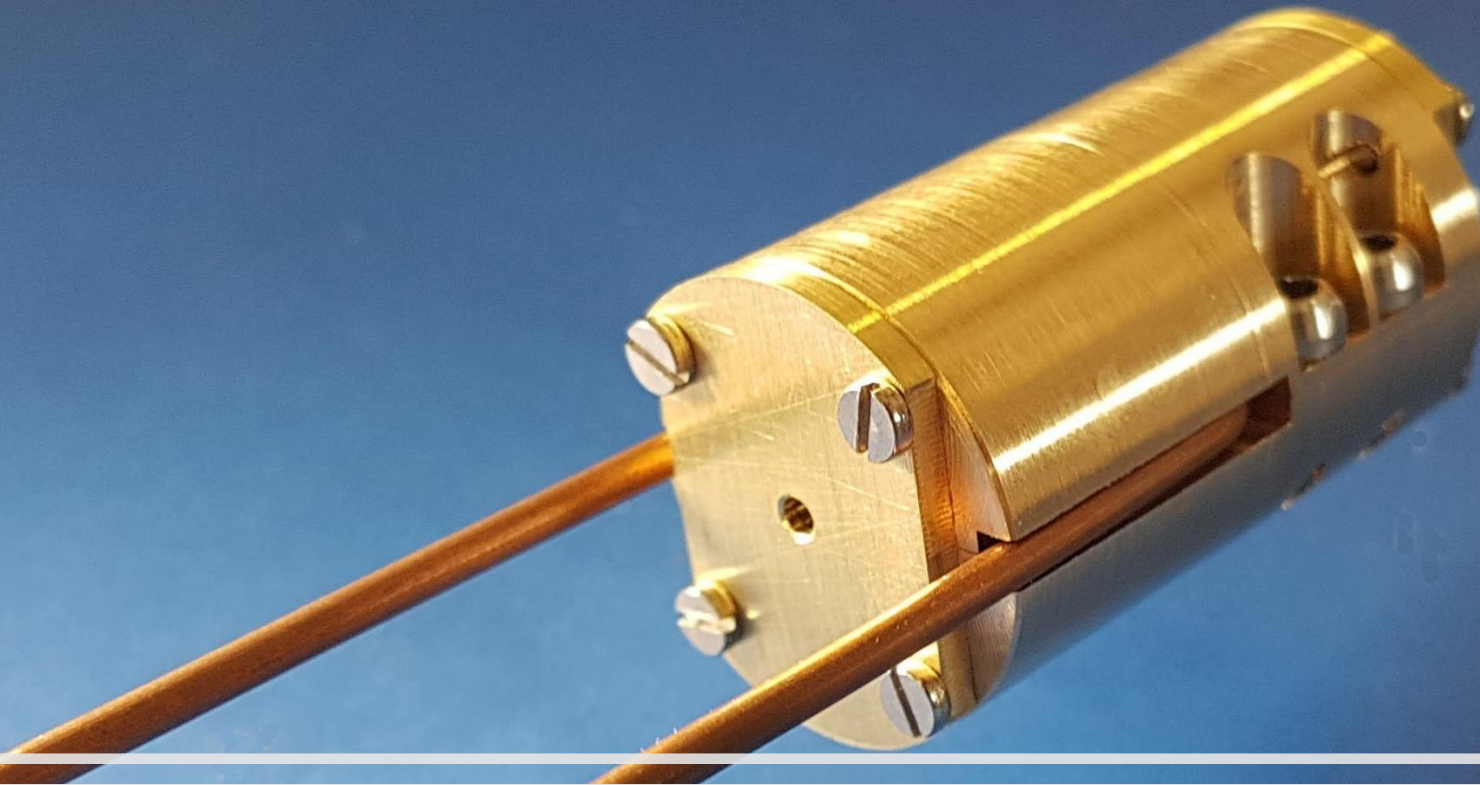
Requirements

- Operating temperature:
 - 50 ± 10 K
- Magnetic field strength:
 - 1 – 16 T
- Emitted synchrotron radiation:
 - 35.4 W/m/beam
- Beam spectrum frequency:
 - up to 3 GHz
- Image current per bunch:
 - 25 A $\rightarrow J_C = 25$ kA/cm²

[Poster Session - Joffre Gutierrez Royo, 'Coating the FCC-hh beam screen chamber with REBa2Cu3O7-x coated conductors'](#)



[1] Ignasi Bellafont *et al.*
[2] Patrick Krkotić *et al.*



Experimental Setup

Dielectric Resonator
(compatible with a PPMS system)

Dielectric Resonator

Surface Resistance

- Shielded Hakki-Coleman type
- Samples replace upper and lower plates
- Operating in the TE_{011} mode
 - insensitive to electrical contact of the sample with the metallic enclosure
 - resonance frequency at 50 K is 7.9 GHz
- Surface Resistance is defined as

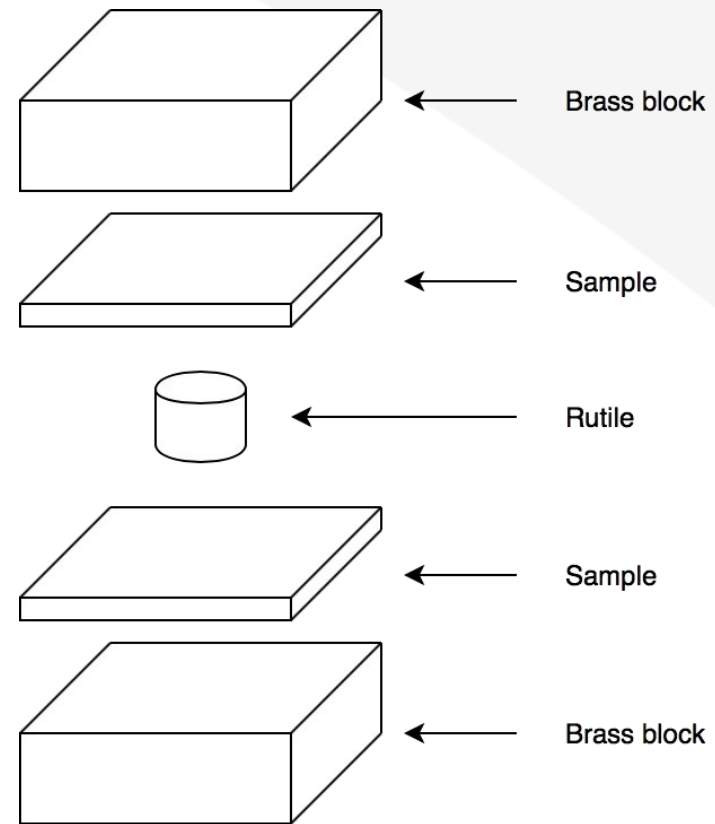
$$R_S = \frac{G_S}{2} \left(\frac{1}{Q_0} - p \cdot \tan(\delta) \right)$$

R_S = Surface resistance

p = Filling factor

G_S = Geometrical factor

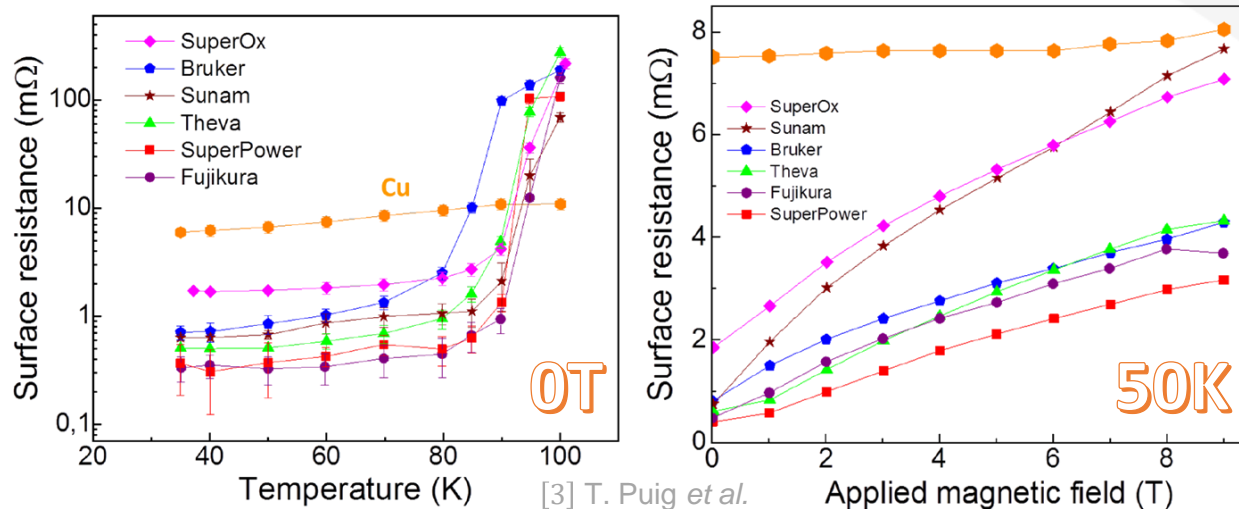
$\tan(\delta)$ = Loss factor



Dielectric Resonator

Surface Resistance

We proved that close to FCC conditions (40-60 K, 8 GHz, 0-9 T), HTS surface resistance is lower than that of copper for most manufacturers.



Surface Resistance

Normal Conductor

vs

Superconductor

$$R_{SCu} \propto \sqrt{f}$$

$$R_{SSC} \propto f^2$$

Surface Current Density

Magnetic Field Amplitude

- Estimated value of the magnetic rf field for the FCC

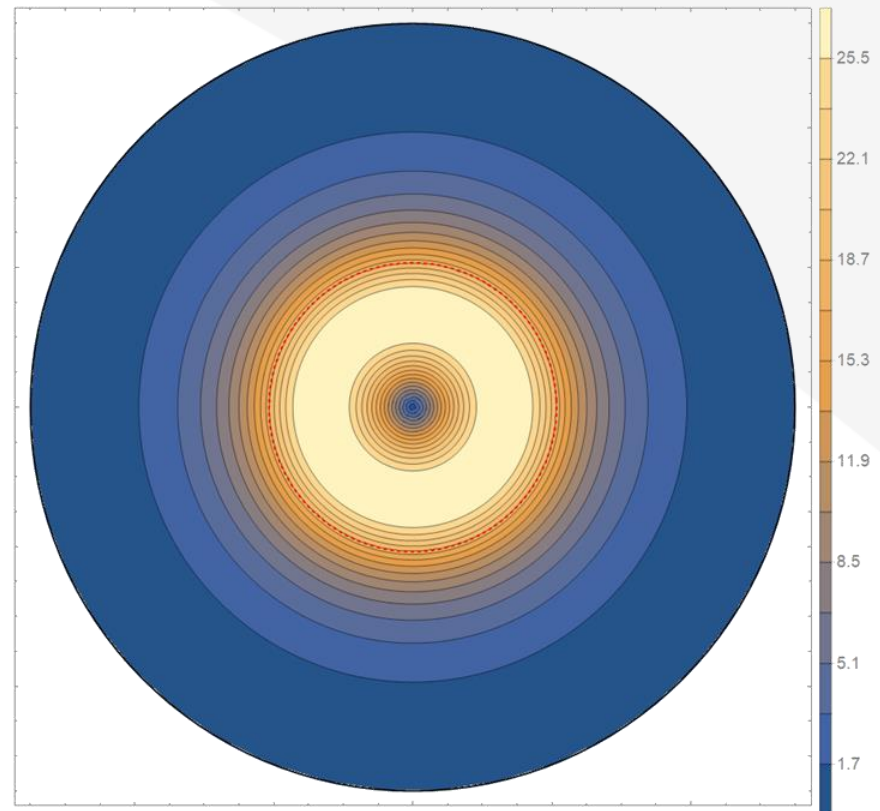
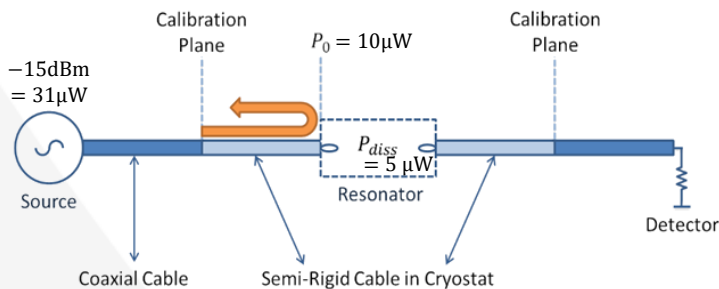
- $H_{max} = 250 \text{ A/m (0.3 mT)}$

- Magnetic field amplitude:

- $A \propto \sqrt{\frac{Q_0 P_{diss}}{\omega_0}}$

$Q_0 = \text{Quality factor}$
 $P_{diss} = \text{Power dissipated}$
 $\omega_0 = \text{Resonant frequency}$

- Experimental set-up and losses



Analytical estimation of the distribution of rf magnetic field strength on a sample in the DR

Surface Current Density

Magnetic Field Amplitude

- Estimated value of the magnetic rf field for the FCC

- $H_{max} = 250 \text{ A/m (0.3 mT)}$

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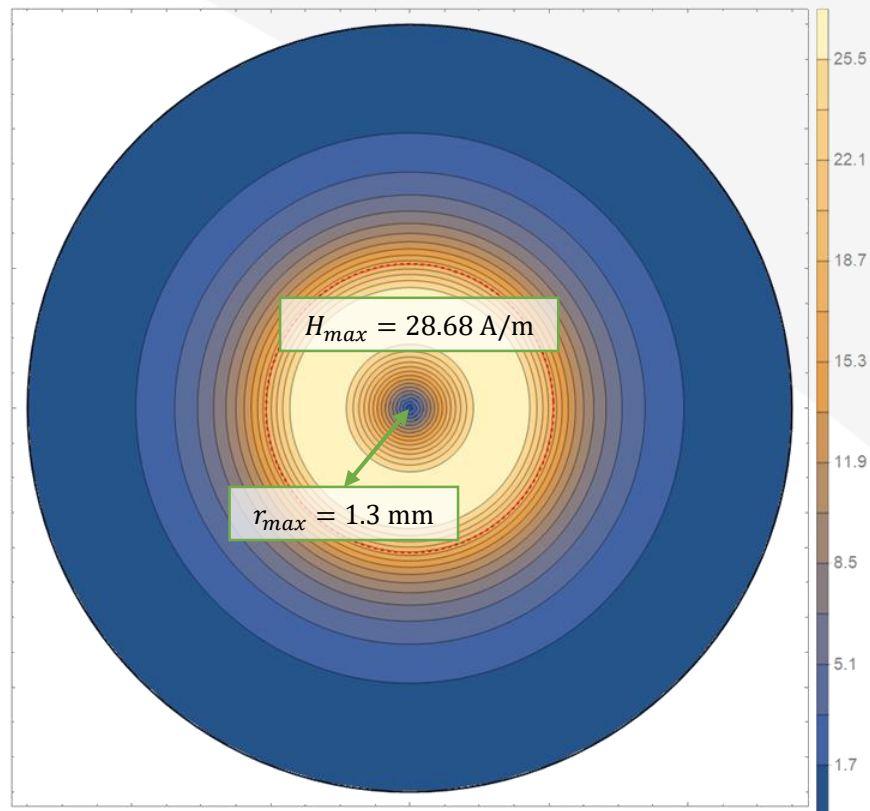
- $A \propto \sqrt{\frac{Q_0 P_{diss}}{\omega_0}}$

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$P_{diss} =$ Power dissipated

$\omega_0 =$ Resonant frequency

Sample	H_{max} (50 K,0T)	H_{max} (50 K,9T)
SuperPower	29 A/m	7 A/m
SuperOx	13 A/m	4 A/m



Analytical estimation of the distribution of rf magnetic field strength on a sample in the DR

Surface Current Density

Magnetic Field Amplitude

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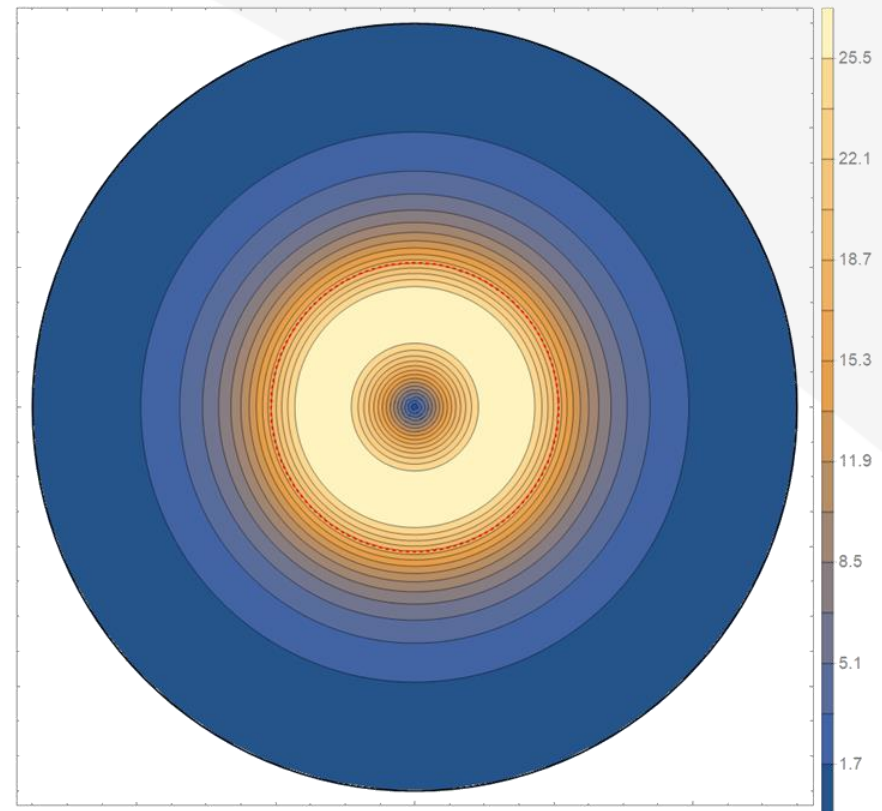
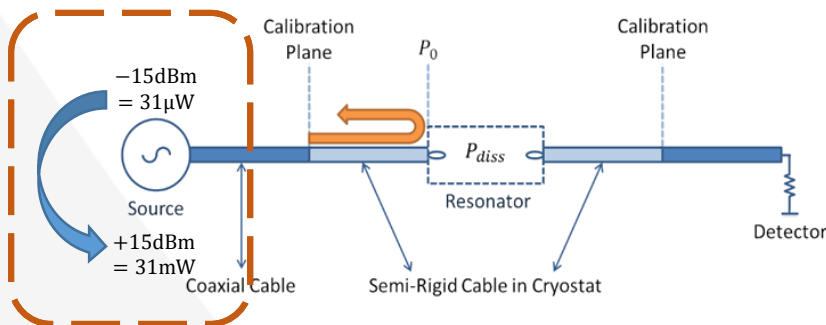
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- Experimental set-up and losses



Analytical estimation of the distribution of rf magnetic field strength on a sample in the DR

Surface Current Density

Power

- Estimated value of the magnetic rf field for the FCC

- $H_{max} = 250 \text{ A/m (0.3 mT)}$

- Magnetic field amplitude:

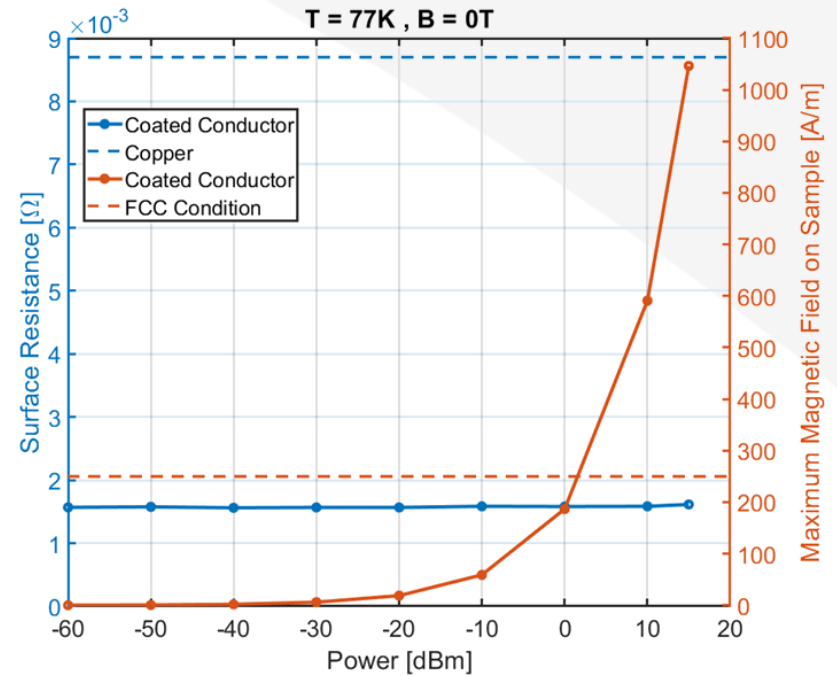
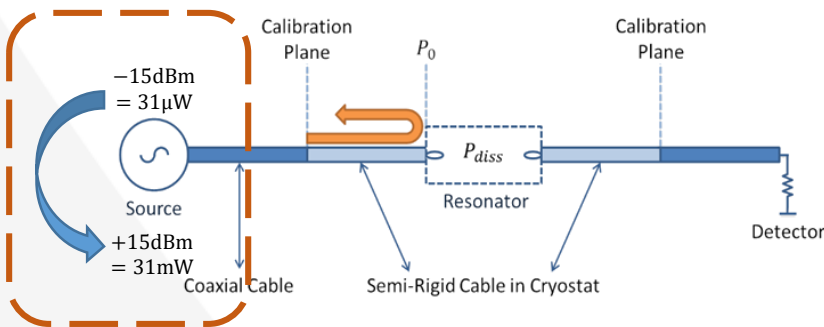
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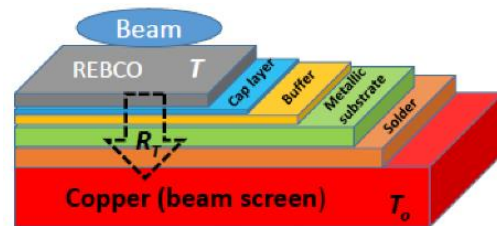
$\omega_0 = \text{Resonant frequency}$

- Experimental set-up and losses



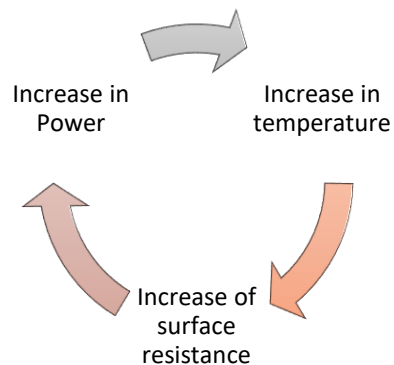
Surface Current Density

Thermal Runaway – R. Vaglio & S. Calatroni



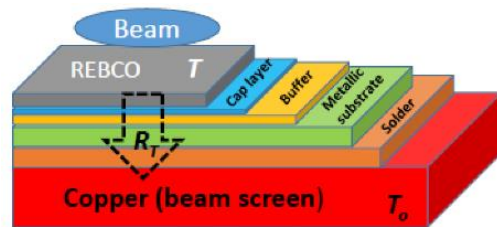
[4] Ruggero Vaglio *et al.*

- Transversal thermal resistance is the sum of individual thermal resistances



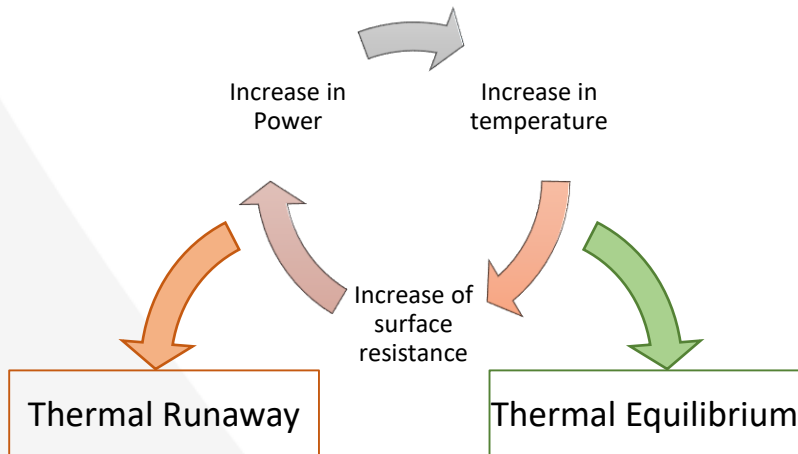
Surface Current Density

Thermal Runaway – R. Vaglio & S. Calatroni



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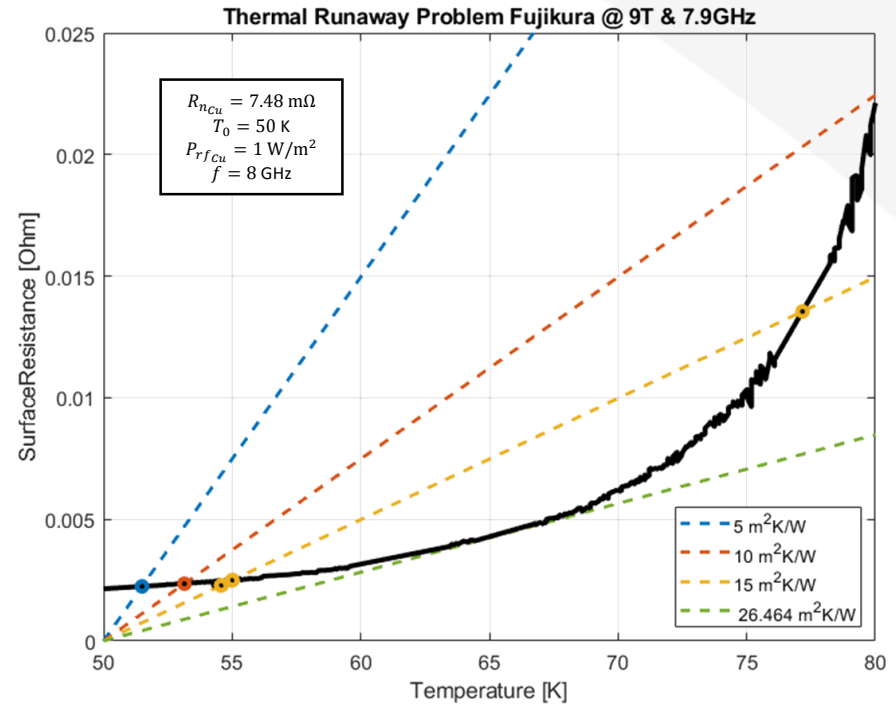
- Linear relationship

$$R_S(f, T) = \frac{T - T_0}{R_T} \frac{R_{nCu}}{P_{rfCu}}$$

$R_S = R_n =$ Surface resistance

$R_T =$ Thermal resistance

$P_{rf} =$ RF power dissipated



Surface Reactance

Magnetic Field

- A perturbation in temperature or/and magnetic field produces a relative change in resonant frequency according to

$$-2 \frac{\Delta f_0}{f_0} = \frac{\Delta X_S}{G_S} + \frac{\Delta X_m}{G_m} + p \frac{\Delta \epsilon_r}{\epsilon_r}$$

[5] Pompeo *et al.*

f_0 = Resonant frequency

X_m = Surface reactance of Brass

X_S = Surface reactance of SC

ϵ_r = Permittivity of dielectric



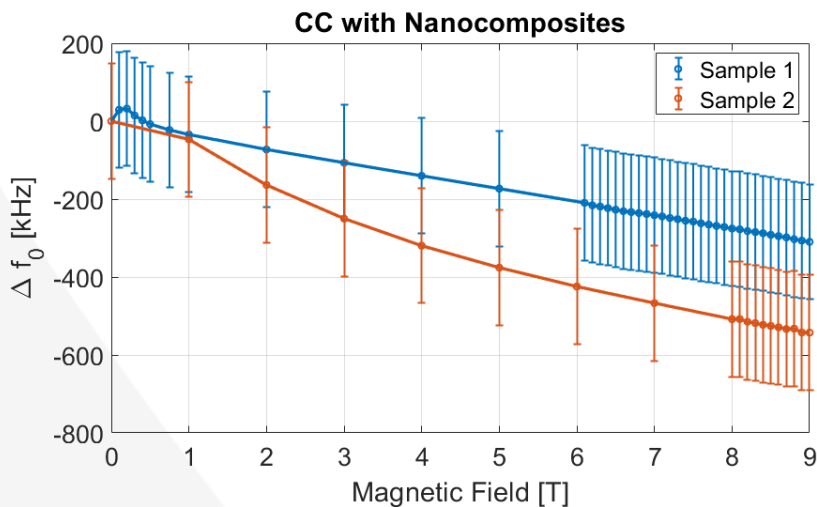
Surface Reactance

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Temperature stability

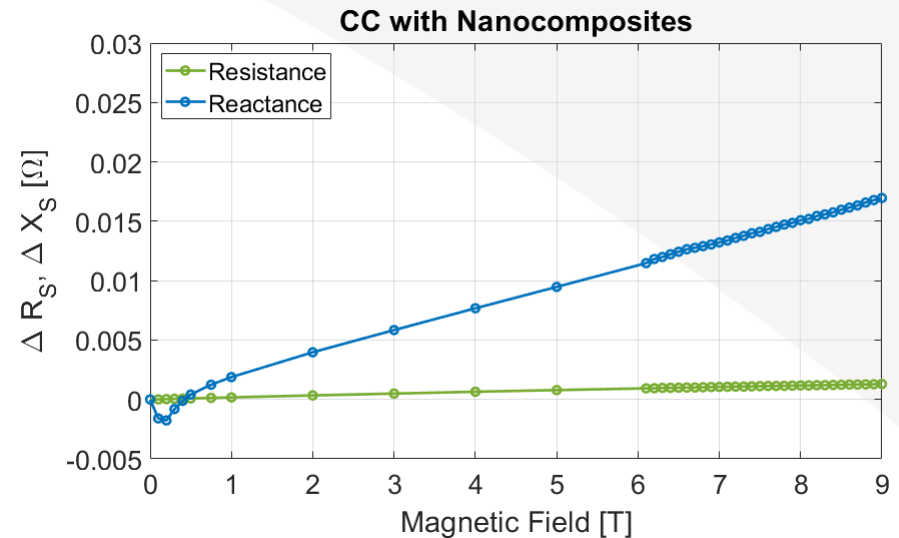
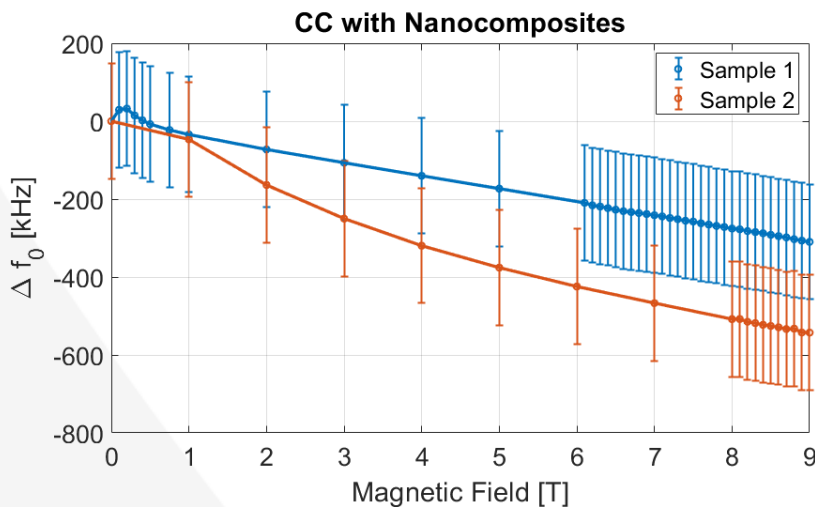


Surface Reactance

Magnetic Field

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- Study the different influences of the real and imaginary part of beam coupling impedance on the beam stability.



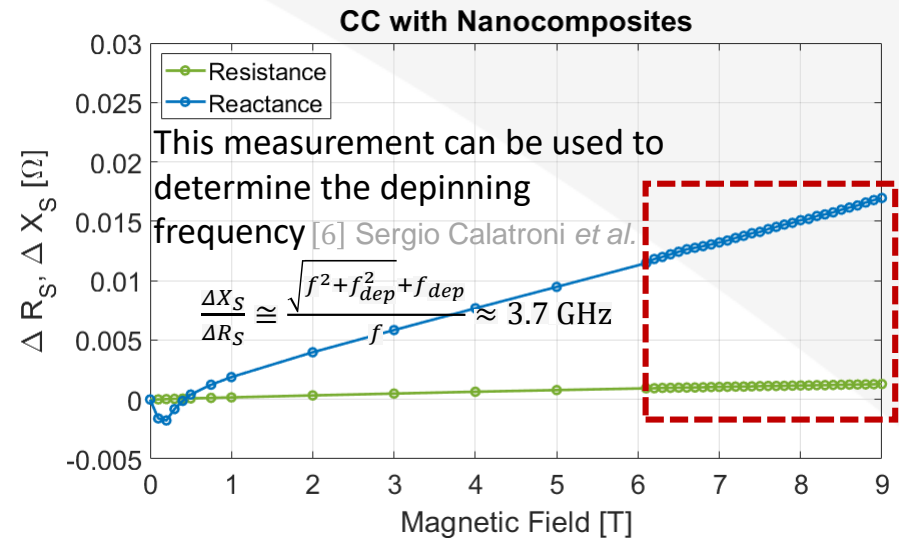
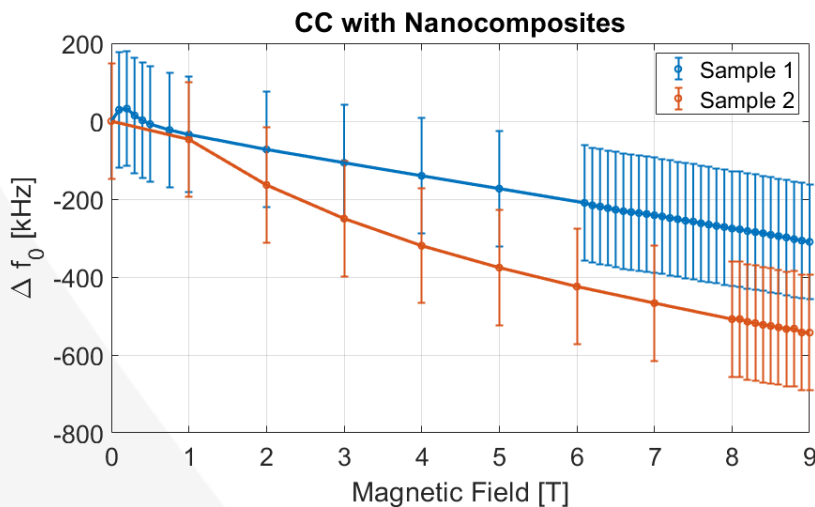
Surface Reactance

Magnetic Field



- A perturbation in temperature or/and magnetic field produces a relative change in resonant frequency according to

$$-2 \frac{\Delta f_0}{f_0} = \frac{\Delta X_S}{G_S} + \frac{\Delta X_m}{G_m} + p \frac{\Delta \epsilon_r}{\epsilon_r}$$



- Study the different influences of the real and imaginary part of beam coupling impedance on the beam stability.

Conclusion & Outlook

- ⌚ Surface Resistance in all samples is significantly lower than that of copper at 8 GHz up to 9 T
- ⌚ RF magnetic field strength on the sample at FCC condition does not significantly change the surface resistance value
- ⌚ Extrapolation to FCC working conditions is favourable for Coated Conductors
- ⌚ First tests showed that the thermal runaway is no problem
 - ✎ Continue studies
- ⌚ Investigation of the depinning frequency
 - Beneficial for surface impedance to operate below depinning frequency
- 🔍 Getting closer to FCC conditions
- 🔍 Improving resonator configurations to lower frequencies, temperature stability
- 🔊 HTS behaviour under synchrotron irradiation
 - ['HTS REBaCuO coated conductors for the FCC-hh beam screen: Performance under photon irradiation at the ALBA Synchrotron Light Source'](#)

References

- [1] [Ignasi Bellafont, Lotta Mether, and Roberto Kersevan ,*Study on the beam induced vacuum effects in the FCC-hh beam vacuum chamber*, FCC Week 2019 – FCC-hh accelerator](#)
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- [3] T. Puig et al. ,*Coated Conductor technology for the beam screen chamber of future energy circular colliders*, SUST, to be published.
- [4] R. Vaglio and S. Calatroni ,*Advances in the study of HTS Superconductors for the Beam Impedance Mitigation in CERN-FCC : The thermal runaway problem*, Eur. Phys. J. Special Topics, 2018, to be published.
- [5] [N. Pompeo, K. Torokhtii, and E. Silva ,*Dielectric Resonators for the Measurements of the Surface Impedance of Superconducting Films*, Measurement Science Review, Volume 14, No 3, 2014.](#)
- [6] [S. Calatroni and R. Vaglio ,*Surface Resistance of Superconductors in the Presence of a DC Magnetic Field: Frequency and Field Intensity Limits*, IEEE Transactions on Applied Superconductivity, Vol. 27, No 5, 2017.](#)