

16 T dipole magnet quench protection

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and Marco Prioli

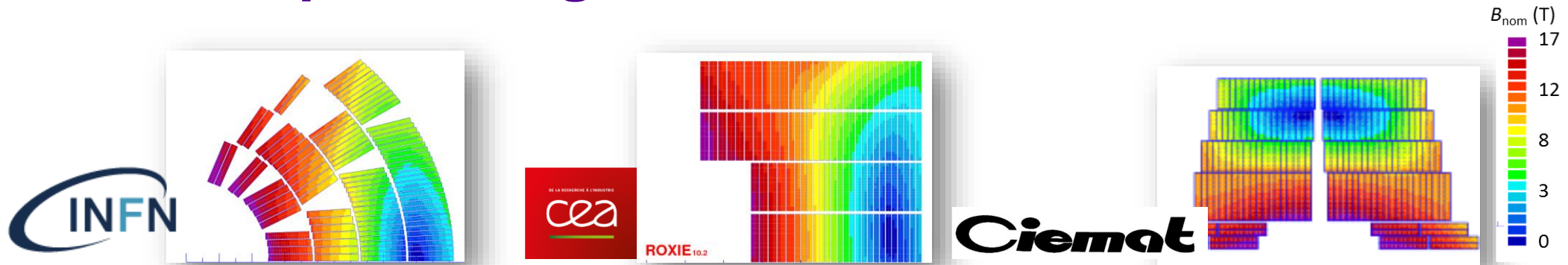
with the EuroCirCol WP5 members

and support from the **STEAM** team at CERN TE-MPE-PE



FCC week 2019, Brussels, 27th June 2019

EuroCirCol 16 T dipole designs*



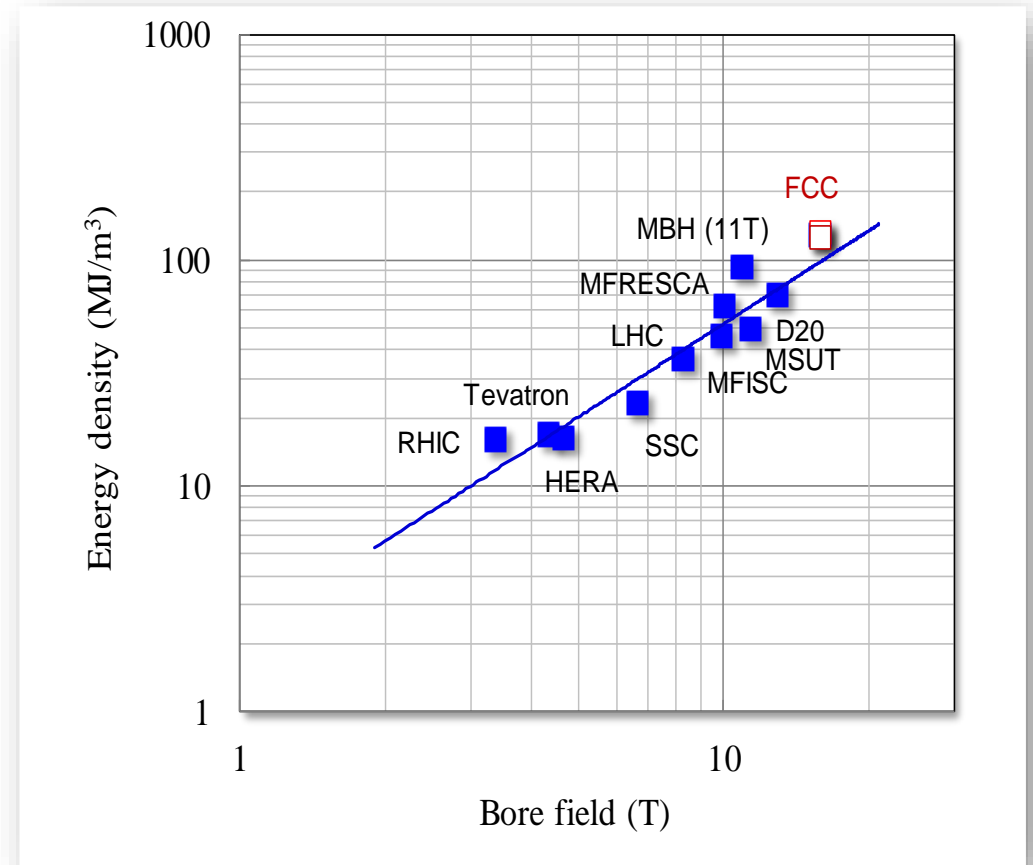
Magnet, version	Cos θ , 22b_38_v1		Block, V2ari204		Common coil, vh12_2ac6	
Inom (A)	11390		10111		16400	
Ld,nom (mH/m)	2 x 19.8		2 x 24.8		21.1	
Cable	HF-cable	LF-cable	HF-cable	LF-cable	HF-cable	LF-cable
Cable $w \times t$ (bare) (mm)	13.2 x 1.95	14.0 x 1.265	12.6 x 2.0	12.6 x 1.27	19.2 x 2.2	12.0 x 2.2
Number of strands	22	38	21	34	30	18
Strand diam. (mm)	1.1	0.7	1.1	0.7	1.2	1.2
Cu/SC	0.82	2.1	0.8	2.0	1.0	2.5

Cable ins. : 0.15 mm, RRR = 100, filament twist = 14 mm, strand twist= 15°

Jc with Bordini fit: $T_{c0} = 16$ K, $B_{c20} = 29.38$ T, $\alpha = 0.96$, $C_0 = 267845$ A/mm²T

Outline

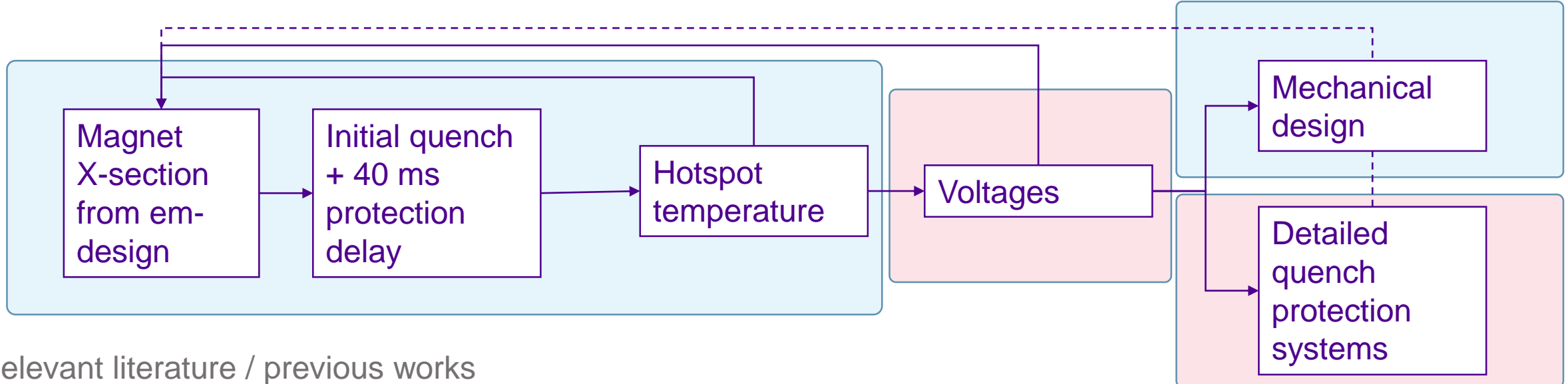
1. Ensuring magnet protectability
2. Simulation tools
3. Conceptual quench protection schemes:
 - CLIQ - Coupling Loss Induced Quench
 - QH - Quench heaters
4. Simulated temperatures and voltages after quench
 - Comparison of CLIQ and QH
5. Conclusions



*Stored energy density in dipoles vs. peak field,
by courtesy of L. Bottura and D. Schoerling*

1. Ensuring magnet *protectability*

- Protetability with a real quench protection system (CLIQ or QH)
- Safe limit of temperature and voltages: **350 K**, **2.5 kV** in circuit, **1.2 kV** in single magnet
- **A simplified quench analysis for fast-feedback – The EuroCirCol protectability criterion**
 - Assume a protection system quenches the entire magnet 40 ms after initial quench
 - **20 ms det + 20 ms QH/CLIQ**
 - At 105% of Inom



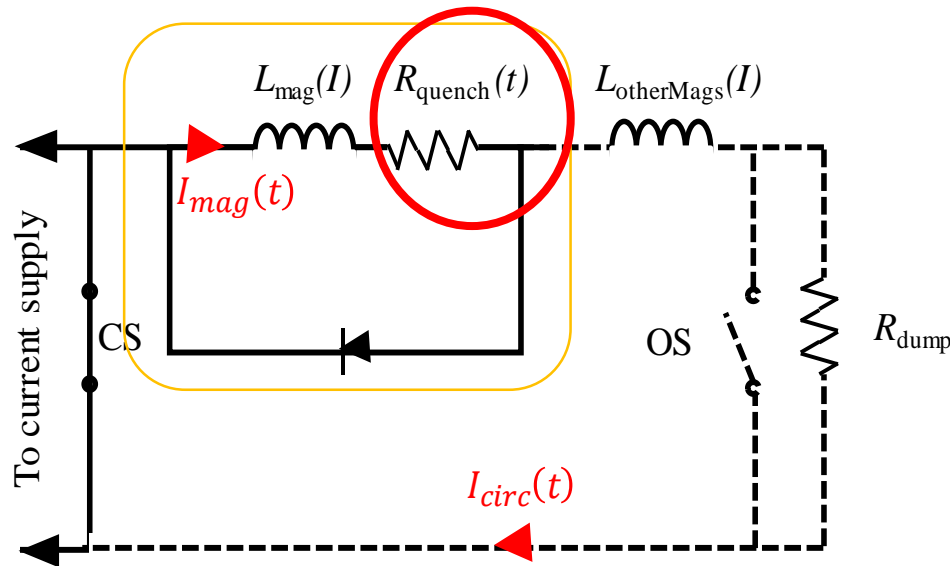
Relevant literature / previous works

E. Todesco, Proc. WAMSDO 2013
G. Amborsio, Proc. WAMSDO 2013

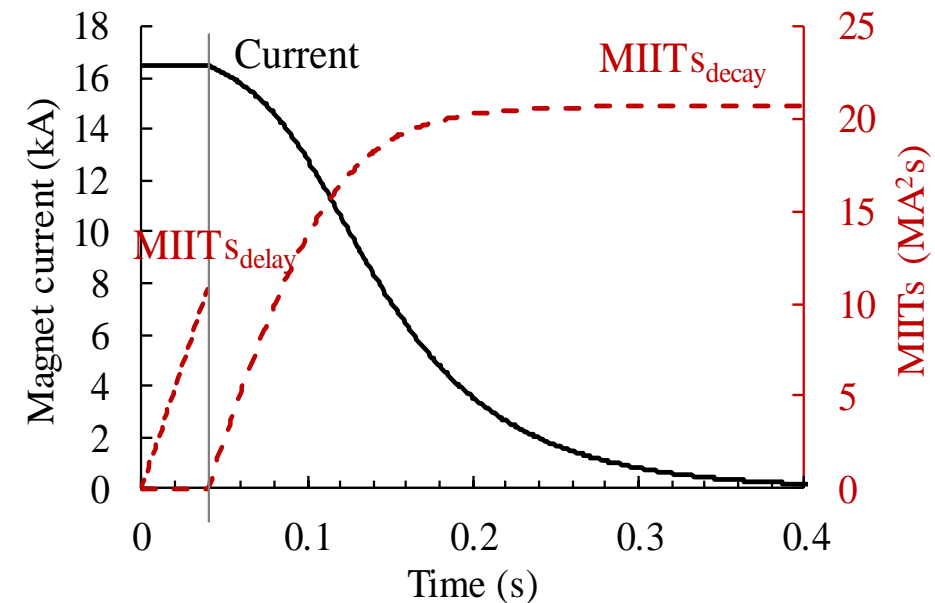
2. Simulation tools

What did we simulate?

- Initial quench and 20 ms detection time with constant current (incl. validation time etc.)
- Coil heating and evolution of normal zones after protection activation (IFCC or CLIQ, or heat from heaters)
- Coil temperature and resistance increase \rightarrow current decay
- Post-process for voltage distribution



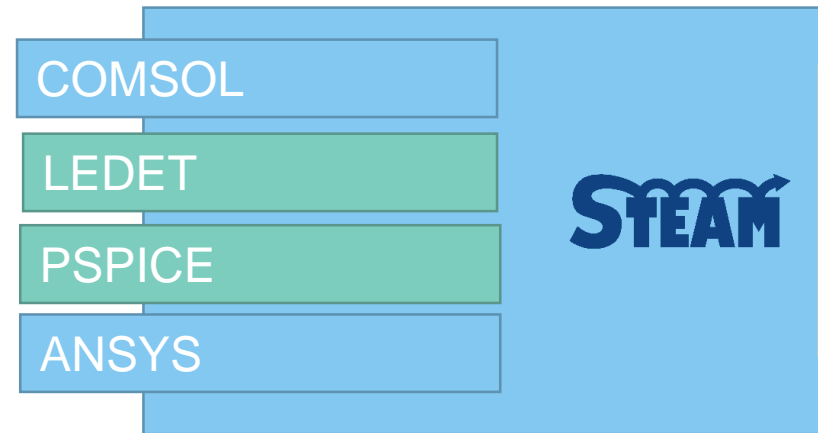
Magnet powering circuit in accelerator



Analysis of MIITs separately before and after quench detection

How did we simulate?

- Initial analysis with 40 ms uniform quench delay:
 - 0 D thermal
- CLIQ design
 - Analytical equations for IFCC
 - Thermal diffusion between turns
- QH design
 - 2D heat transfer model for heater delay
 - Adiabatic thermal based on heater delays and given NZPVs
- Internal voltages with a circuit model
- Profit from tools already used in magnet design for magnetic field, inductance and mechanical modeling



More details and references in appendix!

T. Salmi et al., PRAB 20, 032401
T. Salmi et al., *IEEE TAS*, 26(4), 2016

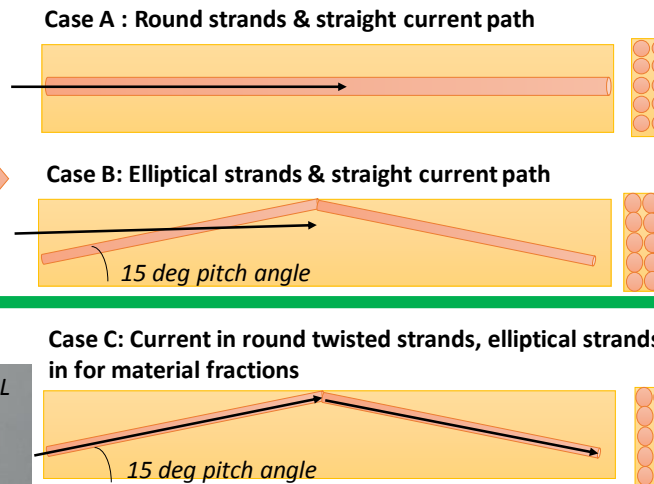
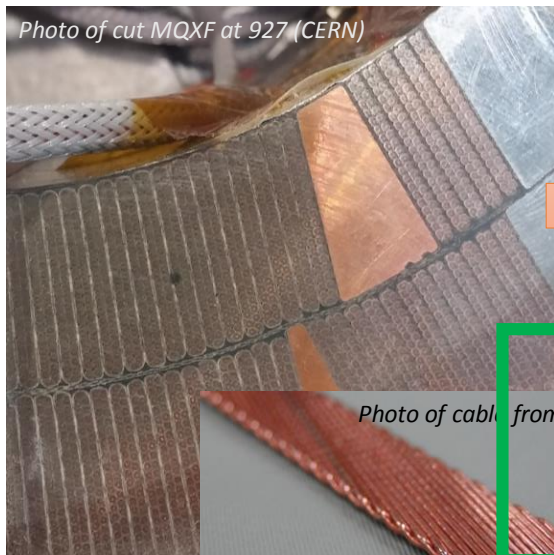
STEAM: Website: <https://espace.cern.ch/steam>
L. Bortot, et al., *IEEE TAS*, 28(3), 2018.
E. Ravaoli, et al., *Cryogenics*, 2016.
L. Bortot et al., *IEEE TAS*, 27(4), 2017.
I. C. Garcia et al *IEEE J. on Multiscale and Multiphysics Comp. Techn.*, 2017.

T. Salmi et al, *IEEE TAS*, 24(4), 2014.

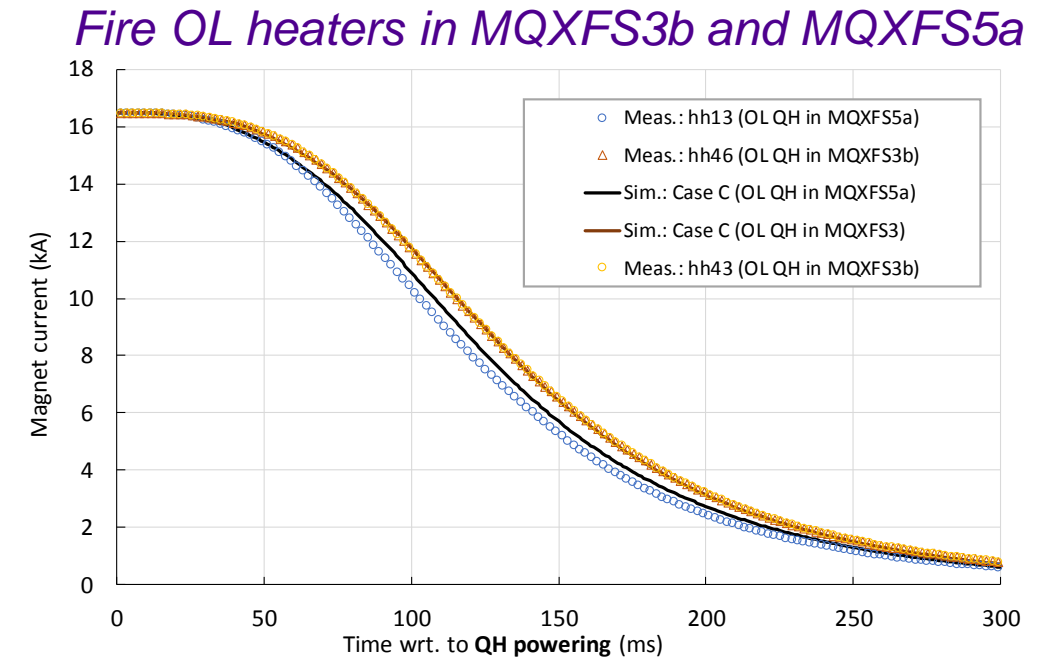
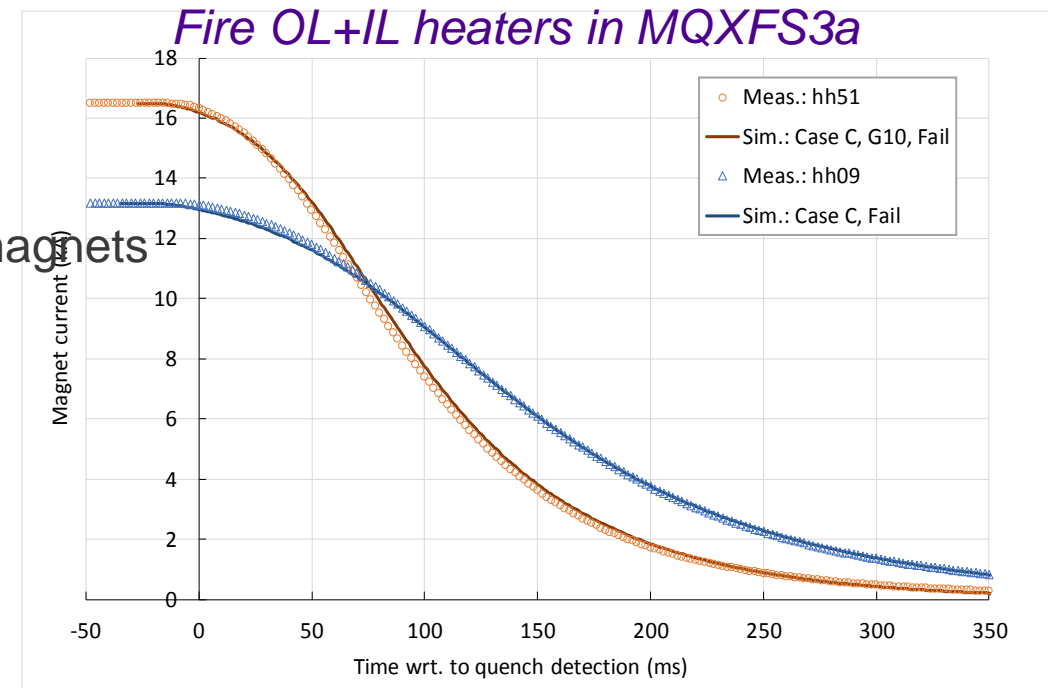
Model validation

- LEDET and CoHDA previously validated with HL-LHC model magnets
- Coodi validated during the time of project
 - Helped to adjust cable simulation method
- Validations mainly are comparison of current decays

Three different cases on cable modeling assumptions.



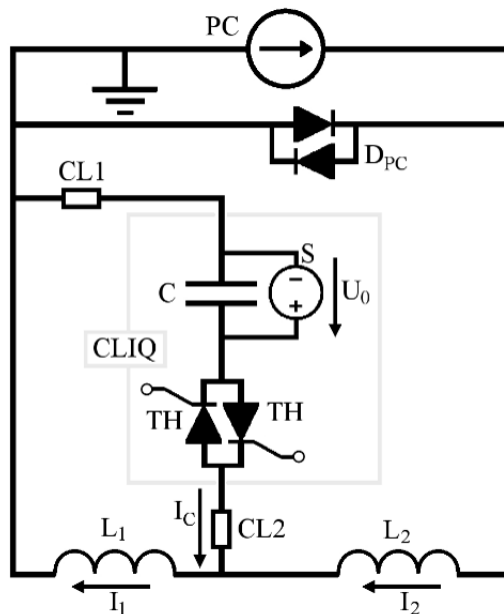
Best match with experimental data



3. Conceptual quench protection schemes

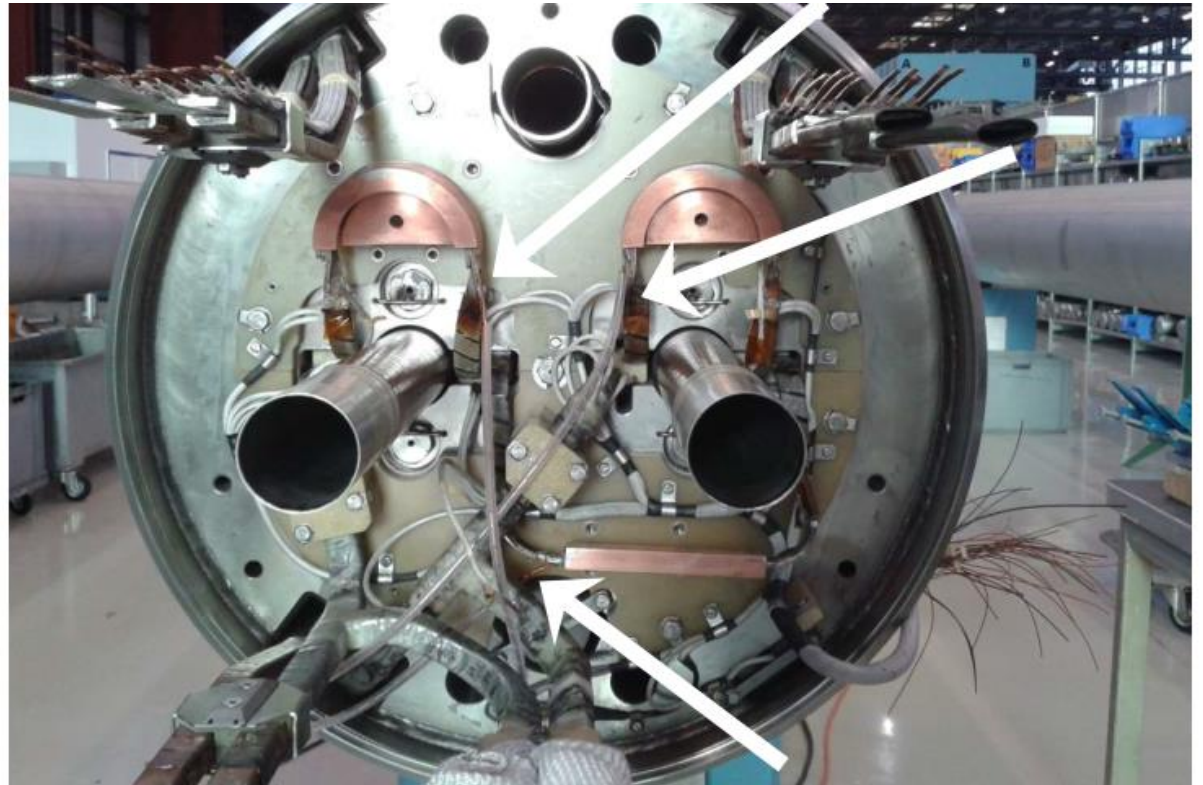
CLIQ – Coupling-Loss Induced Quench

- Discharge capacitor bank across part of the winding
 - ➔ Oscillations of transport current
 - ➔ Coupling losses in strands ➔ Quench



New technology with advantages:

- Connections external to the magnet ➔ Accessible

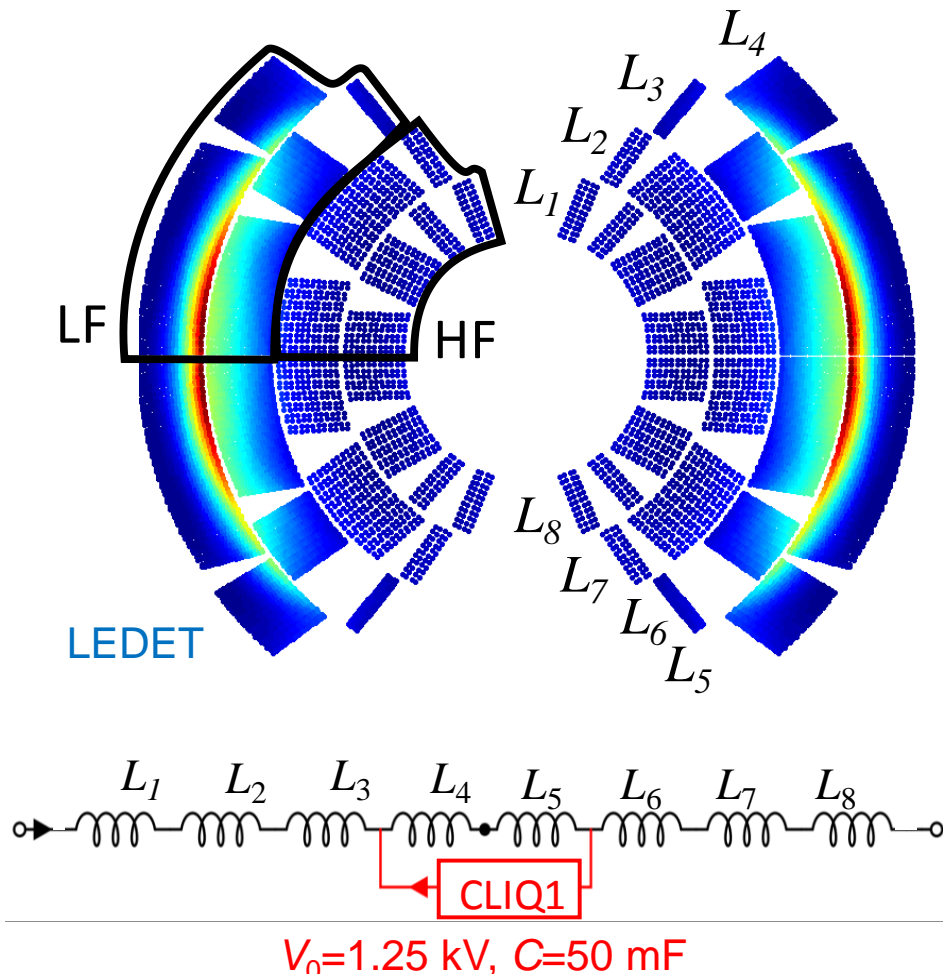


*CLIQ leads in the 15 m long LHC main dipole (Aug 2015),
Photo by courtesy of E. Ravaoli*

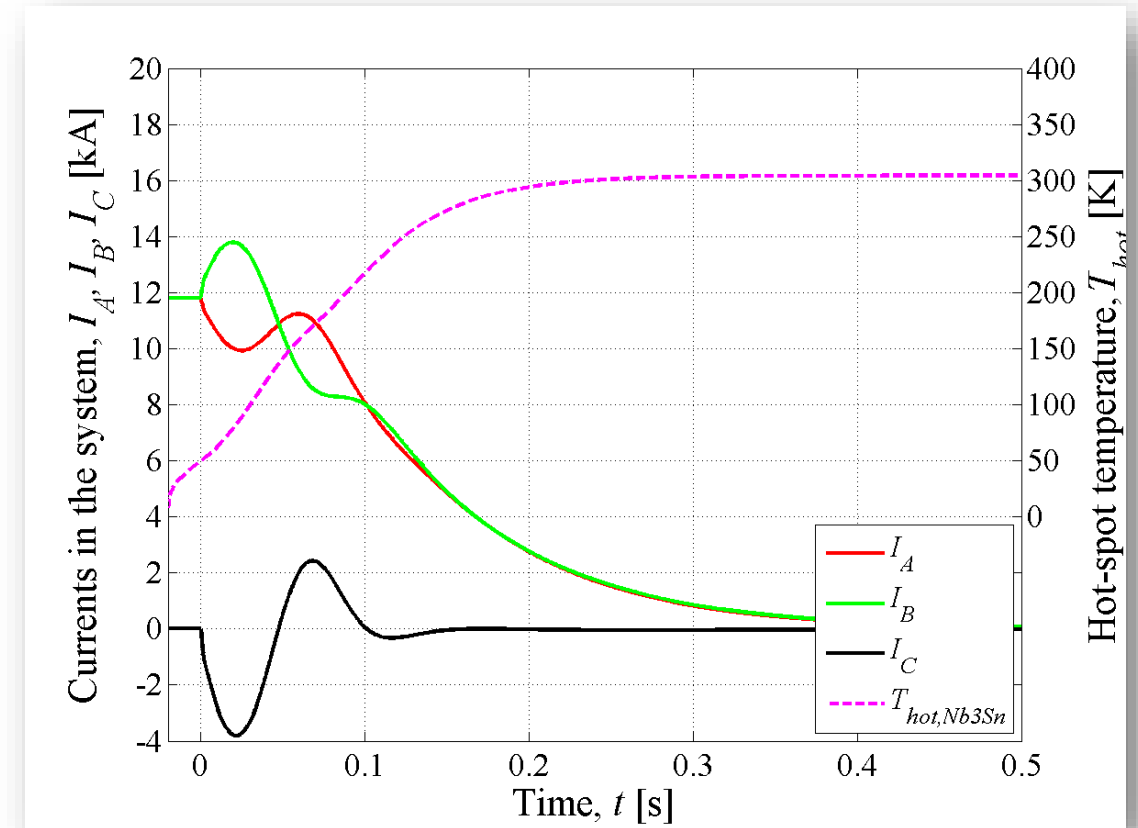
Design of CLIQ-based protection: $\cos\theta$

M. Prioli et al., "The CLIQ quench protection system applied to the 16 T FCC-hh dipole magnets", *IEEE TAS* (under review)
 T. Salmi et al., *IEEE TAS*, 29(5), 2019, 4700905.
 T. Salmi et al., *IEEE TAS*, 27(4), 2017, 4702305.
 J. Zhao et al., *Physica C: Supercond. and Applic.*, 550, 2018, 27.

Connection of CLIQ units and the charging voltage and capacitance

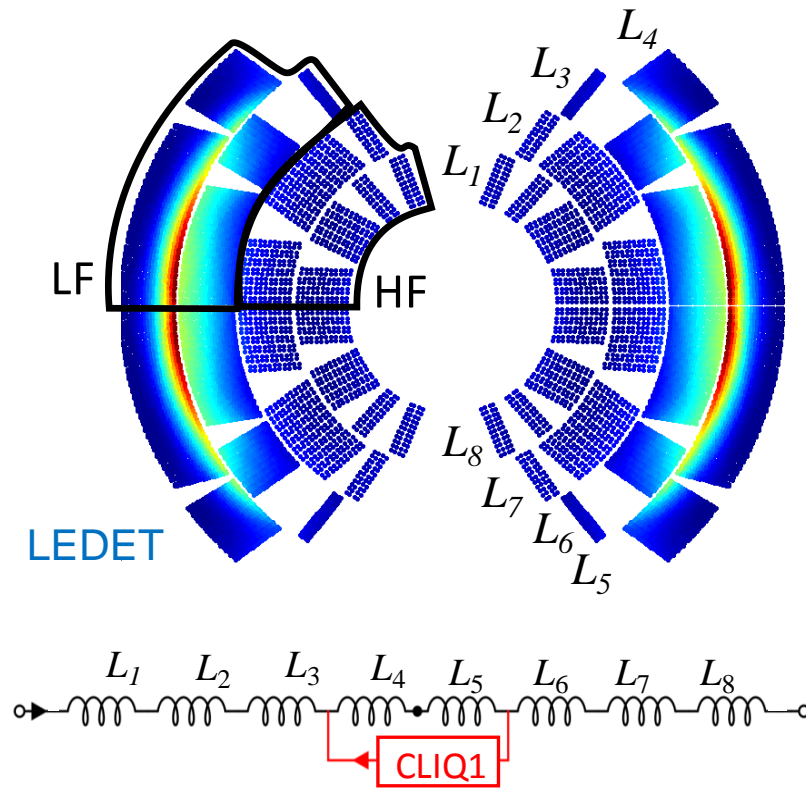


Resulting current oscillations



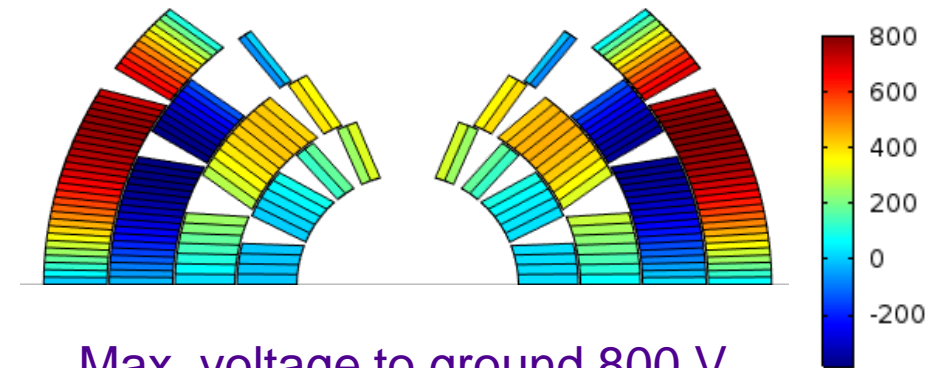
(Example case at 105% I_{nom})

Design of CLIQ-based protection: $\cos\theta$



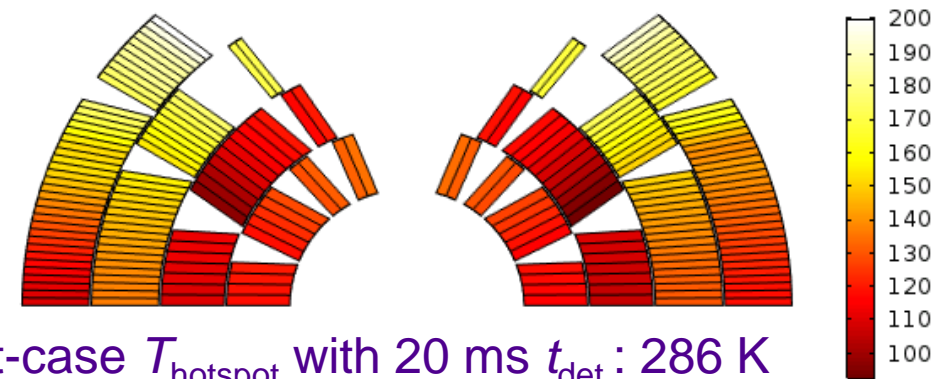
Mechanical stress after quench and protection in part of the circuit, see:

Voltage distribution 120 ms after CLIQ activation



Max. voltage to ground 800 V

Final temperature distribution after CLIQ activation

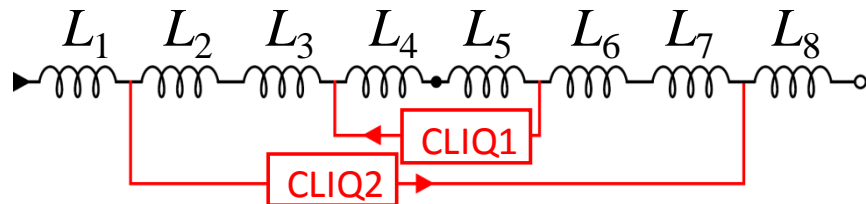
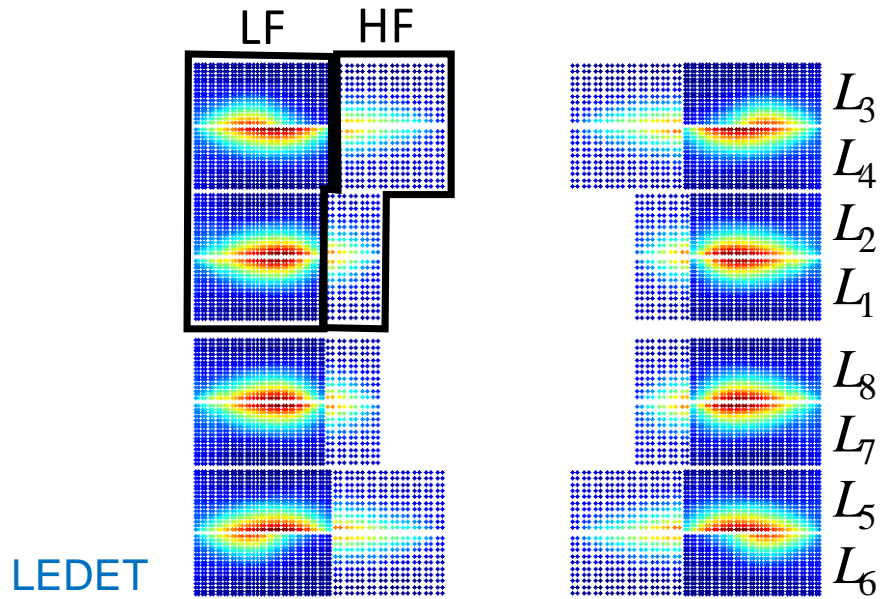


Worst-case T_{hotspot} with 20 ms t_{det} : 286 K

M. Prioli et al., "The CLIQ quench protection system applied to the 16 T FCC-hh dipole magnets", *IEEE TAS (under review)*

M. Prioli et al., "Conceptual design of the FCC-hh dipole circuits with integrated CLIQ protection system", *IEEE TAS (accepted for publication)*

Block

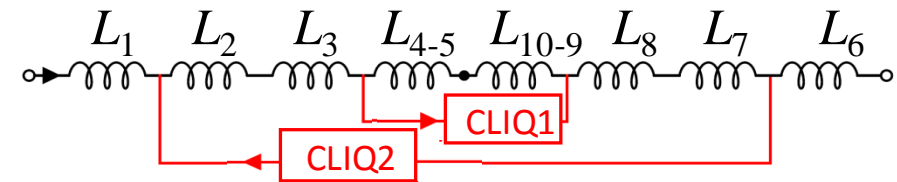
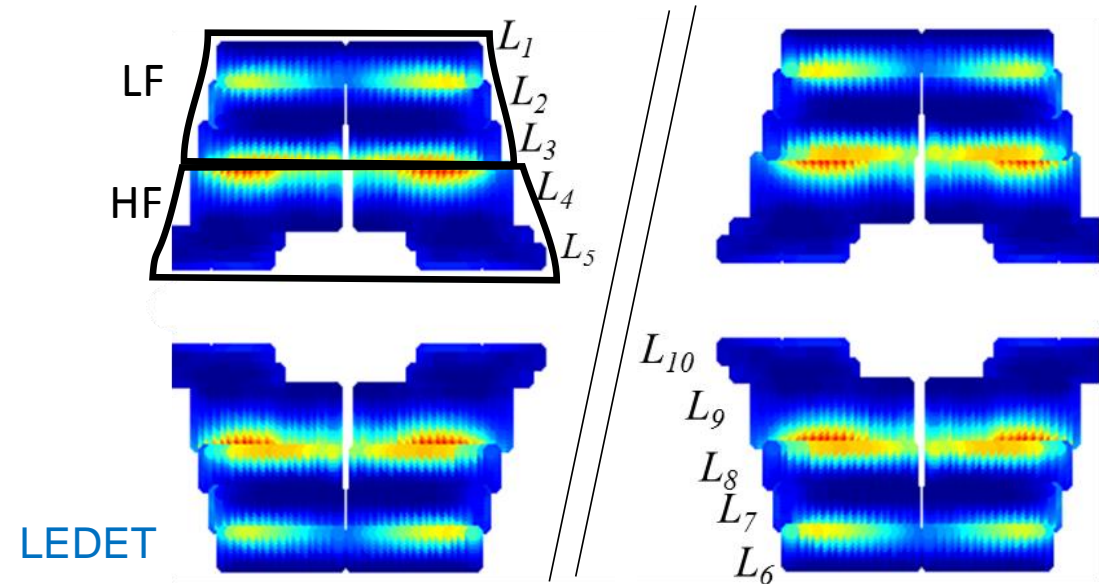


CLIQ1: $V_0=0.6$ kV, $C=50$ mF
 CLIQ2: $V_0=1.2$ kV, $C=50$ mF

COMSOL simulation by M. Prioli:

Hot-spot temperature 286 K
 Max. voltage to ground 0.7 kV

Common-coil

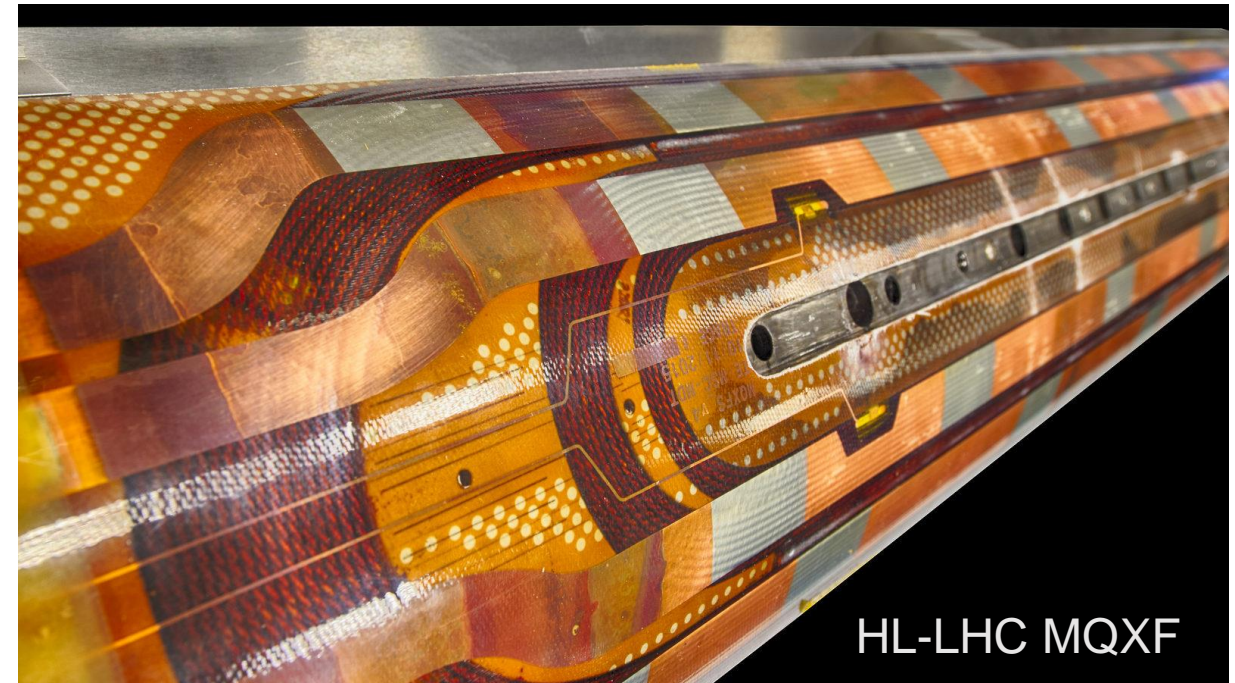
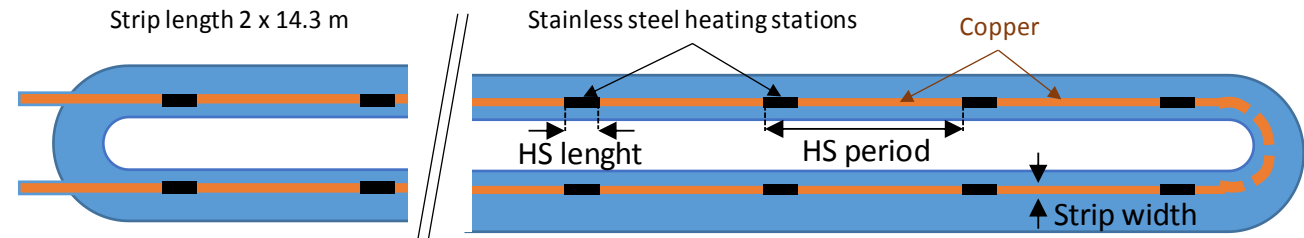


CLIQ1,2: $V_0=0.9$ kV, $C=80$ mF

Hot-spot temperature 284 K
 Max. voltage to ground 1.1 kV

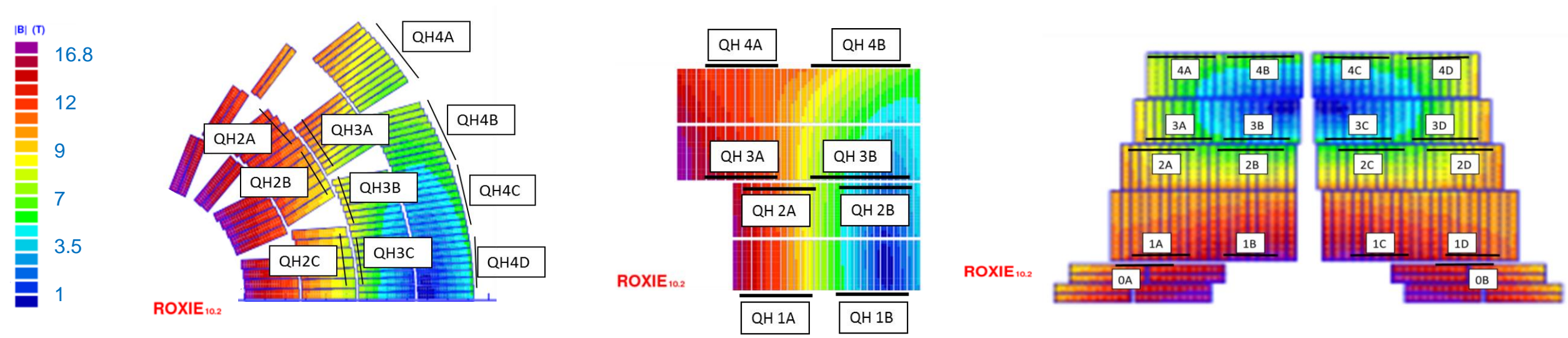
QH – Quench heaters

- Similar technology than in LHC and HL-LHC:
 - Cu-plated stainless steel strips:
 - SS thickn. 25 μm , Cu thickn. 10 μm
 - Insulation to coil: 75 μm polyimide
- Powering with capacitor bank discharge:
 - Heater Firing Unit (HFU): 1.2 kV and 10 mF (LHC: 900 V and 7 mF)
 - 1 Ω for wires etc. / circuit



F. Rodriguez-Mateos and F. Sonneman, "Quench heater studies for the LHC magnets", Proc. of PAC, 2001.
 H. Felice et al., "Instrumentation and Quench Protection for LARP Nb3Sn Magnets", *IEEE TAS*, 19(3), 2009.³ P. Ferracin et al, "Development of MQXF, the Nb3Sn Low- β Quadrupole for the HiLumi LHC ", *IEEE TAS*, 26(4), 2016.

Locations of heater strips



Strip geometry and powering

	Cosθ		Block				Common-coil	
	QH2-3	QH4	QH1-2 HF	QH1-2 LF	QH3-4 HF	QH3-4 LF	QH0-1	QH2-4
w _{strips} (cm)	1	1.3	1.9	1.8	2.1	2.4	1.5	1.75
HS/per. (cm)	4 / 18	6 / 30	5/22	6/30	5/35	6/30	4/19	6/31
P _{QH,t=0} (W/cm ²)	100	150	100	130	100	110	90	140
T _{RC} (ms)	40	50	40	40	20	30	30	40

4. Simulated peak temperatures and voltages

Operation at nominal current

	T_{Hotspot} (K) with 20 ms detection time		V_{gnd} (V)		$N_{\text{Units/magnet}}$	
	CLIQ	QH	CLIQ	QH	CLIQ	QH
Cos θ	286	322	800	870	2	14
Block	281	321	730	870	4	13
C-c	284	330	1100	1040	2	15



- Magnets can be protected with both systems
- 40±5 K lower temperature with CLIQ
- Voltages quite similar
- Simpler system with CLIQ



CLIQ was selected as a baseline, heaters a back-up option

Conclusion

- Quench protection integrated in the magnet em-design to ensure protectable magnets
 - 40 ms/350 K criteria
- Several simulation tools developed for the fast-feedback during initial design, and for the detailed protection designs
- **Protection with CLIQ feasible for all magnet options**
 - Max temperatures below 300 K at nominal current
 - Internal voltages below 1200 V
- Protection with heaters is considered a back-up option
- Experiments with the demo magnets needed to validate the simulation results and adjust designs
- Success is thanks to successful collaboration and communication between the magnet design teams in INFN, CEA and CIEMAT and quench protection teams at TAU and CERN, and project coordination → A winning team!

Thank you!

Appendix

Simulation tools and assumptions 1/2

Common assumptions in all simulations:

- Adiab. Hotspot temperature
- Current decay simulated in 2-D, discretized at turn level
- Material properties based on NIST libraries
- Material properties based on cable average magnetic field
- Tcs for quench computed based on the cable peak field
- Hotspot computed for the worst case cable
- 20 ms detection delay

- **"40 ms delay"**:
 - Coodi: Adiabatic model for current decay, temperature, and voltage computation (no heat diffusion between turns)
 - Quench time and propagation for each turn is an input
 - No AC (interfilament coupling loss)
 - Current follows the strand path after quench
- T. Salmi et al., "Quench protection analysis integrated in the design of dipoles for the Future Circular Collider", *Phys. Rev. Accel. Beams* 20, 032401
- T. Salmi et al., "The Impact of Protection Heater Delays Distribution on the Hotspot Temperature in a High-Field Accelerator Magnet", *IEEE TAS*, 26(4), 2016.

Simulation tools and assumptions 2/2

STEAM

- **CLIQ studies:**
 - LEDET: Lumped element model for interfilament coupling loss after CLIQ activation
 - Current decay, temperature and voltage evolution
 - Co-simulation used to couple with PSPICE for asymmetric multi-CLIQ simulations
 - COMSOL: FEM for electrothermal behaviour after CLIQ discharge
 - Heat diffusion between turns accounted
- E. Ravaioli, PhD Thesis
- E. Ravaioli, B. Auchmann, M. Maciejewski, H. ten Kate, and A. Verweij, "Lumped-element dynamic electro-thermal model of a superconducting magnet," Cryogenics, 2016.
- L. Bortot et al., "A consistent simulation of electrothermal transients in accelerator circuits," IEEE TAS, 27(4), 2017.
- I. C. Garcia et al., "Optimized field/circuit coupling for the simulation of quenches in superconducting magnets," IEEE Journal on Multiscale and Multiphysics Computational Techniques, 2017.
- STEAM: Simulation of Transient Effects in Accelerator Magnets. Website: <https://espace.cern.ch/steam/>, Accessed on Sep 28, 2018)
- L. Bortot, et al., "STEAM: A Hierarchical Cosimulation Framework for Superconducting Accelerator Magnet Circuits, IEEE Trans. Appl. Supercond., 28 3, 4900706, 2018.
- **Heater based protection:**
 - CoHDA: 2-D heat diffusion model for heater delays
 - Accounts for the heater station length
 - Quench when cable maximum temperature reaches T_{cs}
- T. Salmi et al., "A Novel Computer Code for Modeling Quench Protection Heaters in High-Field Nb_3Sn Accelerator Magnets", IEEE TAS, 24(4), 2014.
- T. Salmi et al., "Analysis of uncertainties in protection heater delay time measurements and simulations in Nb_3Sn high-field accelerator magnets" IEEE TAS, 25(4), 2015.
 - Coodi: Current decay when heater delay and quench propagation velocity are input for each turn
 - Quench propagation: 18 m/s btw heating stations, 11 ms btw turns, 20 ms btw layers at nominal current