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Large cryogenic process cycle modeling

Helmholtz-energy-explicit models for fluid mixtures

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Objectives

- Model the thermal properties of mixtures
 - helium-neon
 - neon-argon
 - helium-argon
- Validate the mixture model with existing Brayton / J-T cycle
- Study the process cycles with large cryogenic installations

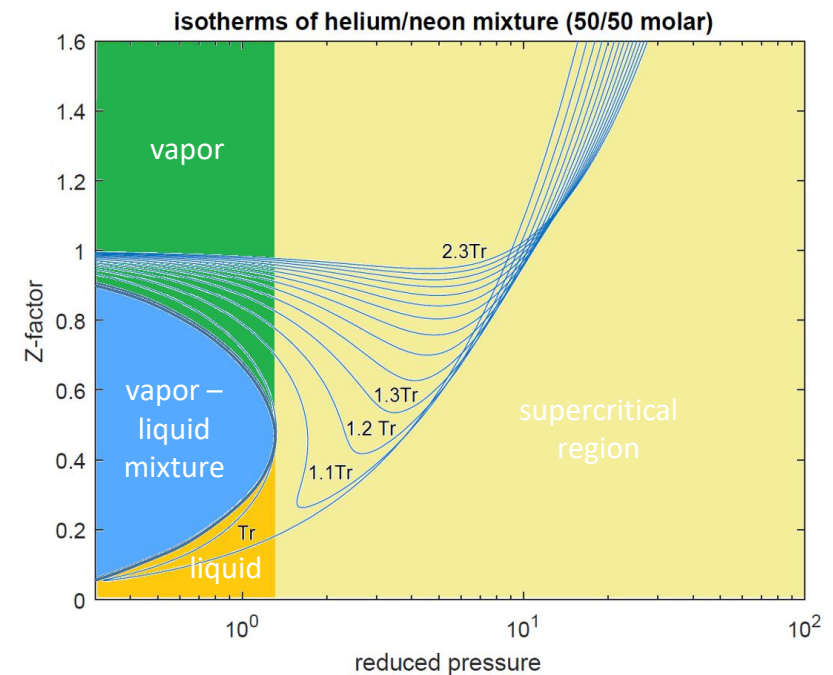
- Van der Waals:
$$p = \frac{RT}{(v - b)} - \frac{a}{v^2}$$
- Virial expansion:
$$\frac{pv}{RT} = Z = 1 + B(T)\rho + C(T)\rho^2 + D(T)\rho^3 + \dots$$
- Peng-Robinson:
$$p = \frac{RT}{v - b} - \frac{a}{v^2 + 2bv - b^2}$$
- Helmholtz energy:
$$\alpha(\delta, \tau, \bar{x}) = \alpha^0(\rho, T, \bar{x}) + \alpha^r(\delta, \tau, \bar{x})$$

$$\rho_N k_B T \alpha = U - TS$$

Potential that measures the useful work obtainable from a closed thermodynamic cycle

Advantages

- Continuous over liquid/vapor boundary
- It is a function of measurable properties
- Purely analytical derivatives



Helmholtz energy formulation

$$\delta = \frac{\rho}{\rho_r}, \tau = \frac{T_r}{T}$$

$$\frac{a(\rho, T)}{RT} = \alpha(\delta, \tau) = \alpha^o(\delta, \tau) + \alpha^r(\delta, \tau)$$

Ideal Helmholtz free energy

Residual Helmholtz free energy

$$\alpha^o(\delta, \tau) = \frac{h_o^o \tau}{RT_r} - \frac{s_o^o}{R} - 1 + \ln \frac{\delta \tau_o}{\delta_o \tau} + \frac{\tau}{R} c_p^o \left(\frac{1}{\tau} - \frac{1}{\tau_o} \right) + \frac{c_p^o}{R} \ln \frac{\tau}{\tau_o}$$

$$\alpha^r(\delta, \tau) = \sum_{k=1}^{I_{pol}} N_k \delta^{d_k} \tau^{t_k} + \sum_{k=I_{pol}+1}^{I_{pol}+I_{exp}} N_k \delta^{d_k} \tau^{t_k} \exp(-\delta^{l_k}) +$$

$$\sum_{k=I_{pol}+I_{exp}+1}^{I_{pol}+I_{exp}+I_{crit}} N_k \delta^{d_k} \tau^{t_k} \exp\left(-\eta_k(\delta - \eta)^2 - \beta_k(\tau - \gamma_k)^2\right)$$

pure fluid
mixtures

Ideal Helmholtz free energy

$$\alpha^o(\rho, T, \bar{x}) = \sum_{i=1}^N x_i \left[\alpha_{oi}^o(\rho, T) + \ln x_i \right]$$

Residual Helmholtz free energy

$$\alpha^r(\delta, \tau, \bar{x}) = \sum_{i=1}^N x_i \alpha_{oi}^r(\delta, \tau) + \sum_{i=1}^{N-1} \sum_{j=i+1}^N x_i x_j F_{ij} \alpha_{ij}^r(\delta, \tau)$$

Reducing variables

$$\frac{1}{\rho_r(x)} = \sum_{i=1}^N \frac{x_i^2}{\rho_{c,i}} + \sum_{i=1}^{N-1} \sum_{j=i+1}^N 2x_i x_j \beta_{v,ij} \gamma_{v,ij} \frac{x_i + x_j}{\beta_{v,ij}^2 x_i + x_j} \frac{1}{8} \left(\frac{1}{\rho_{c,i}^{1/3}} + \frac{1}{\rho_{c,j}^{1/3}} \right)^3$$

$$T_r(x) = \sum_{i=1}^N x_i^2 T_{c,i} + \sum_{i=1}^{N-1} \sum_{j=i+1}^N 2x_i x_j \beta_{T,ij} \gamma_{T,ij} \frac{x_i + x_j}{\beta_{T,ij}^2 x_i + x_j} (T_{c,i} \cdot T_{c,j})^{0.5}$$

Departure function represents Helmholtz energy from mixing

$$\Delta \alpha^r(\delta, \tau, \bar{x}) = \sum_{i=1}^{N-1} \sum_{j=i+1}^N x_i x_j F_{ij} \alpha_{ij}^r(\delta, \tau)$$



Helmholtz energy formulation

$$\delta = \frac{\rho}{\rho_r}, \tau = \frac{T_r}{T}$$

$$\frac{a(\rho, T)}{RT} = \alpha(\delta, \tau) = \alpha^o(\delta, \tau) + \alpha^r(\delta, \tau)$$

Ideal Helmholtz free energy

Residual Helmholtz free energy

$$\alpha^o(\delta, \tau) = \frac{h_o^o \tau}{RT_r} - \frac{s_o^o}{R} - 1 + \ln \frac{\delta \tau_o}{\delta_o \tau} + \frac{\tau}{R} c_p^o \left(\frac{1}{\tau} - \frac{1}{\tau_o} \right) + \frac{c_p^o}{R} \ln \frac{\tau}{\tau_o}$$

$$\alpha^r(\delta, \tau) = \sum_{k=1}^{I_{pol}} N_k \delta^{d_k} \tau^{t_k} + \sum_{k=I_{pol}+1}^{I_{pol}+I_{exp}} N_k \delta^{d_k} \tau^{t_k} \exp(-\delta^{l_k}) +$$

$$\sum_{k=I_{pol}+I_{exp}+1}^{I_{pol}+I_{exp}+I_{crit}} N_k \delta^{d_k} \tau^{t_k} \exp\left(-\eta_k(\delta - \eta)^2 - \beta_k(\tau - \gamma_k)^2\right)$$

pure fluid mixtures

Ideal Helmholtz free energy

$$\alpha^o(\rho, T, \bar{x}) = \sum_{i=1}^N x_i \left[\alpha_{oi}^o(\rho, T) + \ln x_i \right]$$

Residual Helmholtz free energy

$$\alpha^r(\delta, \tau, \bar{x}) = \sum_{i=1}^N x_i \alpha_{oi}^r(\delta, \tau) + \sum_{i=1}^{N-1} \sum_{j=i+1}^N x_i x_j F_{ij} \alpha_{ij}^r(\delta, \tau)$$

Reducing variables

$$\frac{1}{\rho_r(x)} = \sum_{i=1}^N \frac{x_i^2}{\rho_{c,i}} + \sum_{i=1}^{N-1} \sum_{j=i+1}^N 2x_i x_j \frac{\beta_{v,ij} \gamma_{v,ij}}{\beta_{v,ij}^2 x_i + x_j} \frac{x_i + x_j}{8} \left(\frac{1}{\rho_{c,i}^{1/3}} + \frac{1}{\rho_{c,j}^{1/3}} \right)^3$$

$$T_r(x) = \sum_{i=1}^N x_i^2 T_{c,i} + \sum_{i=1}^{N-1} \sum_{j=i+1}^N 2x_i x_j \frac{\beta_{T,ij} \gamma_{T,ij}}{\beta_{T,ij}^2 x_i + x_j} (T_{c,i} \cdot T_{c,j})^{0.5}$$

5+30 variables describing mixture properties
vs
130-150 variables describing pure fluid properties with HEoS

Departure function represents Helmholtz energy from mixing

$$\Delta \alpha^r(\delta, \tau, \bar{x}) = \sum_{i=1}^{N-1} \sum_{j=i+1}^N x_i x_j F_{ij} \alpha_{ij}^r(\delta, \tau)$$



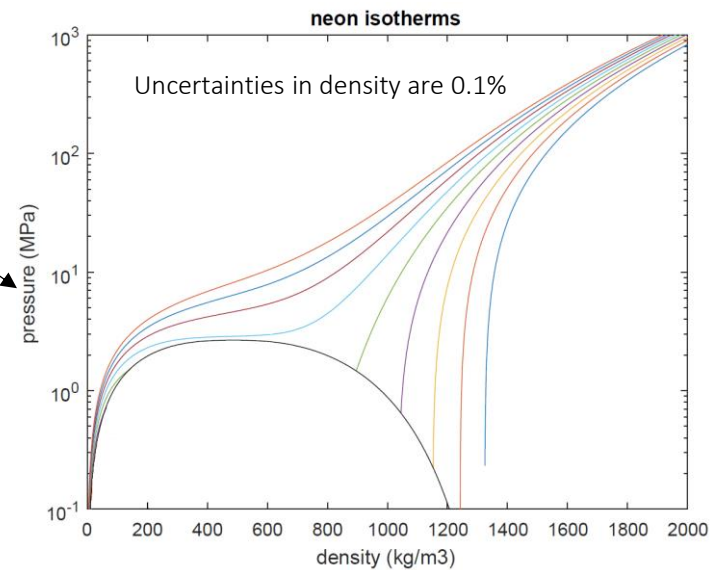
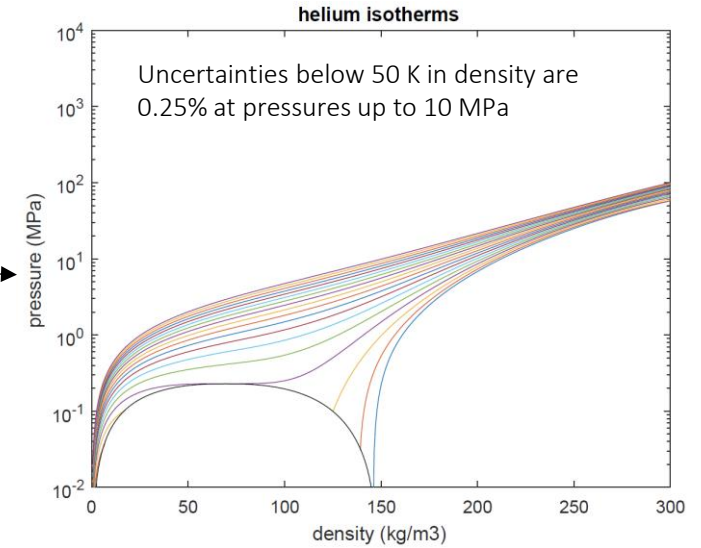
Relation of thermodynamic properties to Helmholtz energy

Property	Relation to Helmholtz free energy
Pressure	$\frac{p(\delta, \tau, \bar{x})}{\rho RT} = 1 + \delta \alpha_{\delta}^r$
Compression factor	$Z(\delta, \tau, \bar{x}) = 1 + \delta \alpha_{\delta}^r$
Entropy	$\frac{s(\delta, \tau, \bar{x})}{R} = \tau(\alpha_{\tau}^o + \alpha_{\tau}^r) - \alpha^o - \alpha^r$
Internal energy	$\frac{u(\delta, \tau, \bar{x})}{RT} = \tau(\alpha_{\tau}^o + \alpha_{\tau}^r)$
Enthalpy	$\frac{h(\delta, \tau, \bar{x})}{RT} = 1 + \tau(\alpha_{\tau}^o + \alpha_{\tau}^r) + \delta \alpha_{\delta}^r$
Isochoric heat capacity	$\frac{c_v(\delta, \tau, \bar{x})}{R} = -\tau^2(\alpha_{\tau\tau}^o + \alpha_{\tau\tau}^r)$
Isobaric heat capacity	$\frac{c_p(\delta, \tau, \bar{x})}{R} = -\tau^2(\alpha_{\tau\tau}^o + \alpha_{\tau\tau}^r) + \frac{(1 + \delta \alpha_{\delta}^r - \delta \tau \alpha_{\delta\tau}^r)^2}{1 + 2\delta \alpha_{\delta}^r + \delta^2 \alpha_{\delta\delta}^r}$
Gibbs free energy	$\frac{g(\delta, \tau, \bar{x})}{RT} = 1 + \alpha^o + \alpha^r + \delta \alpha_{\delta}^r$
Speed of sound	$\frac{w^2(\delta, \tau, \bar{x})M}{RT} = 1 + 2\delta \alpha_{\delta}^r + \delta^2 \alpha_{\delta\delta}^r - \frac{(1 + \delta \alpha_{\delta}^r - \delta \tau \alpha_{\delta\tau}^r)^2}{\tau^2(\alpha_{\tau\tau}^o + \alpha_{\tau\tau}^r)}$
J - T coefficient	$\mu_{JT} R \rho = \frac{-(\delta \alpha_{\delta}^r + \delta^2 \alpha_{\delta\delta}^r + \delta \tau \alpha_{\delta\tau}^r)}{(1 + \delta \alpha_{\delta}^r - \delta \tau \alpha_{\delta\tau}^r)^2 - \tau^2(\alpha_{\tau\tau}^o + \alpha_{\tau\tau}^r)(1 + 2\delta \alpha_{\delta}^r + \delta^2 \alpha_{\delta\delta}^r)}$



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J - T coefficient	$\mu_{JT} R \rho = \frac{-(\delta \alpha_{\delta}^r + \delta^2 \alpha_{\delta\delta}^r + \delta \tau \alpha_{\delta\tau}^r)}{(1 + \delta \alpha_{\delta}^r - \delta \tau \alpha_{\delta\tau}^r)^2 - \tau^2(\alpha_{\tau\tau}^o + \alpha_{\tau\tau}^r)(1 + 2\delta \alpha_{\delta}^r + \delta^2 \alpha_{\delta\delta}^r)}$



Algorithms employed so far:

- Sum of squares: $SSQ = \sum_{i=0}^n c(w_i X_i - \bar{X})^p$ with constrains and points weights
- Complex marching algorithm – no success so far
- The first algorithm is more successful (so far)

Institutes and universities developing the EoS:

- NIST Boulder, U.S.
- Ruhr-Universität Bochum, Germany
- Kyushu Sangy University, Japan
- Others? NTNU, KIT, ...?



(My) methodology

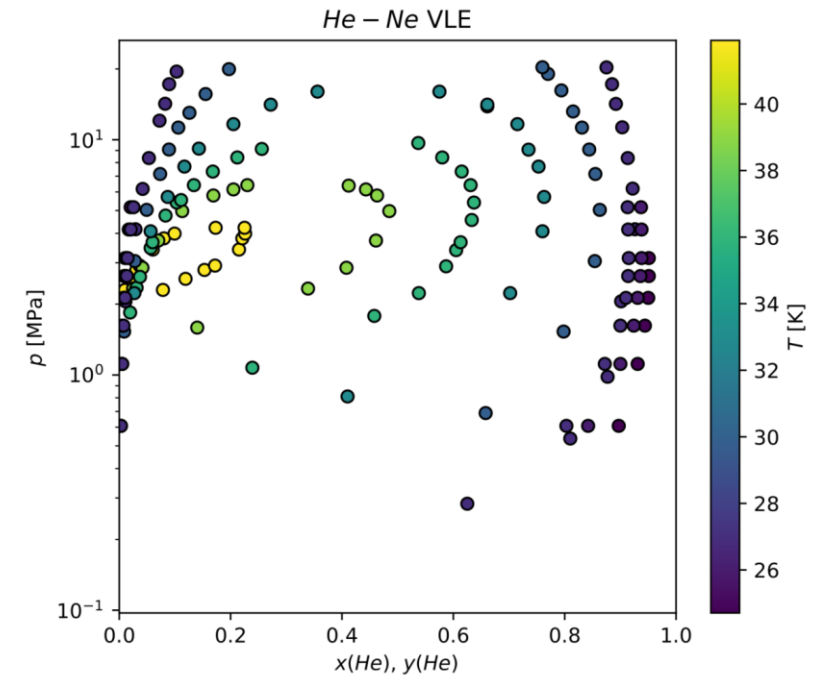
- *Obtain good VLE model*

- Assess the credibility of all datasets / each diverging experimental point
- Fit the reducing parameters and the excess function

$$\alpha^r(\delta, \tau, \bar{x}) = \sum_{i=1}^N x_i \alpha_{oi}^r(\delta, \tau) + \sum_{i=1}^{N-1} \sum_{j=i+1}^N x_i x_j F_{ij} \alpha_{ij}^r(\delta, \tau)$$

$$\alpha_{ij}^r(\delta, \tau) = \sum_{k=1}^{K_{Pol,ij}} n_{ij,k} \delta^{d_{ij,k}} \tau^{t_{ij,k}} + \sum_{k=K_{Pol,ij}+1}^{K_{Pol,ij}+K_{Exp,ij}} n_{ij,k} \delta^{d_{ij,k}} \tau^{t_{ij,k}} e^{-\eta_{ij,k}(\delta-\varepsilon_{ij,k})^2 - \beta_{ij,k}(\delta-\gamma_{ij,k})}$$

- Constrain the fugacity coefficients at the phase envelope
- Fit the densities
- Fit the speed of sound (if available)
- Constrain the derivatives



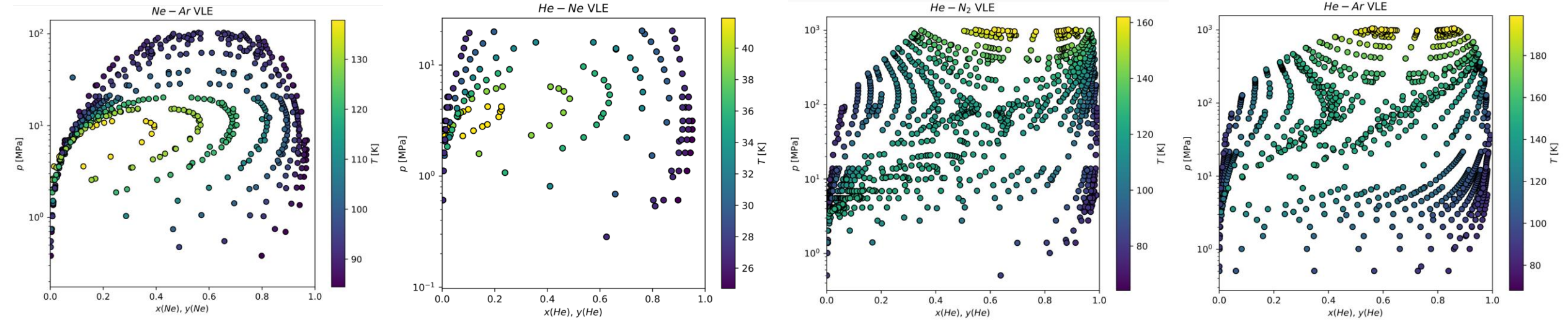
T_{c1}/T_{c2}

3.4

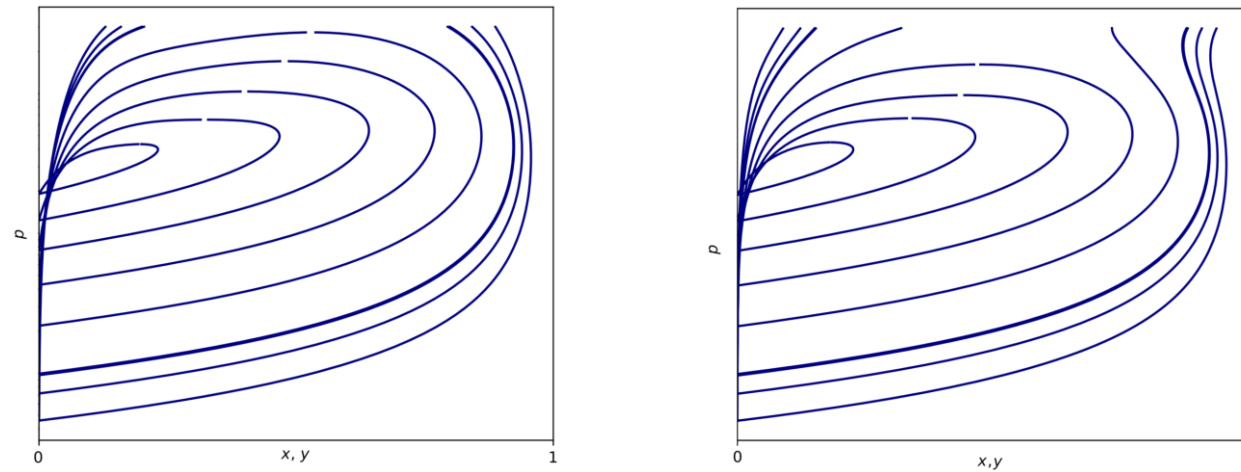
8.5

24.3

29.0



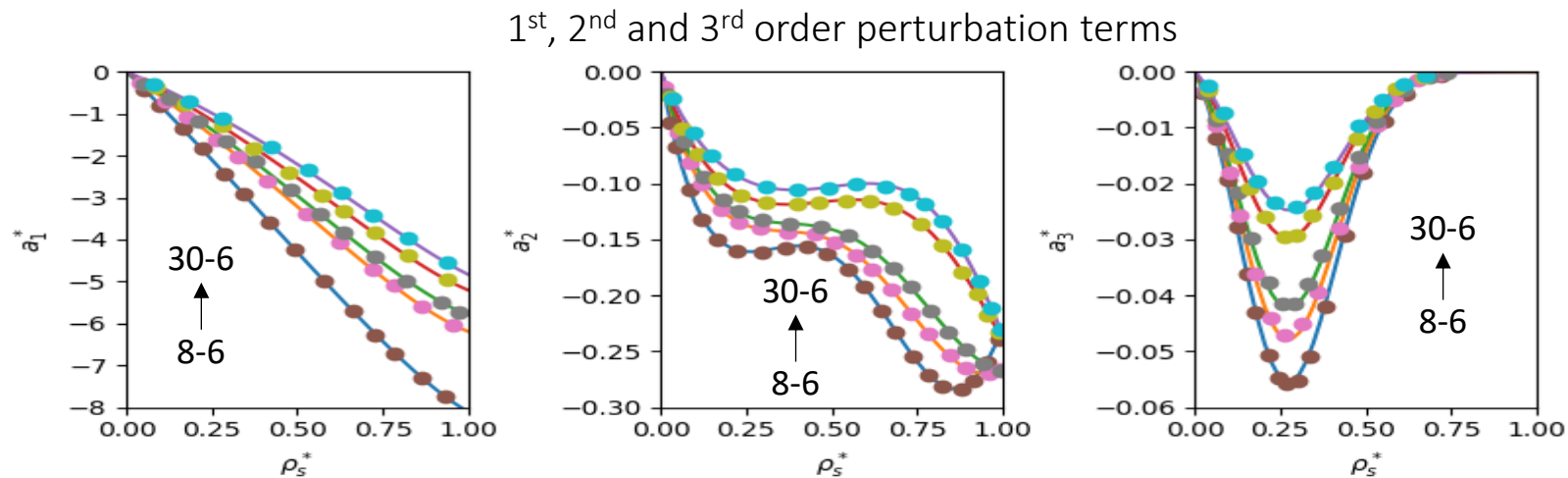
Closed or open - is there a LLE or just the VLE?



Hard sphere diameter of a segment: $d_{ii} = \int_0^{\sigma_{ii}} \left(1 - \exp\left(-\beta u_{ii}^{Mie}(r)\right) \right) dr$

Interaction potential between two species: $u_{ij}^{Mie} = C_{ij} \epsilon_{ij} \left(\left(\frac{\sigma_{ij}}{r_{ij}} \right)^{\lambda_{r,ij}} - \left(\frac{\sigma_{ij}}{r_{ij}} \right)^{\lambda_{a,ij}} \right)$

potential depth
distance between the spherical segments
segment diameter



Quantum effects

Thermal de Broglie wavelength: $\lambda_{th} = \sqrt{\frac{h^2}{2\pi m k_B T}}$

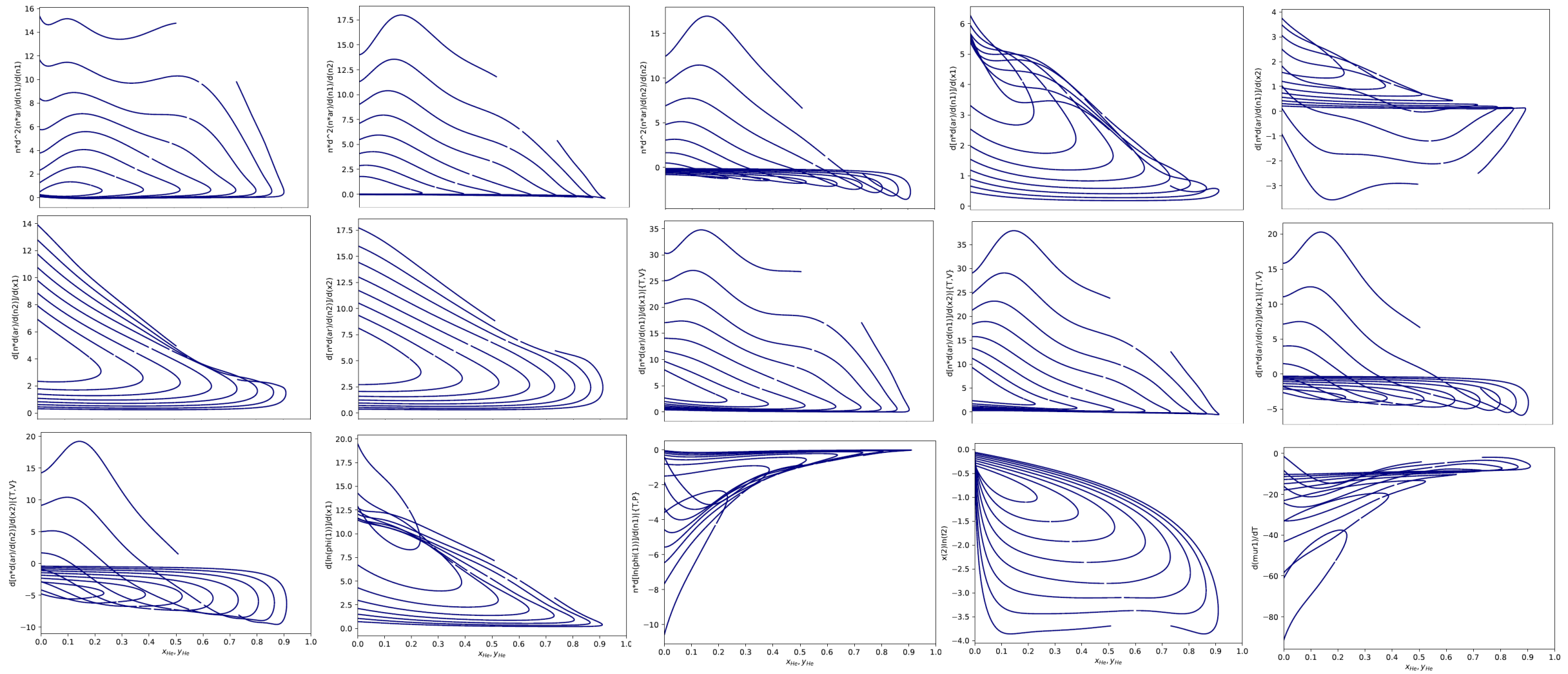
$d_{eff} \gg \lambda_{th} \Rightarrow$ Maxwell-Boltzmann statistics

$d_{eff} \sim \lambda_{th} \Rightarrow$ quantum gas (Bose-Einstein, Fermi-Dirac statistics)

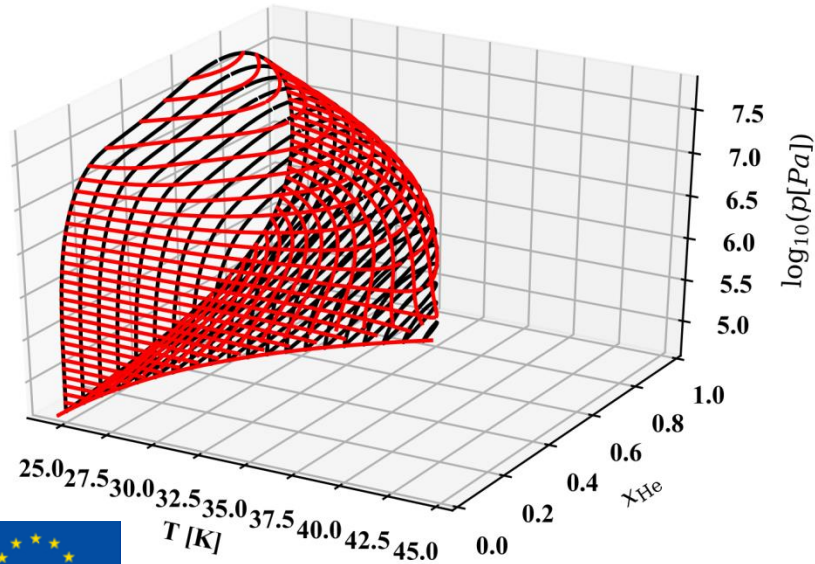
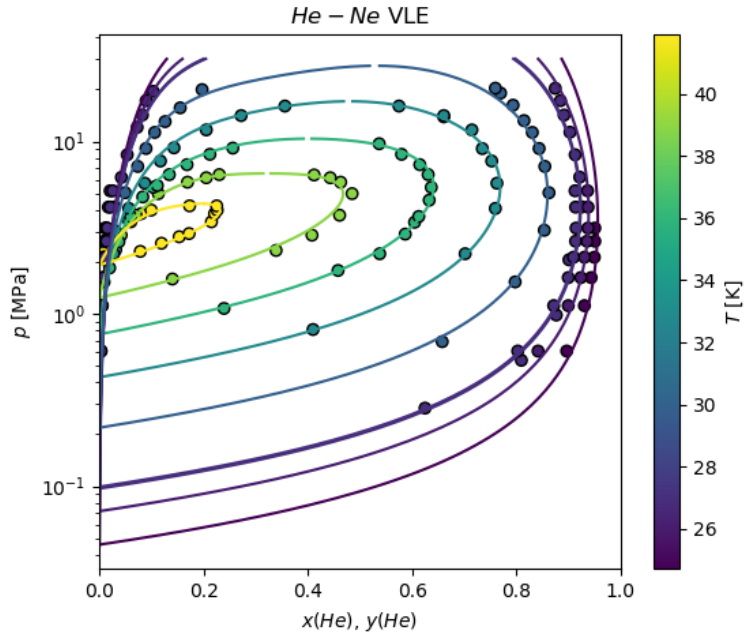
	Tc [K]	m [u]	T [K]	$\lambda_{th}[A]$	$d_{eff}[A]$
He	5.2	4.002	5	3.90	0.31
H2	33.1	2.016	22	2.62	...
Ne	44.4	20.180	30	0.71	0.38
N2	126.2	28.013	80	0.37	...
Ar	150.7	39.948	90	0.29	0.71



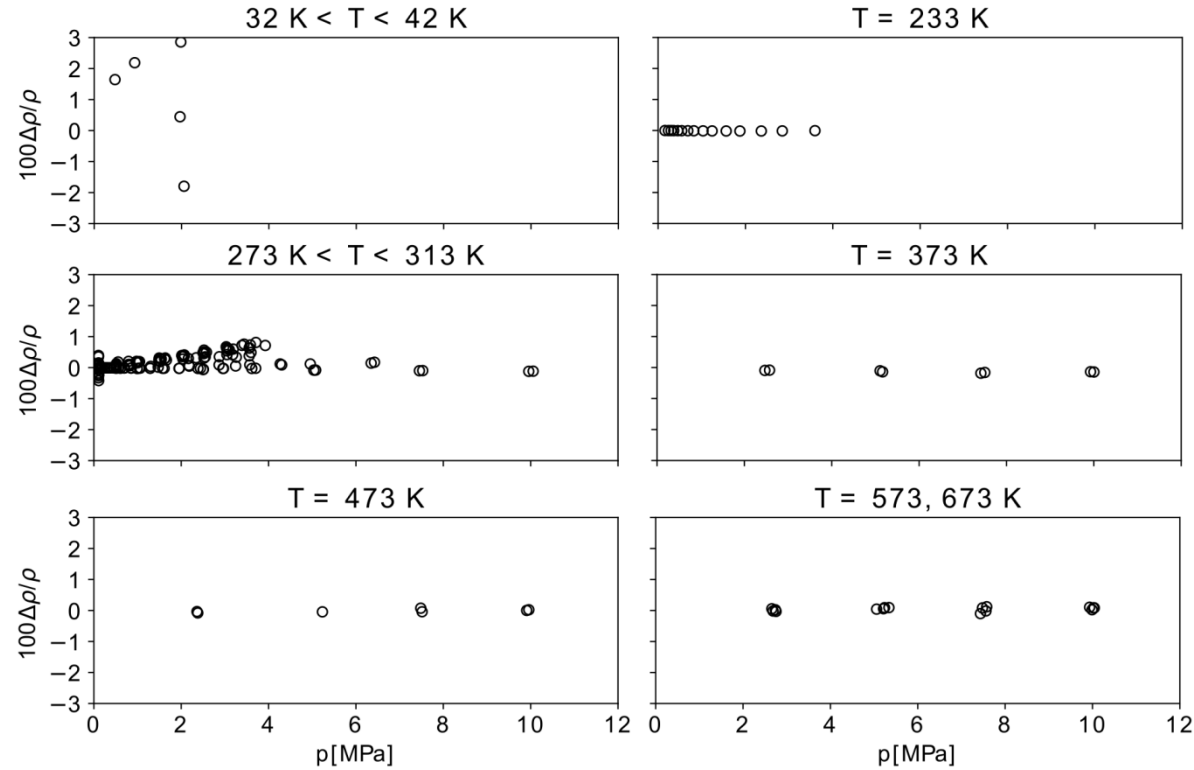
Derivatives



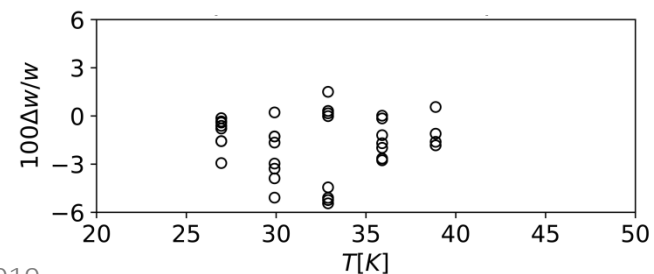
Empirical fit results



Uncertainty



density



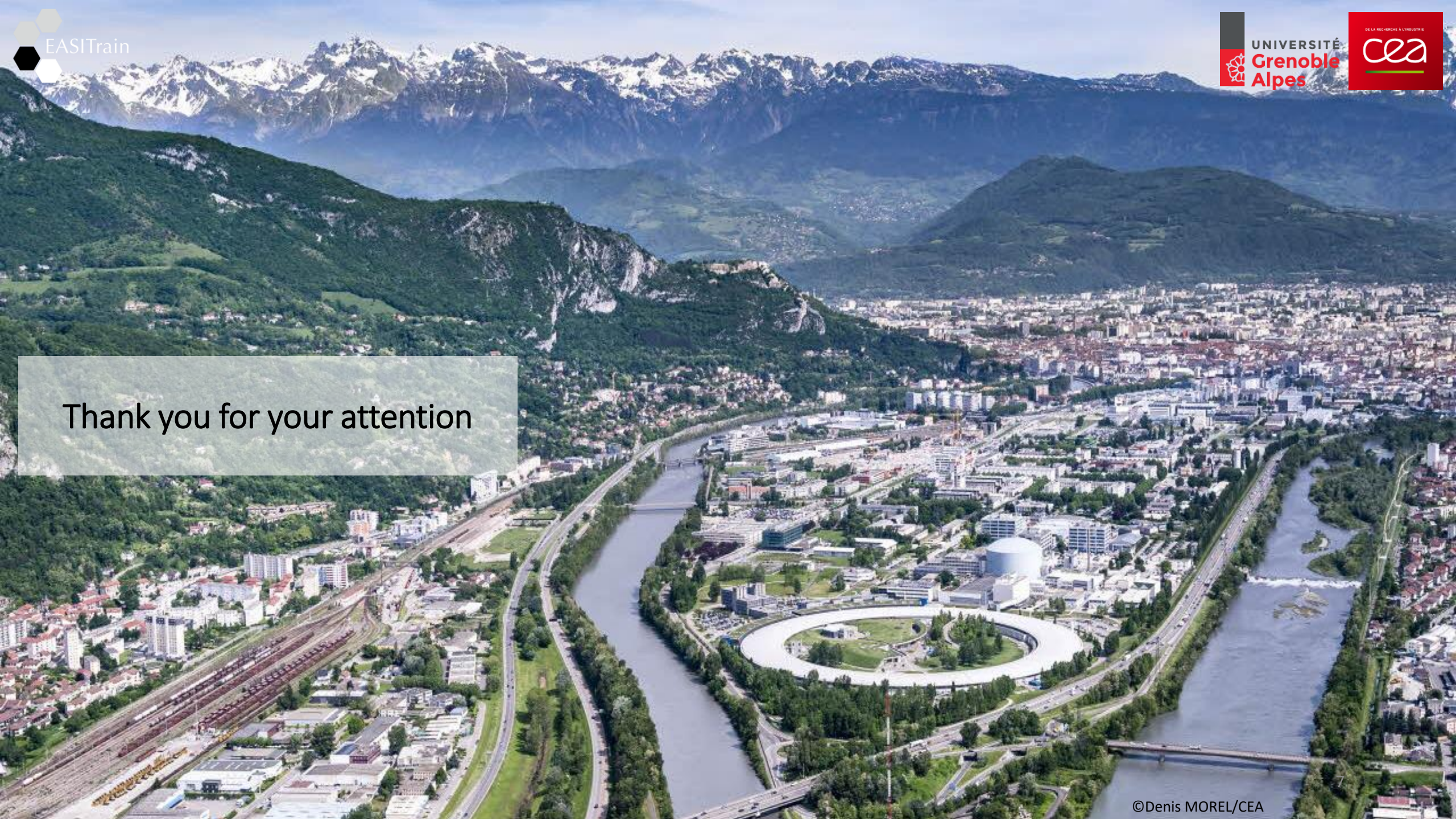
speed of sound
in liquid



Next steps

- Finalize the empirical fit for three mixtures (He-Ne, He-Ar, Ne-Ar) and publish the models
- Finalize the general SAFT model for mixtures and release a python library
- Confirm the obtained results / extend the experimental data set





Thank you for your attention