

# New nTOF target: Design Issues

**Abstract:** Following the radiation safety requirement that nTOF **lead target shall not be in contact with the cooling water**, an entirely new target assembly must be developed. The concept of a **clad target** is described.

**Preliminary designs** of target geometry and target integration in the existing cooling loop are shown, as well as structures for positioning and installation.

# Outline

- **Introduction**
  - Old Target versus New
- **Design issues**
  - Radiation Safety → Target Cladding
  - Cooling → Geometry of Target Assembly
  - Integration → Supports & Installation
- **Summary**
- **Estimated cost, manpower, time**

# Introduction

## ➤ Satisfy the safety requirements of SC/RP

- Clad lead target cooled by existing system

## ➤ Guidelines for the new target design

- Keep the neutron flux characteristics
- Reduce radioactive waste (target mass)
- Reduce overall activation

From ABMB meeting, 12 June 2006

# Remark

This presentation shows:

- **First studies** to identify design issues
- **First simulations** (thermal, mechanical) give preliminary results to guide design
- **Estimations** for cost, manpower & time
- Work and results from:  
SBM Ingénierie & AB/ATB & TS/MME

# Introduction



## Old Target

- Lead blocks directly in contact with cooling water
- Target mass > 4 tons
- Support structure entirely stainless steel (water basin in aluminium → corrosion risk)



## New Target



- No direct contact between target lead & water circuit
- Smaller target (~1 ton)
- Optimised support structure (corrosion, activation, etc.)

# Design issues: Radiation Safety

## ➤ Target Cladding

Metal<sup>(\*)</sup> clad lead target with lead core

Consequences of cladding:

1. Thermal contact resistance between lead and cladding. Need for good contact pressure between core and shell.

2. Core and shell will have different temperatures

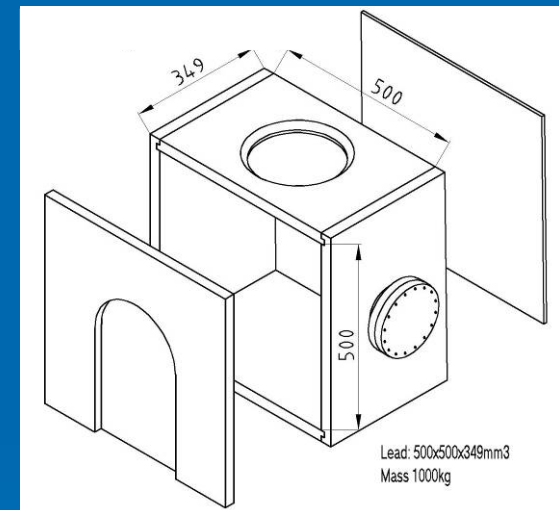
→ different expansion → large forces on shell

Proposal: Introduce initial clearance between core and shell, to have contact at normal working temperature. Needs to be studied!

**Challenge**

(\*) Aluminium is used in the calculations. Material may have to change for reasons of radioactive waste disposal (see talk Luisa ULRICI, today at 12:00)

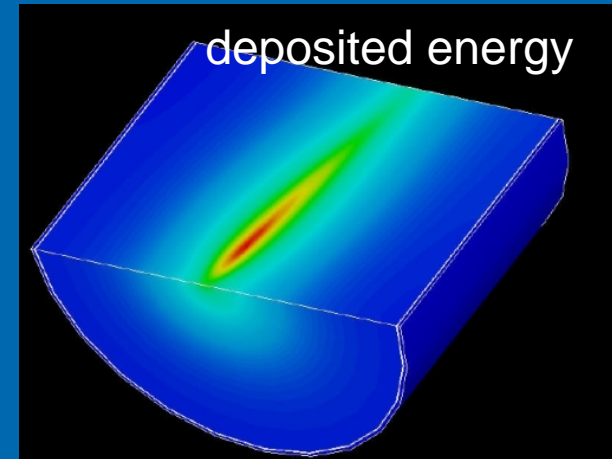
Possible production method



# Cladding: Thermal equilibrium

Cylindrical target (R=26.5cm)  
with 5mm aluminium cladding

- 3.4kW(\*) to be evacuated
- Assume adequate cooling
- Results from thermal calculations:
  - Temperature rise from lead to aluminium ~ 75K
  - Estimated temperature rise of 130K between start-up and equilibrium → **Target temperature** reaches **150 °C** which is **acceptable** (45% of lead melting temperature)
  - **Cylindrical shape better** cooled and generally easier for production

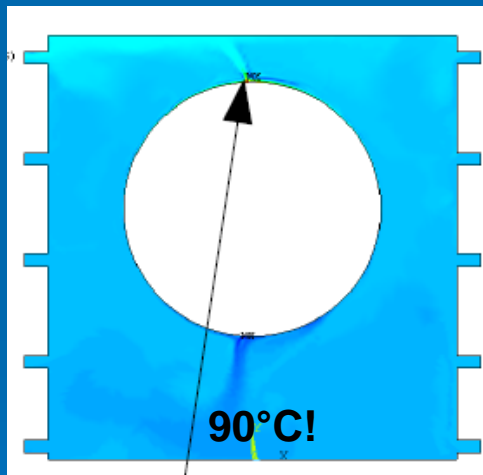


(\*)Load case = 5 pulses/16.8s supercycle

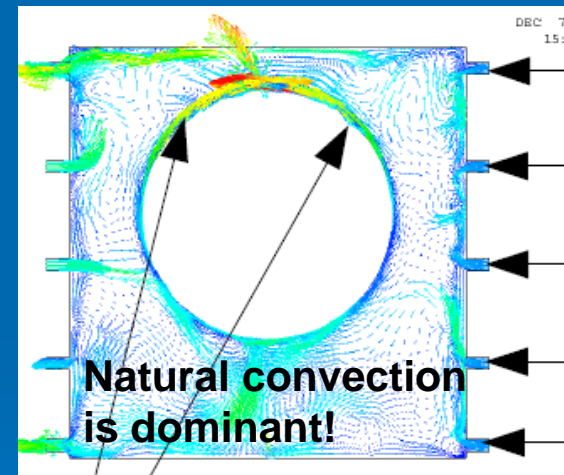
# Design issues: Cooling

## ➤ Cooling → Target Assembly Geometry

Maximum temperature:  
Target: 150°C Water: 90°C



Water Inlet Nozzles:  
Flow=6l/s Velocity=0.01m/s

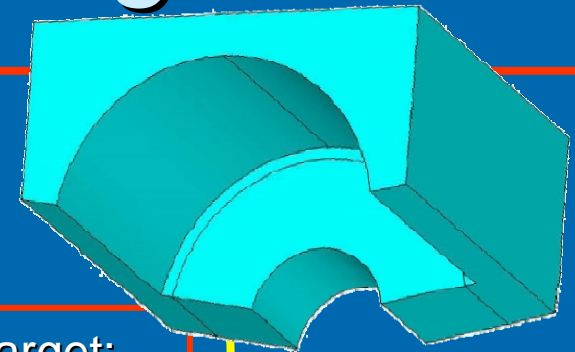


Existing water flow not adapted to size of new target  
Target is sufficiently cooled, but water temperature locally high  
→ Need to **redirect / concentrate / guide** the water flow around the target

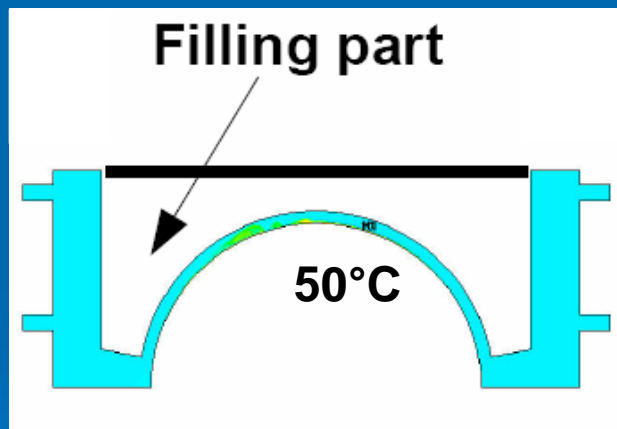


# Optimized for cooling

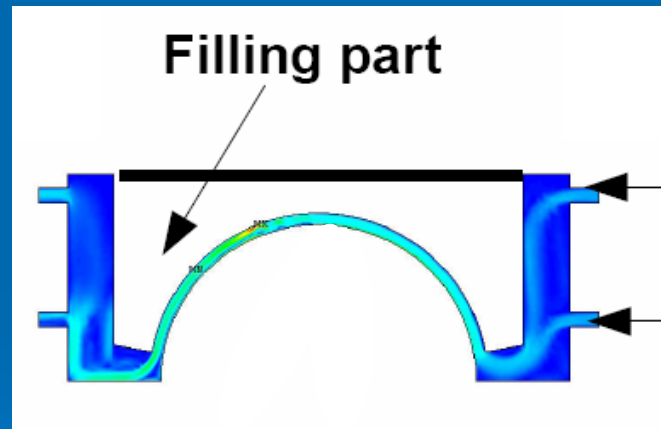
Proposal: Filling part to help guide the water and increase local velocity



Water temperature:  
Average: 22°C - Local: 50°C



Water velocity around target:  
Average: 0.02 m/s - Local: 0.1 m/s



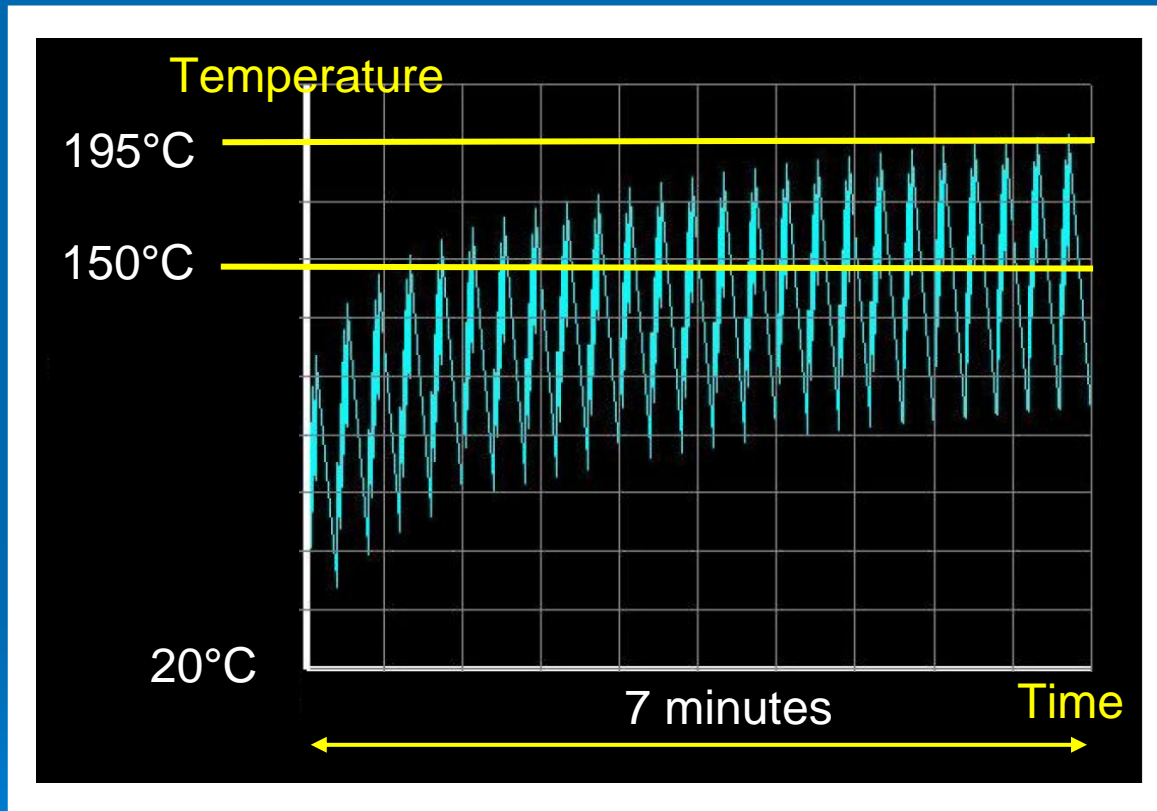
Filling parts  
are efficient

- Filling parts: complex geometry, minimize mass
- Support structure to be adapted
- Impact on target integration to be evaluated

**Challenge**

# Transient behaviour

Maximum target temperature vs. time → effect of each pulse and supercycle<sup>(\*)</sup>



Dynamic effect  
will cause shockwaves  
and cyclic stresses.  
(time-scale = msec)

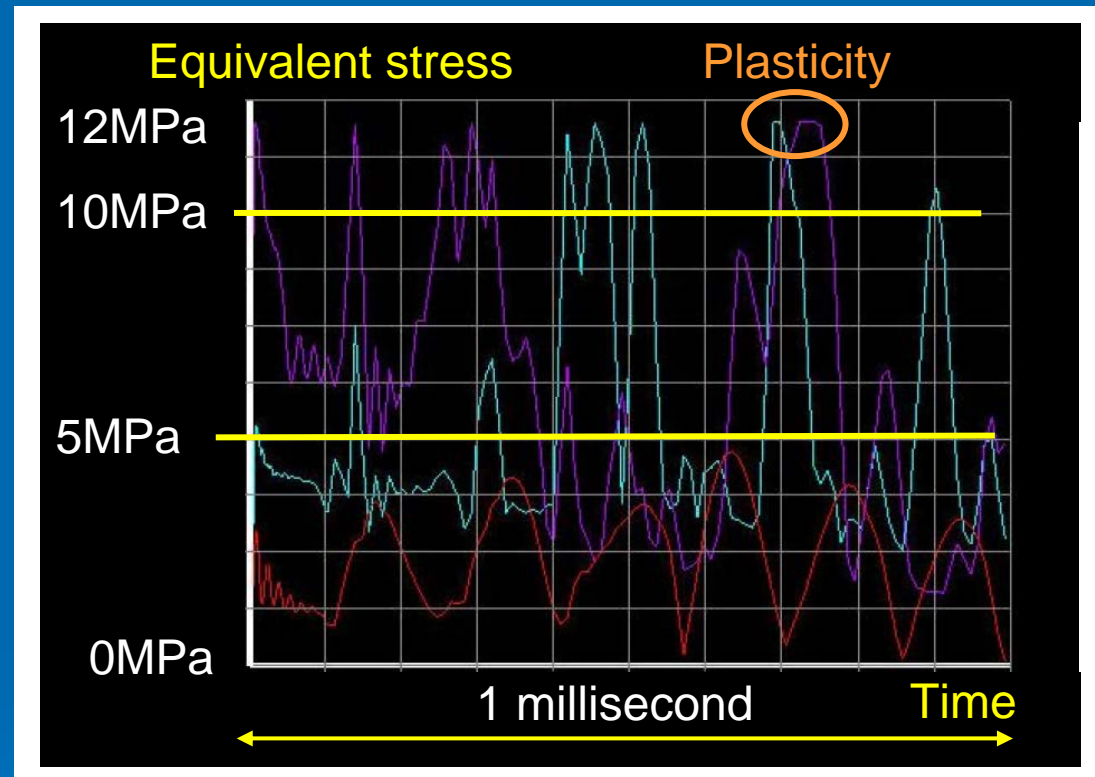
Fatigue?  
Cracks?  
Lifetime?

<sup>(\*)</sup>Load case = 7ns burst, 1.2s pulse,  
5 pulses/16.8s supercycle

# Transient elasto-plastic behaviour

## First results:

- Presence of plasticity
- Fatigue driven failure of the material will occur in central region (number of cycles to be determined).



## Next steps:

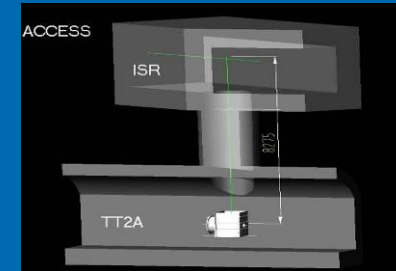
- Get detailed material properties (literature / experiment)
- Take into account the initial gap and the cladding material
- Fatigue analysis of both lead and cladding materials

**Challenge**

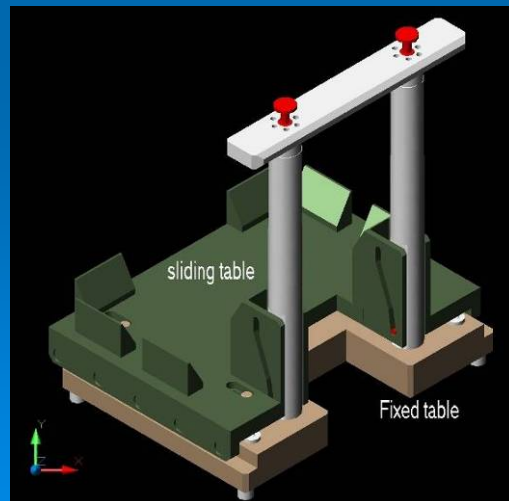
# Design issues: Integration

## ➤ Supports and guiding system

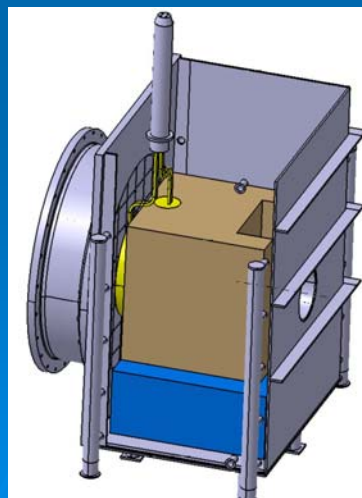
- Need for precise positioning (access!)
- Limited space available
- Integrate “filling parts”
- Installation vertical + horizontal (moderator)



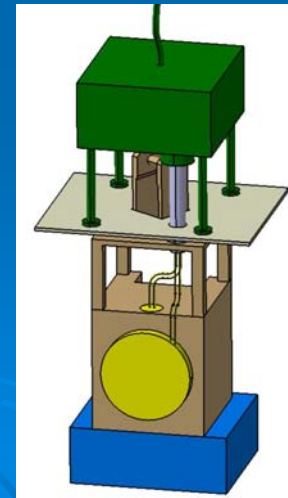
First ideas: remotely actuated sliding table, tubes for moderator



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ABOC Days 22-24/01/2007



To do:

➤ Design

➤ Prototyping

Challenge

# Summary: Remaining design work

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- Cladding & gap  
(define material, geometry, production method)
- Optimise cooling circuit  
(define geometry, link to target support)
- Simulate dynamic behaviour  
(perform material tests & calculations)
- Integration of components  
(define supports, guides)

# Estimated Cost, Manpower & Time

- **Cost target & supports:**  
240 kCHF
- **Manpower**  
AB/ATB: 1.5 FTE - SC/RP: 0.5 FTE - TS/MME: ?
- **Time for design (internal)**  
4 – 6 months
- **Time for target production (external)**  
6 – 9 months