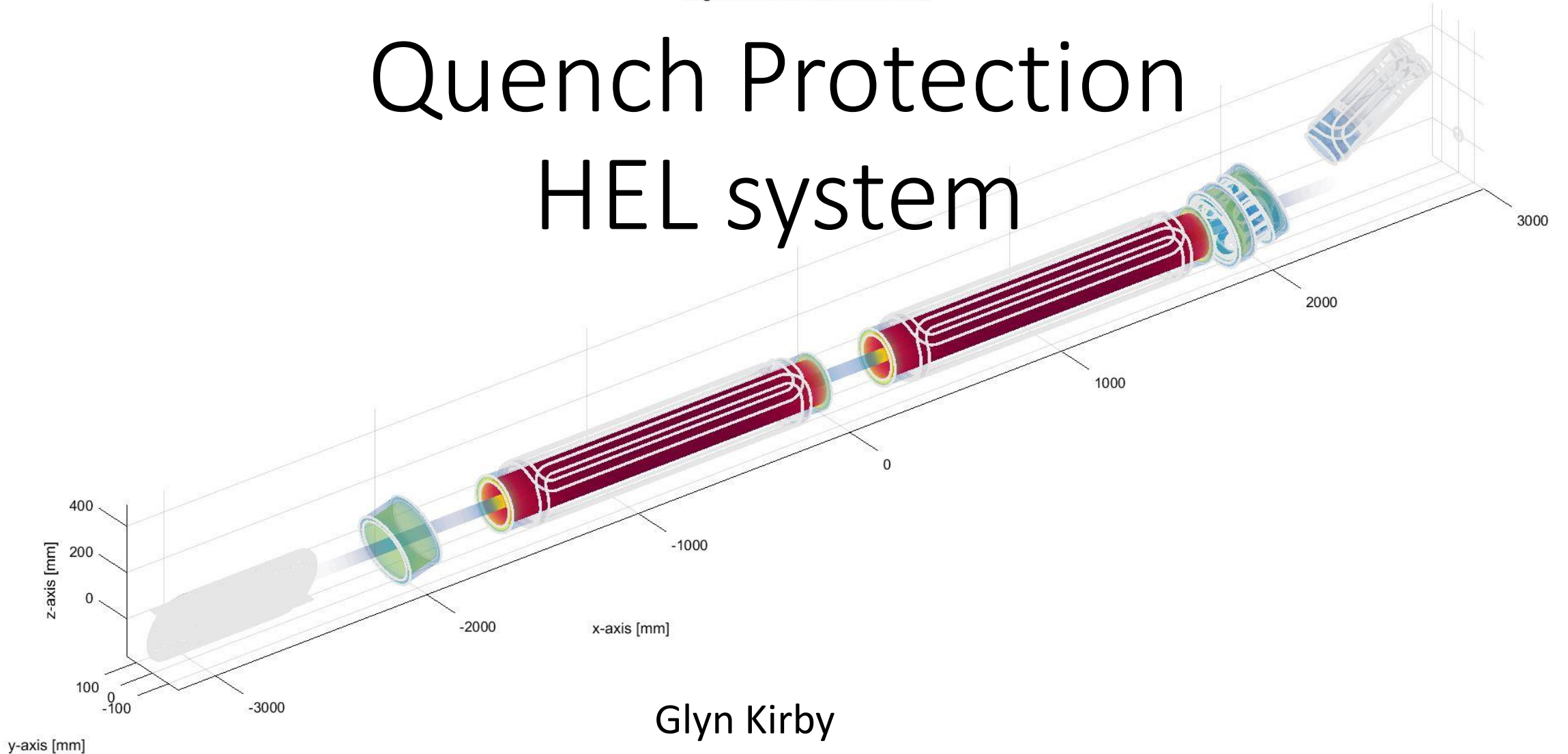


Magnetic field on surface of model

# Quench Protection HEL system



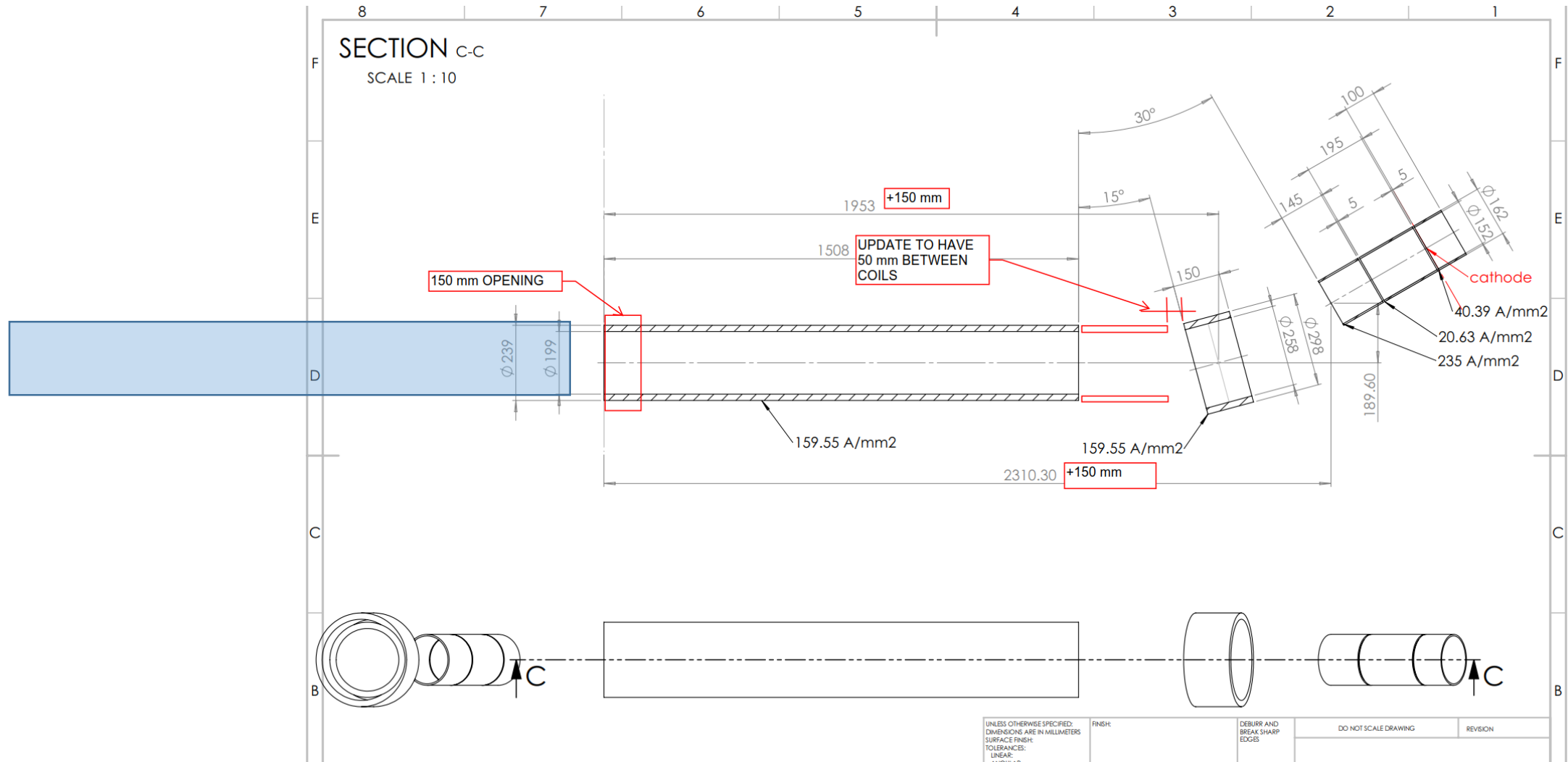
Glyn Kirby

Matthias Mentink & Jeroen Van Nugteren

# Overview

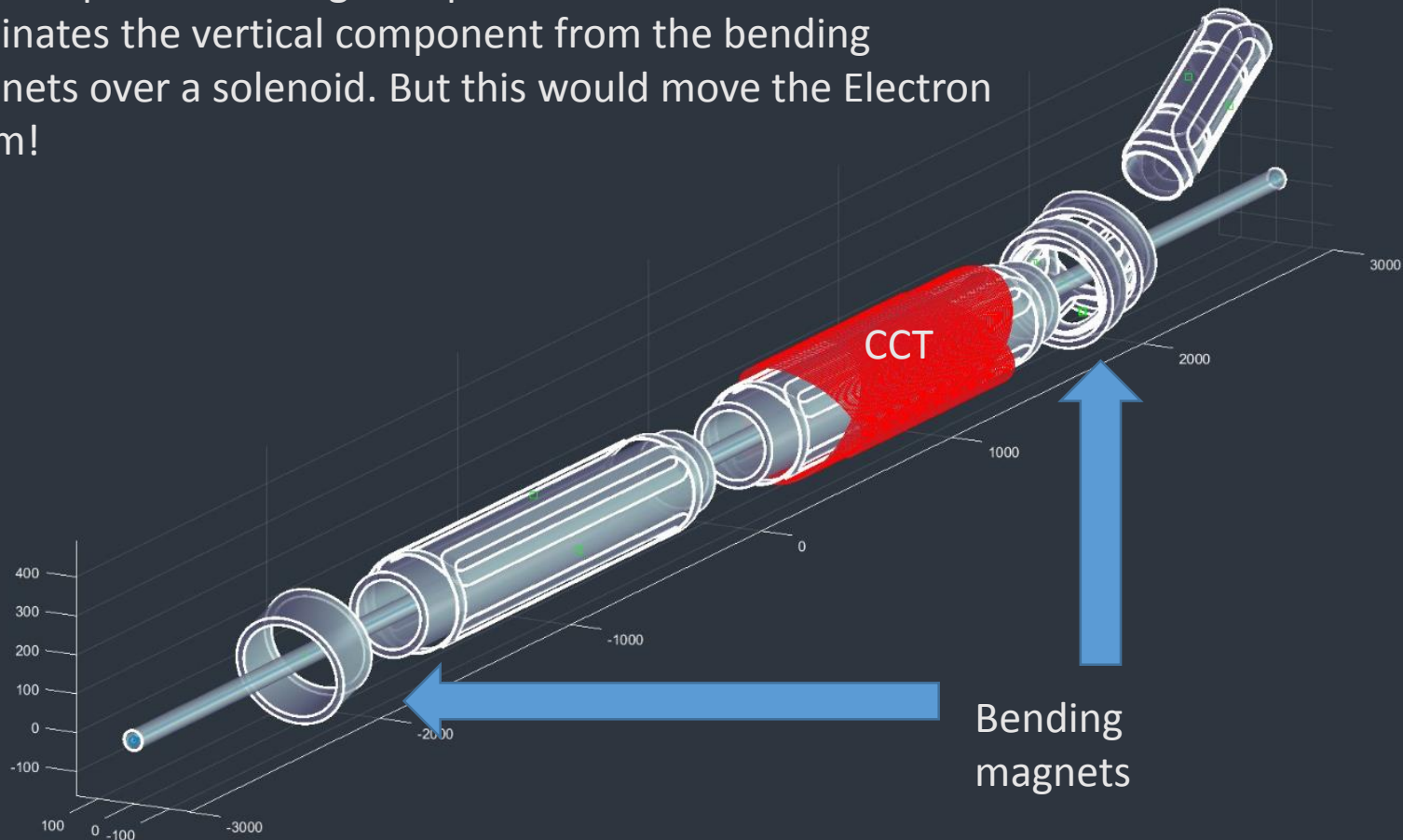
- Coil designs and some evolution
- Coil features, complexity, inductances matrix, forces,
- Quench calculation evolution.
- Conclusions / quench protection proposals for consideration.

# Fine tuning and simplifying the design



# Initial idea to CCT location that was an error !

To save space we thought to put the CCT corrector that eliminates the vertical component from the bending magnets over a solenoid. But this would move the Electron beam!

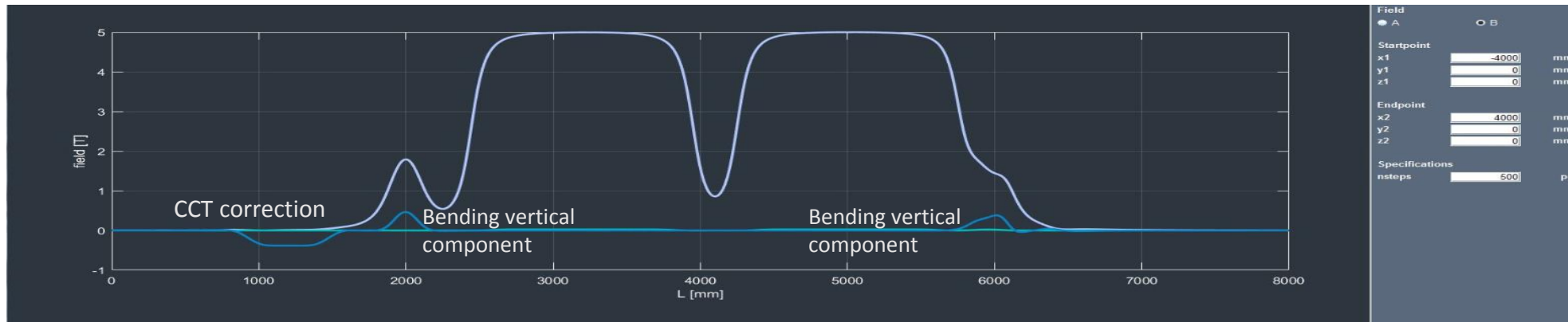
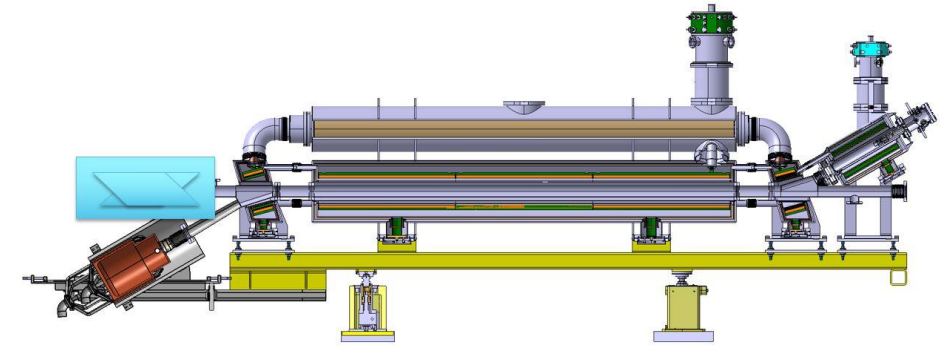
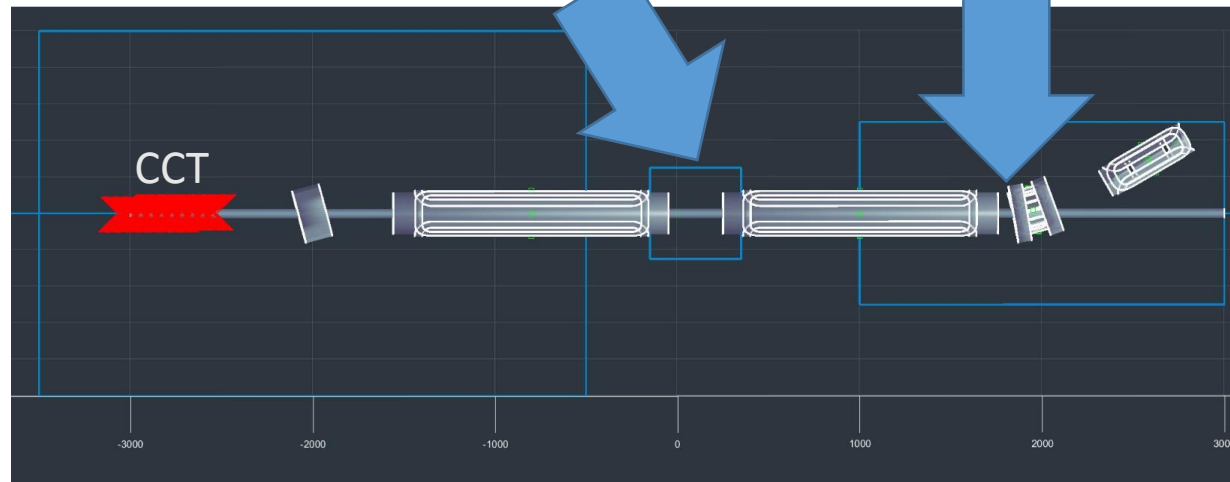


# Magnet systems

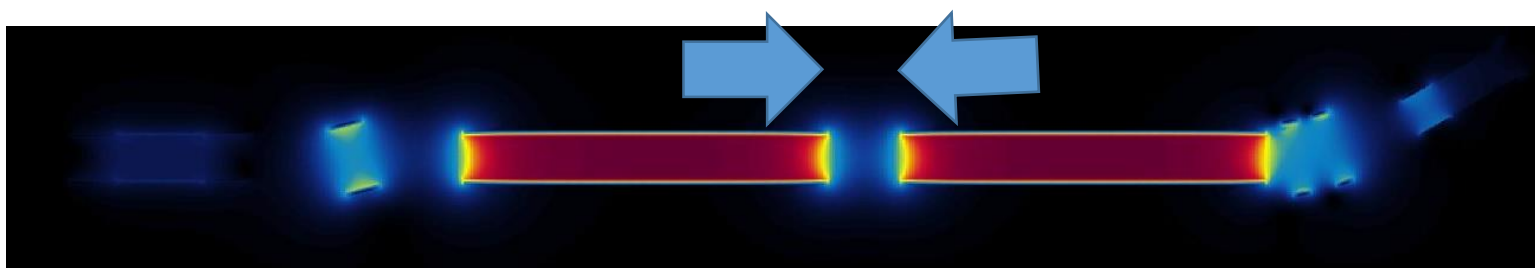
Partly updated to new proposed design

300 mm Gap between coils this will give space for cryostat open access for gas curtain added

Gap between coil reduced



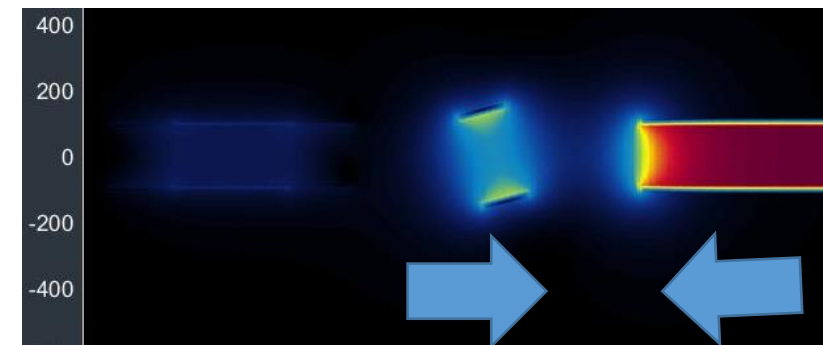
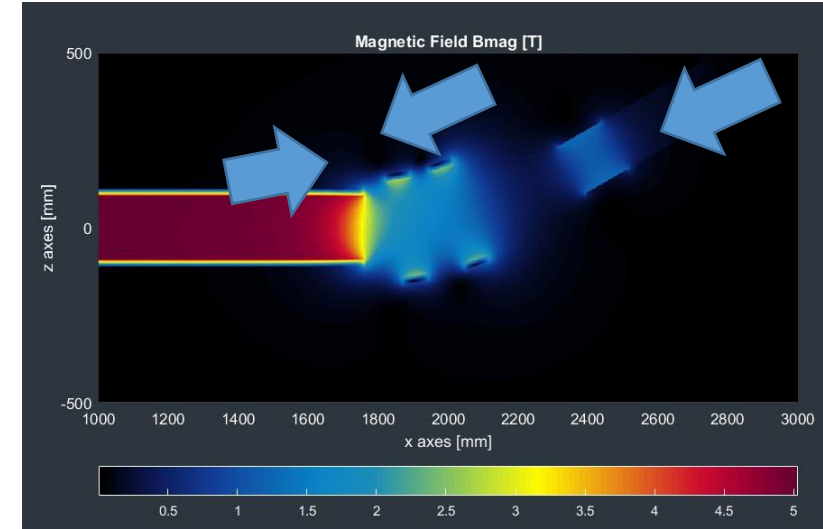




Mechanical design next steps !

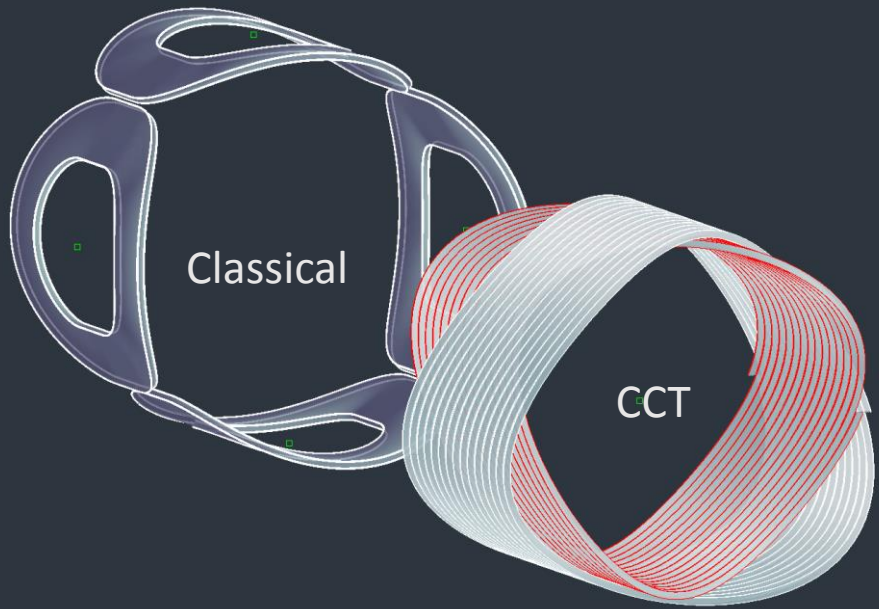
# Force matrix between coils

Name	x [mm]	y [mm]	z [mm]	Fx [N]	Fy [N]	Fz [N]	Fmag [N]	Tx [N.mm]	Ty [N.mm]	Tz [N.mm]	Tmag [N.mm]	
BlueWhale Inner	-2800	0	0	0	419.5939	-142.283	137.8501	464.0108	-0.00117	1.362151	-0.00032	1.362151925
BlueWhale Outer	-2800	0	0	0	-275.371	224.8831	170.0032	394.0846	0.000328	-1.57579	0.000659	1.575792106
Dump Solenoid	-2003	0	0	0	6606.085	43.12382	-948.576	6673.98	0.000286	0.276781	-0.00106	0.276782743
Bend Solenoid 2	1880	0	0	0	-14831.4	-2119.74	8349.828	17151.79	-0.04995	0.079012	0.283393	0.29841198
Bend Solenoid 1	2030	0	0	40	-47107.8	2292.043	-10328.2	48281.12	-0.07133	-0.27555	0.195932	0.345551928
Gun 3	2413.5	0	200	-713.628	-26.5563	-86.0654	719.2896	0.000527	0.037969	-0.00091	0.037984043	
Gun 1	2733.5	0	388.76273	-64.0543	-0.11955	-37.9795	74.46748	1.09E-05	0.000181	-1.9E-05	0.000182683	
Gun 2	2583.5	0	298.150005	-533.785	-0.5751	-298.567	611.612	2.59E-05	0.001215	-4.5E-05	0.001216559	
dipole y3 B	-800	0	125.5	0	0	0	0	0	0	0	0	
dipole y3 A	-800	0	-125.5	0	0	0	0	0	0	0	0	
dipole x3 B	-800	-130.5	0	-478.077	43.29852	-0.92312	480.0349	-0.00072	0.000834	0.155905	0.155909354	
dipole x1 B	1000	-130.5	0	-411.108	39.77156	-0.27669	413.0276	-0.00163	0.001185	0.124855	0.124870996	
dipole x3 1	-800	130.5	0	477.9714	-73.1284	1.079853	483.5345	-0.00066	-0.00025	0.155335	0.15533654	
dipole x1 A	1000	130.5	0	410.5824	-77.4883	0.41131	417.8307	-0.0015	-0.00108	0.124221	0.124235248	
Gun Dipole y B	2540.5	0	372.628185	0	0	0	0	0	0	0	0	
Gun Dipole y A	2626.5	0	223.671631	0	0	0	0	0	0	0	0	
Gun Dipole x B	2583.5	-91	298.15	0	0	0	0	0	0	0	0	
Gun Dipole x A	2583.5	91	298.15	0	0	0	0	0	0	0	0	
dipole y1 B	1000	0	125.5	0	0	0	0	0	0	0	0	
dipole y1 A	1000	0	-125.5	0	0	0	0	0	0	0	0	
Bend Dipole x B	1950	-128	20	-956.312	-52.3112	-298.292	1003.119	0.180272	-0.07553	-0.72624	0.752085176	
Bend Quadrupole 1	1950	-120	20	0	0	0	0	0	0	0	0	
Bend Dipole x A	1950	128	20	0	0	0	0	0	0	0	0	
Bend Quadrupole 3	1950	120	20	0	0	0	0	0	0	0	0	
Bend Dipole y B	1917.906438	0	139.774802	0	0	0	0	0	0	0	0	
Bend Quadrupole 2	1918.941715	0	135.911099	0	0	0	0	0	0	0	0	
Bend Dipole y A	1982.093562	0	-99.7748025	0	0	0	0	0	0	0	0	
Bend Quadrupole 4	1981.058285	0	-95.9110992	0	0	0	0	0	0	0	0	
tube	0	0	0	0	0	0	0	0	0	0	0	
Solenoid - 1	1004	0	0	48546.32	161.9534	2065.729	48590.52	-2.8E-05	-1.71414	-0.39234	1.75846782	
Solenoid - 2	-804	0	0	8787.729	177.2842	77.13138	8789.856	-2.8E-05	0.543656	-0.32524	0.633515815	

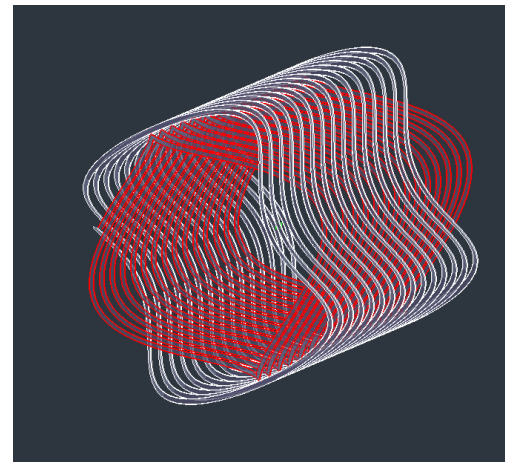
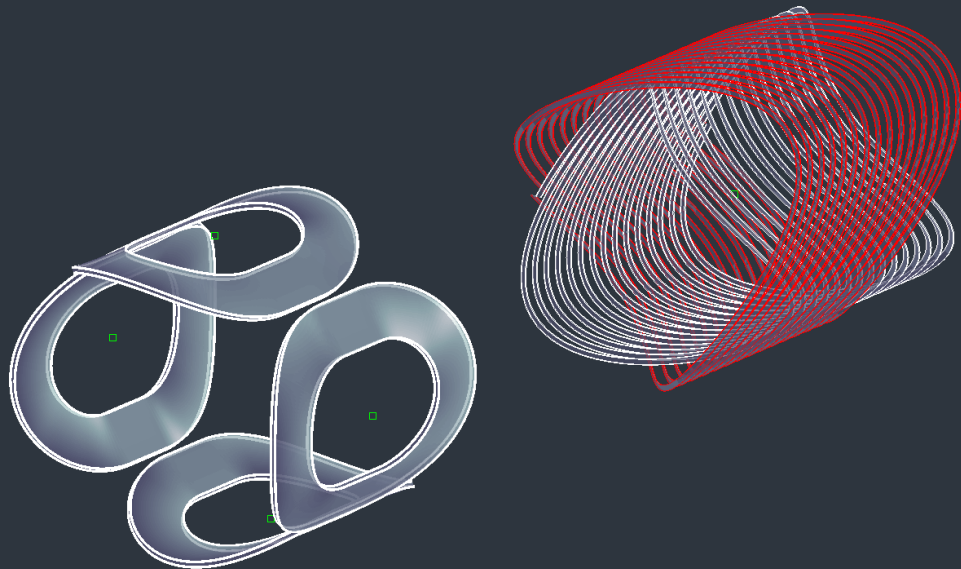


Not final but very close !

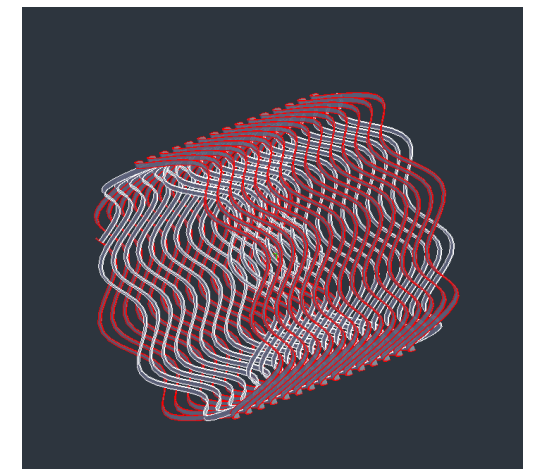




CCT Quad alternating to classic

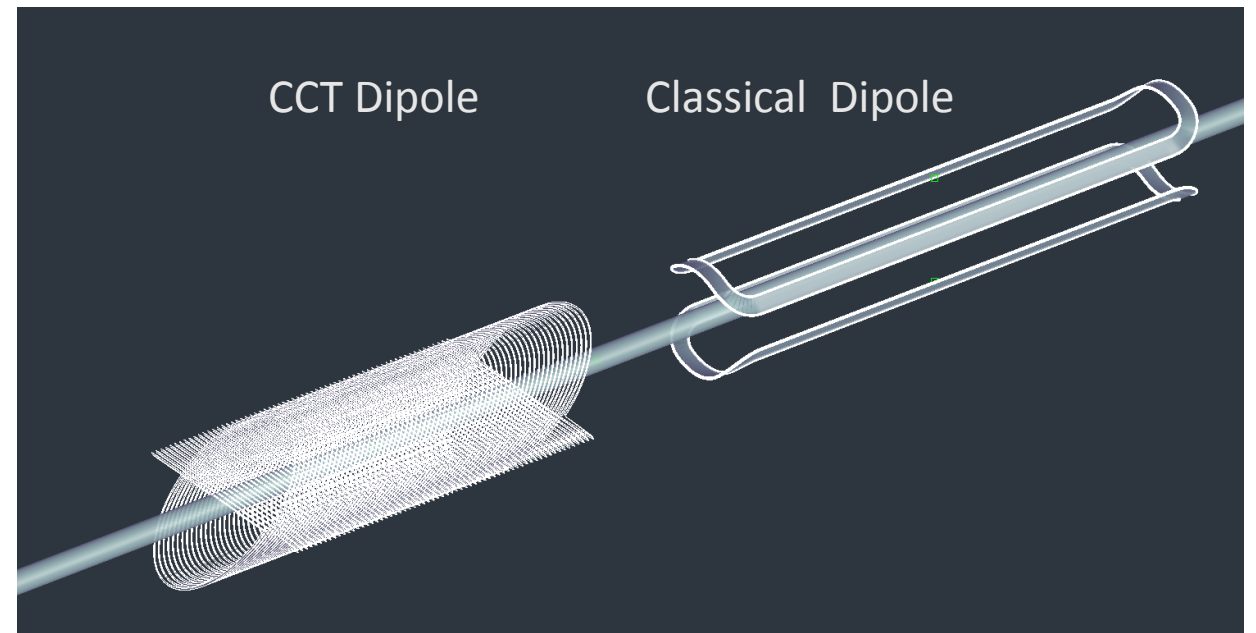


Sextepole



14 pole

Examples, we can make any harmonic correction coil  
Need to look at cost! of low current CCT, but forces will be easier to support !

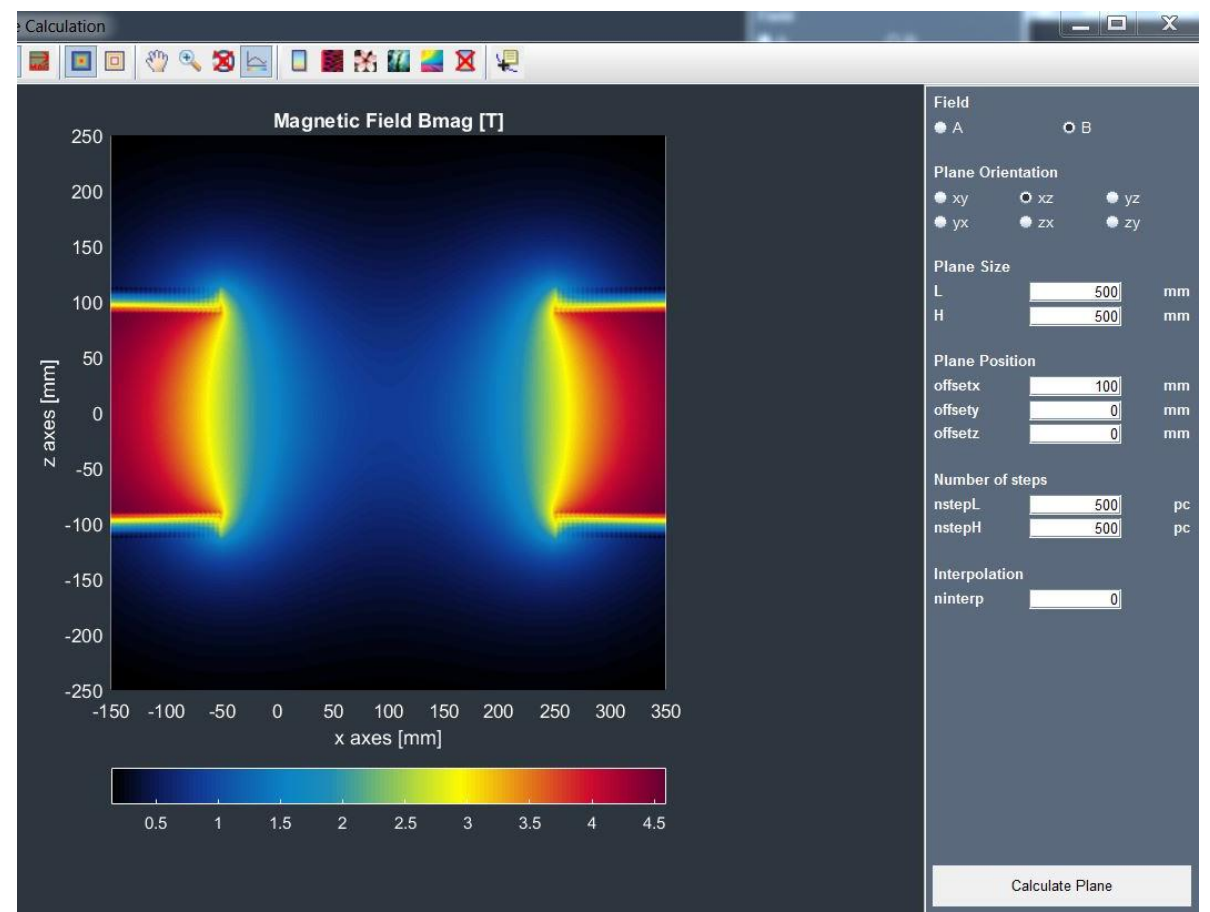
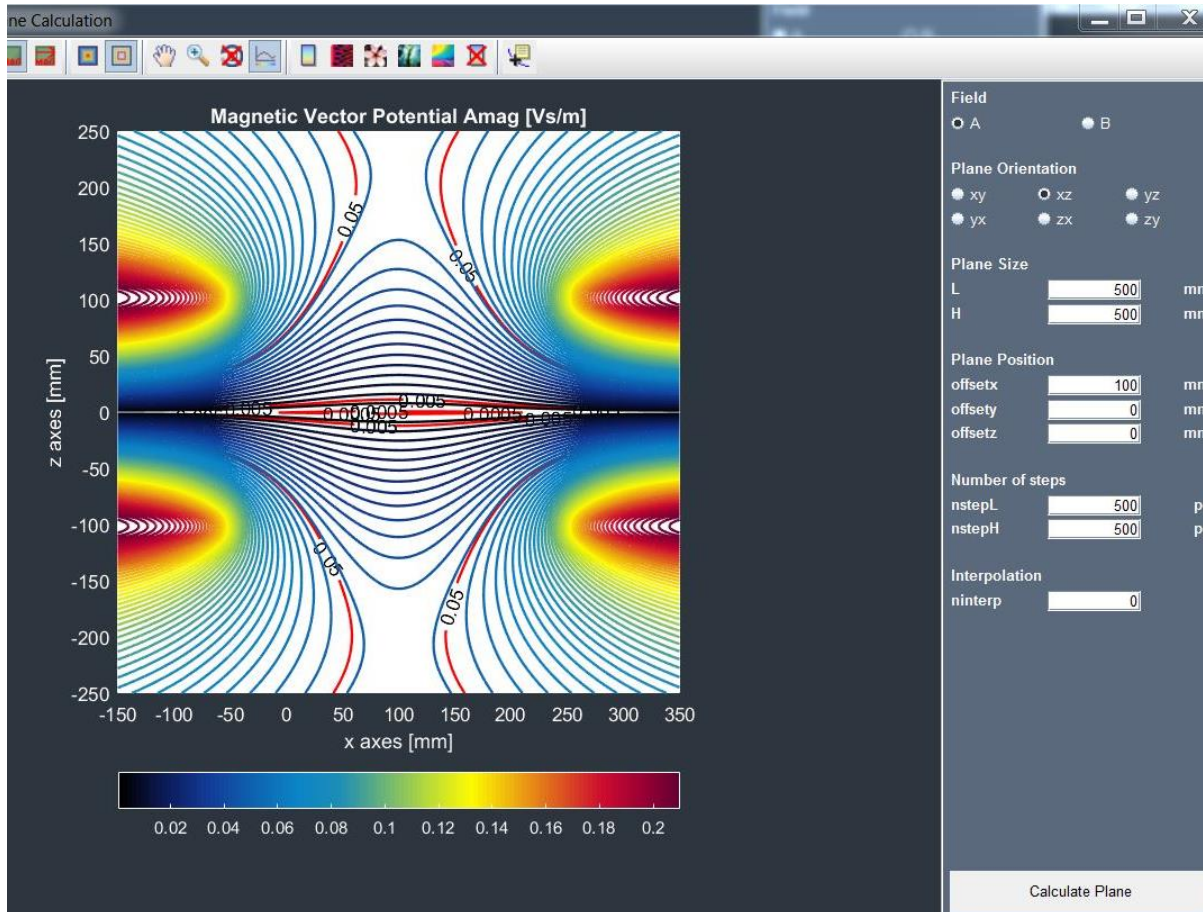




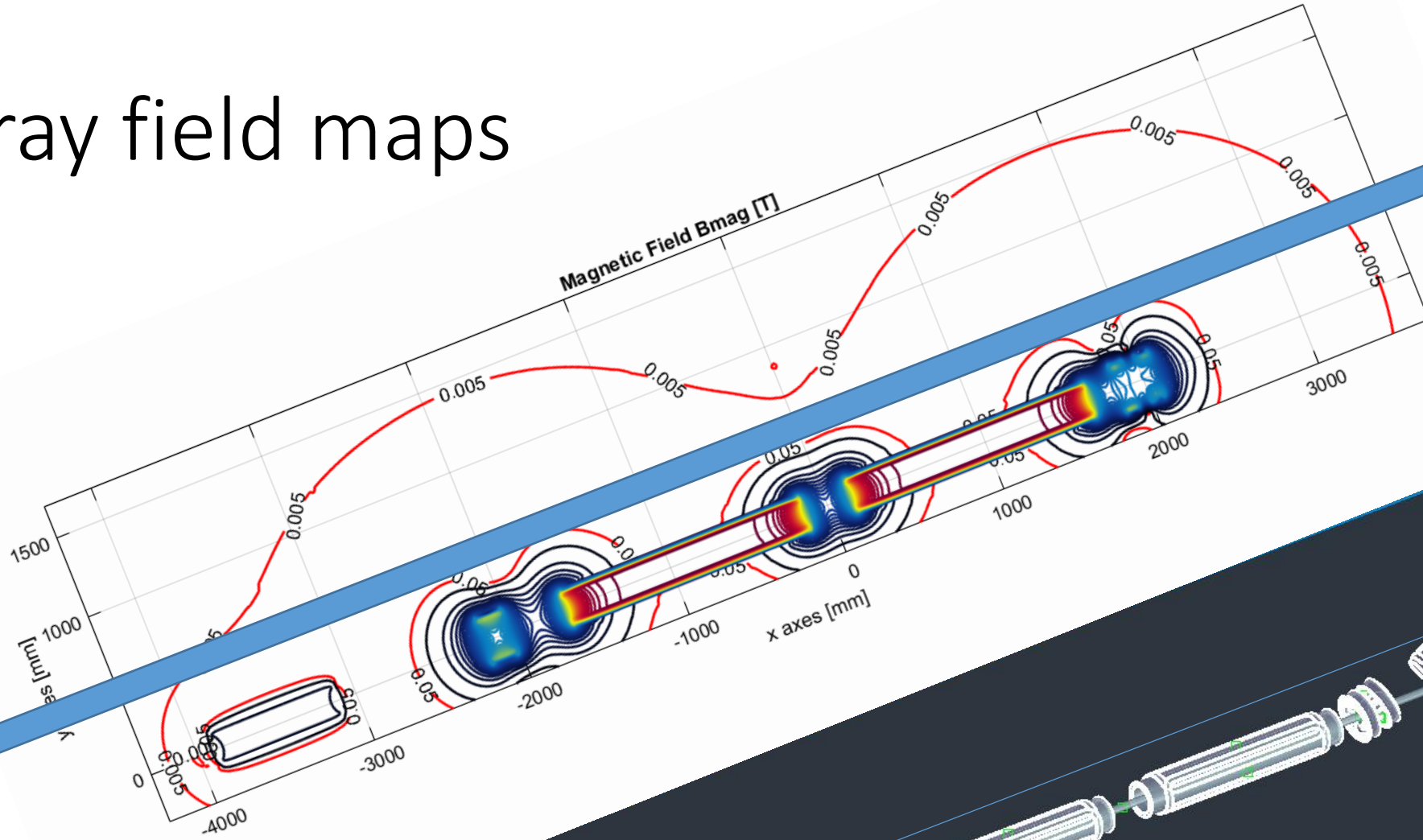
# Gap between the the two 5T 1.5 m long coils

Vector potential between the two 5T coils  
so can think of it as flux lines, could play with  
the gap!

Field in the gap

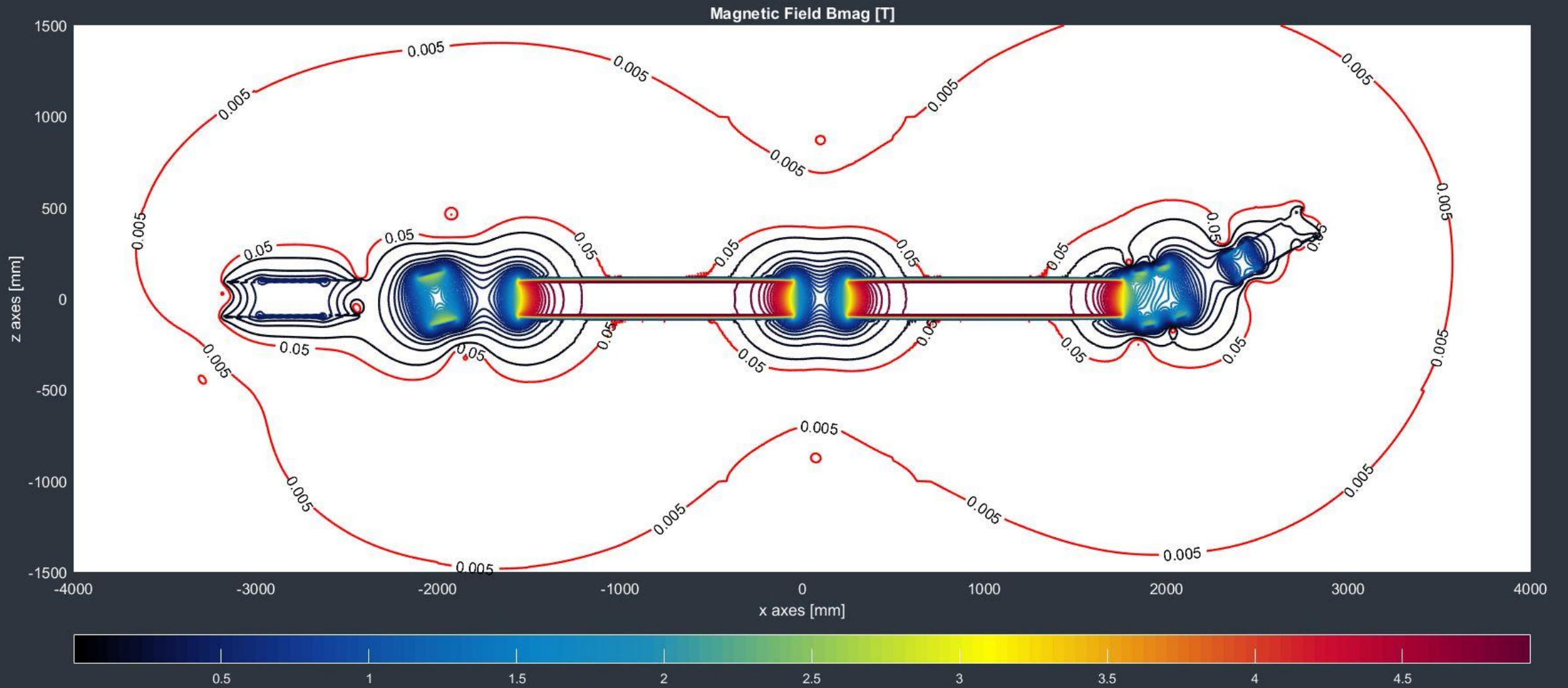


# Stray field maps



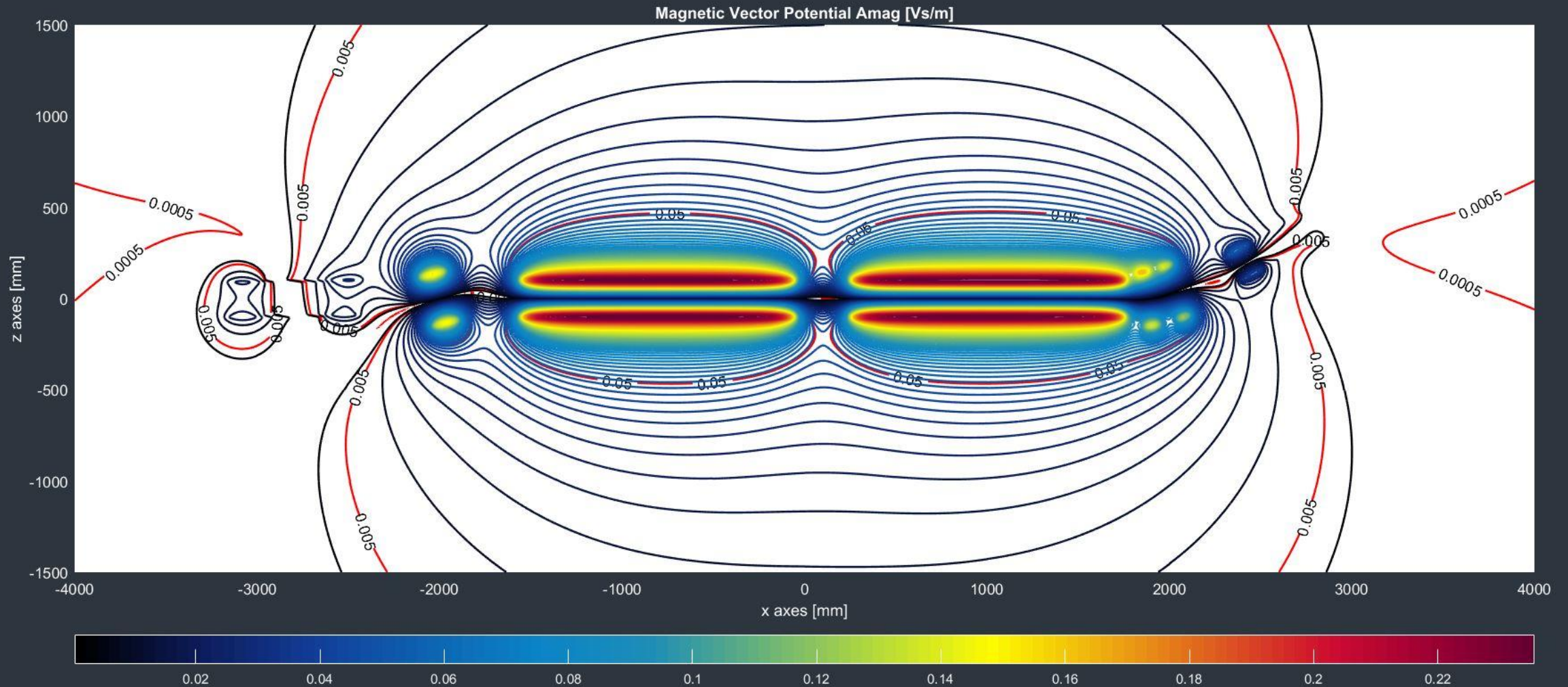
Stray field T need to look at the fields in the other adjacent beam when we have final design .

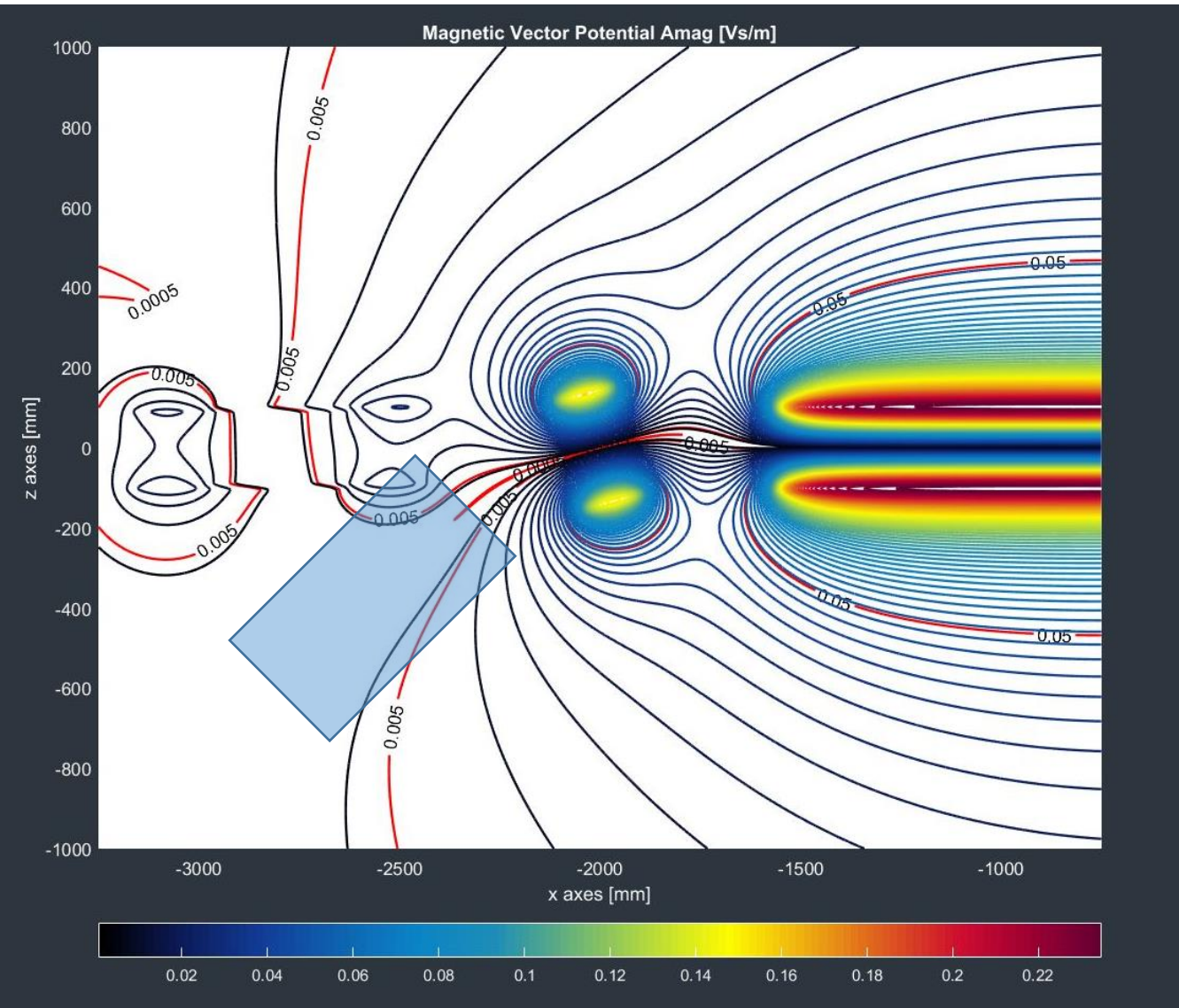
# Vertical stray field map



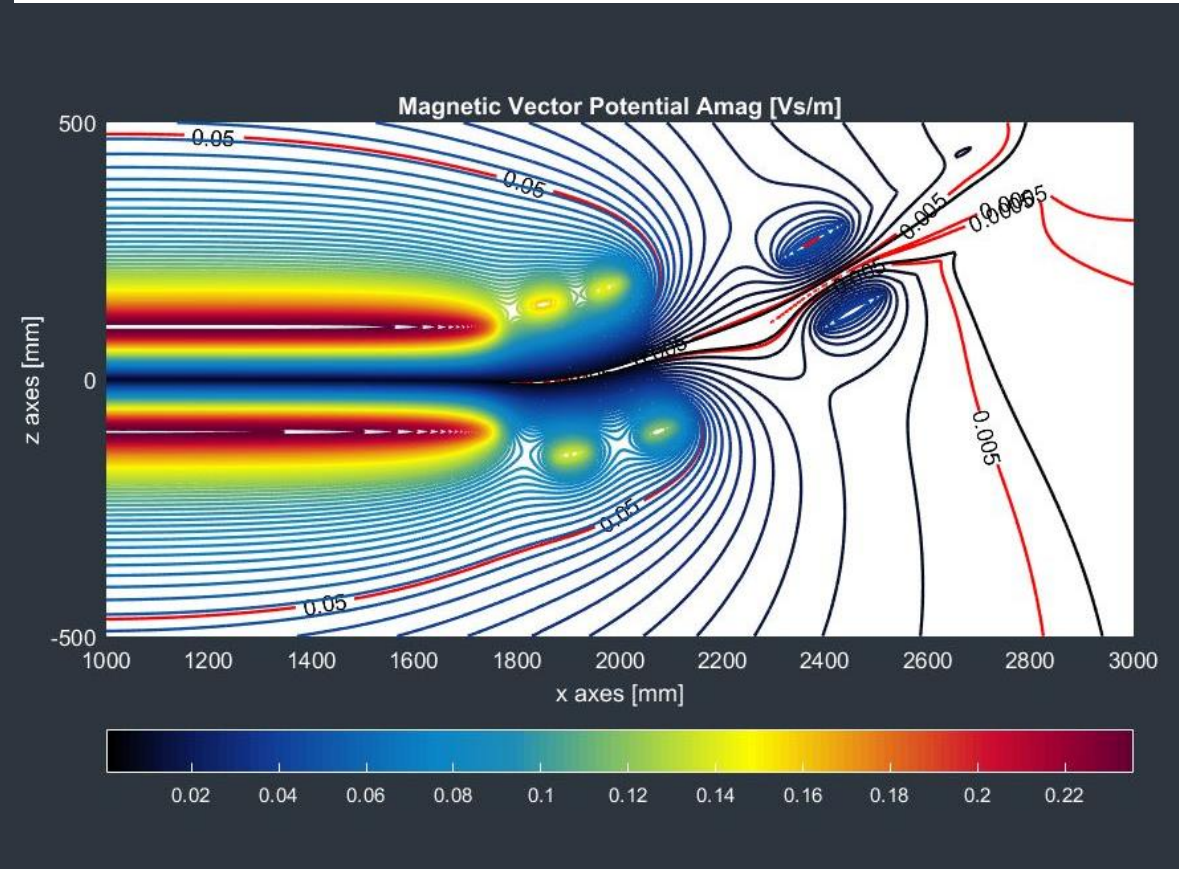


# Vector Potential $\sim$ flux lines





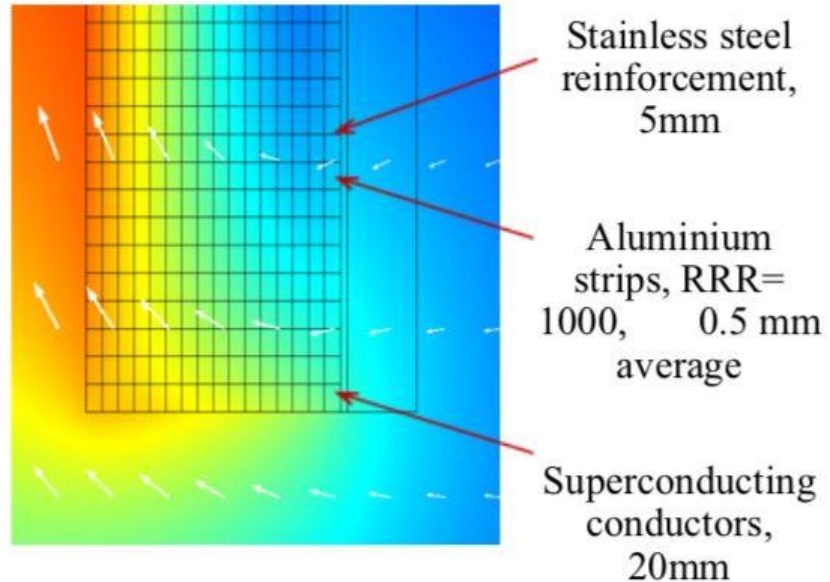
Path from solenoid to dump



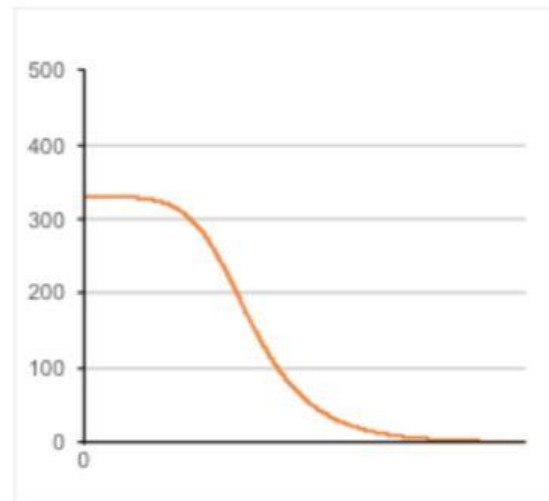
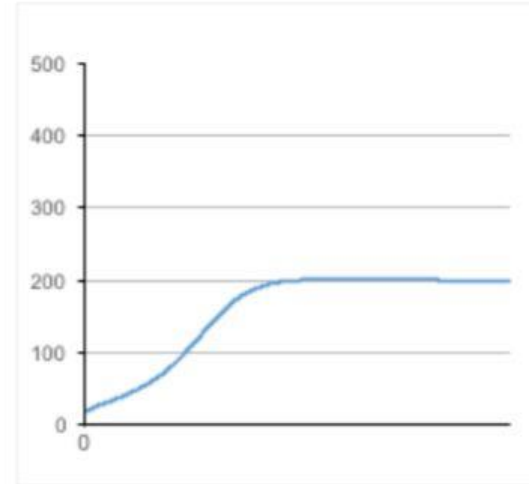
Path from electrons gun to bend coils to main solenoids



## Aluminium quench propagation strips



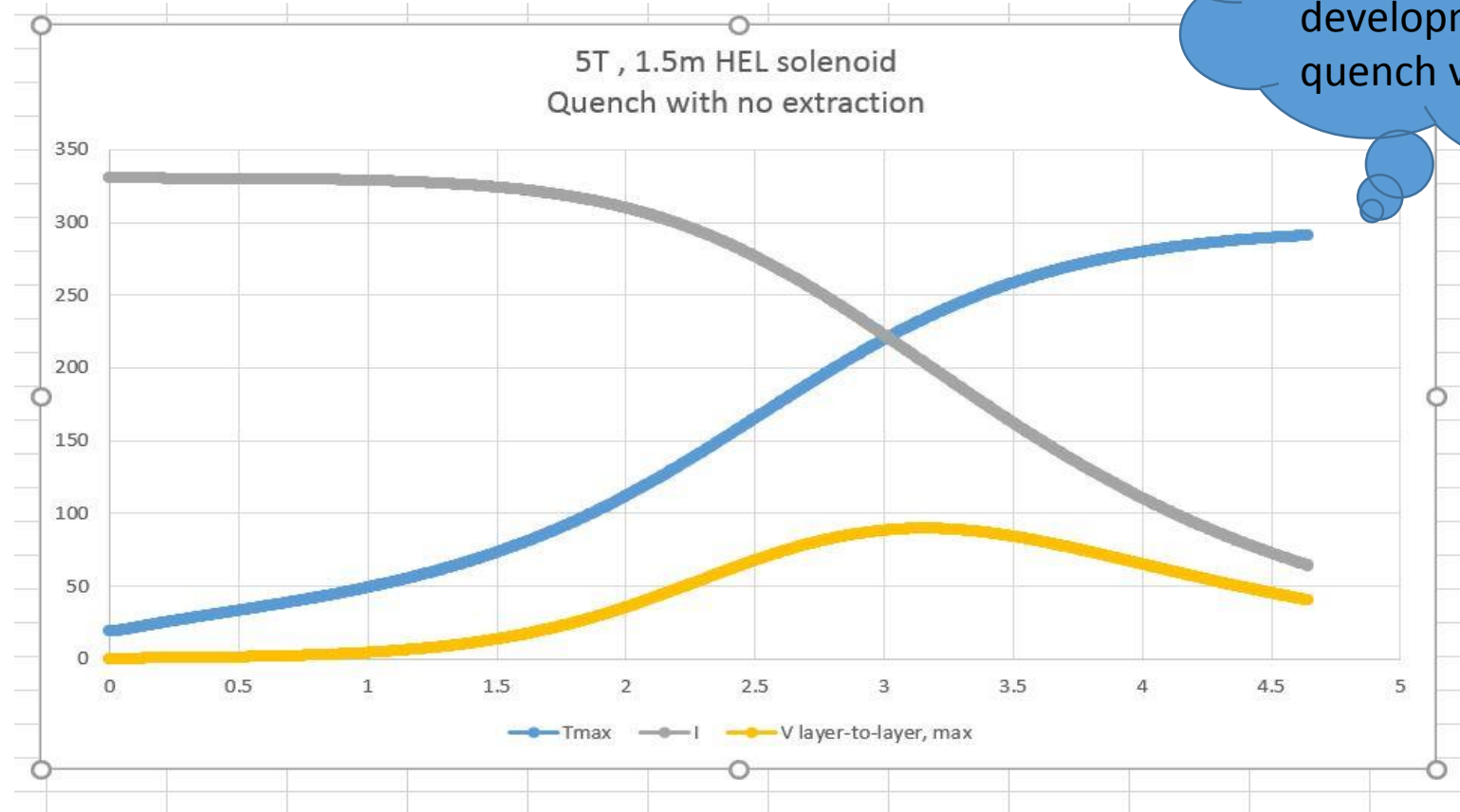
- Aluminium quench propagation strips □ Accelerates quench propagation
- Hotspot temperature reduced from 440 K to 202 K
- Intrinsically self-protected magnet
- Compatible with extraction (redundant protection mechanism in case of dump extraction switch failure)



natural quench, no extraction system, but with high purity aluminium strips. its the 4 T ` 3m coil , so we need to repeat the calculation for the 5T ~ 1.5m coil hot spot should go down as energy/volume magnet half as long/coil.



# 5T coil 1.5m long



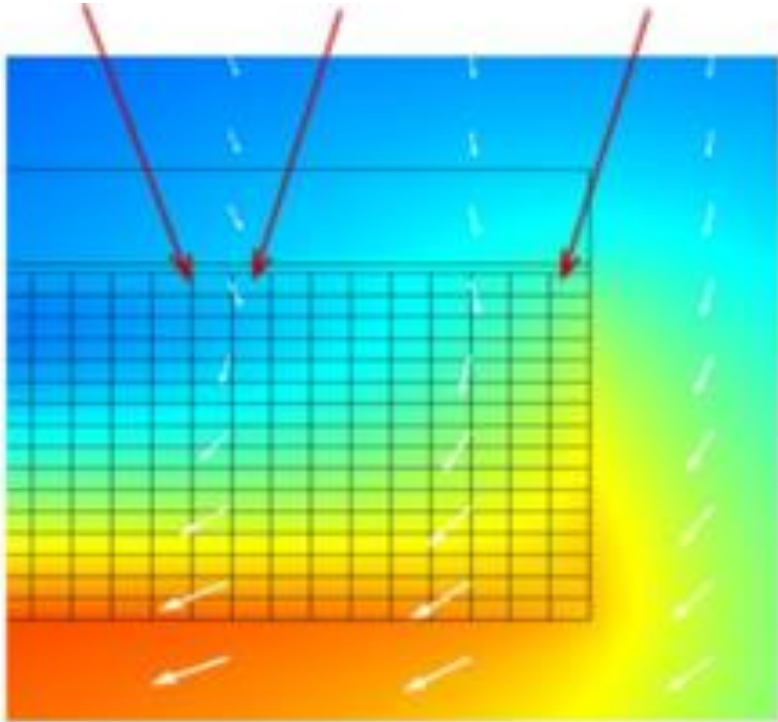
A little too hot for me!  
So! EE or some coil development to accelerate quench velocity

Natural quench no extraction 5T -1.5m coil. 300K 100V

Hot spot too high! Voltage ok

# 5T coil 1.5 m long with high purity Aluminum Propagation strips.

Aluminium  
strips, RRR=  
1000, 0.5 mm  
average



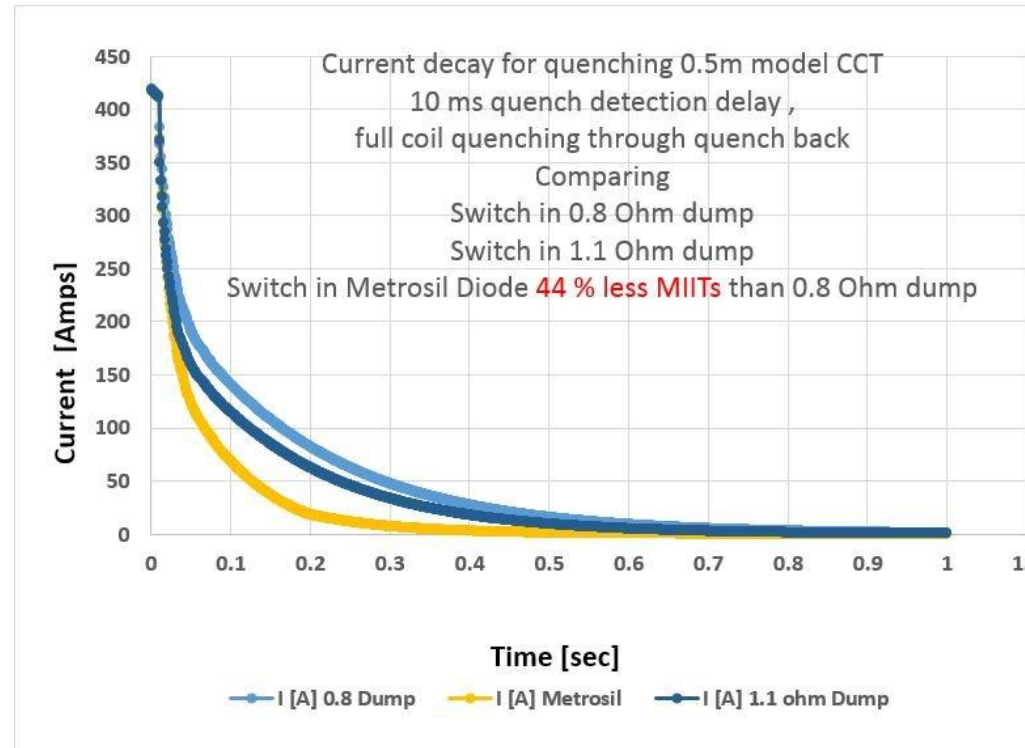
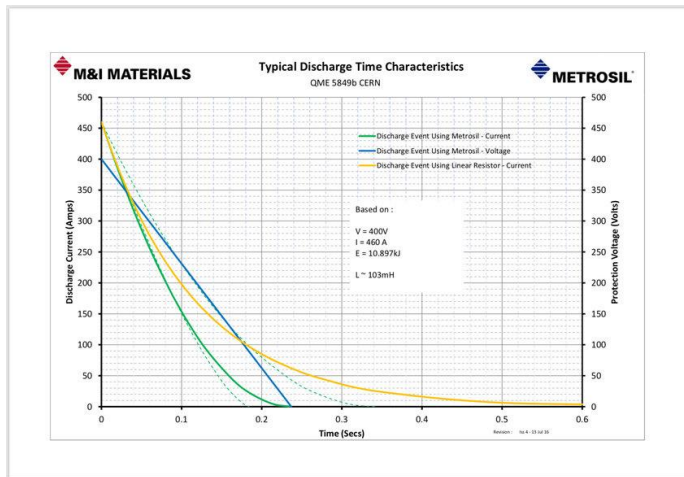
- With Aluminium quench propagation strips, the 1.5 m 5T HEL solenoids would be self-protected. But it ended up above 200 K, something like 240?.
- There are some other things to look at:  
Quench-back cylinder would help a lot.

Base line!! should be that we protect these magnets with **extraction**, so an active system with detection, to trigger switch and either, std Resistor or Metrosil!  
Constant voltage extraction.



# Metrosil new High performance energy extraction system

We see an impressive reduction in MIITs with the Metrosil 44% for the High Luminosity D2 CCT orbit corrector being tested



**METROSIL**

### DISC INTRODUCTION

**Metrosil discs introduction**  
 Metrosil discs are available in sizes from 25mm to 150mm diameter. They can be supplied as plain connected discs or mounted on central studs either as single discs or as multiple assemblies arranged in series or parallel. The smallest size can be supplied with suitable wire terminations and encapsulated in PVC or other materials as required.

**Metrosil applications**  
 Most of the applications of Metrosil make use of its unique properties to provide an "electrical safety valve" for protecting equipment and insulation from the effects of over voltage.

**Protection of field coils, contactor coils, relay coils and solenoids.**  
 When an inductive coil is broken suddenly, there is a transient rise in voltage across the inductance, which can be 10 to 20 times the supply voltage and may damage insulation or other components. The source of this overvoltage is the energy that is stored in the magnetic field of the inductance at the moment of switching off. It is therefore essential to provide some means for this energy to dissipate itself harmlessly.

**Other applications**  
 • Current and voltage transformer protection  
 • Telecommunication equipment protection  
 • Improving the sensitivity and protection of high impedance relays.  
 • Negative line protection.

**Fig 1**  
 V-I relationship for Metrosil resistors

**Specification**  
 Varying the composition and processing conditions provided in the manufacture of Metrosil discs can achieve a broad spectrum of electrical characteristics. A large number of electrical specifications are available as standard items and others can be manufactured on request.

**EMAP protection**  
 • Tractor units  
 • Motor protection

**4-95kV**  
 Without Metrosil protection

**600V**  
 With Metrosil type 300A(1) passing 150kA connected across the coil

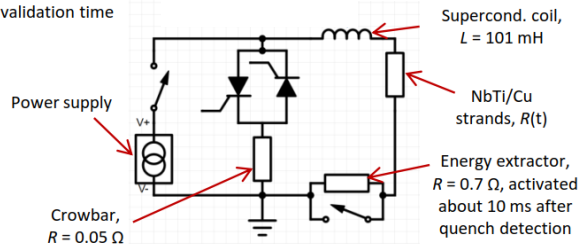
**Typical waveforms of voltage surge across a 600V relay contact coil during 150kA current in interrupting the supply**

**Both the linear resistor and Metrosil limit the overvoltage to 800V at 1 sample. The use of Metrosil reduces the power losses at 250V to 2.5 watts compared to 160 watts in the linear resistor.**

**SILICON CARBIDE BURST PROTECTION**

## Extraction switch and dump

Quench detection:  
 $V_{thr} = 0.1V$ ,  
 10 ms quench  
 validation time



# Conclusions (1): Magnetic design

- The two - 5 tesla 1.5 m coil design is in the fine tuning stage.
- The other solenoid will use the same conductor and follow the detailed insulation and construction.
- The CCT coil used to correct the vertical integral component of the two bending coils. Is a copy of the 0.5m D2 corrector with smaller aperture.
- The coil layout in terms of relative position is still evolving but will not effect the coil design.
- The Vertical, Horizontal, Dipole low current coils could follow a classical design or possibly a CCT design. Just need to look at which has the lowest cost.

# Conclusion (2): Quench

- The 5 Tesla 1.5 m long solenoids.
  - Base line, is energy extraction (EE) with switch and ether classical resistor or Mertosil (better result).
  - Need to check bus bar protection, but if we stay with the EE this is probably covered.
  - Still looking for a fully passive solution (this will require a model test coil, may be the E-gun coil to fully understand quench velocity through insulation).
- Bending coils
  - This is a low inductance coil identical constriction to the 1.5 m so the Aluminum propagation will give low hot spot and voltages.
- CCT integral correction
  - Coil is very close to the CCT LHC High-Lumi D2 corrector 0.5 m model, this is self protecting.
- Vertical , Horizontal ,and Quad - fine tuning Correctors.
  - All very low current so can be self protecting.
- Bus Bar Protection
  - Assumption: short superconducting bus distance  $\sim 3$ m max from coil to cold-to-warm current leads, then resistive leads to power supply. The cold section can be sized to be self protecting using copper shunt.

