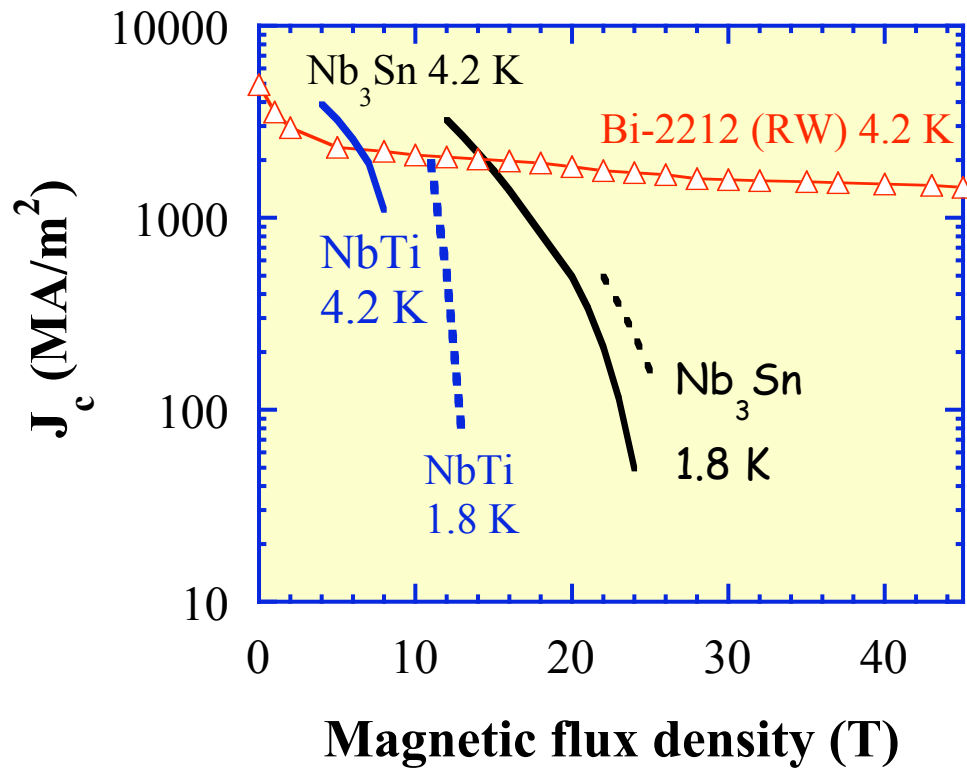




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Task 4:
Very high field HTS dipole insert
P. Tixador (G-INP)

Motivation: quest for higher fields



LTS:
Limit ≈ 23 T

HTS:
Attractive
No $J_c(B)$ limit

Introduction: task 4 objective

Construction of an **6 T** HTS dipole insert within the **14 T** Nb₃Sn 100 mm dipole magnet (20 T)

Three subtasks defined:

- 4.1 Specification, characterization and quench modelling
- 4.2 Design, construction and test of solenoid insert coils
- 4.3 Design, construction and test of dipole insert coils

Particular constraints:

- high mechanical stress
- conductor bending radius

State of the art: HTS dipoles

- Many HTS solenoids (5.4 T (Bi) - 9.8 T (Y))
- Only a few HTS dipoles

T
e
s
t



LBL

- 2x6 turn Racetrack, Impregnated
- 17 wire Bi-2212 Rutherford Cable
- W & R at 890° in pure O₂
- 1.11 T @ 4.2 K (1.48 T designed)

Design



Danish
Technolog.
Institute
InnovAcc

- 18 YBCO coils
- T₀ = 20 K
- I₀ = 167 A (80% load line)
- Aperture field: 3.6 T (Ø = 52 mm)

EuCARD
Challenge!

WP7 task 4 partners



TAMPERE UNIVERSITY OF TECHNOLOGY

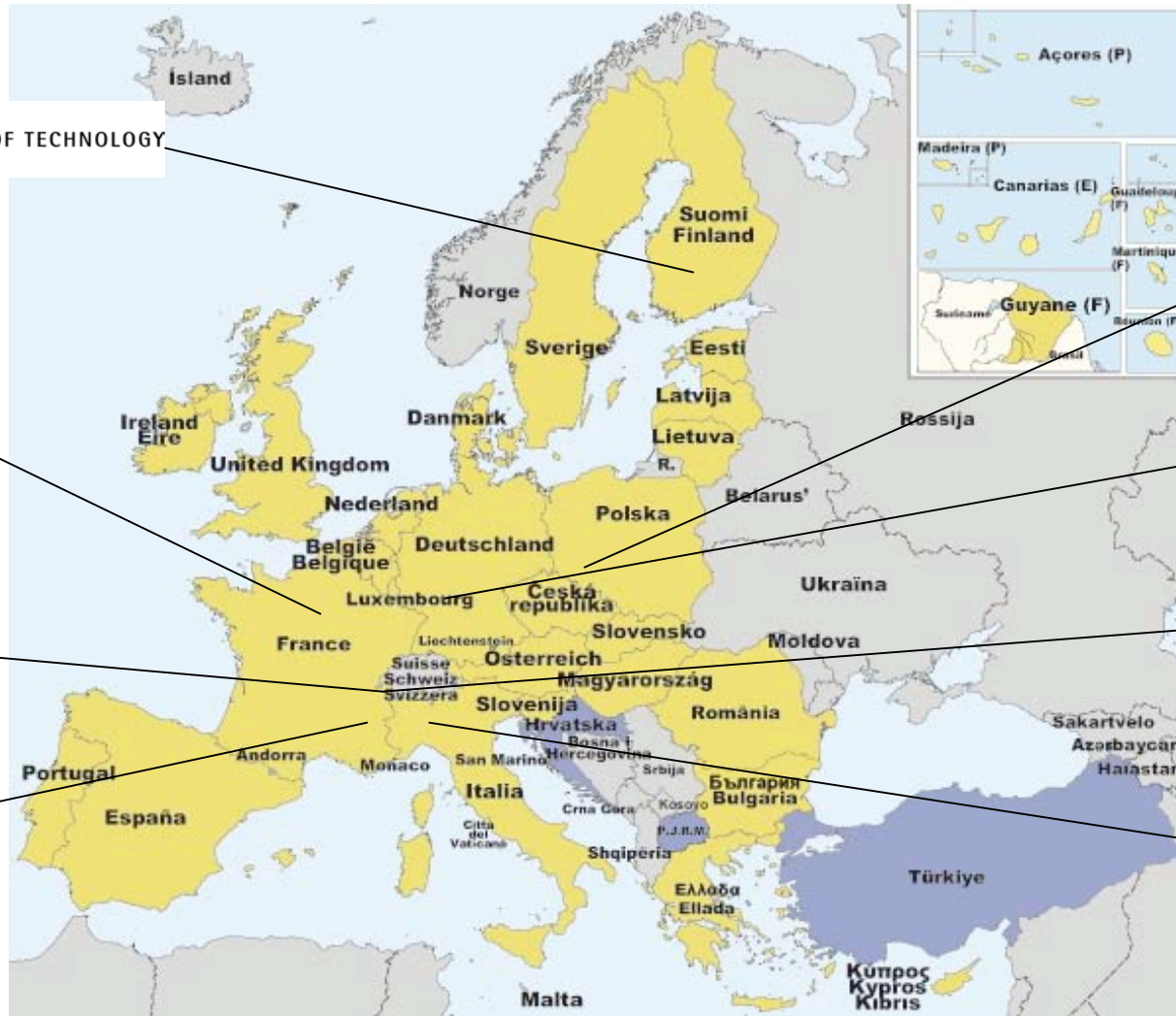
Irfu

cea

saclay



Wroclaw
University
of Technology



Outline



- HTS wire/conductor
- New characterization equipment
- Modelling works and protection
- Preliminary magnet designs & construction
- Conclusion and future works

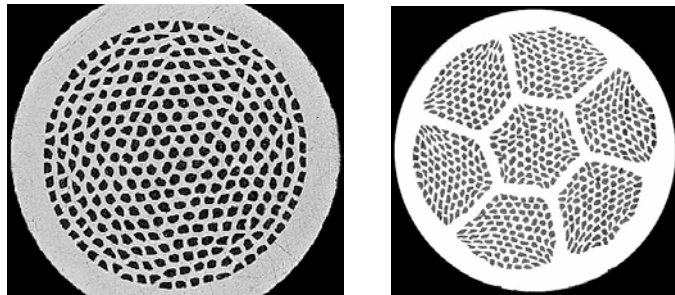


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HTS wire / conductor
for high field dipole

Bi-2212 (1G) / YBaCuO (2G)

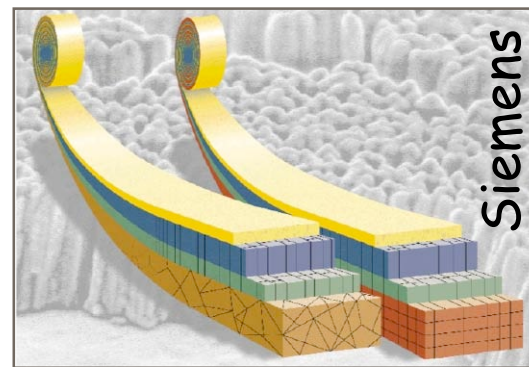
1 G (BiSrCaCuO)
PIT round wires



Metallurgical process

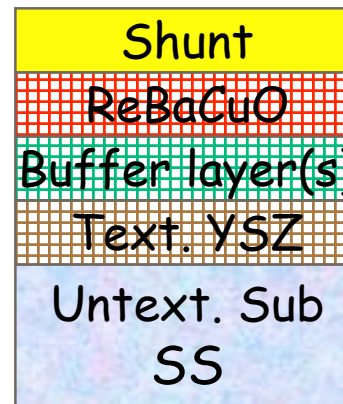
- R & W
- **W & R**

2 G (YBaCuO)
Coated Conductors / tapes

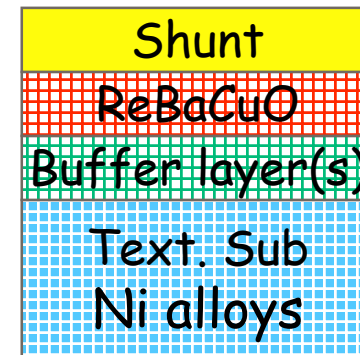


Thin film technology

- IBAD
- RABiTS



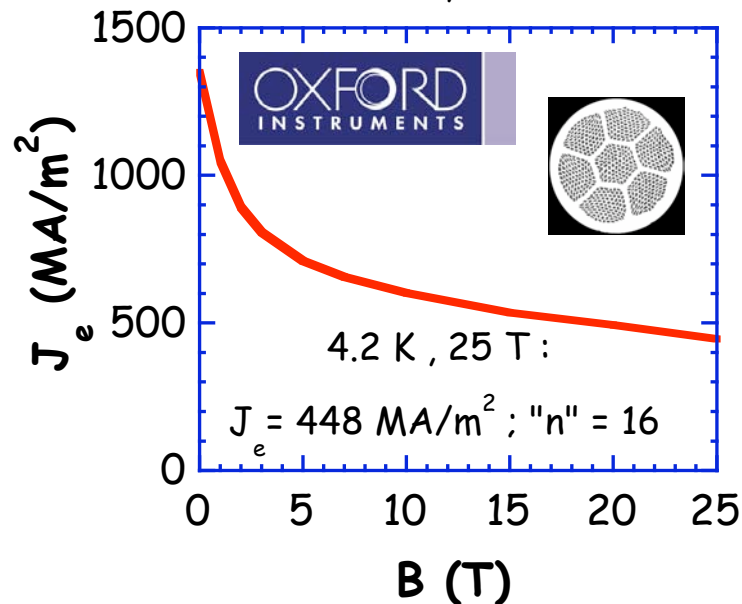
Ion Beam Assisted Deposition



Rolling Assisted Biaxially Textured Substrates

Bi-2212 : OST

OST 2212 Wire (Billet PMM030224)
 $\varnothing = 0.8 \text{ mm}$, SC : 28 %



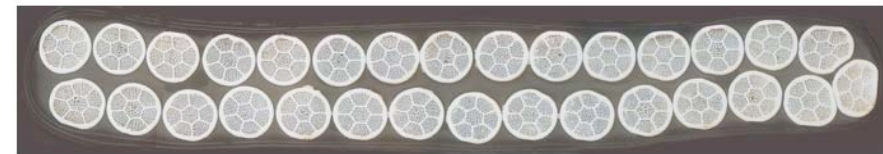
A. Vostner

(EFDA meeting, Barcelona 8-9 May 2007)

But: $J_e = 200 \text{ MA/m}^2$ (15 T, 4.2 K)
(Bi-2212 purchased by CERN for EuCARD)



20 strand Rutherford cable
 $I_c > 3\,000 \text{ A}$ @ 4.2 K



30 strand Rutherford cable
 $I_c > 4\,000 \text{ A}$ @ 4.2 K

Nexans Korea

Courtesy A. Allais



But large degradations
LBL: 2.6 T => 1.48 T

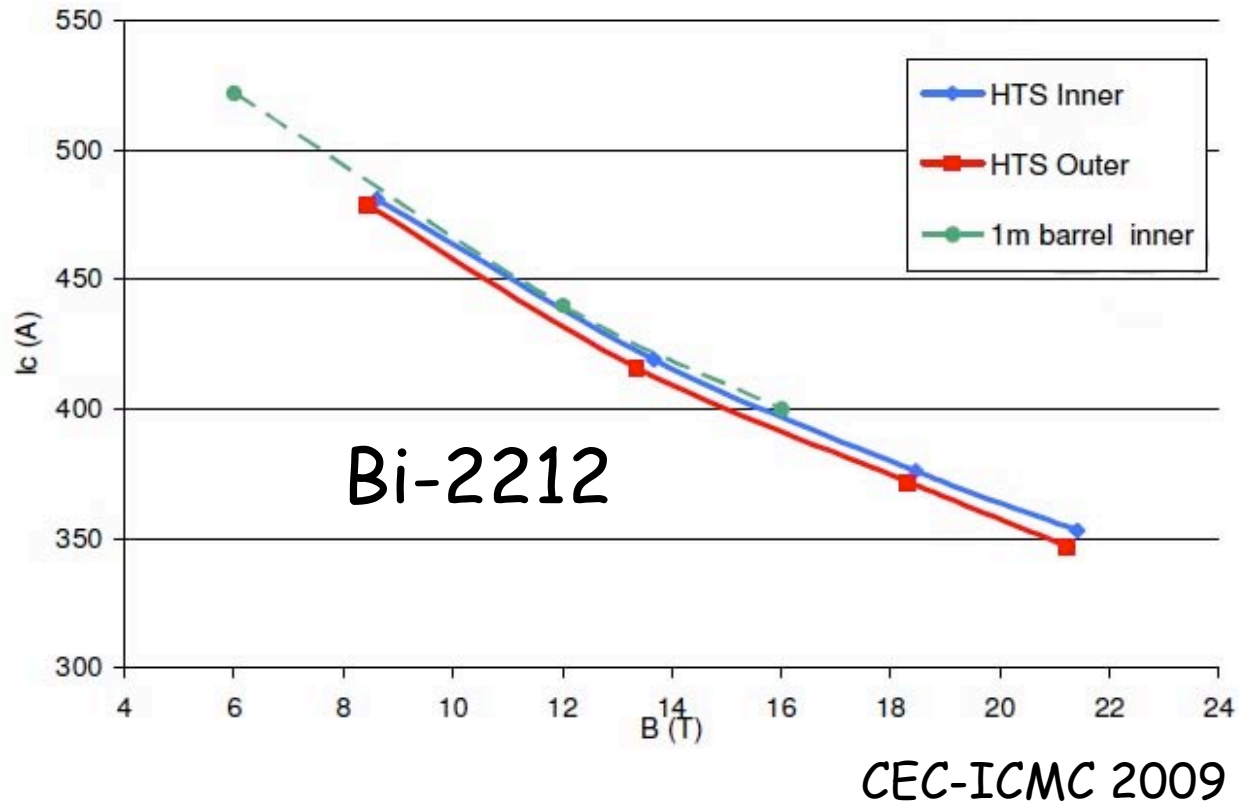
Bi-2212 heat treatment: a challenge!

One of the major issues for Bi-2212

- Accurate temperature profile (ΔT : a few K)
- Temperature homogeneity over the conductor volume
 - Not a real issue for sample/Vamas
 - Difficult for a coil (furnace dimensions)
- Sensitive to C, C contaminations, ...
- Oxygenation is a key part
- Relative brittleness after reaction (less / Nb_3Sn)
- Degradations after treatments (LBL: 1.48 T \Rightarrow 1.11 T)

Bi-2212 Heat treatment

- OST has achieved progress in heat treat^t



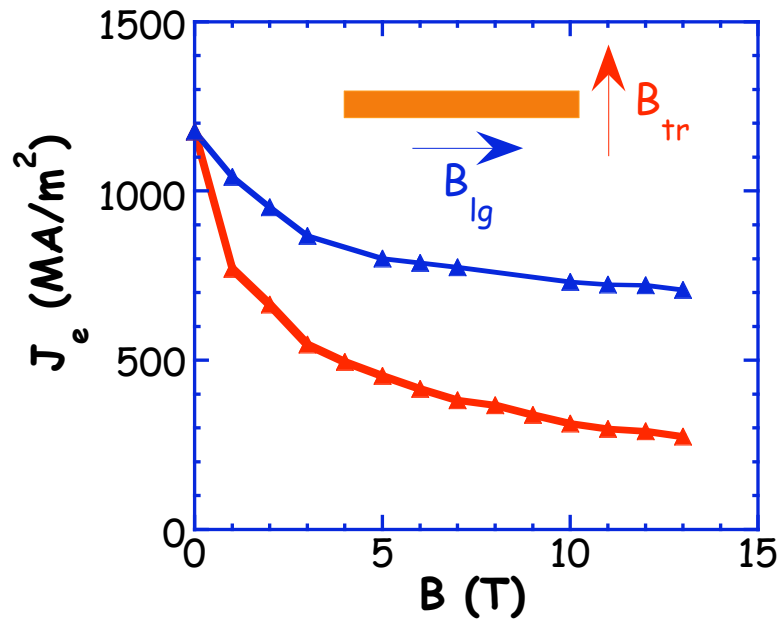
Heat treatment:
task in itself!



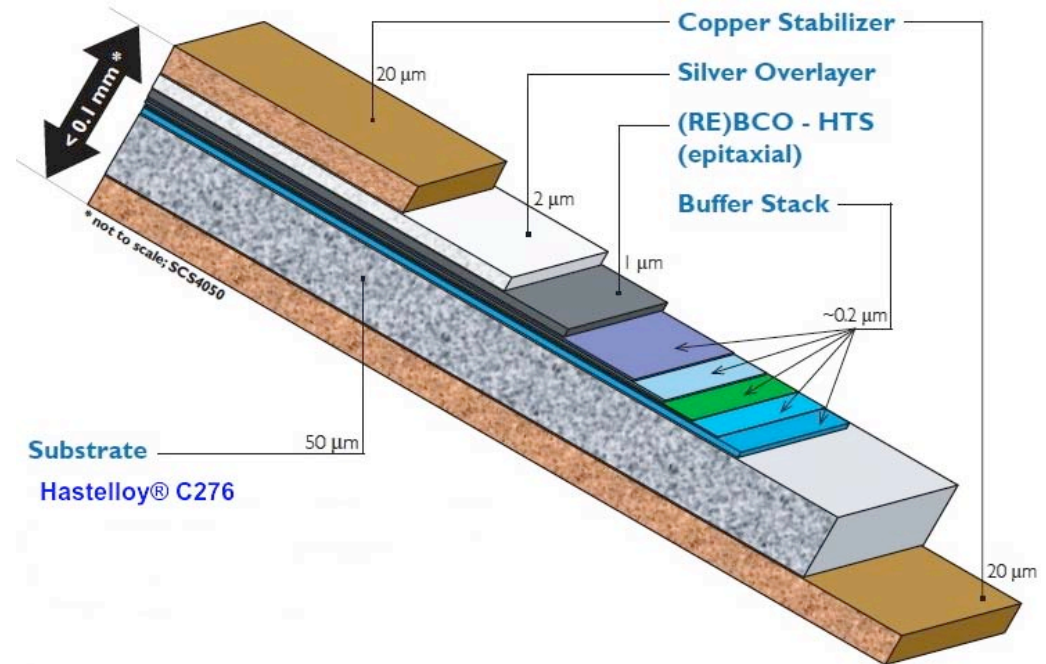
OST agrees to
help and make

YBCO Coated conductor

YBaCuO coated conductor @ 4.2 K
 Super Power - 4.1 mm x 0.095 mm



Measured data (LNCMI)



IBAD route ($\sigma = 550 \text{ MPa}$)
 2 x 20 μm Cu stabilizer layers

YBCO Coated conductor cable

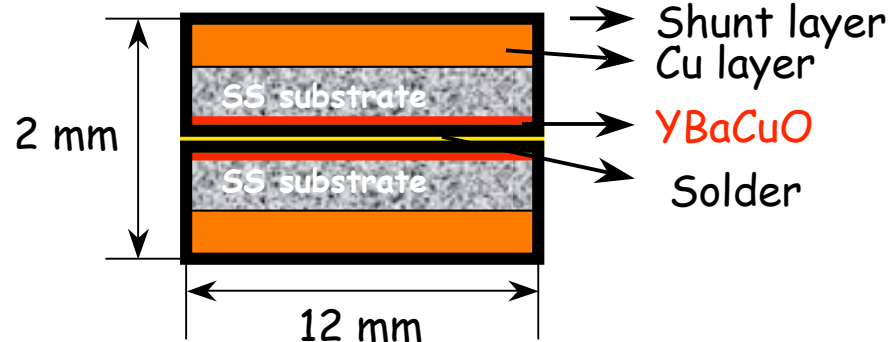
Today solution: Roebel bar



© 2009 General Cable Superconductors

- Transposed
- Expensive (29 k€ 10 m 3000 A (15T 4K))
- Some I_c degradation

Possible alternative:
double YBaCuO tape conductor



YBaCuO:

- close to the neutral fibre/axis
- low AC losses (no transposition)



2 x this conductor

Conductor transposition pole to pole

$$\Rightarrow \approx 4 \times 700 = 2800 \text{ A (15 T 4K)}$$

2.4 k€ 10 m (59 \$/m)

Bi-2212 versus YBCO: summary

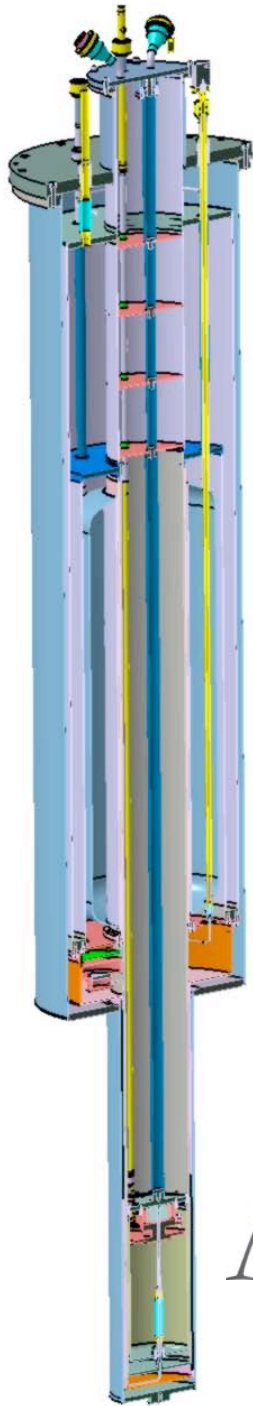
	Bi-2212	YBaCuO
	High current cable (Rutherford cable) Isotropic	W & O Material of the future Perf. (J_c & stress (IBAD))
	Heat treatment (R & W) Mechanical performances Long lengths without defect	High current cable Lengths Coil ends Anisotropic



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New characterization equipment
Solenoid test station

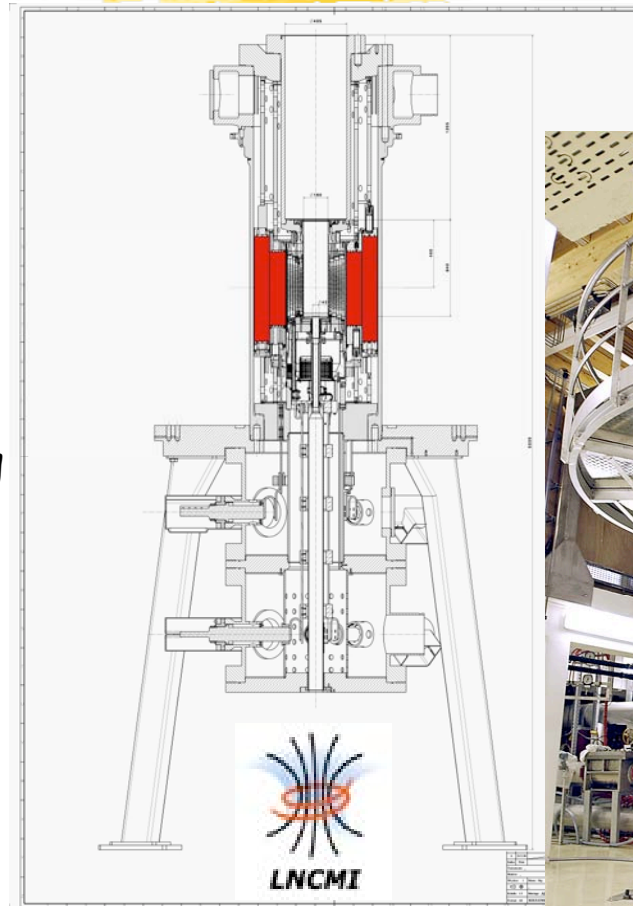
Solenoid test bench



Variable
temperature
cryostat
(4.2 K - 80 K)

- Gas cooling
- Conduction cooling

$\varnothing_e = 130 \text{ mm}$



20 T facility





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Modelling works
Benchmark of quench programs
Results for NbTi test winding
TUT (Tampere University of Technology)
LASA (Lab. for Accelerators and Applied Supercond.)

Quench programs

- TUT:
 - heat diffusion equations
- LASA:
 - propagation velocities

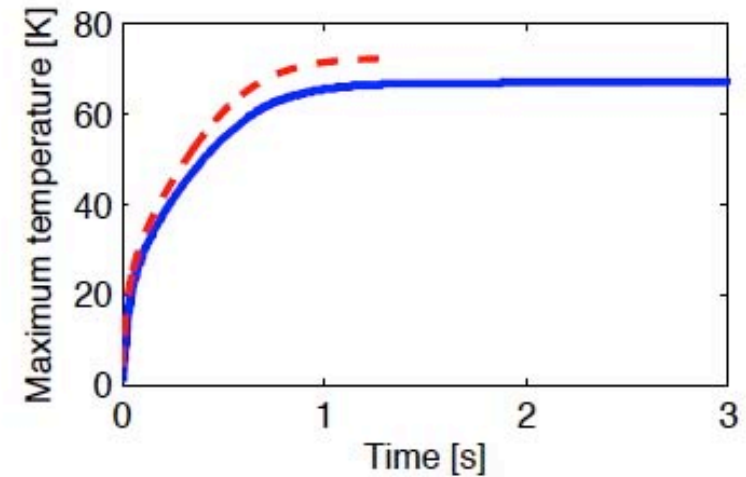
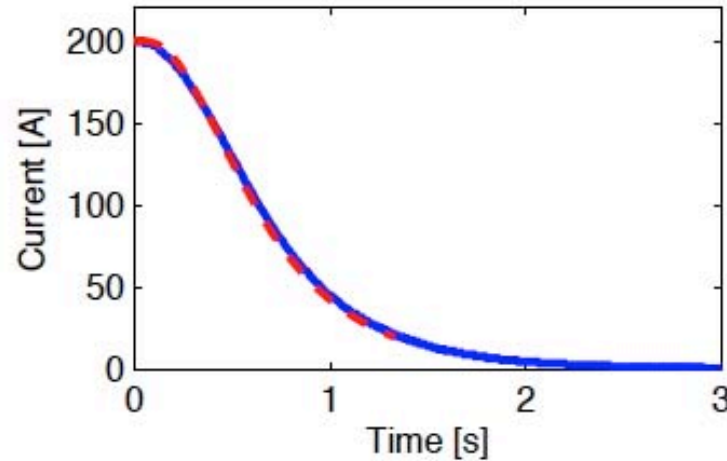
Bench mark problem:
NbTi solenoid
Result comparisons

$\varnothing_e / \varnothing_i$ (mm)	25/50
h (mm)	200
Radial layers	26
Turn per layer	182
I_o	200 A
T_o	4.2 K
SC	NbTi
SC:Cu ratio	2
\varnothing_e isolated (mm)	1.1
rrr	170

Benchmark results: comparisons 1/2

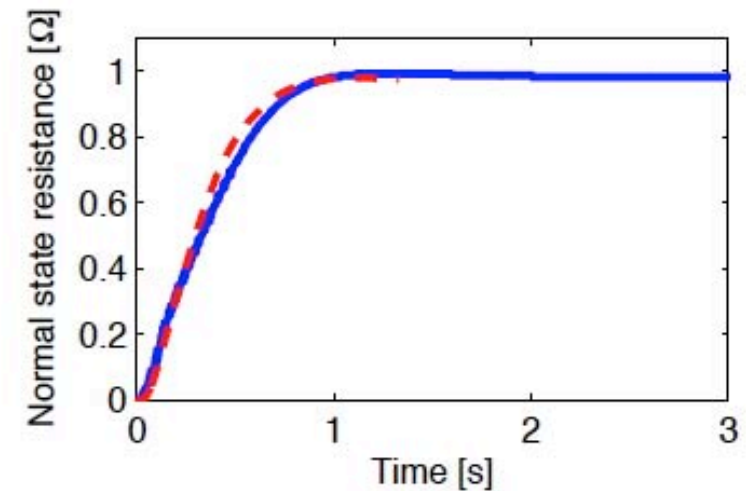
Red:
TUT

Blue:
INFN



Conclusions

- The two different approaches work well on a coil where the transition is characterized by current sharing model
- Codes are now validated

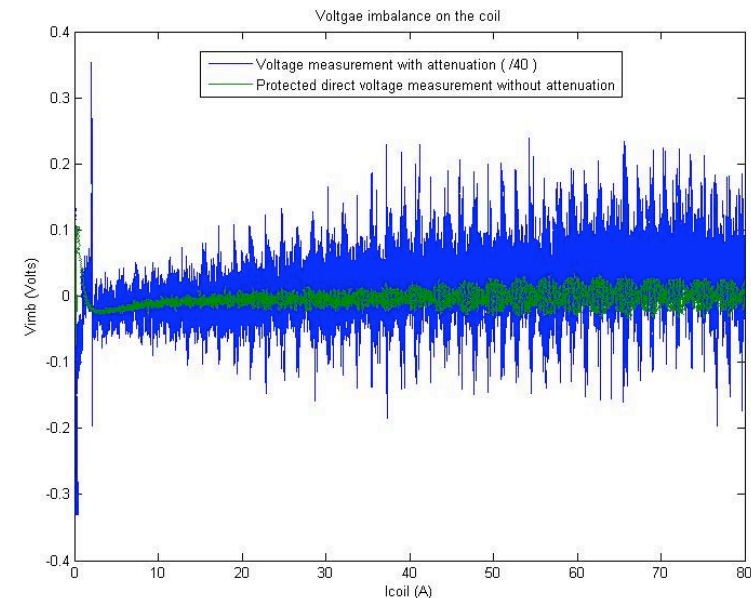


Quench: HTS magnet issue



HTS:

- Operation far from T_c
- Low propagation velocities
- Concentrated quench



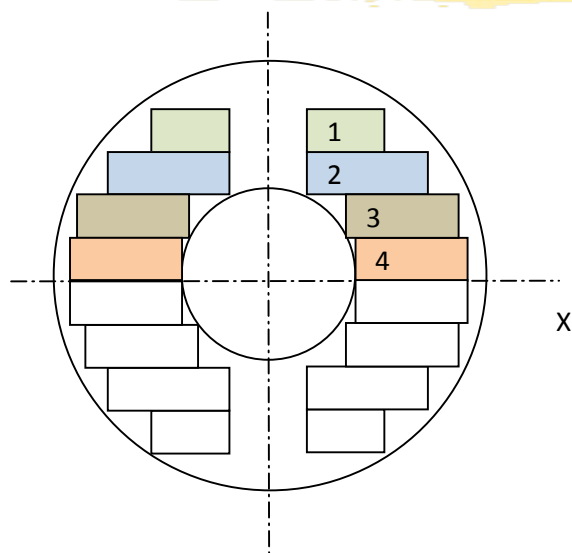
Improved detection
(patented)



Preliminary magnet designs & construction

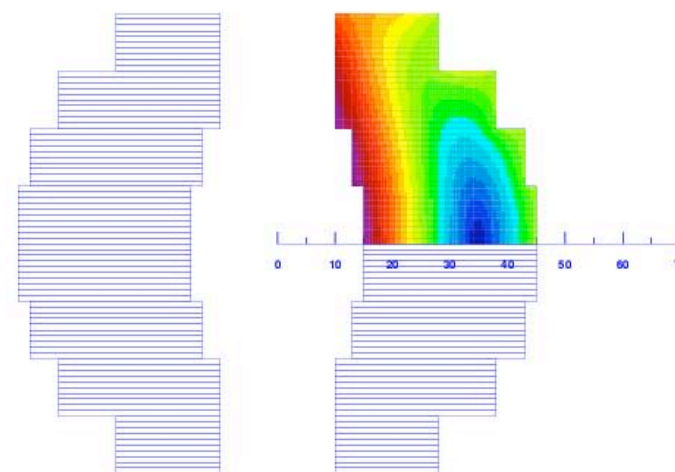
- | Dipole
- | Solenoid

Dipole design with blocks



- 4 double pancakes
- 2 flat one
- 2 with bent end
- \varnothing_e : 98 mm

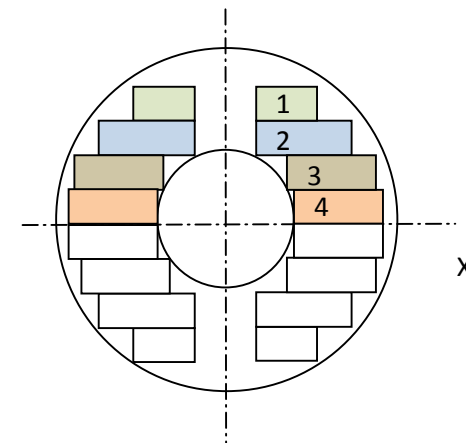
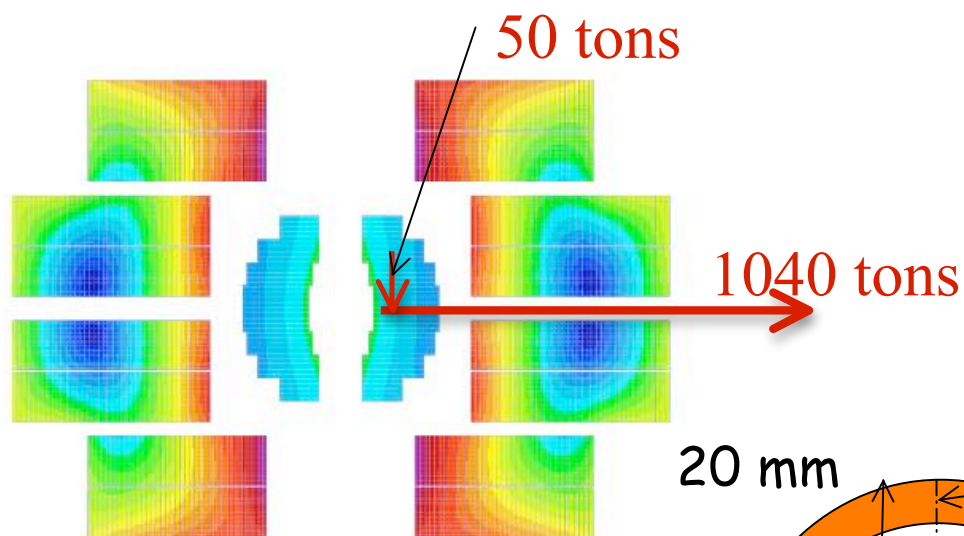
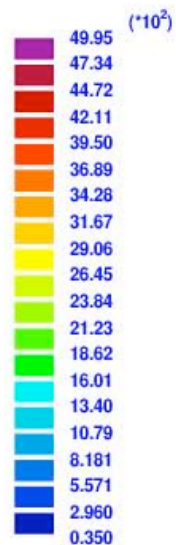
Inner bore diameter: 30 mm
287 A/mm² needed to reach 6T
Peak field 6.1T



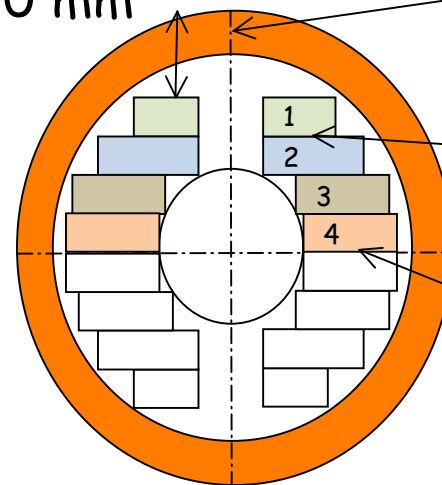
Courtesy J.M. Rey

Rough mechanical approach

|F|/L (N/M)



20 mm



Stress 540 MPa
SS tube 10 mm

Interblock
Stress 9 MPa

Mid plane
Stress 17 MPa

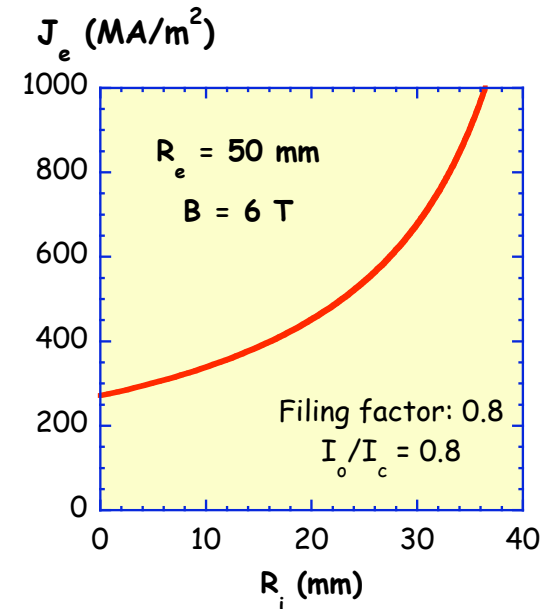
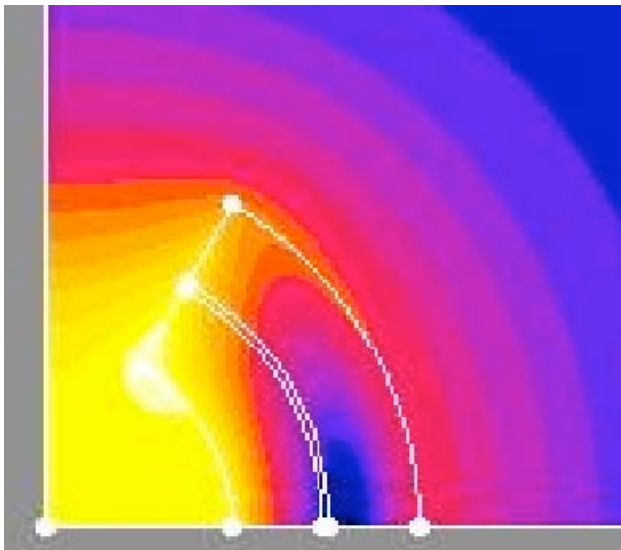
Courtesy J.M. Rey

Preliminary insert design

Magnetic flux density for an ideal cosine coil:

$$B \approx \frac{2}{\pi} \mu_o \sin\left(\frac{\beta}{2}\right) J_e (R_e - R_i)$$

(no mag. shield)

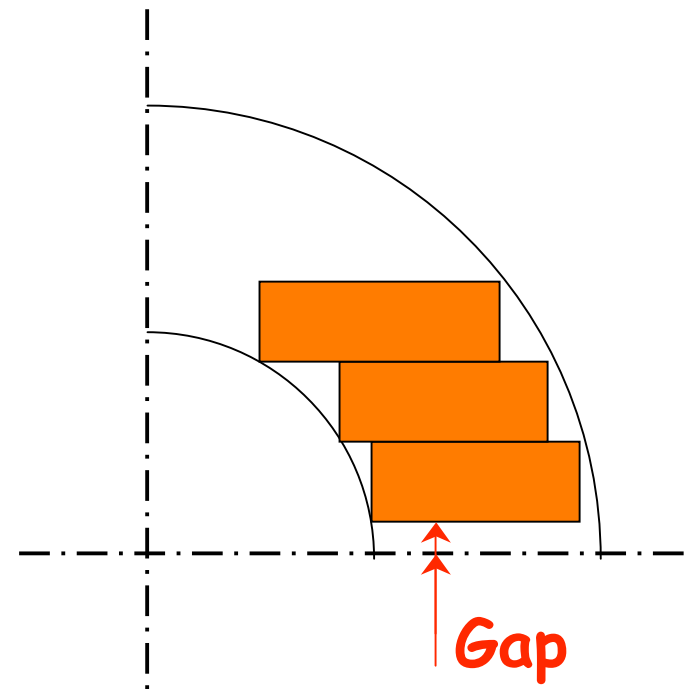
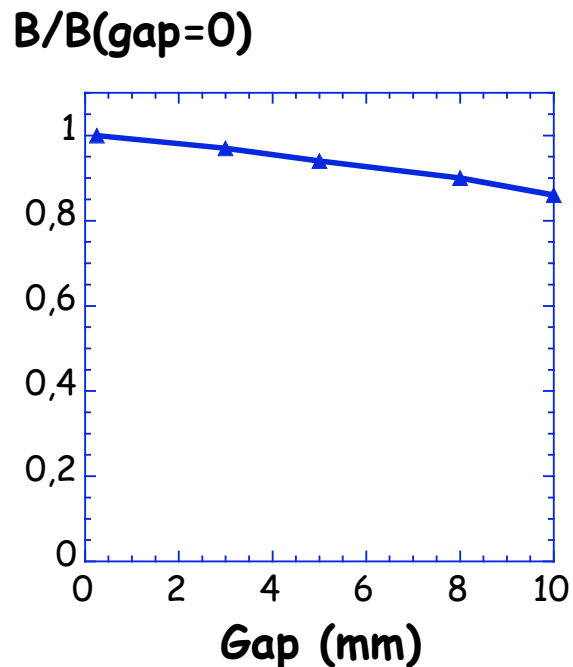


$J_e > 400$ MA/m² (20 T)

Similar result J.M. Rey

Insert with YBaCuO

Coil end issue:
influence of central airgap for the beam for flat coils



J.M. Rey configuration

Very promising way



Danish Technological Institute
InnovAcc



Courtesy N. Zangenberg

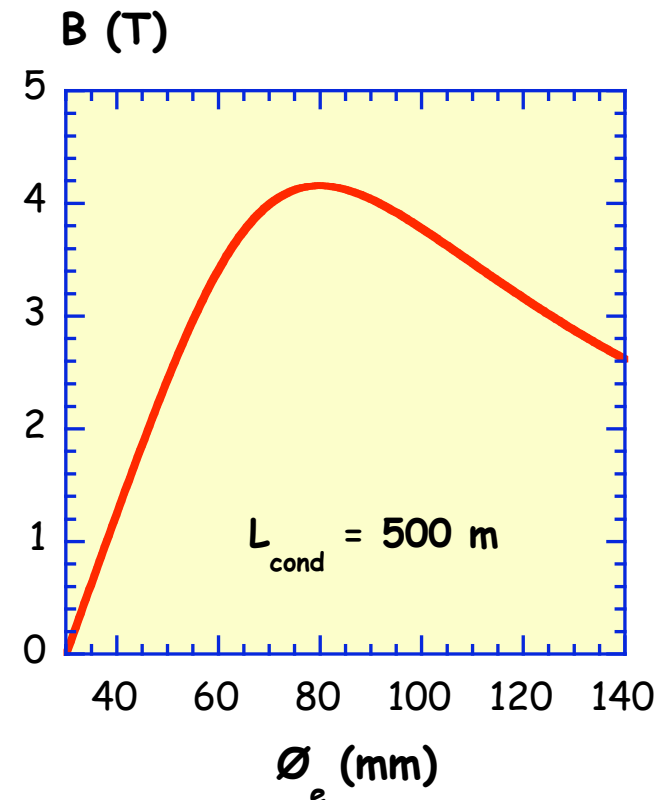
No (little) I_c degradation

Solenoids, preliminary works

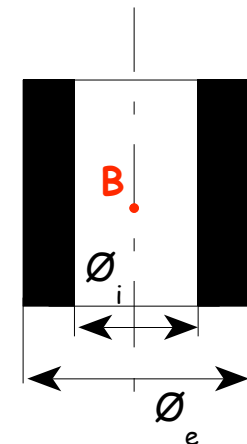
■ Optimization (B_{\max}) from given conductor length

$$B = \frac{\mu_o J_e h}{2} \ln \frac{D_e + \sqrt{D_e^2 + h^2}}{D_i + \sqrt{D_i^2 + h^2}}$$

$$vol = c_f \frac{\pi}{4} (D_e^2 - D_i^2) h = S L$$

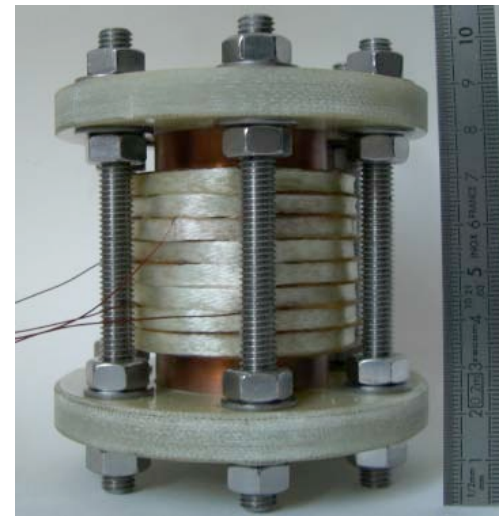
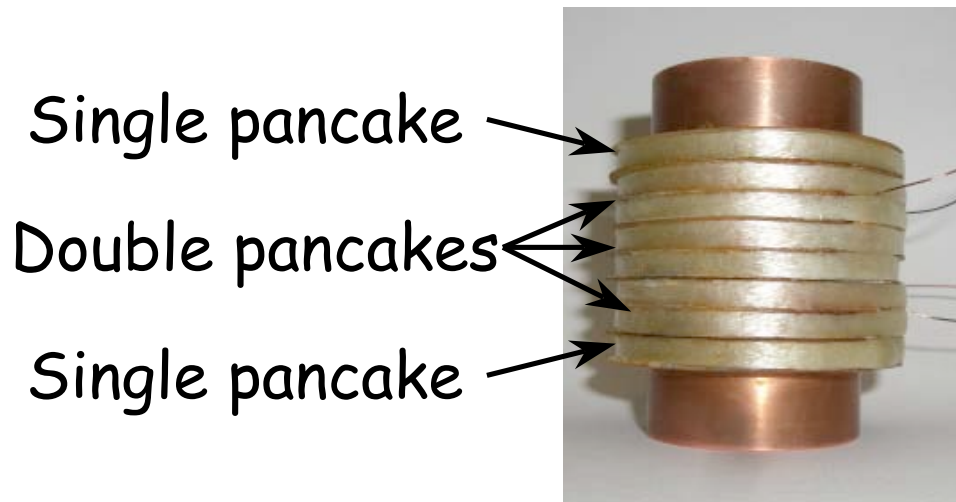
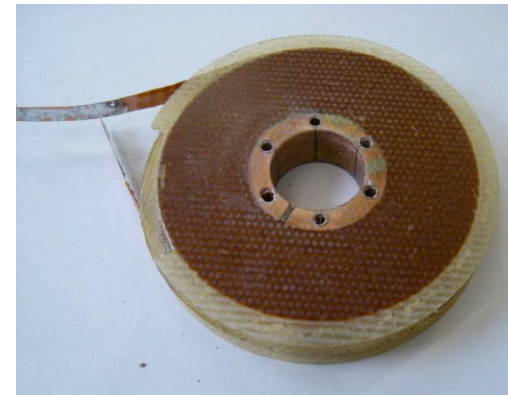


$\varnothing_i = 30 \text{ mm}$
 $J_e = 250 \text{ MA/m}^2$
 $c_f = 0.8$
Tape : 4 mm x 0.1 mm



Solenoids, first realization (40 m YBCO)

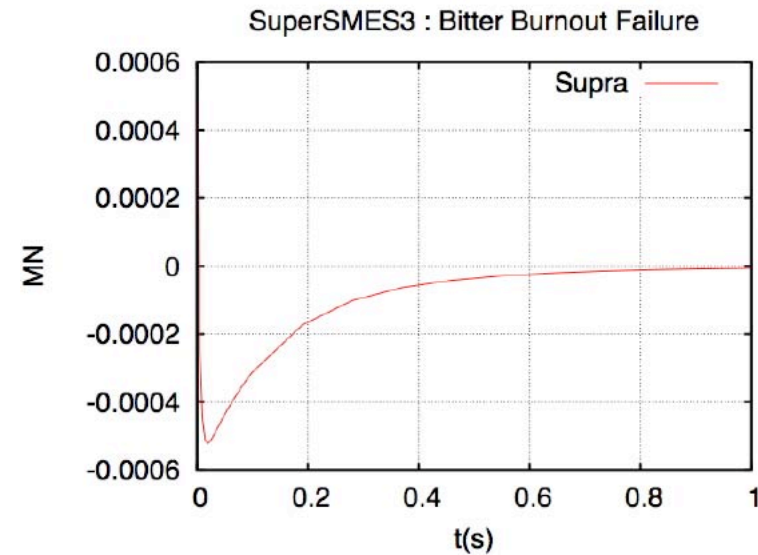
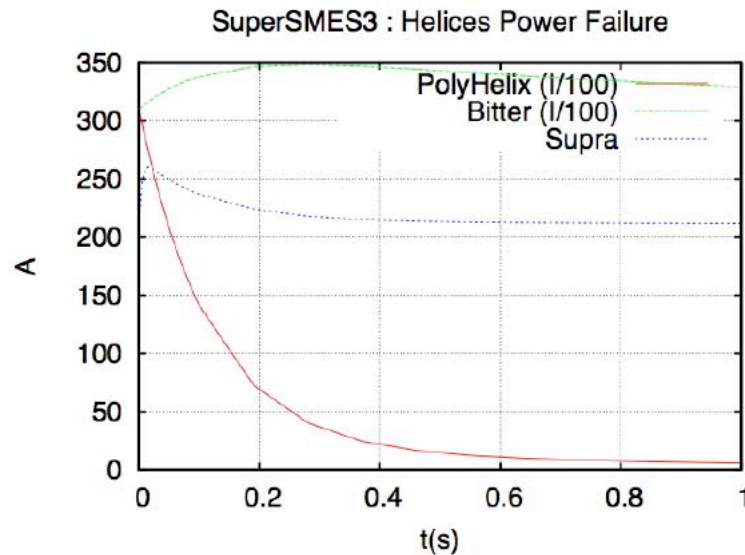
Pancakes	8
Turn number	8 x 44
$\varnothing_i - \varnothing_e$ (mm)	22 / 52
h_{tot} (mm)	37
B (100 A)	0.9 T



Fault scenari



- Consequences of failures (overcurrent, forces)
 - Poly-helix magnet failure
 - Bitter magnet burnout





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Conclusions
&
Future works

Main conclusions

- 6 T HTS insert dipole in 100 mm: real challenge!
- High J_e (400 MA/m²) for 6 T in Ø 100 mm
 - Issue to protect (stabilize) the insert
- Bi-2212 and YBCO possible options
 - Heat treatment: BSSCO main issue
 - I_c perf. on long lengths: another issue for BSSCO
 - High current cable: YBCO main issue
- Quench code validated for NbTi solenoids

Future works

- Carry on the characterization works
- Two YBCO tape conductor
 - Realization & mechanical characterizations
- Protection of the insert (with main dipole)
- First solenoid test
- Working group with main dipole
- Carry on the two quench models for solenoids
 - Data for HTS and model between T_{cs} and T_c
 - Define the required instrumentation



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Thank you!

