



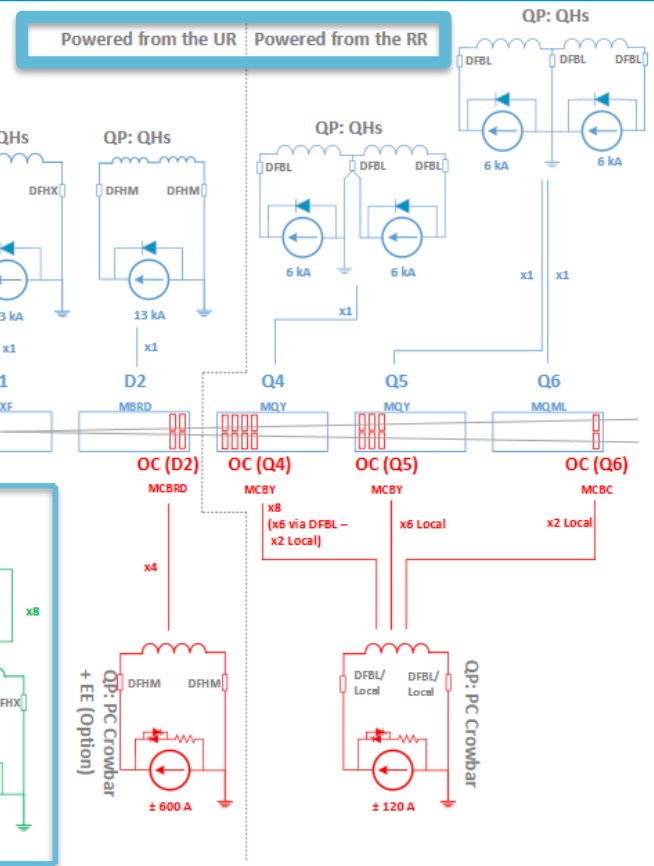
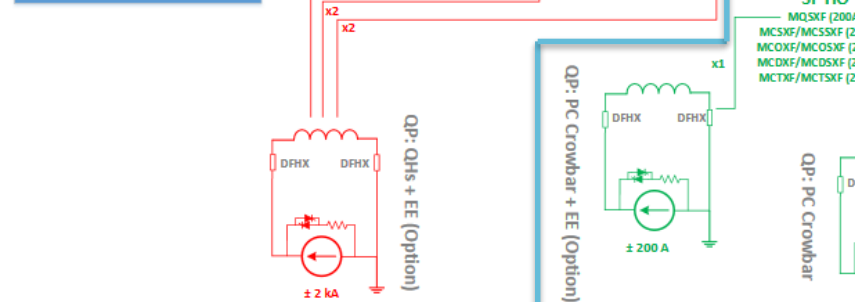
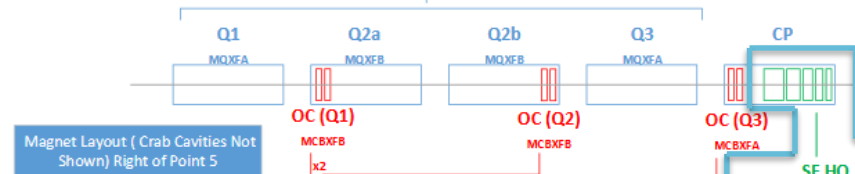
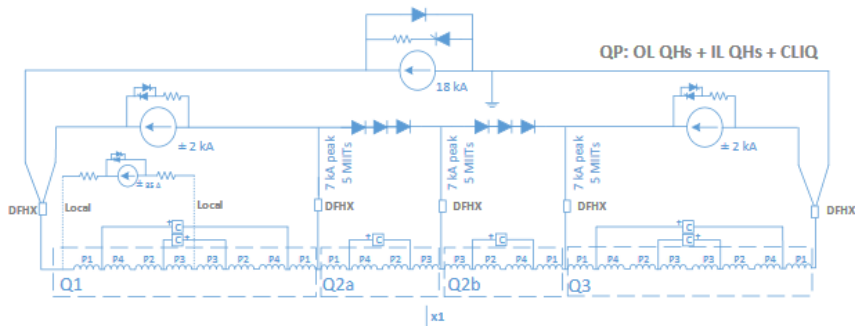
Local Powering of the Corrector Package in the Inner Triplet

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Content

- 1. Baseline and options**
- 2. Reasons for the ECR**
- 3. Change impacts to the different WPs**
- 4. Summary of TCC and follow up**

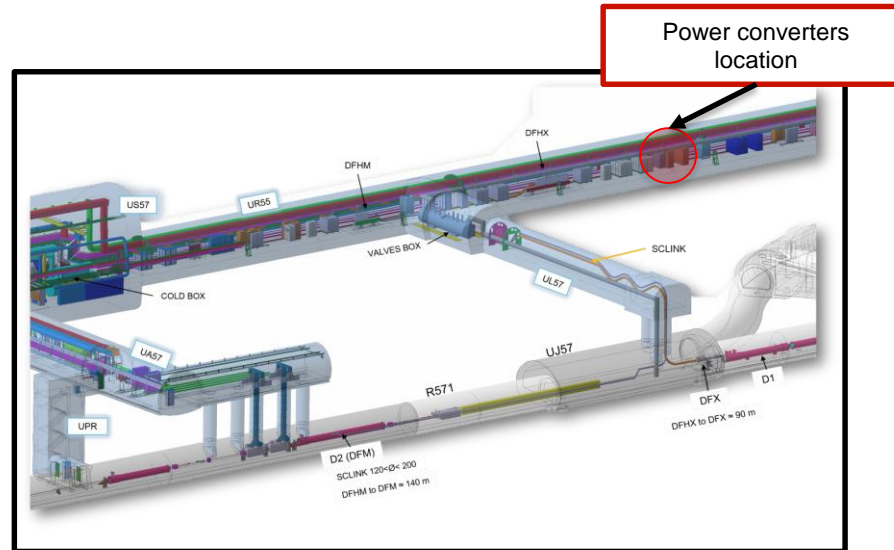


QP: Quench Protection
 QHs: Quench Heaters
 EES: Energy Extraction System
 PC: Power Converter
 OC: Orbit Correctors
 xN: Number of Circuits per IP Side
 SF HO: Superferic High Order
 Current Leads Connection

Legend

The HL-LHC Cold Powering baseline envisaged powering the Inner Triplet Corrector Package (CP) circuits rated at 200 A and below via the MgB_2 Superconducting Link and associated cryo-electrical equipment.

An ECR presented to HL-LHC TCC on September 20 2018 proposes to remove the cold powering equipment related to these circuits replacing them by warm cabling from the converters location to LHC-type conduction-cooled current leads integrated in the CP magnet cryostat.



Reasons for the ECR (WP6a)

- **Simplification** of the HL-LHC Cold Powering
- Adopting for HL-LHC the **same strategy as for LHC**, where low-current (60 A and 120 A) corrector circuits are fed via conduction-cooled current leads integrated in the magnet cryostats

The **main advantages** of the proposed change with respect to the present Cold Powering baseline are the following:

- ***Elimination of the about 100 m long electrically insulated MgB_2 cables, rated for DC currents of 200 A or 120 A, housed inside the superconducting link (18 cables per Triplet);***
- ***Elimination of the cabling process related to the assembly of the 200 A/120 A MgB_2 cables in the final MgB_2 cable assembly developed for feeding the magnets in the Triplets;***
- ***Elimination of the 200 A/120 A gas cooled High Temperature Superconducting (HTS) current leads located in the UR – replaced by conduction-cooled current leads;***
- ***Elimination of the control valves and warm recovery lines associated with gas-cooled current leads;***
- ***Elimination of the protection equipment needed for the superconducting part of the circuit, i.e. for the MgB_2 cables and for the HTS part of the leads (each requiring dedicated protection with different voltage thresholds);***
- ***Reduction of the number of the electrical splices in the Cold Powering System, i.e. elimination - per Triplet- of eighteen HTS to MgB_2 splices in the DFH cryostat and eighteen MgB_2 to Nb-Ti splices in the DFX cryostat;***
- ***Simplification of DFH cryostat by reduction of number of HTS cables routed out of it and number of splices it shall host .***

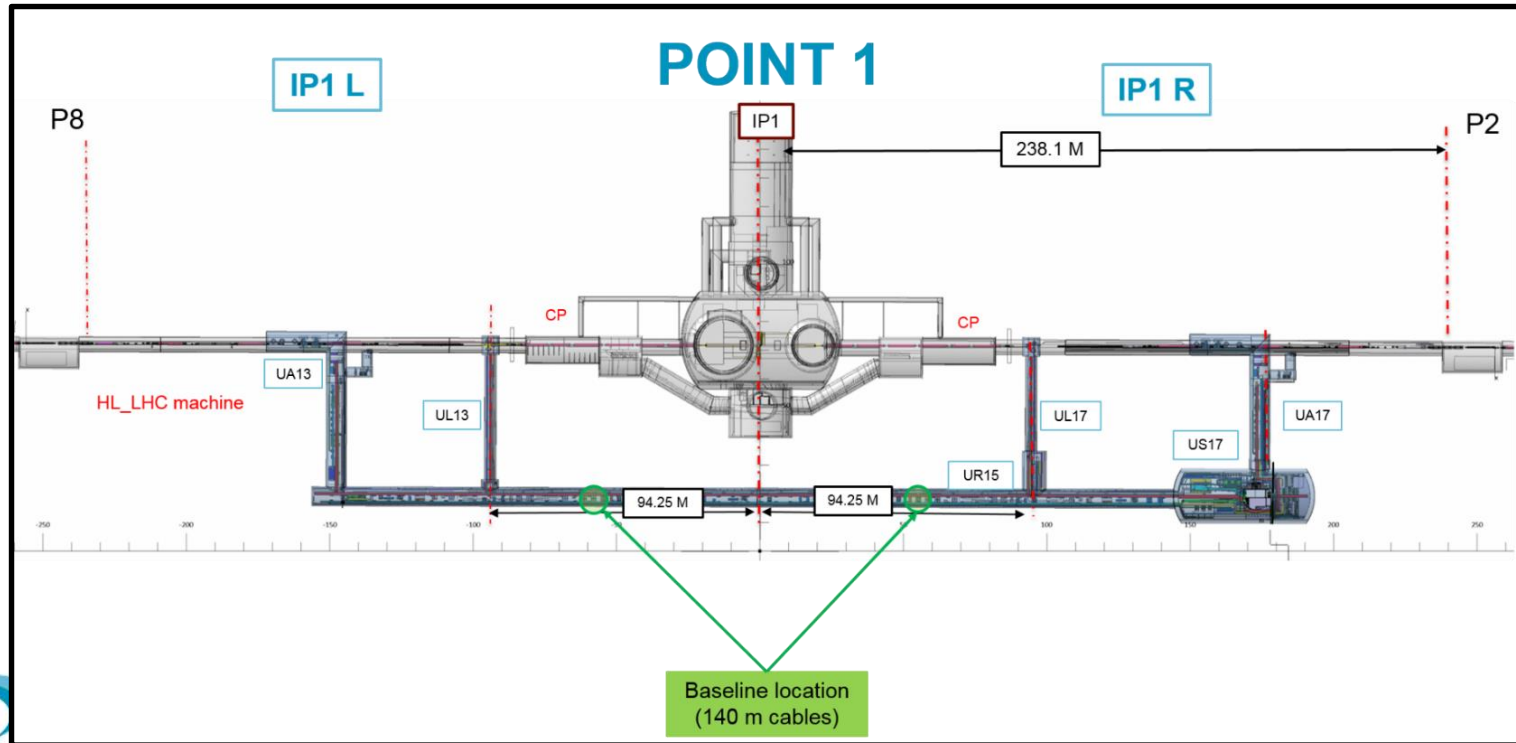
“Local” powering of the corrector circuits can be achieved by

- either leaving the concerned power converters in the present baseline location, i.e. in the UR (case A),***
- or by re-locating the power converters in the **LHC's** UL14, UL16, UL557 and USC55 (case B).***

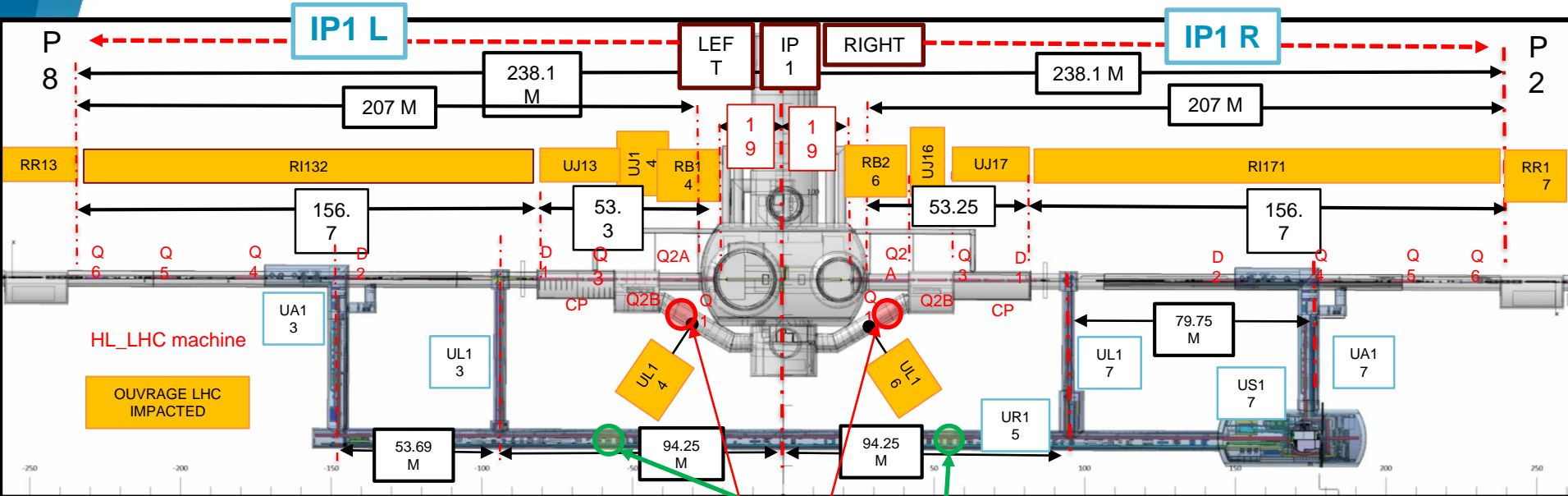
2 Options

Case A

- add new power cables trays routing in the ULs , and use the vertical shaft



Case B (P1)



3 racks PC 120 A
(R2E design) , (8 pc).

1 rack PC 200 A
(R2E-LHC600A-10V)

¼ rack energie
extraction
for 200A → 1 rack

1 rack spare
contrôle
(RYSC01)

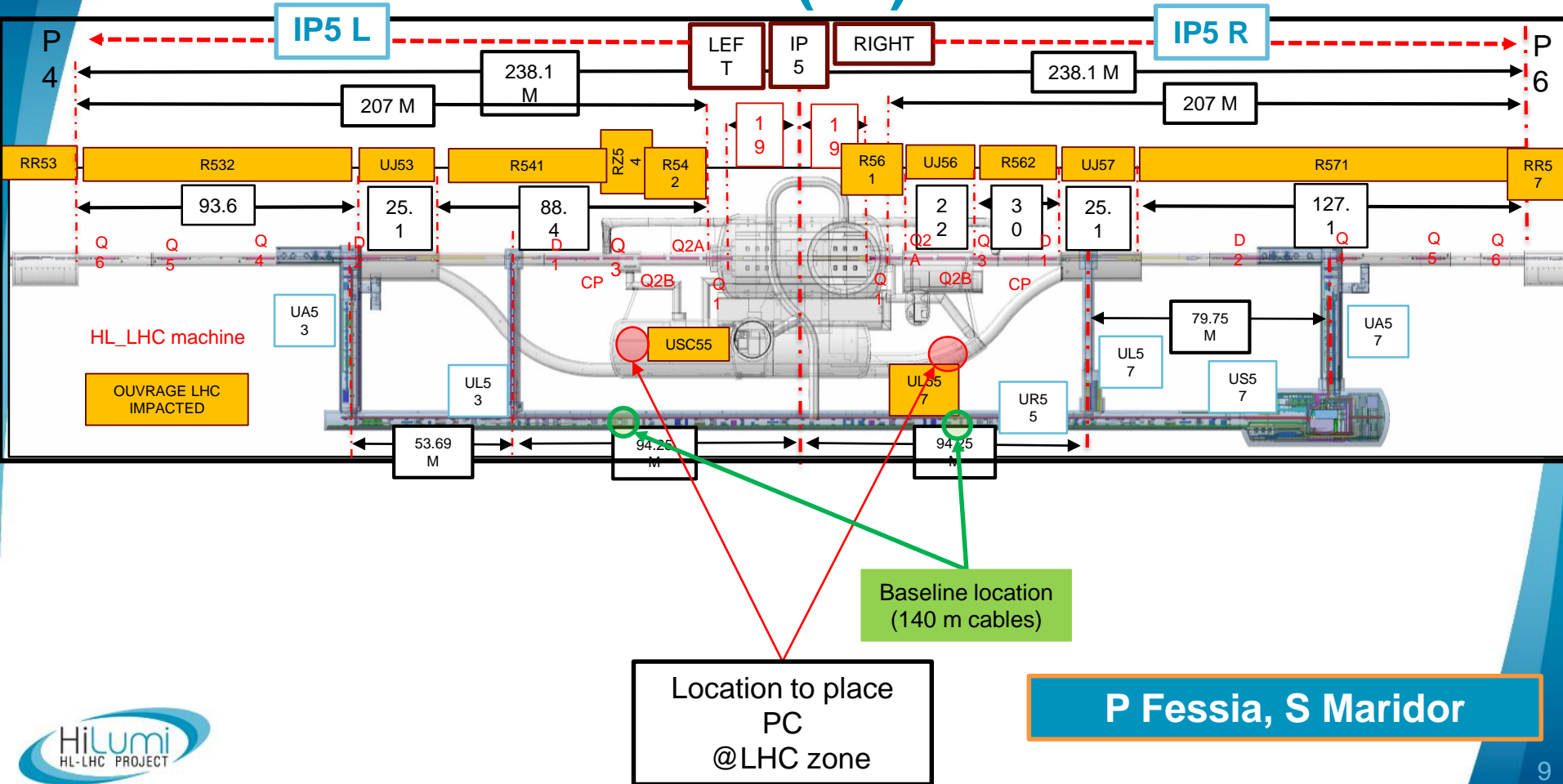
2 racks spare
modules
(RYSA01-RYSA02)

Baseline location
(140 m cables)

Location to place
PC
@LHC zone

P Fessia, S Maridor

Case B (P5)



TECHNICAL EVALUATION PER WP

Work-package	CASE A	CASE B
WP3	<ul style="list-style-type: none"> Saving the work associated with the interconnection of the Nb-Ti bus - in the line N - in the LHC tunnel Reduction of the number of cool-downs and reconnections work in different test configurations - reduction by a factor of three with respect to the present baseline Integration of the conduction-cooled leads in the CP cryostat can be achieved 	
WP6b	<ul style="list-style-type: none"> The cross-section of the cables needs to be chosen to fit available voltage compliance 	<ul style="list-style-type: none"> UL14 and UL16 → Power Converters radiation tolerant 120A and 200A Power Converters to be controlled by FGCLite. Two configurations cannot co-exist in the same Gateway. Access!
WP7	<ul style="list-style-type: none"> Remove the need of dedicated quench detection equipment MQSXF monitoring and protection of the conduction cooled leads will be ensured by two uQDS units 	<ul style="list-style-type: none"> MQSXF protection equipment to be placed next to the PCs. Adding an extra complexity in the de-installation and installation planning Additional signal cables (PCs, EE)
WP9	<ul style="list-style-type: none"> Elimination of the control valves and associated thermometers and piping needed for operation of gas cooled current leads Operational cost would give an increase of cost over 10 years 	
WP15	<ul style="list-style-type: none"> Technical challenge in the removal of the heat generated from the copper cables in the vertical sections Addition of an extra element in the planning 	<ul style="list-style-type: none"> 3 different integrations and the preparation of the installation in 4 different areas leading to an increase in complexity in integration and installation Adding extra complexity in the de-installation and installation planning
WP17	<ul style="list-style-type: none"> DC cables power dissipation in the vertical shaft to be verified Cross section of cables to be increased 	<ul style="list-style-type: none"> Partial re-use of existing infrastructure and cable trays

Summary of TCC and follow up

- To **decouple the decision on the sc link from location of power converters**
 - **Approve** the changes in the link
 - Study on going to **keep converters in UR**
- Only **Option A has no implication on radiation issues** and thereby fits to the HL-LHC upgrade goal of providing accessibility for the new hardware.
- WP15 is verifying with Civil Engineering the possibility of **displacing the radiation shield** to the bottom of the shaft
- First indications from WP15 say that there is **no issue concerning the cooling/ventilation** in the shaft for case A



***Thanks
Questions?***