



## Electrical Quality Control (QC): coil to coil parts

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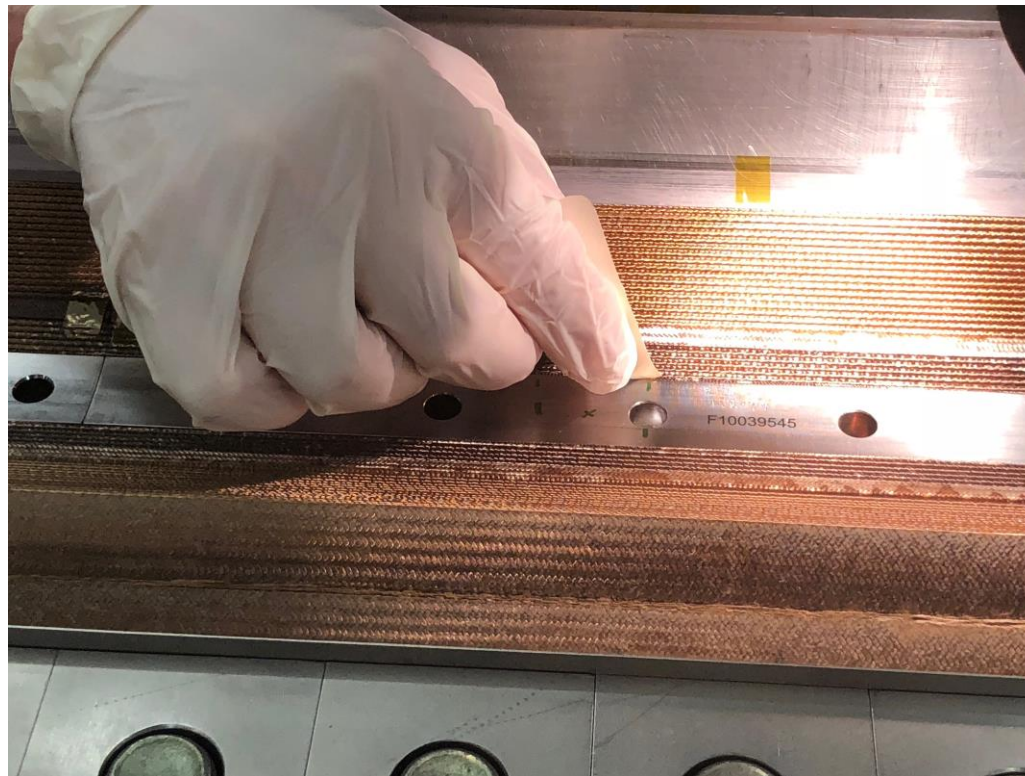


## Main electrical issues with coil parts

- Before coil impregnation, resistance between coil and coil parts (pole, end-shoe) is measured
  - Sometimes resistance  $< 1 \text{ G}\Omega$  can be observed
- Different causes/mechanisms have been identified
- Really difficult to determine if contact points are more than one
- Sometimes not possible to repair
- Question: which resistance can we consider the safe limit?
  - We want to discuss and re-define our electrical QC criteria for coil parts based on the analysis we are going to present (not available before now)

## Example: coil QXFA108

- Showed 170 k $\Omega$  resistance to pole before epoxy impregnation
  - Short location identified
  - Tried to repair, with no good results
  - Large contact area  $\rightarrow$  **binder** issue



## Present QC tests


QXFA Coil Fabrication Electrical QA  
HiLumi doc 521

- HiPot Coil – pole : 500 V
- HiPot Coil – end-shoe: 1000 V
- HiPot end-shoe – end-shoe: 1000 V
  
- Peak voltages:
  - Pole turn – pole turn: ~ 50 V for MQXFA and MQXFB
  - Midplane turn – midplane turn: ~ 300 V for MQXFA, ~ 500 V for MQXFB
  
- Options for updated QC criteria:
  - Criterion 1: HiPot at  $V_{\text{max}} * f + c$ 
    - $V_{\text{max}}$  = maximum voltage during a quench
    - $f, c = ?$  - typical values are  $f = 2$  and  $c = 500$  V
    - Note:  $c = 500$  V looks excessive if  $V_{\text{max}} = 50$
  - Criterion 2: Resistance measurement, after defining minimum acceptable resistance based on power dissipation

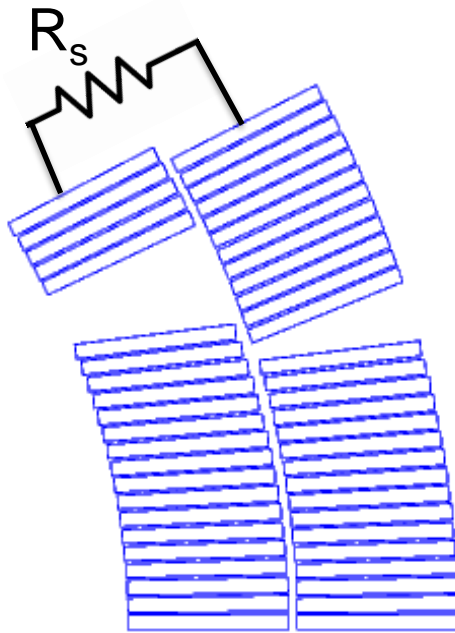
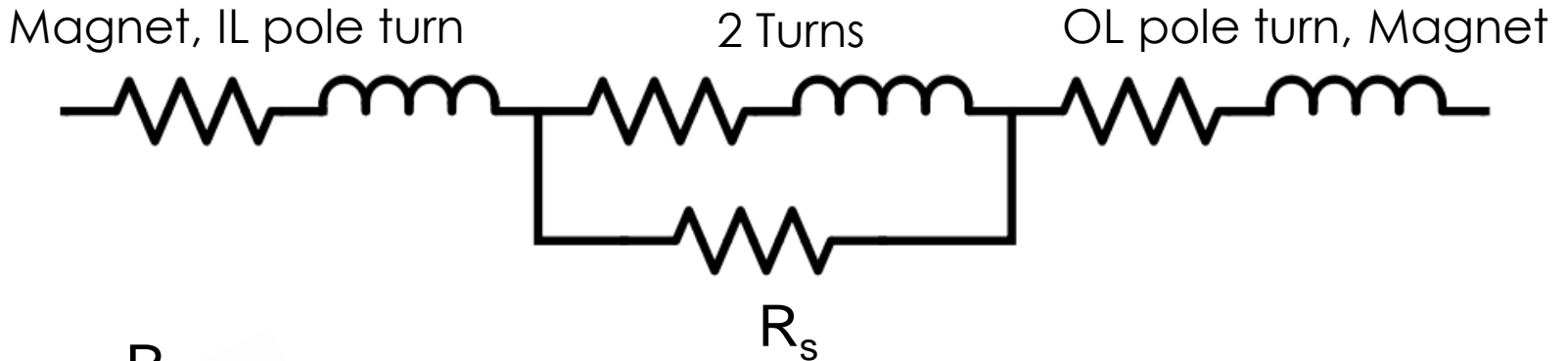
## Target for criterion 2

- Identify risks due to short between coils and parts. Evaluate minimum acceptable short resistance
  - Goal: try to avoid high-voltage hipots with coil parts
  - Needed: simulations of coil-parts shorts
- Cases considered:
  - Short from IL pole-turn to OL pole-turn through the pole
  - Short from IL midplane-turn to OL midplane-turn through the end-shoe
  - Simulations done for MQXFA and MQXFB in nominal protection system (with CLIQ and OL heaters, and no dump)
  - Single shorts could be considered not worrying
    - But, it is difficult to identify them

# Assumptions for simulations

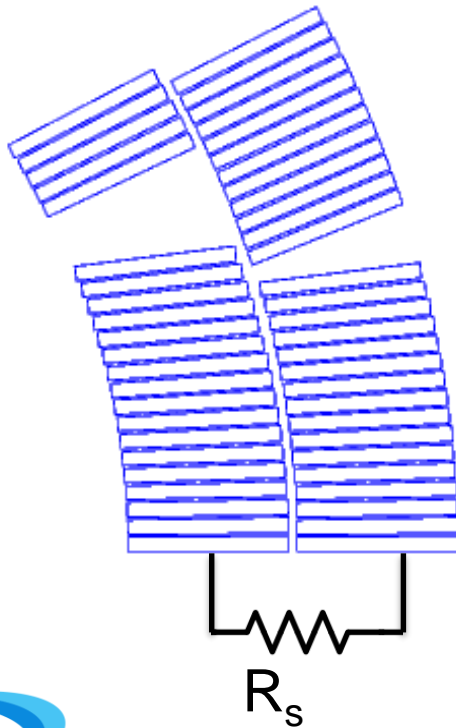
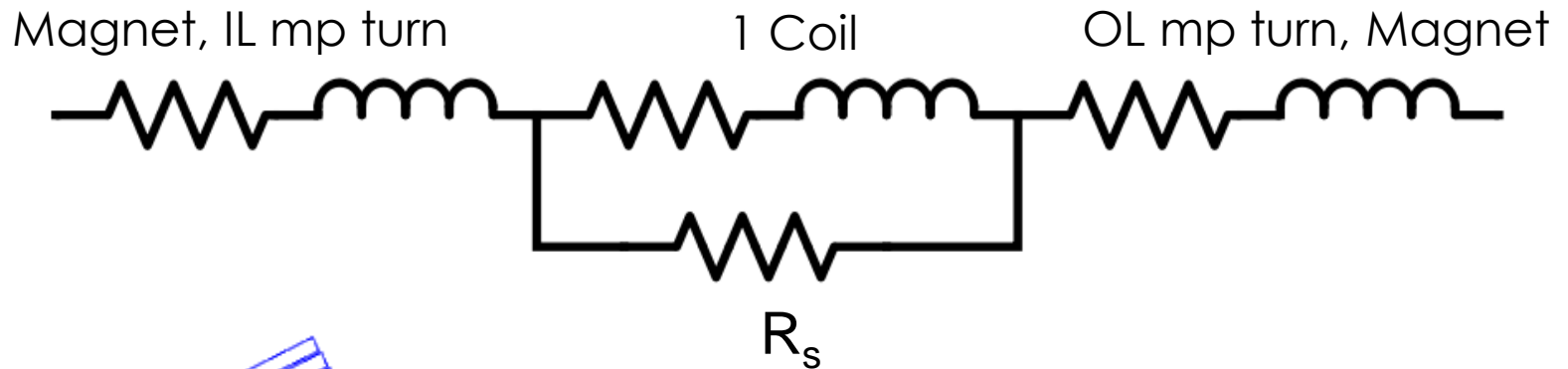
- Simulations performed with 
- Current: 17980 A (ultimate)
- No dump resistor
- Quench heaters: Outer Layer (600 V MQXFA, 900 V MQXFB)
- CLIQ:
  - 600 V, 40 mF for MQXFA
  - 1000 V, 40 mF for MQXFB
- Nominal conductor parameters
- Constant short resistance
  - Measured at warm

## Short from IL pole-turn to OL pole-turn through the pole



$R_s$	10 $\Omega$ , 1 k $\Omega$ , 0.1 M $\Omega$ , 10 M $\Omega$ , 1 G $\Omega$
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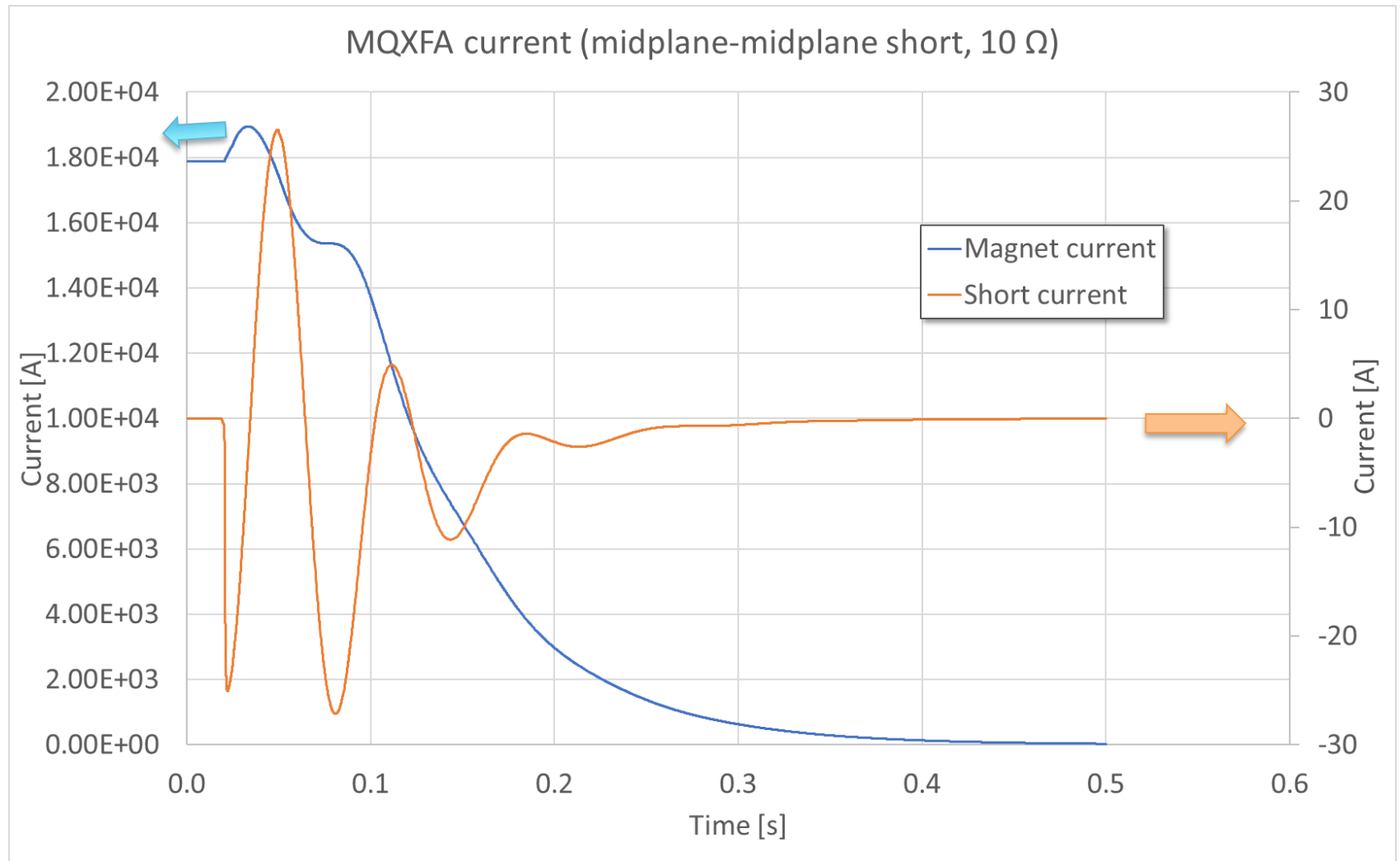
# Short from IL midplane-turn to OL midplane-turn through the end-shoe



$R_s$	10 $\Omega$ , 1 k $\Omega$ , 0.1 M $\Omega$ , 10 M $\Omega$ , 1 G $\Omega$
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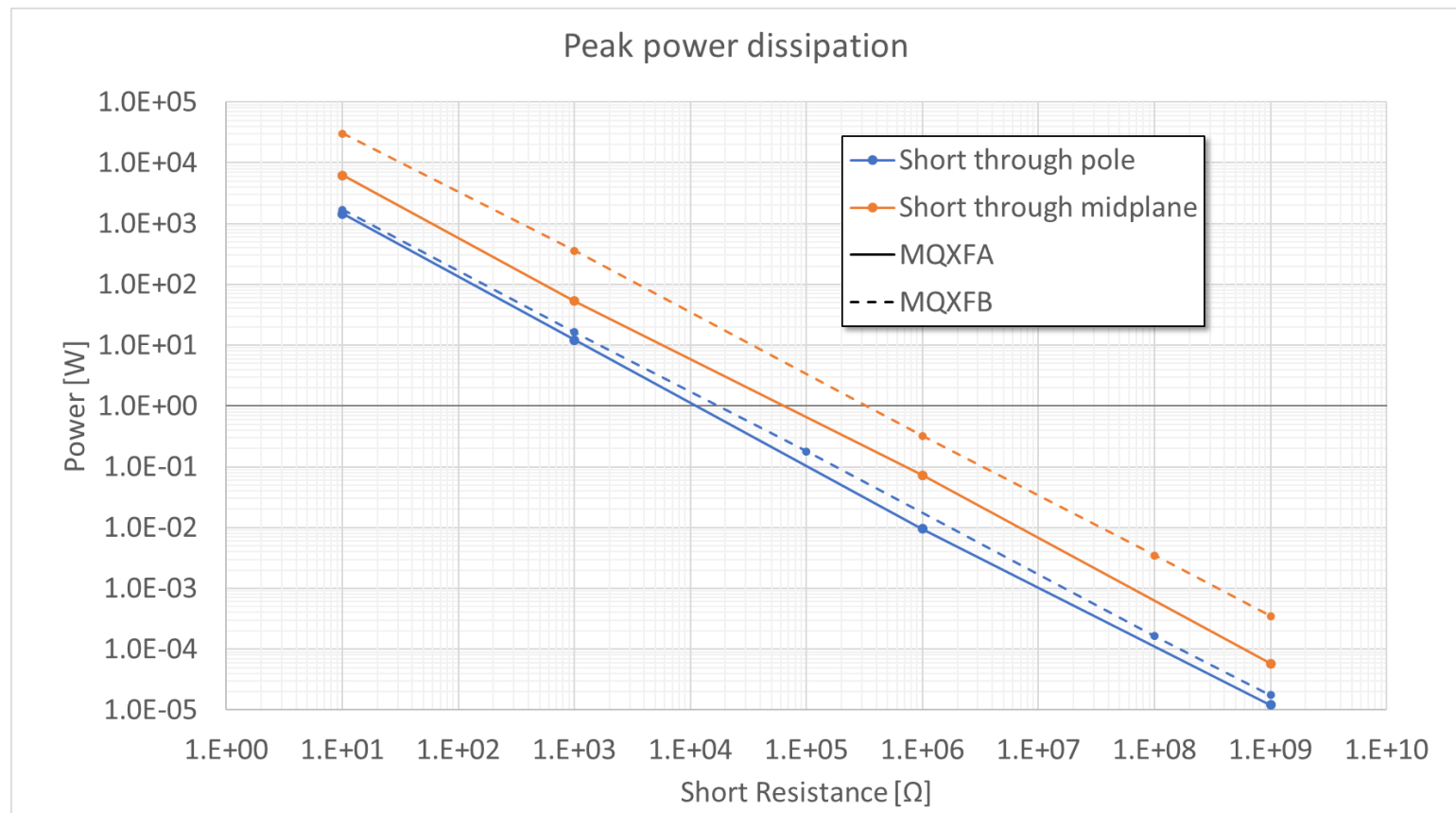


## Example of Current Discharge



## Possible criteria: peak power dissipation

- Define a maximum acceptable peak power dissipation, in order to define minimum acceptable resistance between coil and parts



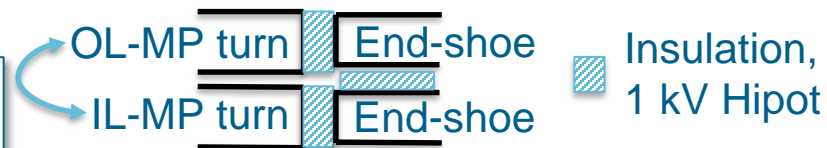
## Examples of power criterion

- Maximum peak power dissipation is set to **10 mW**. Coils are accepted if:
  - Resistance to pole is greater than **1 MΩ** for MQXFA, **2 MΩ** for MQXFB
  - Resistance to end-shoe is greater than **7 MΩ** for MQXFA, **30 MΩ** for MQXFB
- Maximum peak power dissipation is set to **1 mW**. Coils are accepted if:
  - Resistance to pole is greater than **10 MΩ** for MQXFA, **20 MΩ** for MQXFB
  - Resistance to end-shoe is greater than **70 MΩ** for MQXFA, **300 MΩ** for MQXFB
- Possible criterion to choose maximum power:
  - Typical hipot voltage x typical leakage current: 1000 V x 10 μA = **10 mW**

## Some discussion

- Criterion based on power dissipation through a short can be suitable for coil to pole
  - Likely, contact resistance due to binder, with “large” contact area
  - We had coil-pole shorts in the past magnet tests, with no issues during powering tests
- Criterion based on power dissipation may be unsuitable for coil to end-shoe
  - Possibly, short due to damage of the insulation due to sharpness of end-shoe, with small contact area and difficulty of evaluation of power density and temperature increase
  - Hi-pot may be best solution, even though the present 1 kV level could be revised, considering also that there are three layers of insulation from IL to OL midplane turns through end-shoes, and that each coil shall pass Impulse test at 2.5 kV.

Peak voltage: 300 – 500 V  
Impulse test: 2.5 kV



## Proposed QC tests and criteria (to be discussed):

- **Coil to pole resistance**
  - **> 1 M $\Omega$**  for MQXFA
  - **> 2 M $\Omega$**  for MQXFB
  - Power dissipation < 10 mW in case of double short
- **Coil to End-Shoe HiPot, and**
- **IL End-Shoe to OL End-Shoe HiPot at**
  - **300 V** for MQXFA
  - **500 V** for MQXFB
  - Redundancy provided by having three layers of insulation between midplane turns through end-shoes; direct path tested during impulse test at 2.5 kV
- More ideas?

**Thank you**