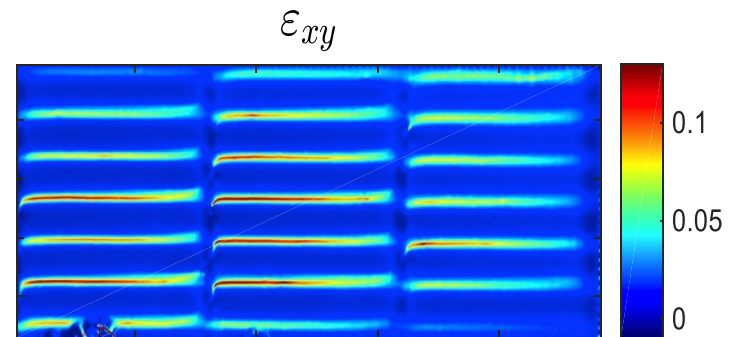


Measuring in-plane displacement and strain fields with the grid method. A feasibility study on superconducting magnet

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Objective:

- measuring displacement and strain fields on a superconducting magnet specimen subjected to a mechanical loading
- applying a suitable full-field measurement technique: the grid method
- are the heterogeneities due to the heterogeneous nature of the material observable?

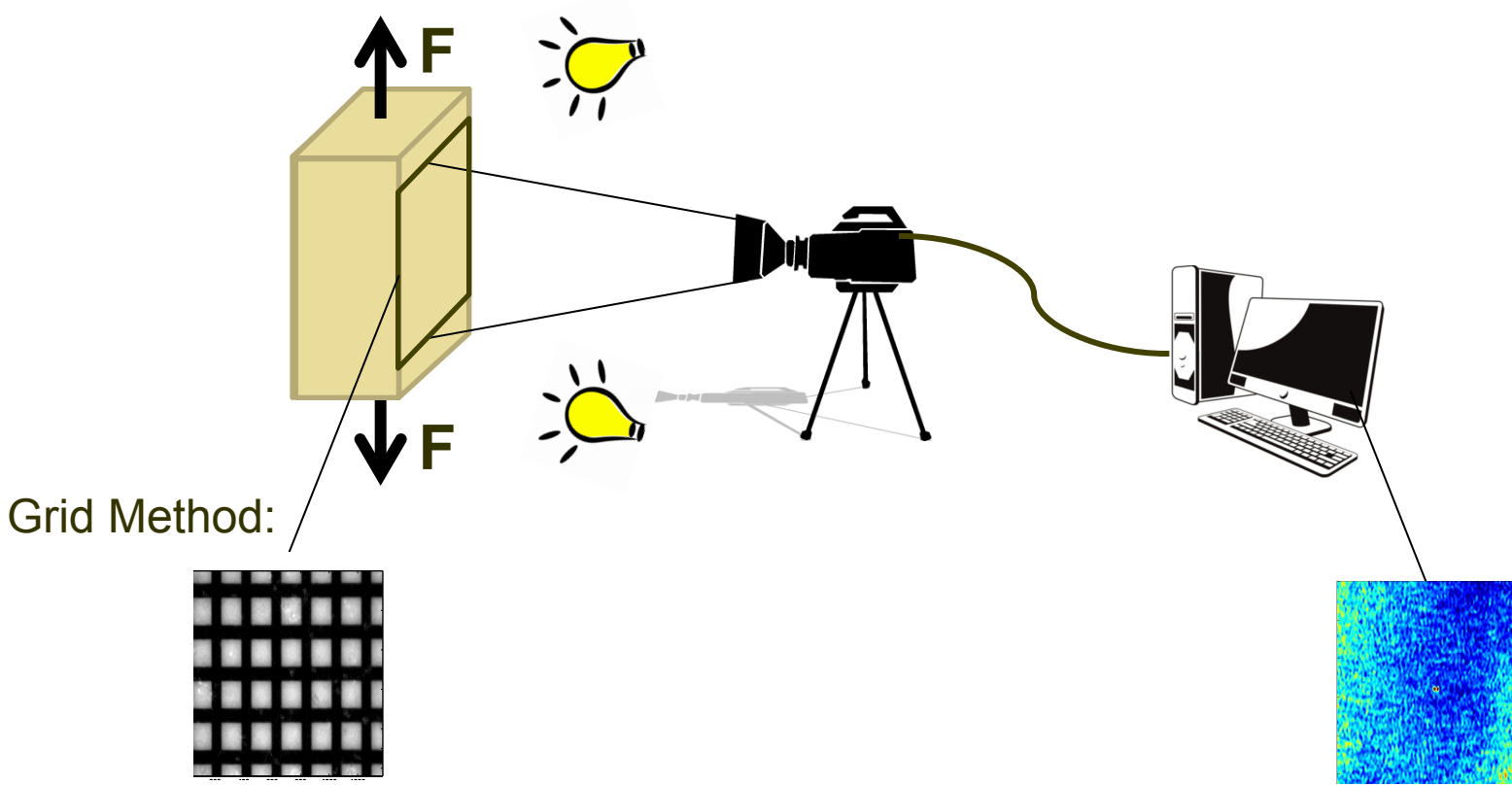
Outline:

- 1- Basics on the grid method
- 2- Preparation of the specimen
- 3- How to extract displacement/strain fields from the images?
- 4- Results
- 5- Conclusion

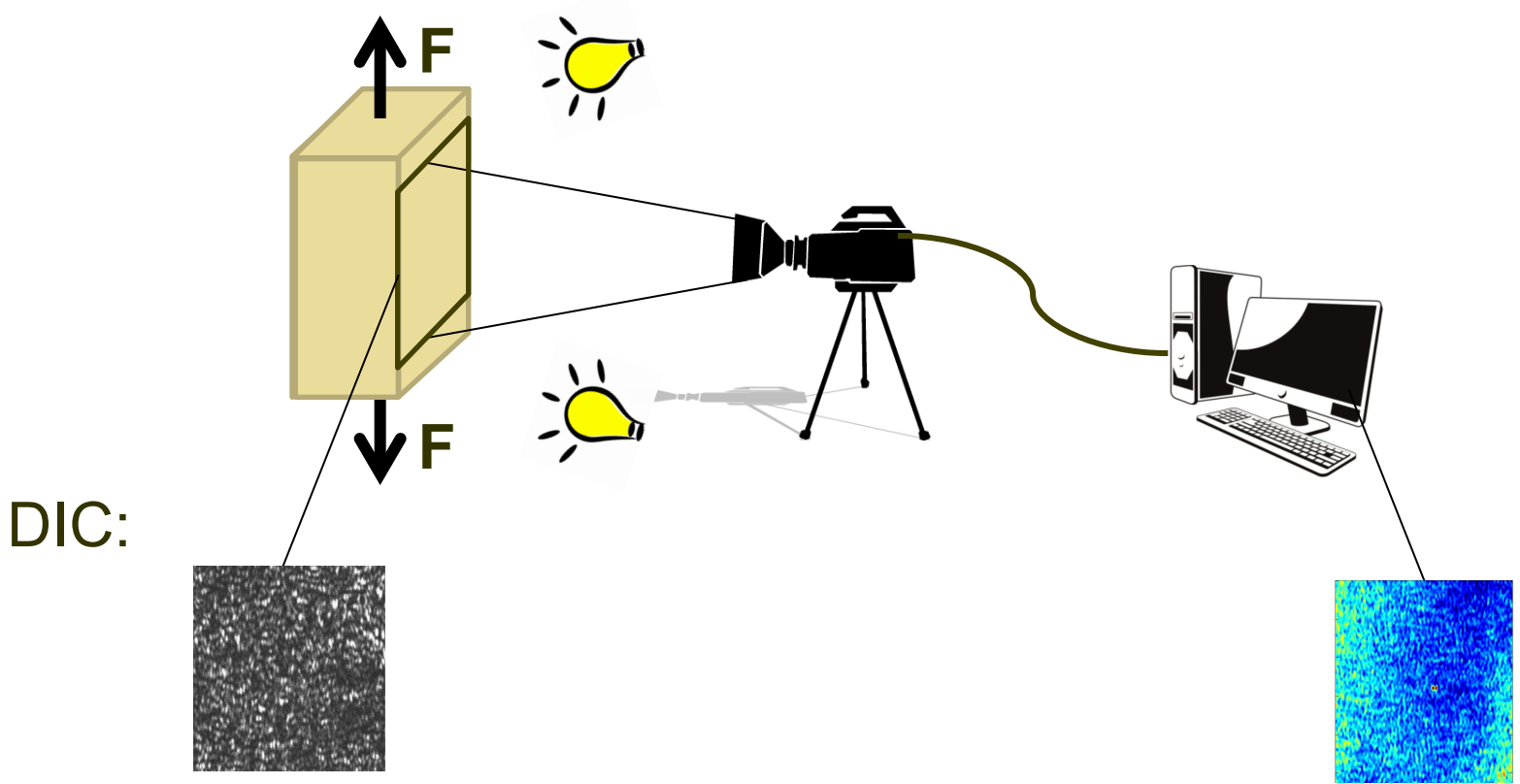
Outline

- 1- Basics on the grid method**
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- 1- Grid bonded/engraved/transferred on the specimen
- 2- Image of the **grid** captured by a camera before and after loading
- 3- Displacement and strain fields deduced by processing these images



- 1- Speckle deposited on the specimen
- 2- Image of the **speckled pattern** captured by a camera before and after loading
- 3- Displacement and strain fields deduced by processing these images



- a priori knowledge on the pattern with grid → better compromise between noise level and spatial resolution with grids than with speckles [1]
- price to pay: depositing a regular marking

Outline

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Step 1:

- cutting the specimen in a superconducting magnet
- polishing the surface of the specimen

Specimen:

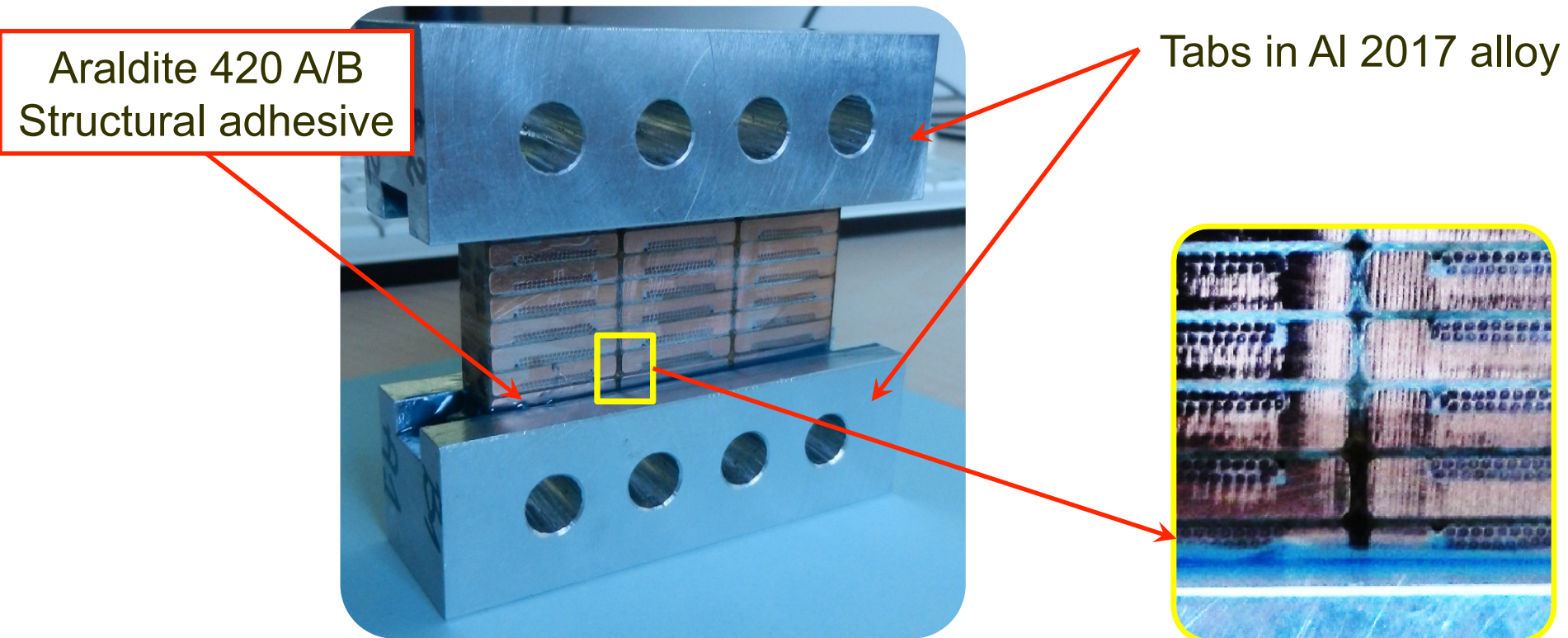
- selected and thoroughly polished and prepared by François NUNIO, CEA Paris-Saclay, France
- cable from JLab magnet for CLS12 torus magnet



dimensions: 60x35x10 mm³

Step 2:

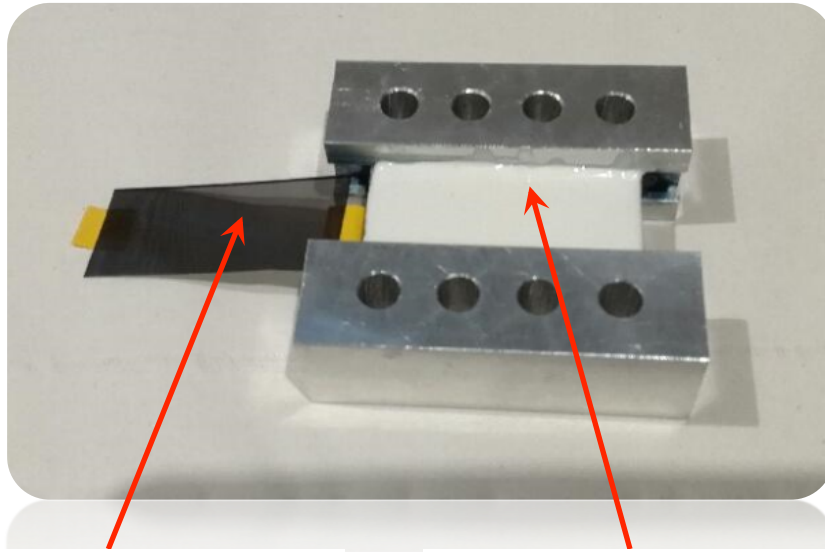
- bonding tabs onto the specimen, suitable for an ARCAN fixture



- special attention while machining the tabs to ensure the symmetry of the resulting specimen
- adjusting the thickness of the glue (200 μm) with slip gauges
- polymerisation: 5 hours, 80°C

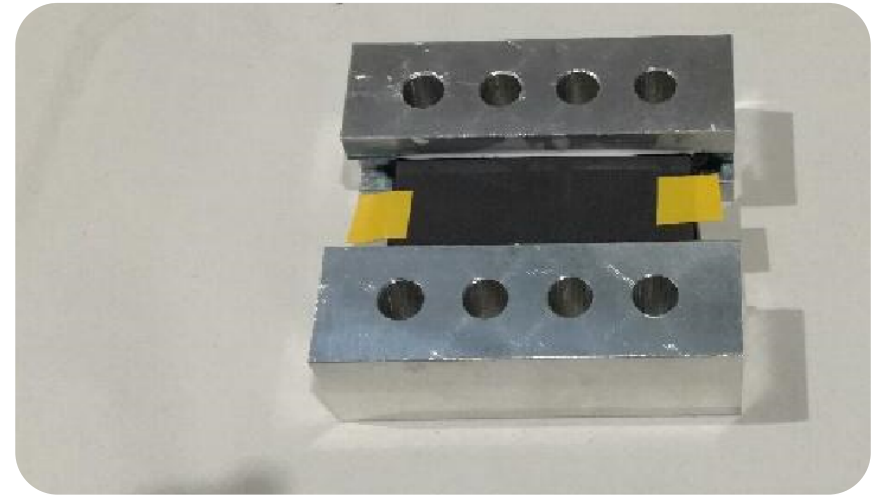
Step 3:

- transferring a 2D grid onto the specimen



2D grid printed
onto a polymeric sheet
pitch: 0.2 mm

adhesive for
transferring the grid
(ink only)

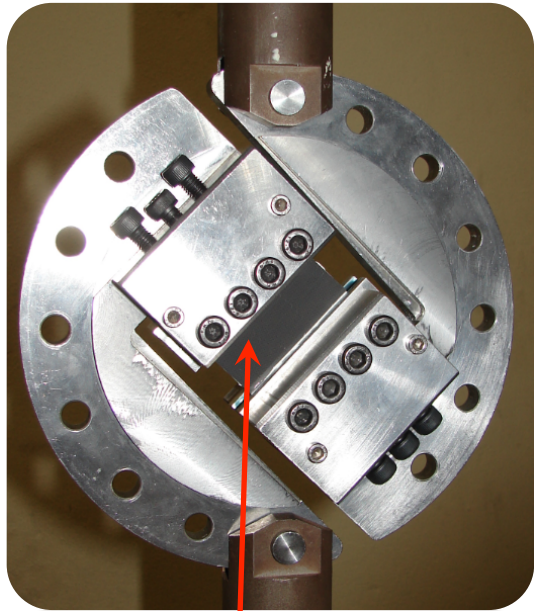


polymerisation + peeling off the
polymeric sheet

- grid printed on the polymeric sheet with a high-resolution photoplotter (64,000 dpi)
- white epoxy adhesive to ensure a good visual contrast with black ink

Step 4:

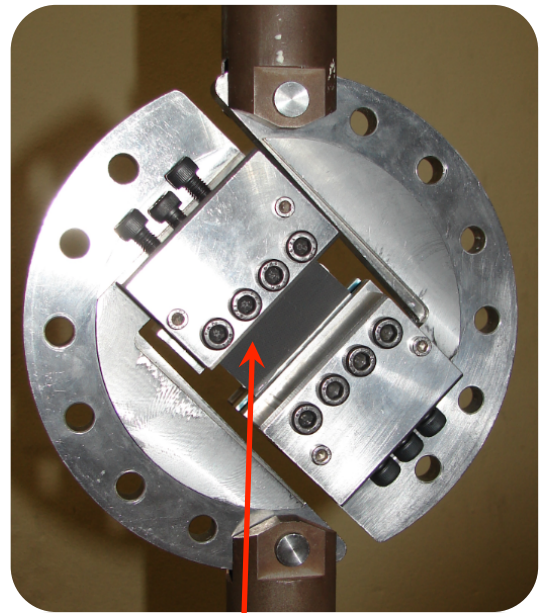
- mounting the specimen in an Arcan fixture + testing it



Arcan fixture +
specimen

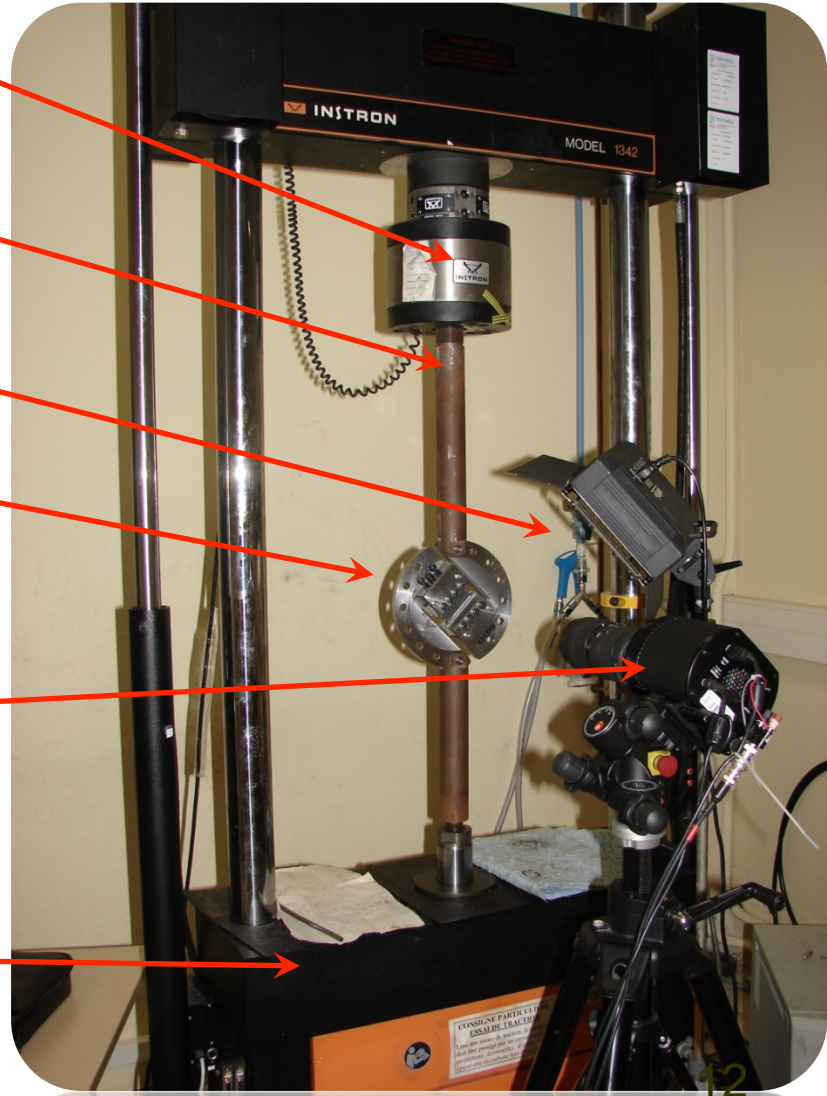
Step 4:

- mounting the specimen in an Arcan fixture + testing it



Arcan fixture + specimen

- force cell
- pièces d'interfaces
- Lighting system
- Arcan fixture
- Retiga 6000 CCD BW 14-bit camera 2758 x2208 pixels
- Hydraulic INSTRON tensile machine Fmax=100kN



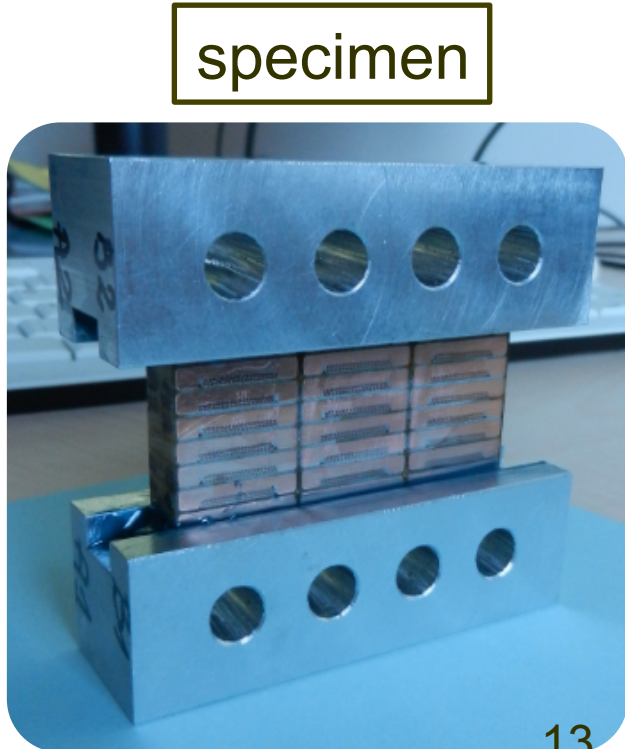
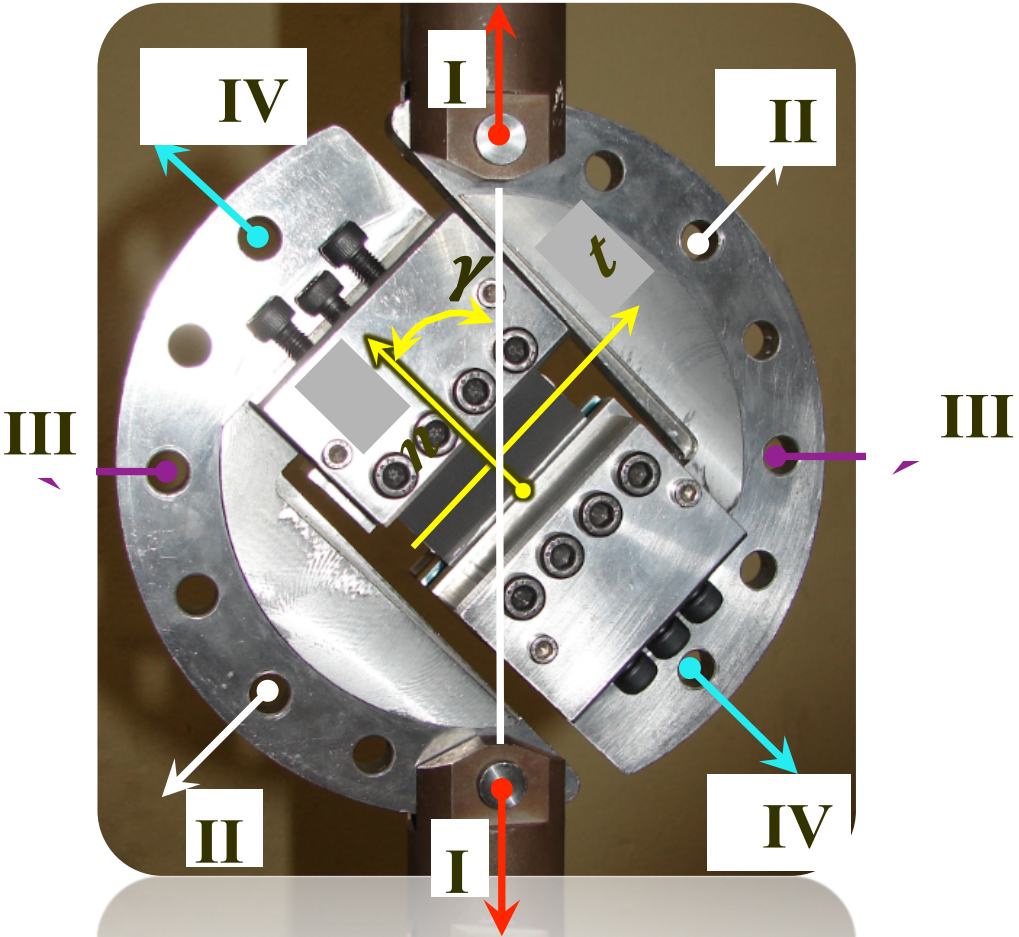
Various (potential) 2D loading configurations with the Arcan fixture

I-I → **compression + shear**

II-II → shear

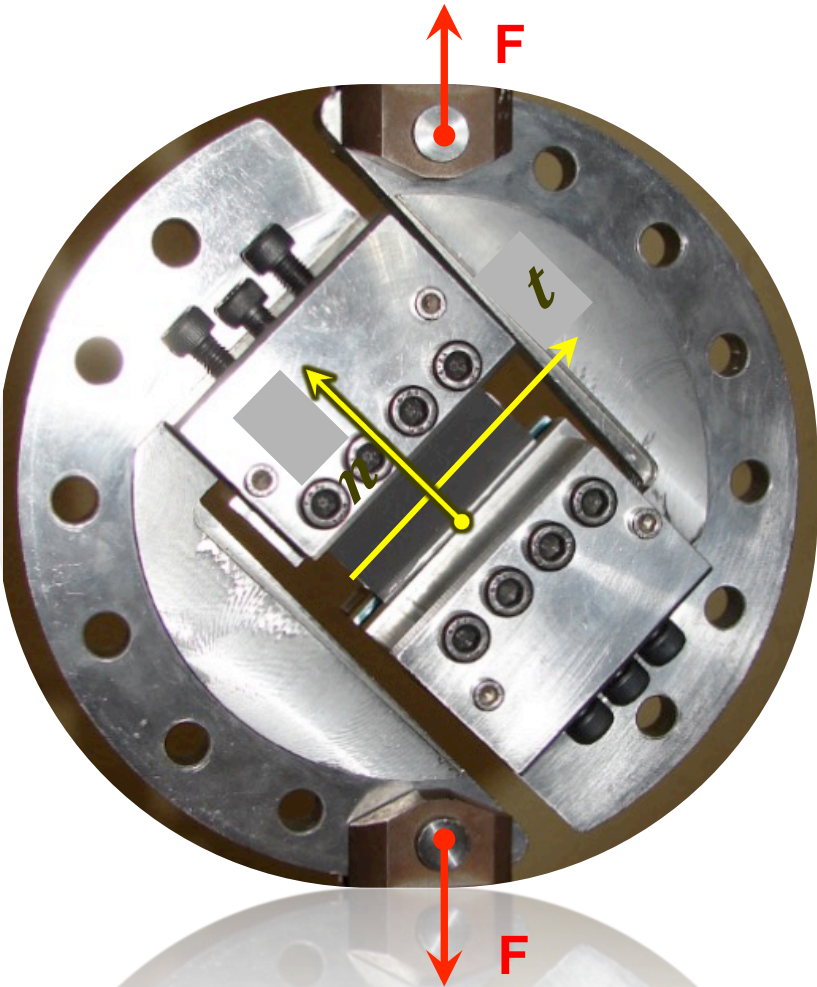
III-III → **tensile load + shear**

IV-IV → **tensile load**

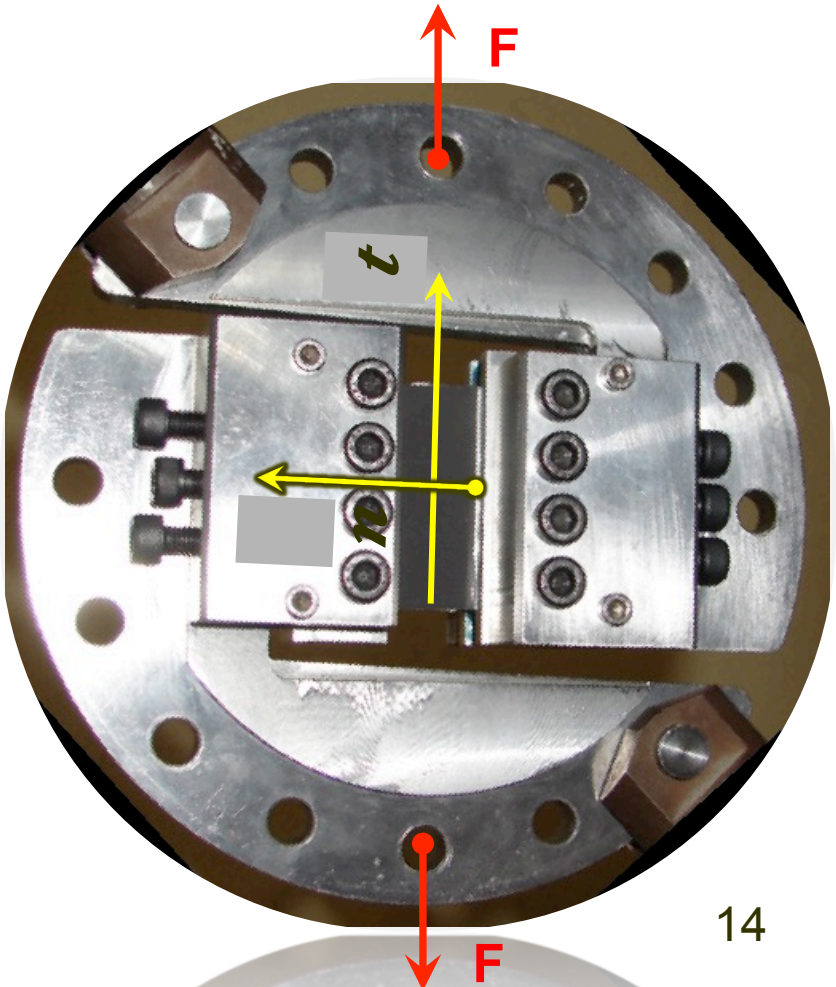


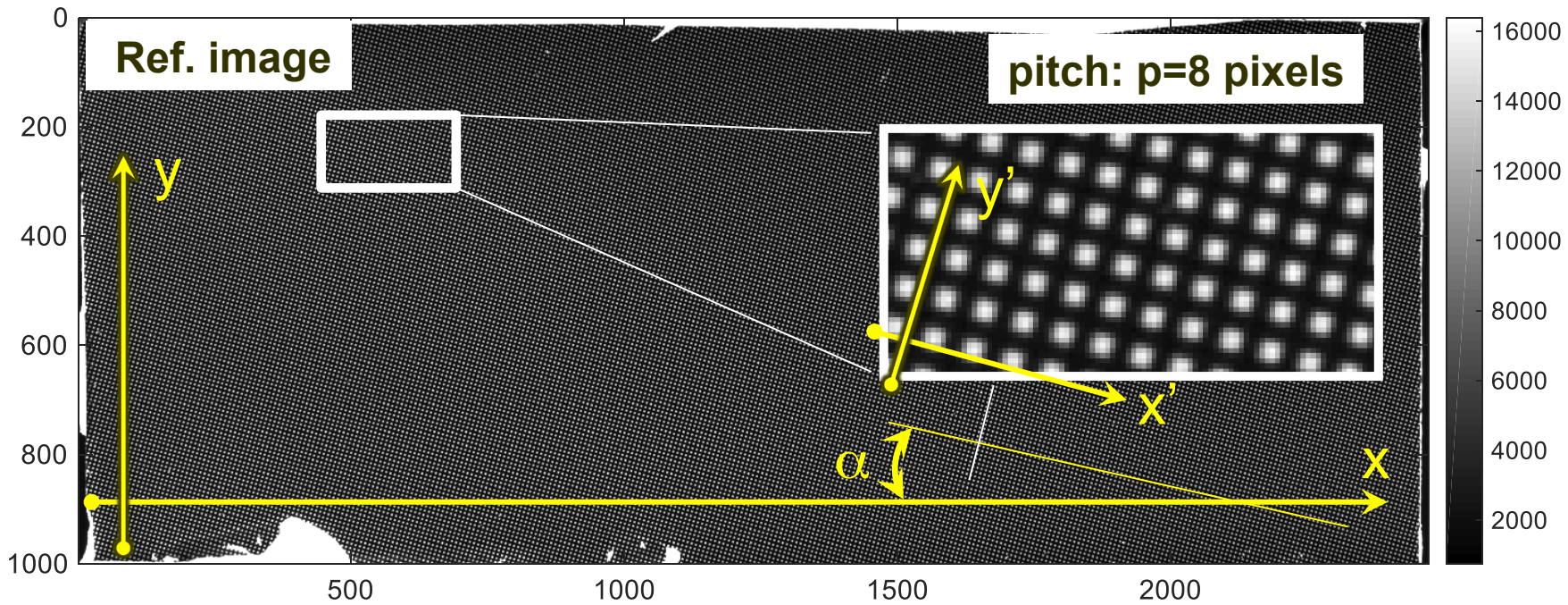
Tested configurations

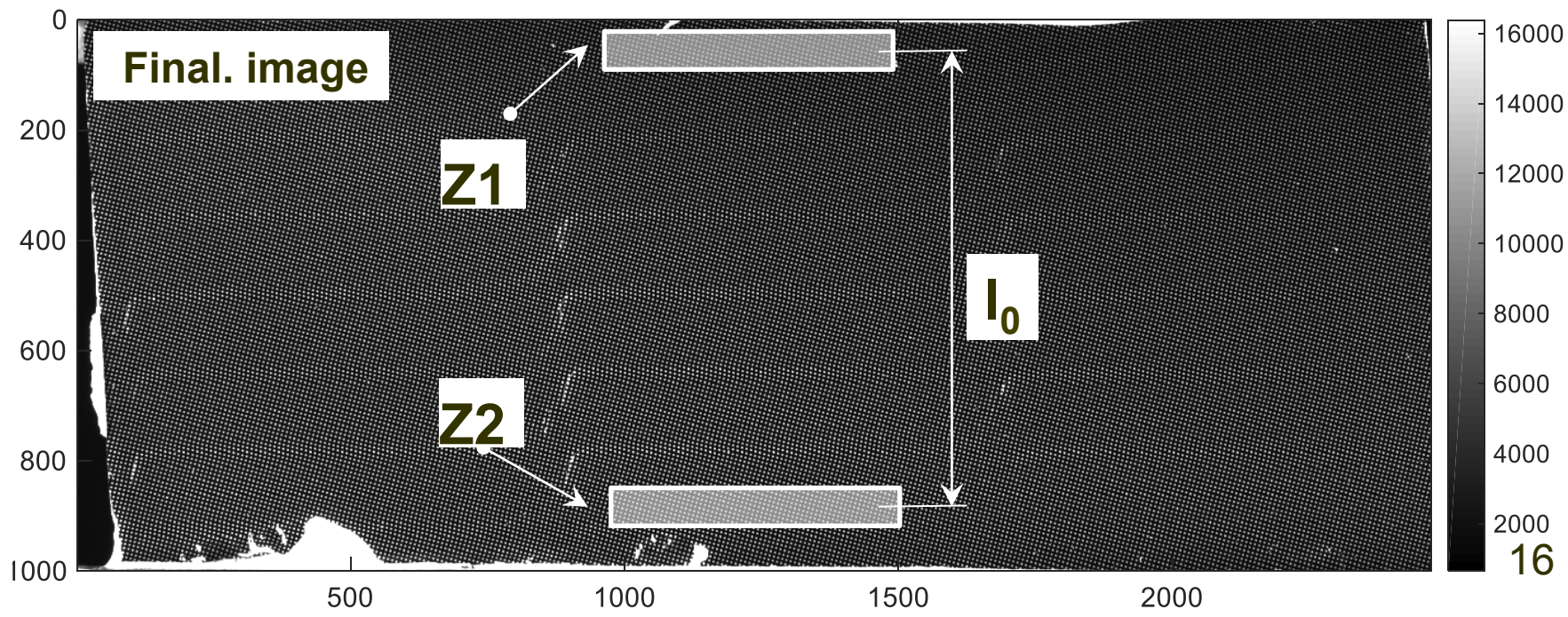
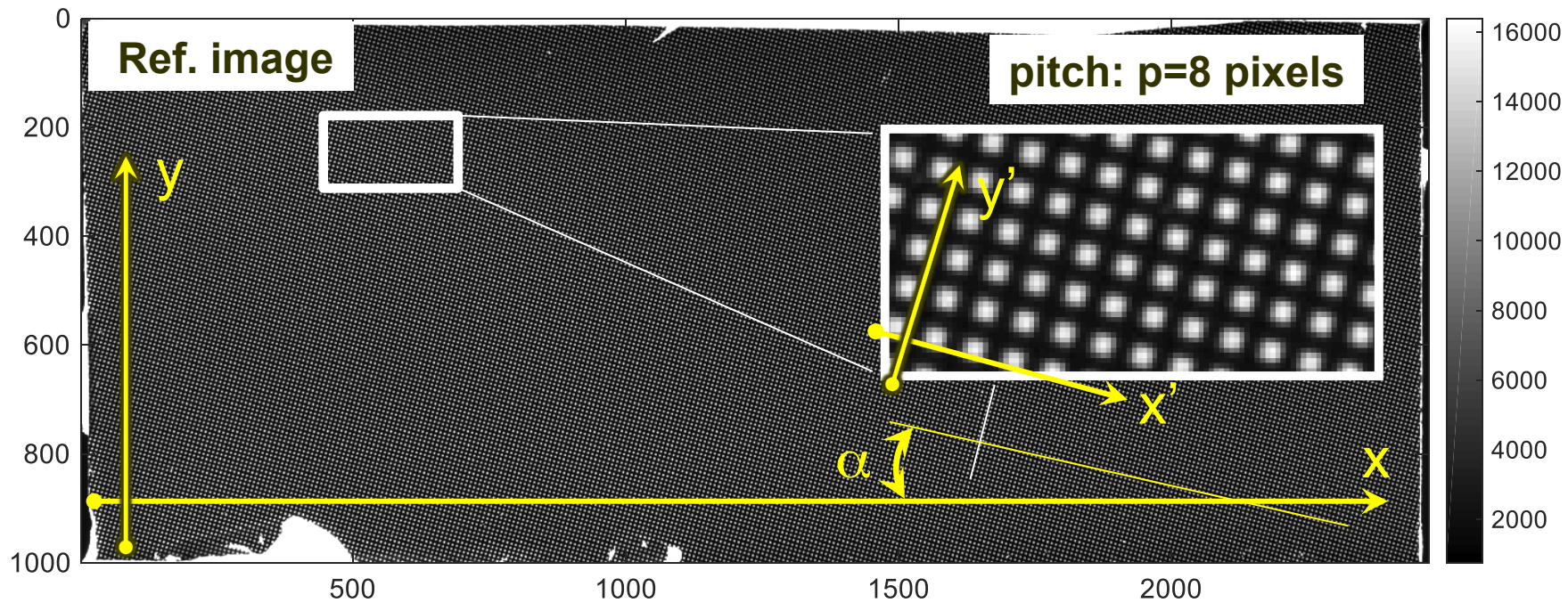
A: compression + shear



B: shear





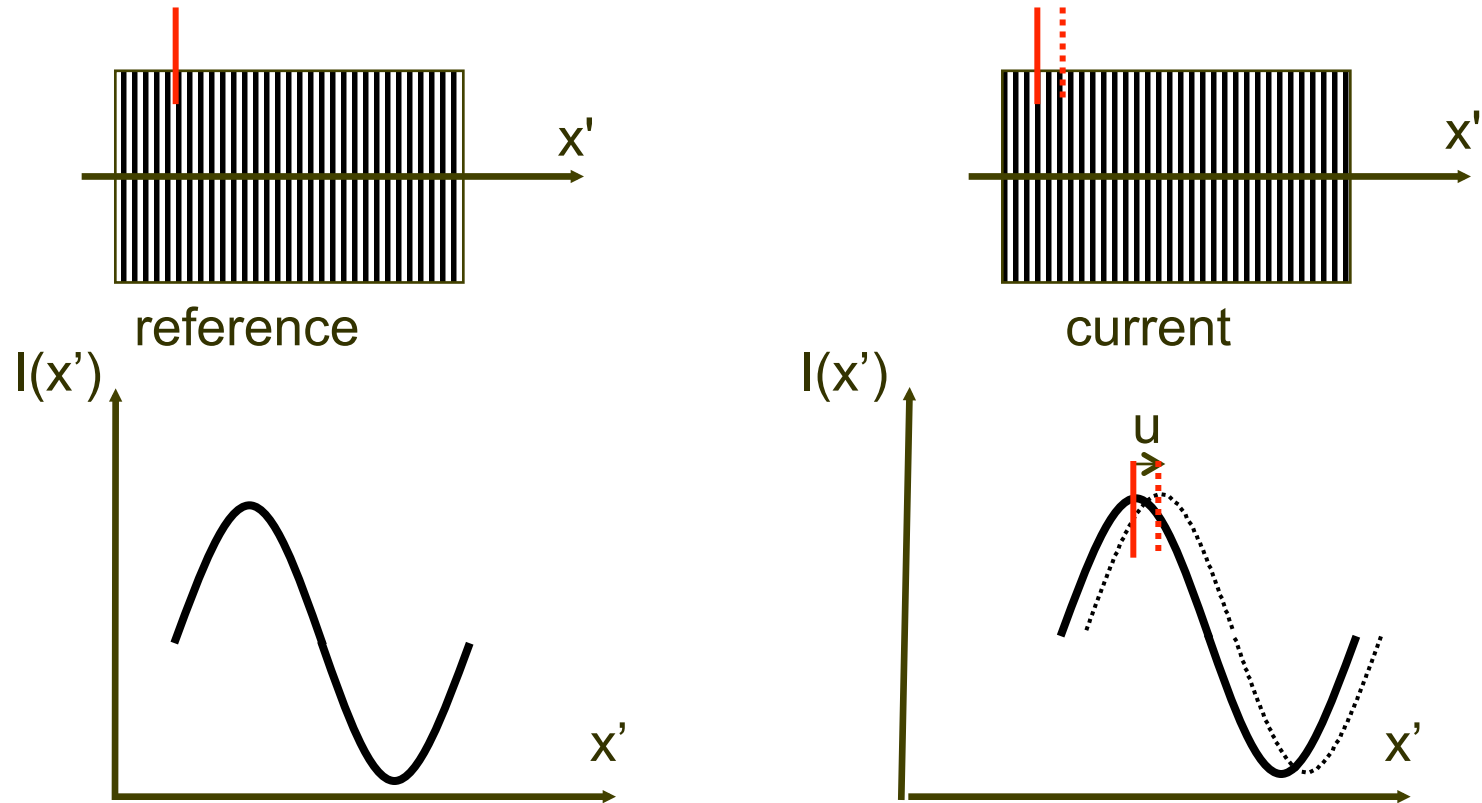


Outline

- 1- Basics on the grid method
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Link between displacement and phase [1] :

in the coordinate system of the grid :

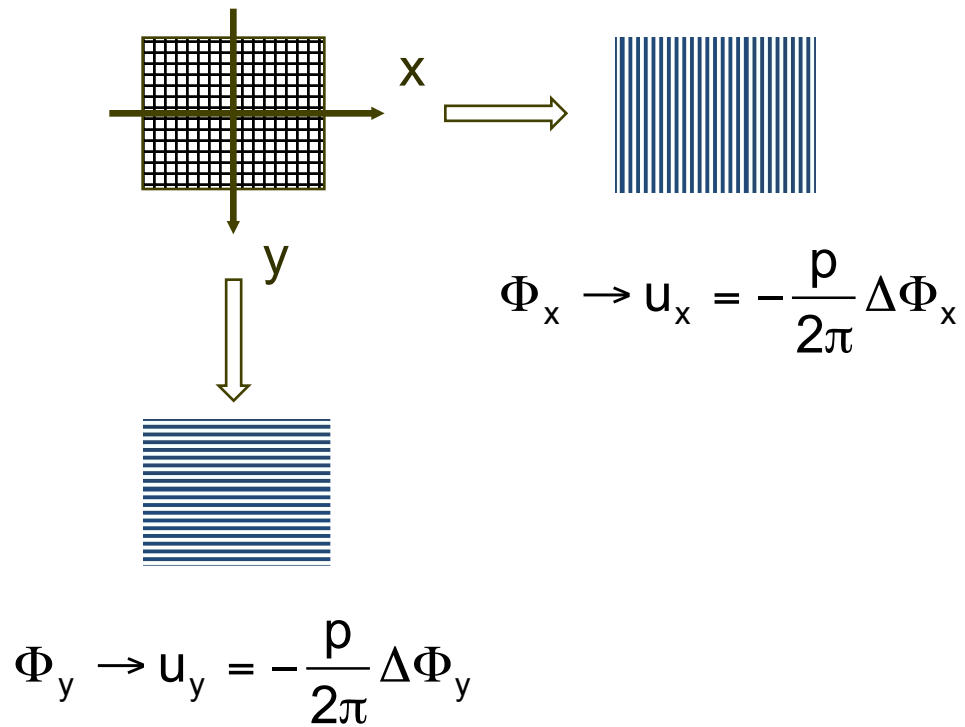


Displacement proportional to the **change in phase**

$$\rightarrow u = -\frac{\rho}{2\pi} (\Phi_{\text{current}} - \Phi_{\text{reference}}) = -\frac{\rho}{2\pi} \Delta\Phi$$

Case of 2D-grids:

2D grids \rightarrow 2 displacements u_x and u_y



Extracting the phases from the images

- by using a Fourier-based method such as:
 - the Geometric Phase Analysis [1] (the whole spectrum)
 - the windowed Geometric Phase Analysis [2] (windows in the spectrum)
 - the Localized Spectrum Analysis, LSA [3] (points in the spectrum)

- LSA:

$$\widehat{s}(x, y, f, \theta, \alpha) = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \underline{s(u, v)} \underline{g(x - u, y - v)} e^{-2i\pi fu(\cos\alpha + fvsin\alpha)} dudv$$

with:

1. $s(u, v)$: signal = matrix of gray levels
2. $g(x-u, y-v)$: Gaussian window

[1] M. J. Hytch, E. Snoeck, R. Kilaas, Ultramicroscopy, 74:131-146, 1998

[2] X. Dai, H. Xie, H. Wang, Optics and Laser Technology, 58(6):119-127, 2014

[3] M. Grédiac, F. Sur, B. Blaysat, Strain, 52(3):205--243, 2016

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- LSA:

$$\widehat{s}(x, y, f, 0, \alpha) = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \underline{s(u, v)} \underline{g(x-u, y-v)} e^{-2i\pi fu(\cos\alpha + fvsin\alpha)} dudv$$

with:

1. $s(u, v)$: signal = matrix of gray levels

2. $g(x-u, y-v)$: Gaussian window

- $\widehat{s}(x, y, f, 0, \alpha)$ and $\widehat{s}(x, y, 0, f, \alpha)$: two complex numbers for each image
→ 2 arguments → 2 phases for each image → 2 displacement components

[1] M. J. Hytch, E. Snoeck, R. Kilaas, Ultramicroscopy, 74:131-146, 1998

[2] X. Dai, H. Xie, H. Wang, Optics and Laser Technology, 58(6):119-127, 2014

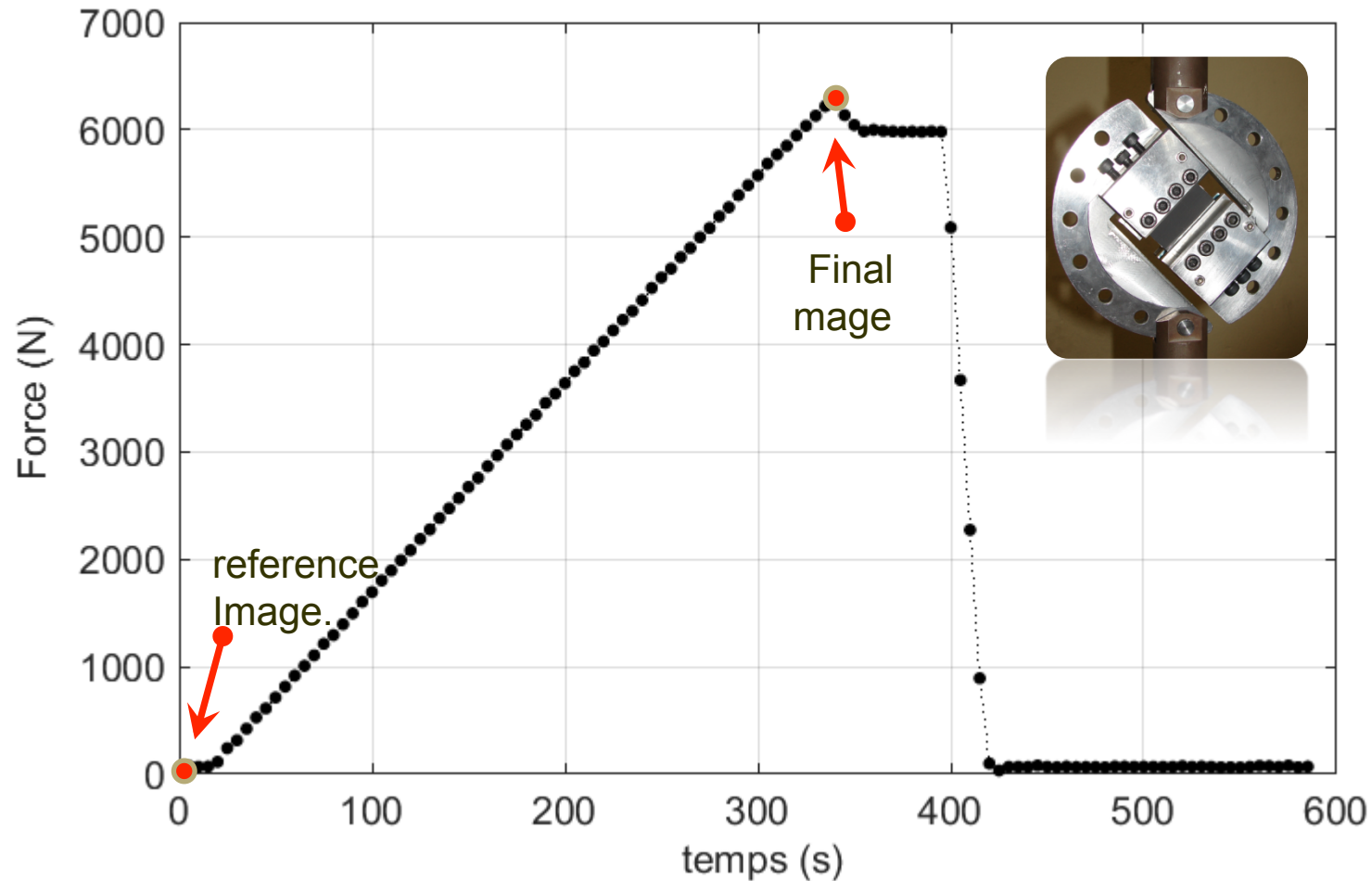
[3] M. Grédiac, F. Sur, B. Blaysat, Strain, 52(3):205--243, 2016

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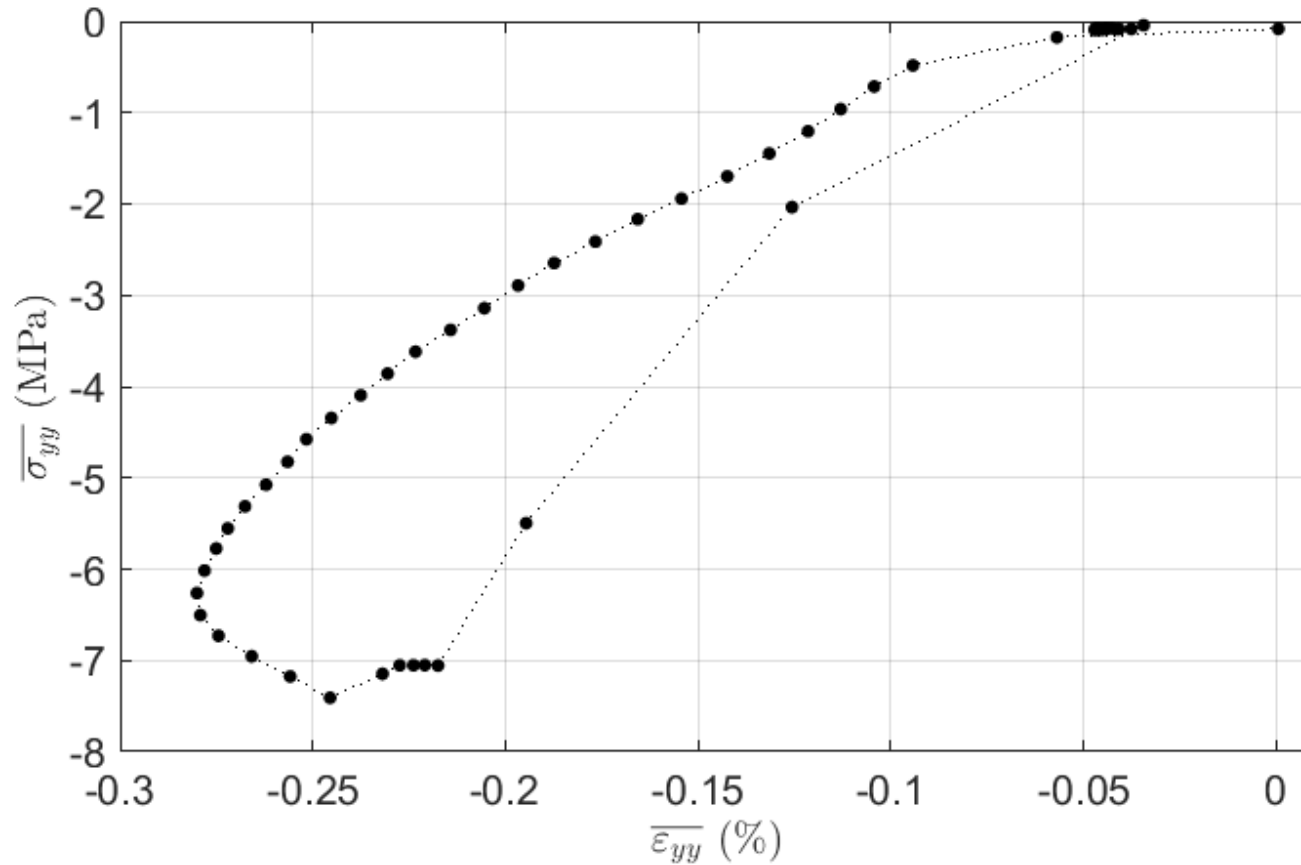
Test A: compression + shear

- force-driven: 0,02 kN/s, $F_{max}=6,3$ kN (...)
- frequency: 2 images/s

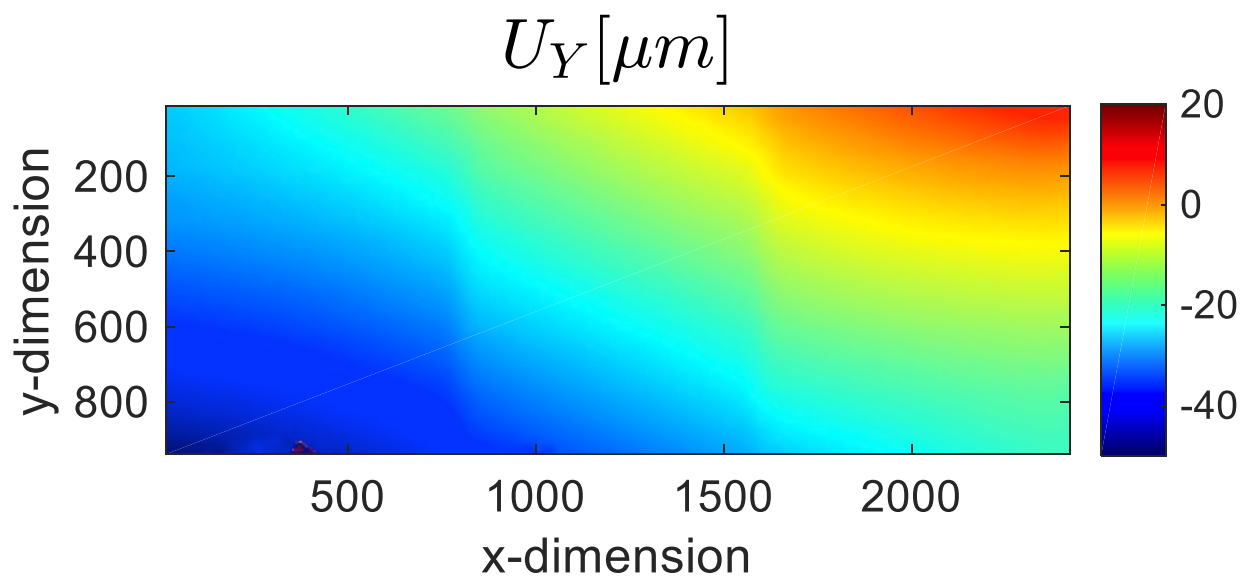
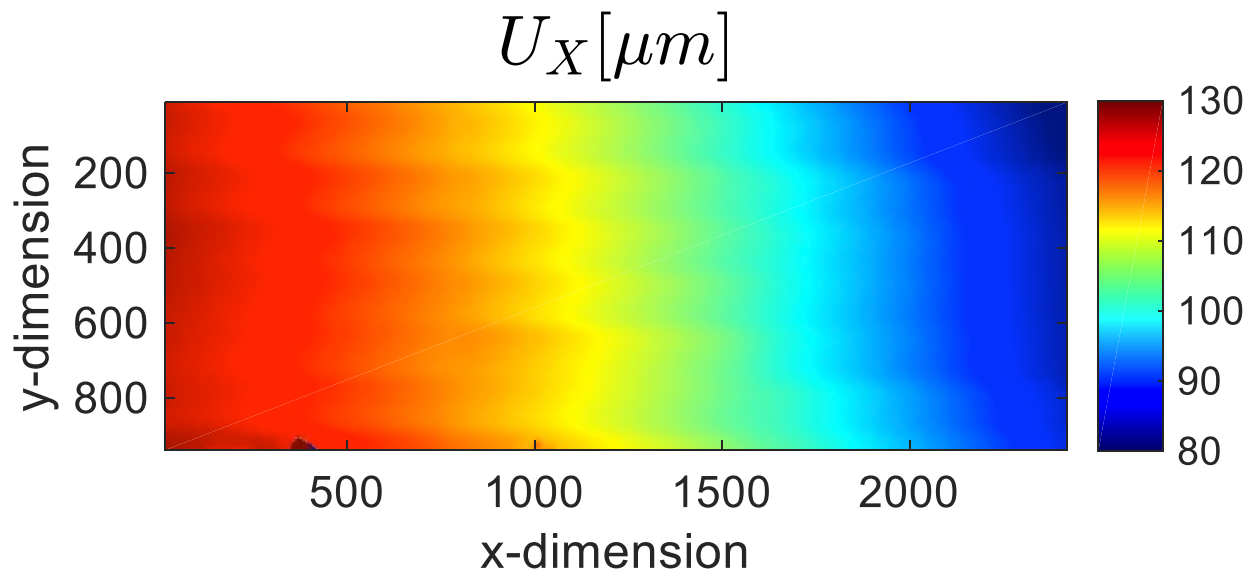


mean stress $\overline{\sigma_{yy}}$ vs. mean strain $\overline{\varepsilon_{yy}}$

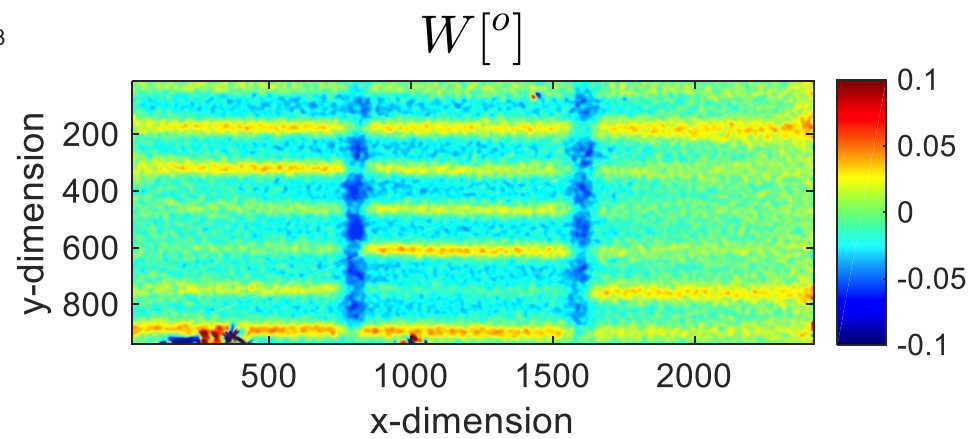
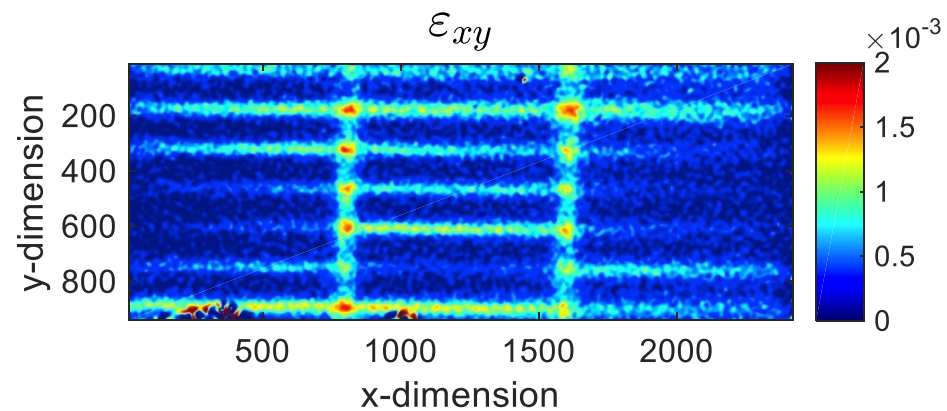
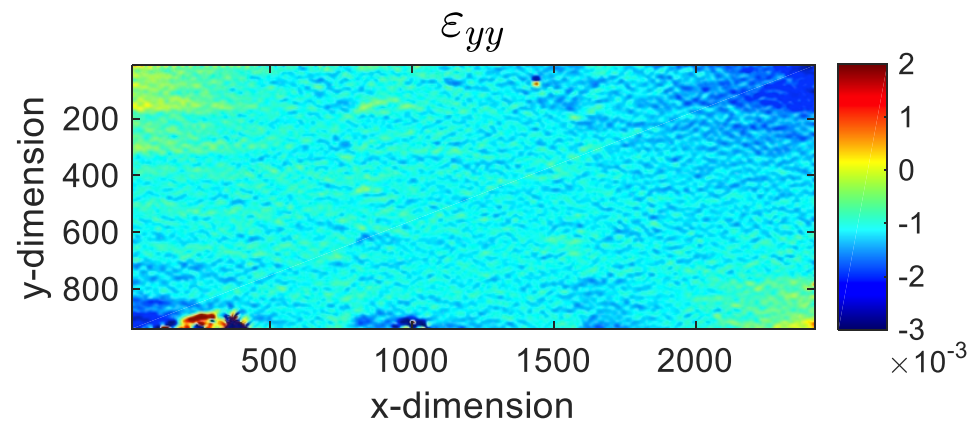
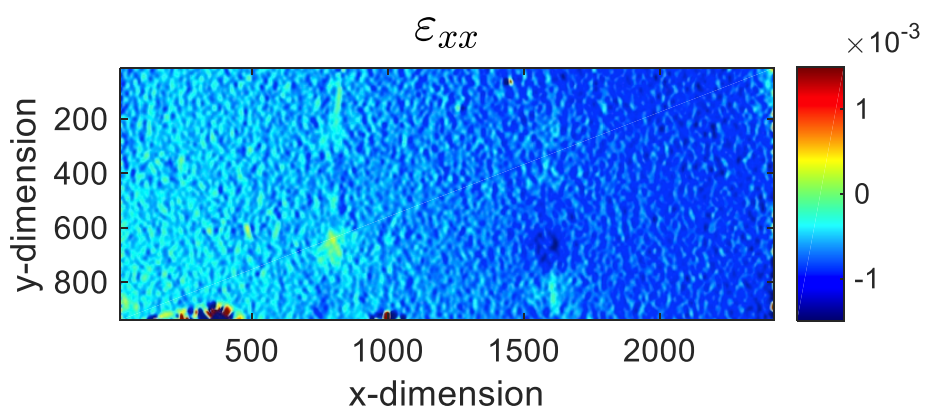
$$\overline{\sigma_{yy}} = \frac{F}{S} \times \frac{\sqrt{2}}{2} \quad \overline{\varepsilon_{yy}} = \frac{\overline{u_y}(Z_1) - \overline{u_y}(Z_2)}{\text{distance}(Z_1, Z_2)}$$



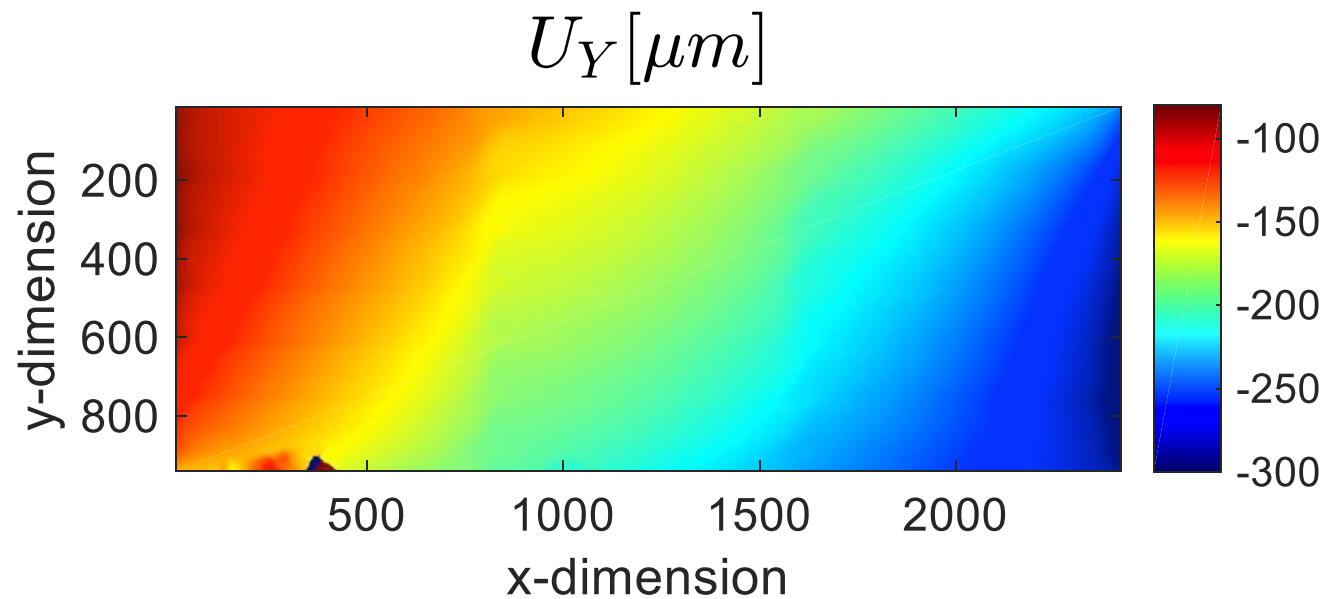
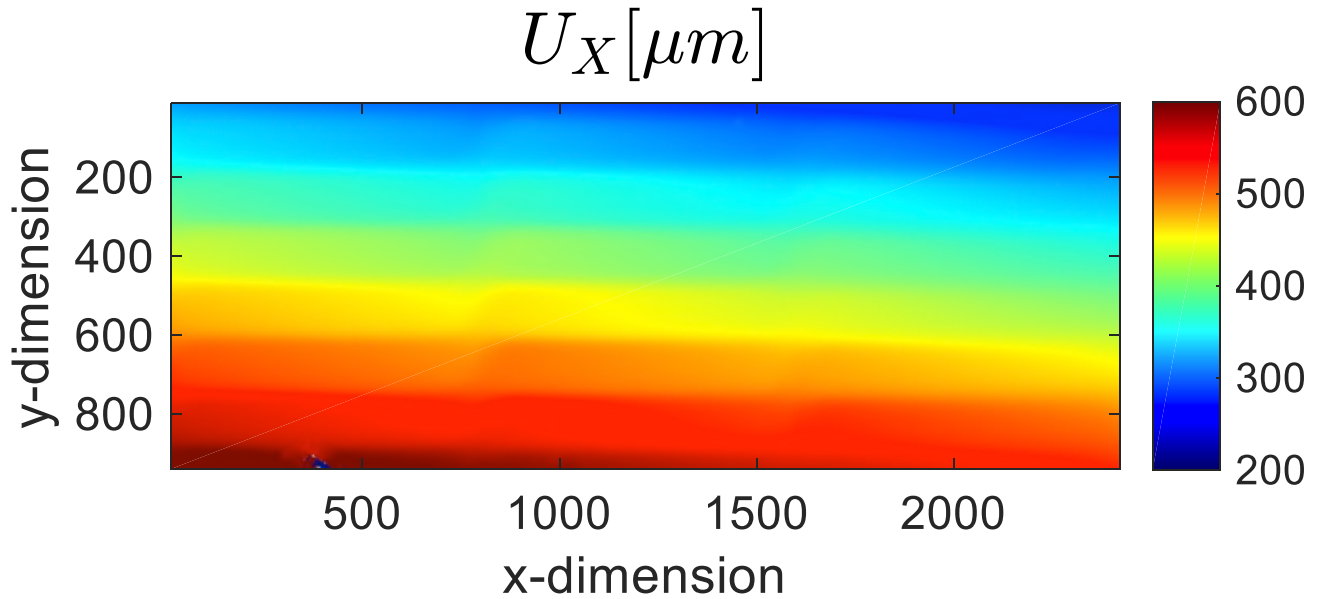
Displacement maps at Point P₁



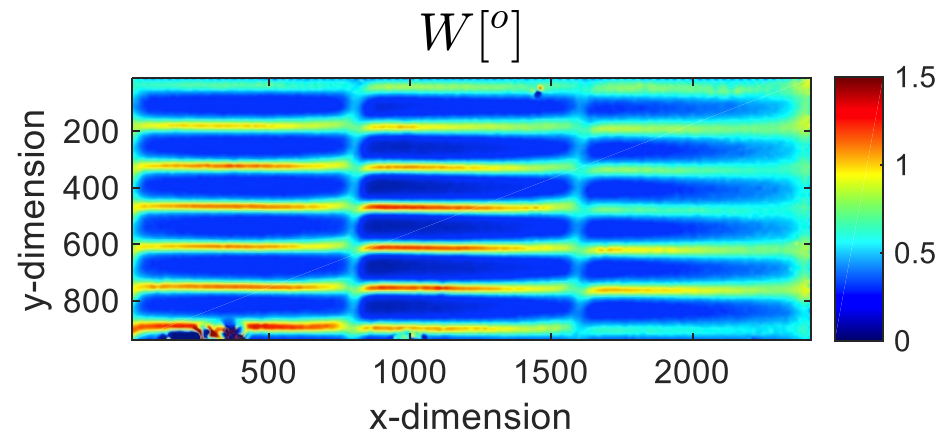
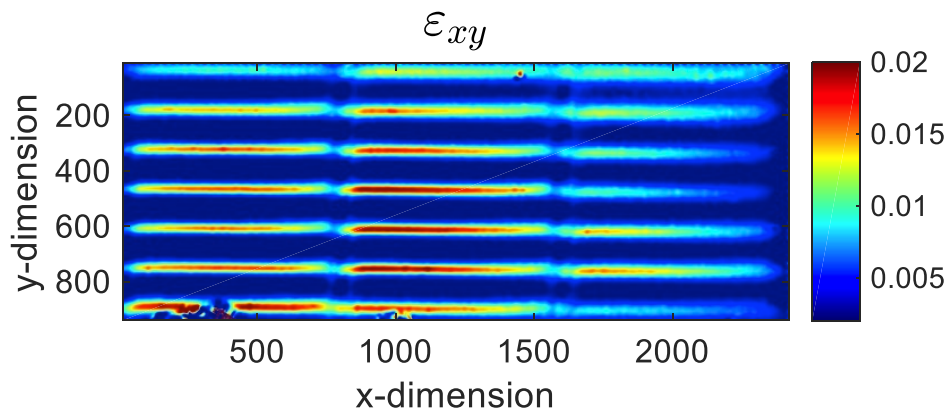
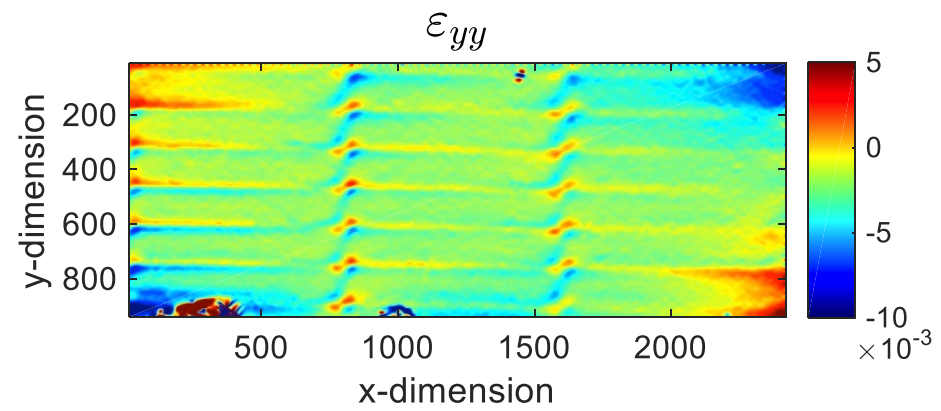
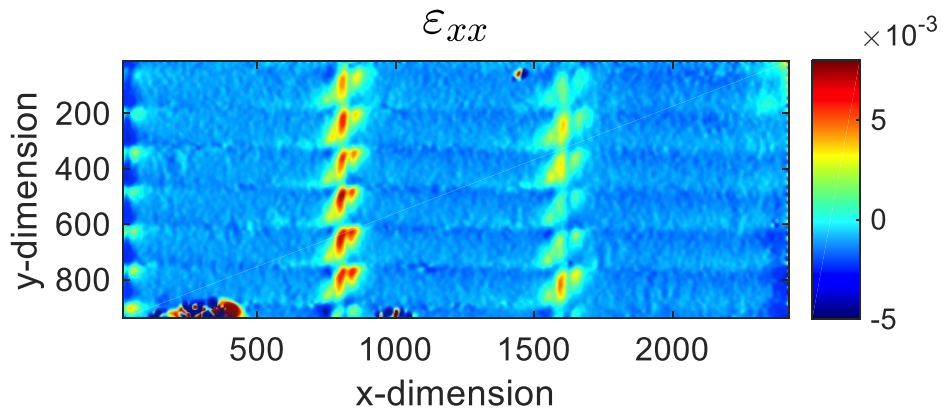
Strain and rotation maps at Point P_1



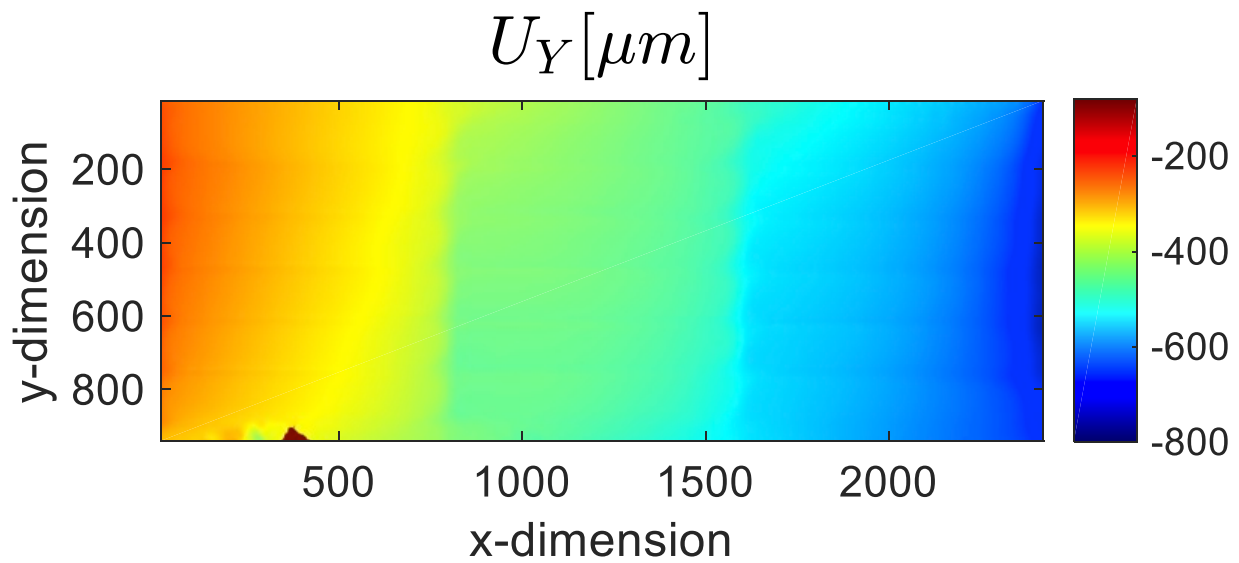
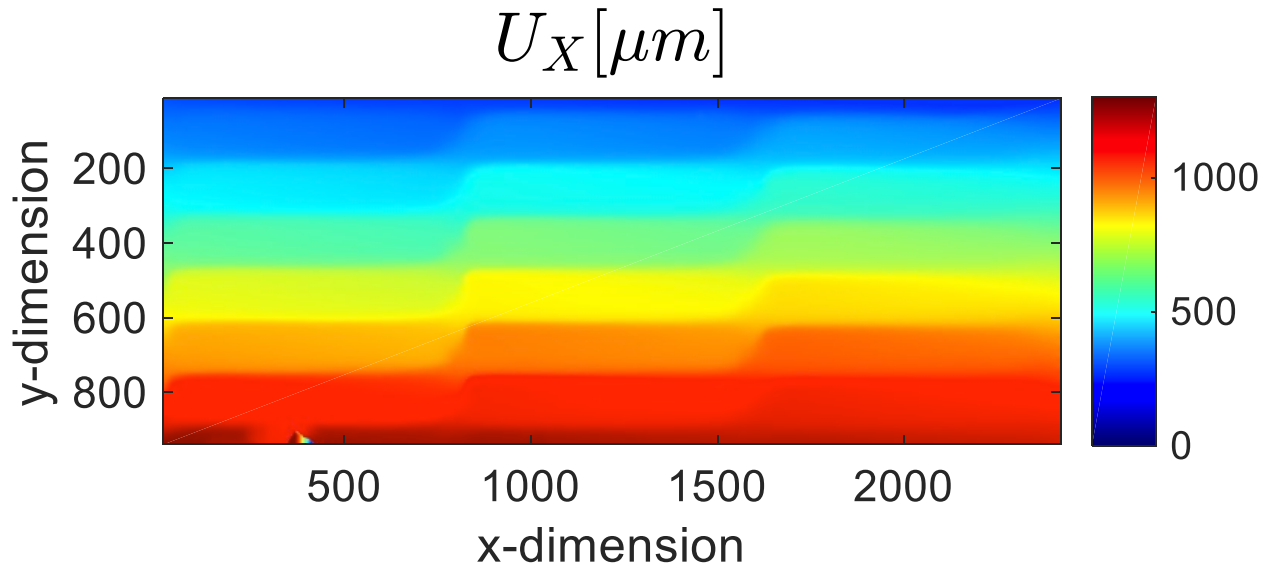
Displacement maps at Points P₂



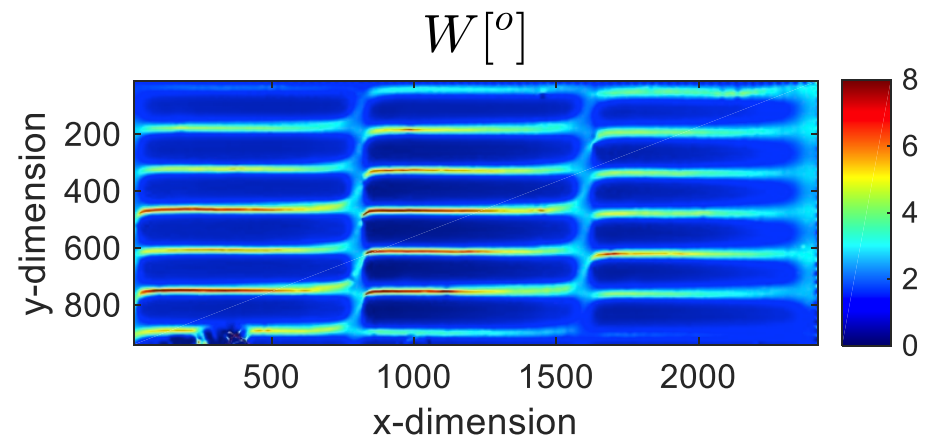
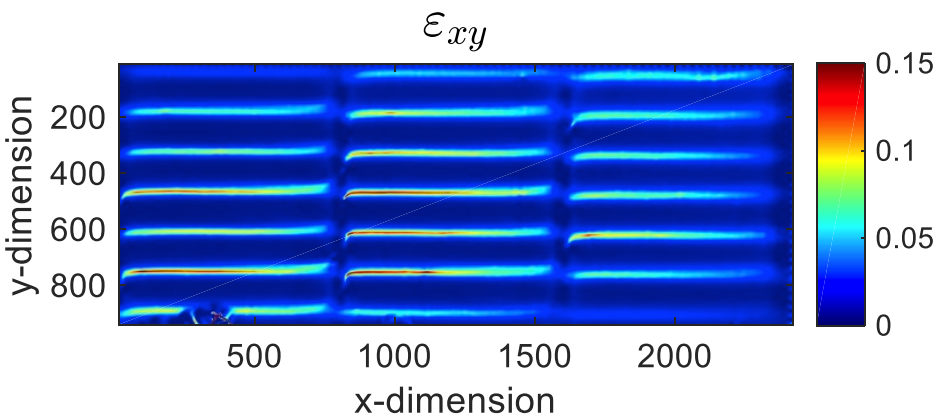
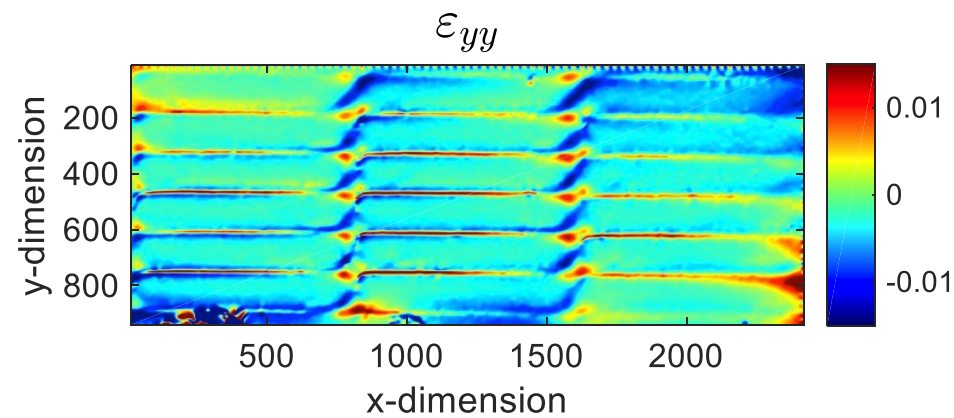
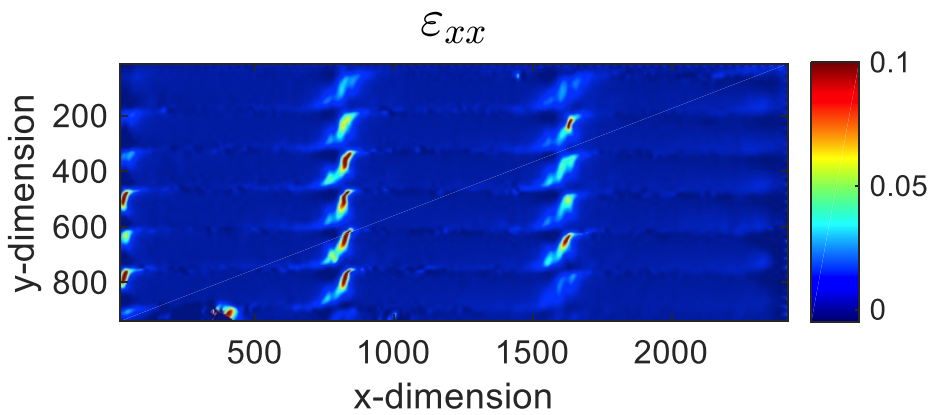
Strain and rotation maps at Point P₂



Displacement maps at Points P₃

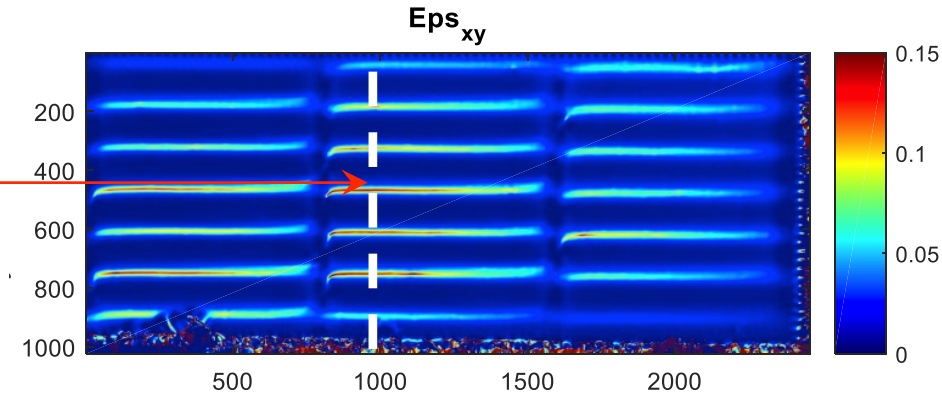


Strain and rotation maps at Point P₃



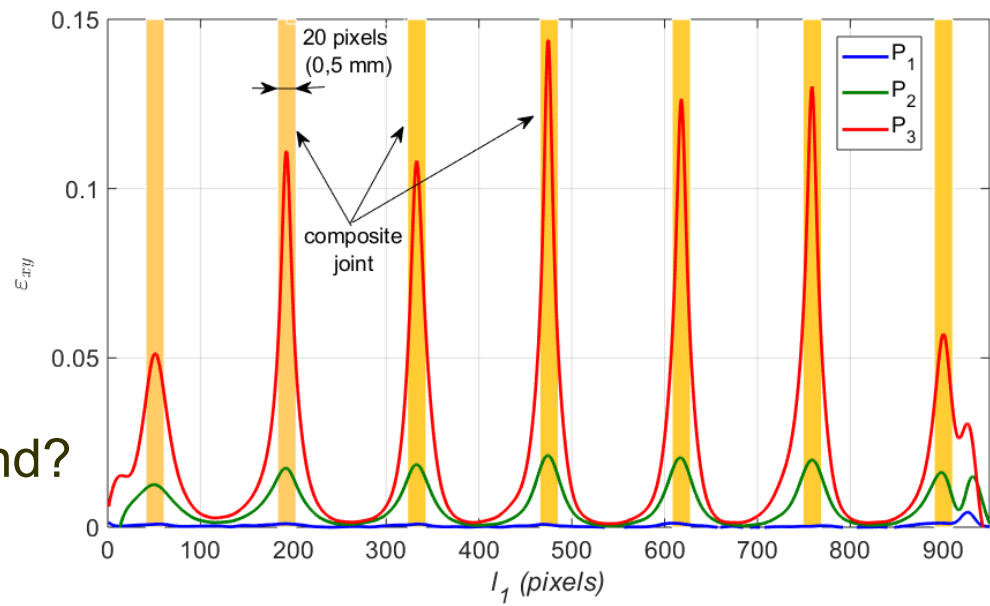
Strain field: cross-section of the ϵ_{xy} map for various loading amplitudes

Cross-section along this line



Remarks:

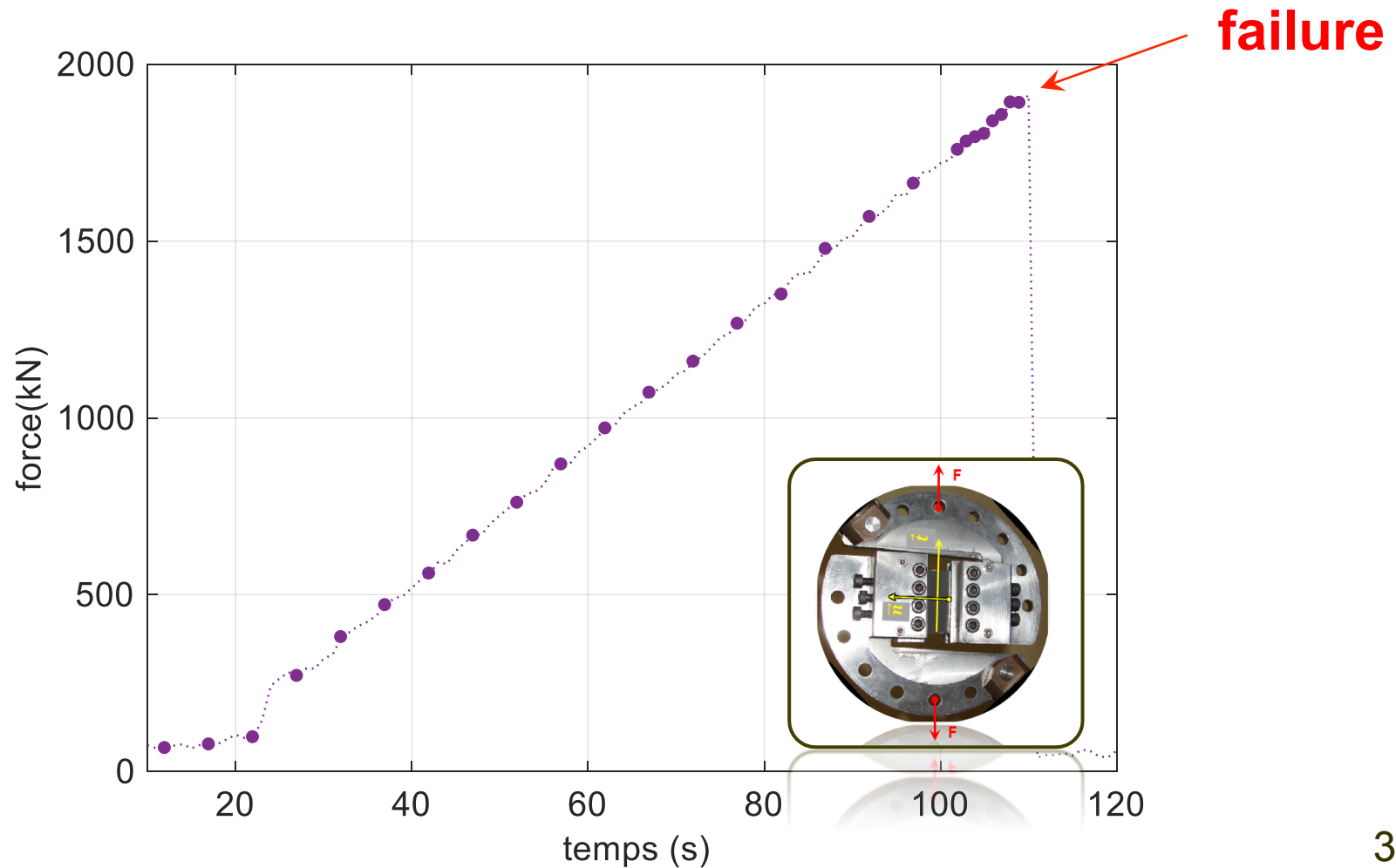
- peaks ↗ as the load ↗
- smooth distribution...
- ... but blur = systematic error
- actual value within these narrow band?
- systematic error removed up to a certain frequency [1]



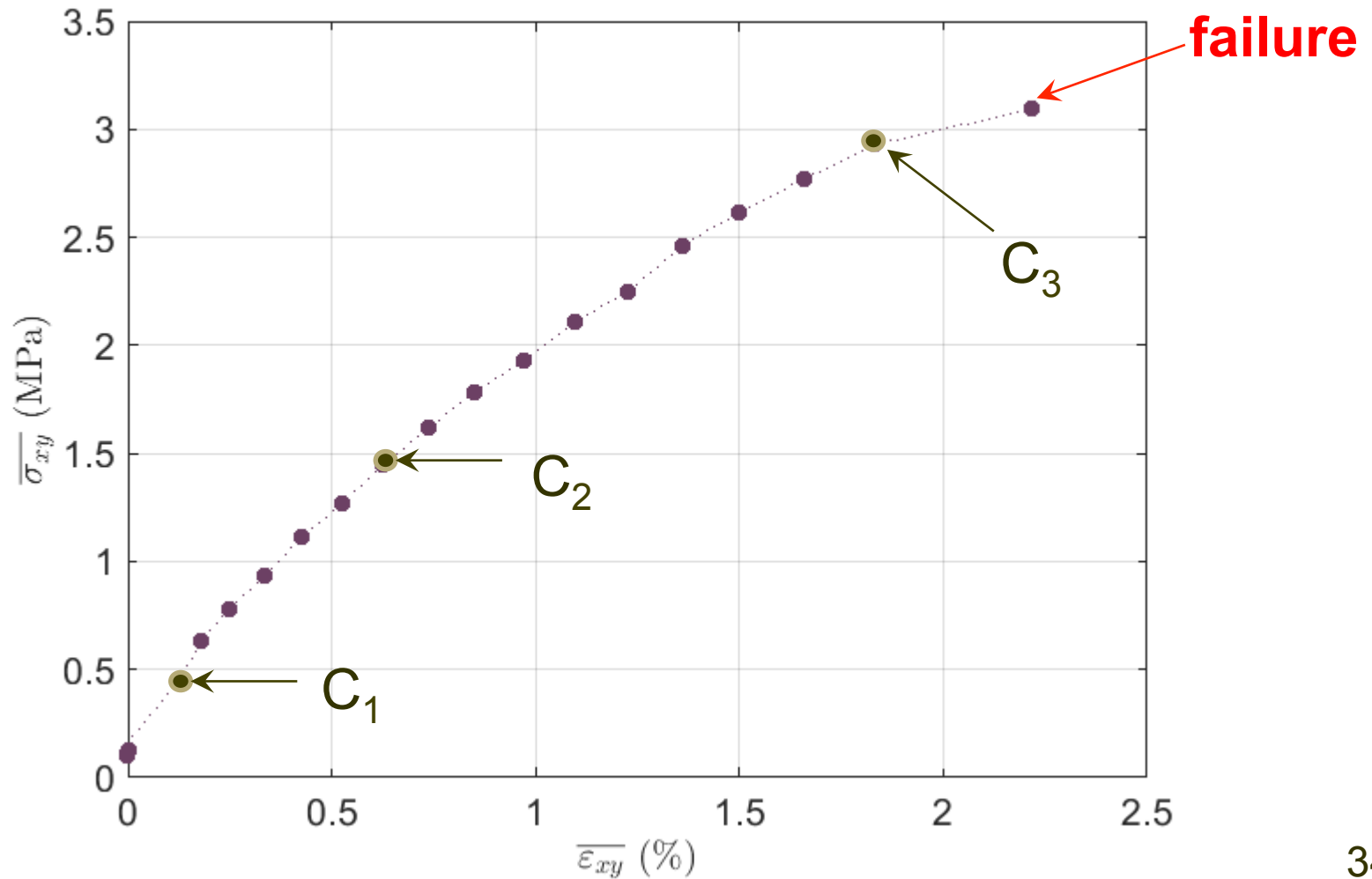
[1] M. Grédiac, B. Blaysat, F. Sur, *Experimental Mechanics*, in revision, 2018

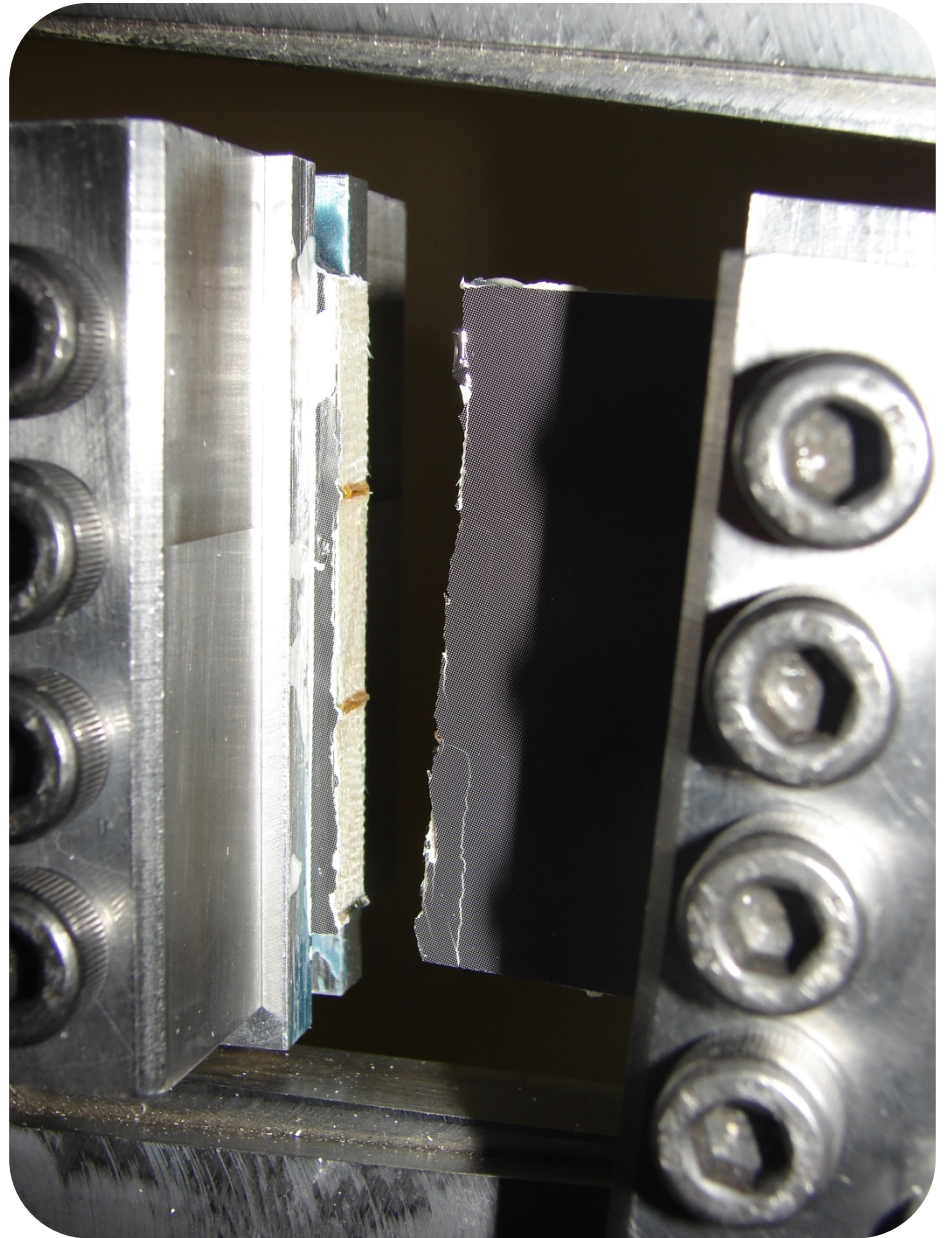
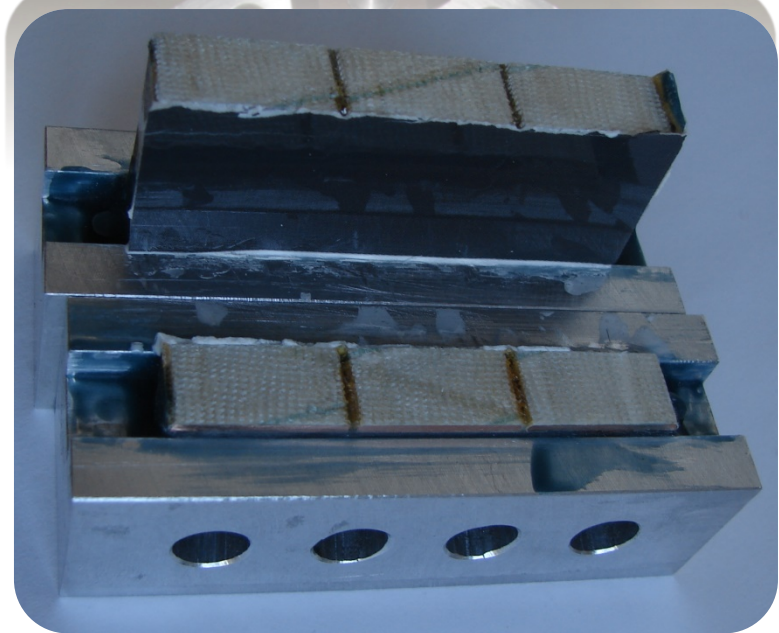
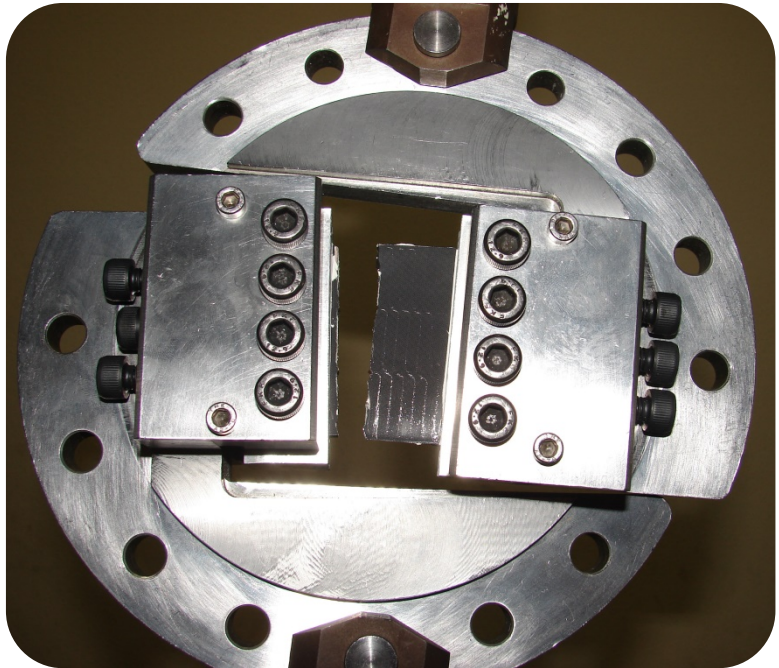
Test B: shear

- force driven 0,02 kN/s, $F_{\max}=1,9$ kN
- frequency: 2 images/s
- lighting issues \rightarrow noiser strain maps

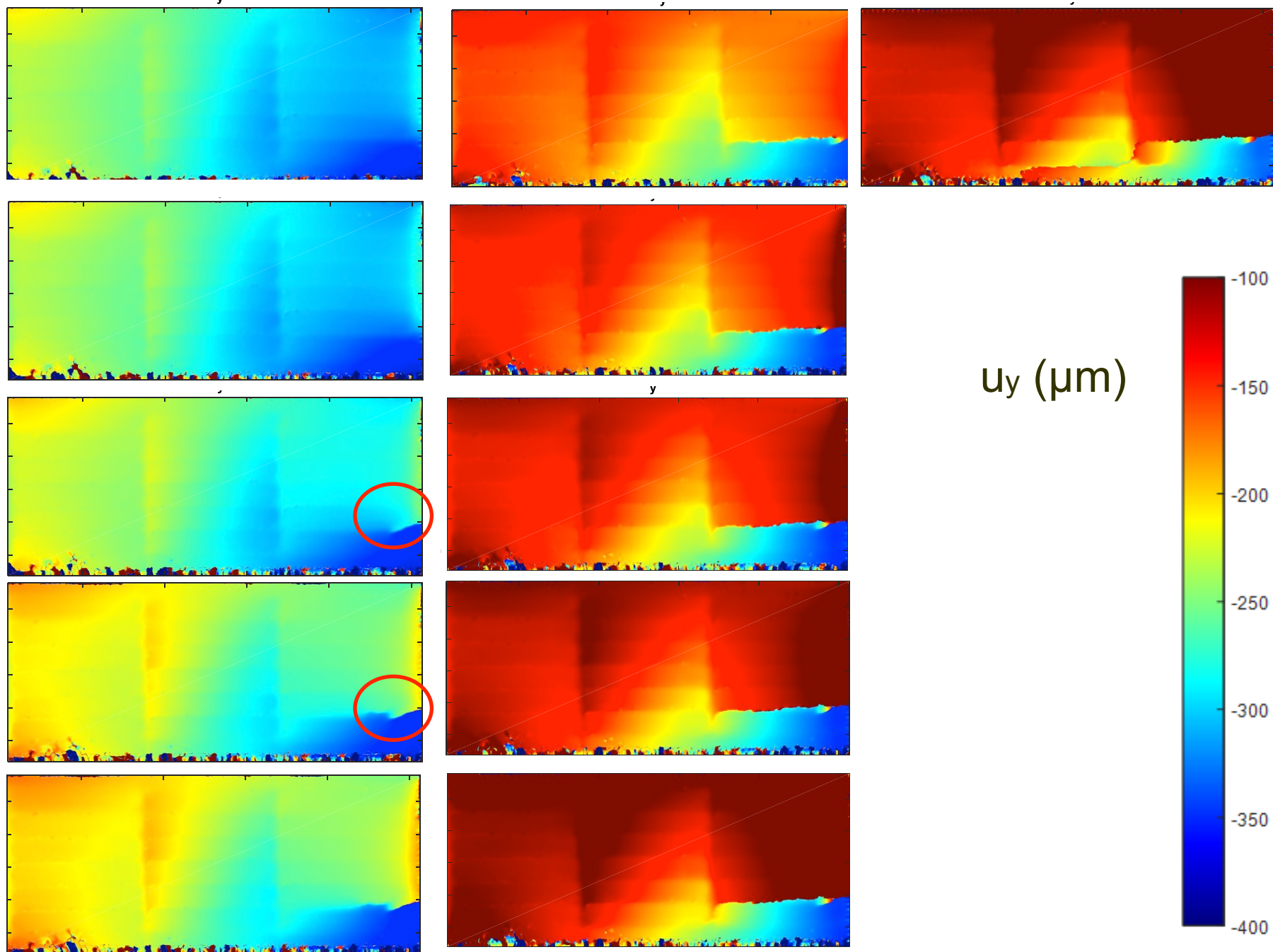


$$\overline{\sigma}_{xy} = \frac{F}{S} \quad \overline{\varepsilon}_{xy} = \frac{\overline{u}_x(Z_1) - \overline{u}_x(Z_2)}{\text{distance}(Z_1, Z_2)}$$





Crack initiation + propagation



Outline

- 1- Basics on the grid method
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Conclusion:

- feasibility study, in-plane displacement/strain measurement with the grid method
- strong heterogeneities in the strain field due to the heterogeneous nature of the materials
- crack detection (appearance + propagation) in the displacement field

Conclusion:

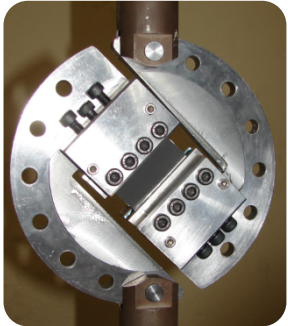
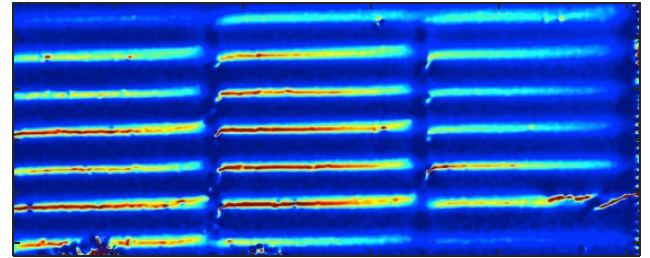
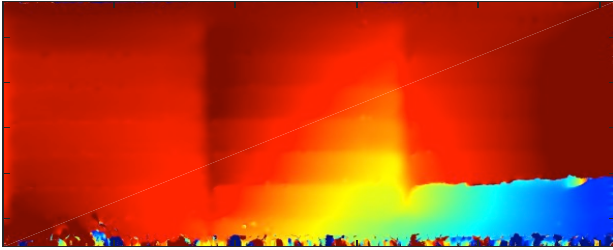
- feasibility study, in-plane displacement/strain measurement with the grid method
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- information potentially valuable for the design of superconducting magnets

Conclusion:

- feasibility study, in-plane displacement/strain measurement with the grid method
- strong heterogeneities in the strain field due to the heterogeneous nature of the materials
- crack detection (appearance + propagation) in the displacement field
- information potentially valuable for the design of superconducting magnets
- qualitative or quantitative measurement? → two recent improvements:
 - 1- decreasing the noise level in the map → optimizing the pattern
2D grids → checkerboards [1]
 - 2- strain maps blurred because of convolution → systematic error → deconvolution algorithm suitable for strain maps [2]

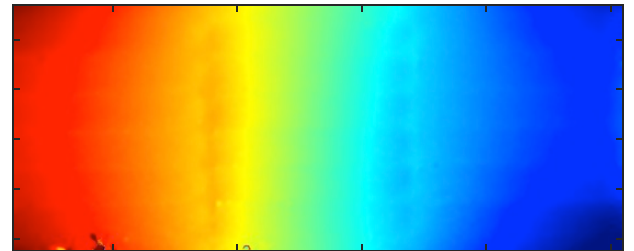
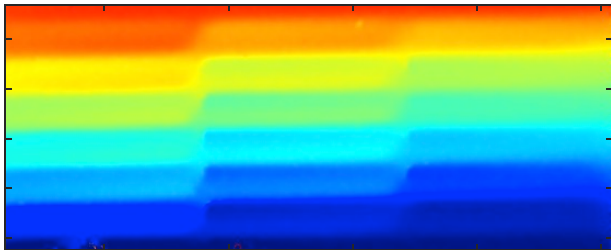
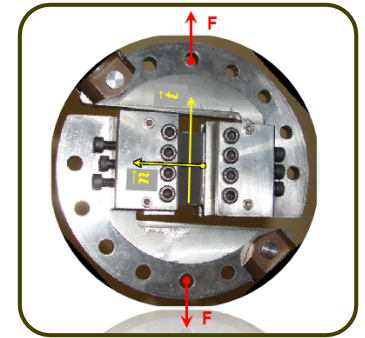
[1] M. Grédiac, B. Blaysat, F. Sur, *Experimental Mechanics*, in press, 2018

[2] M. Grédiac, B. Blaysat, F. Sur, *Experimental Mechanics*, in revision, 2018

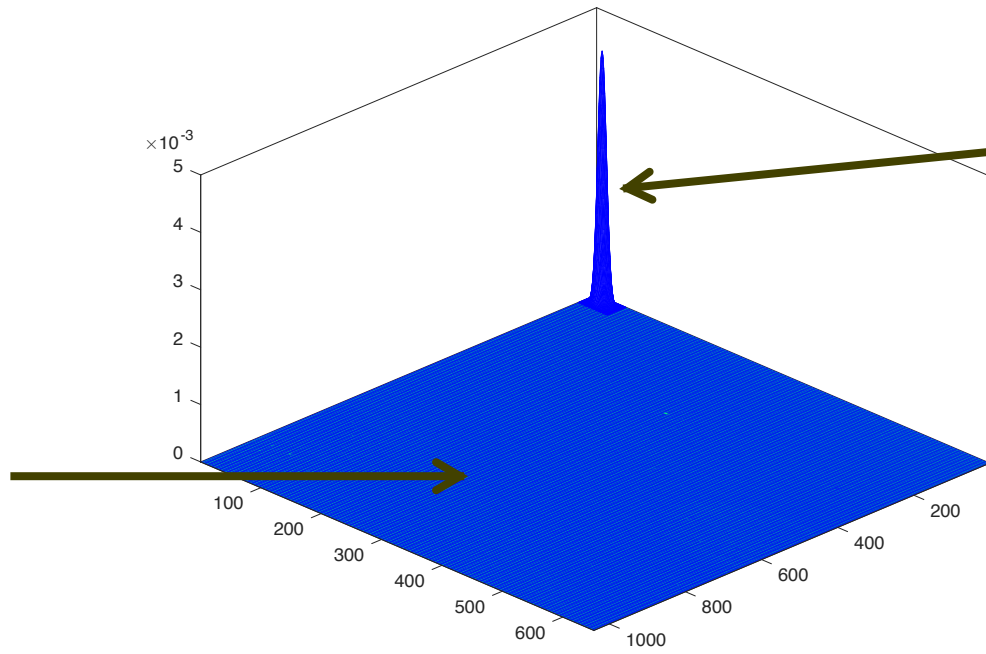


Thank you for your
attention

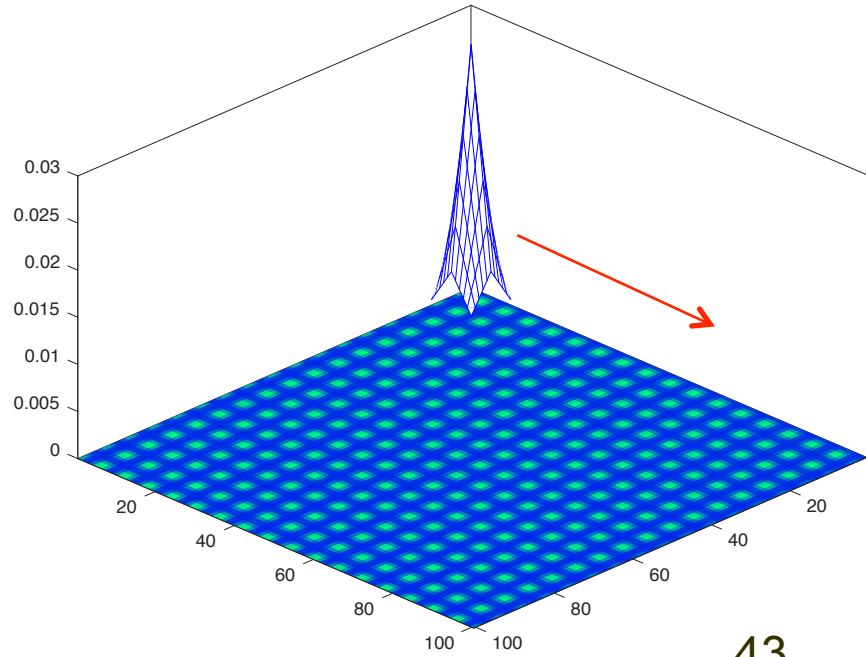
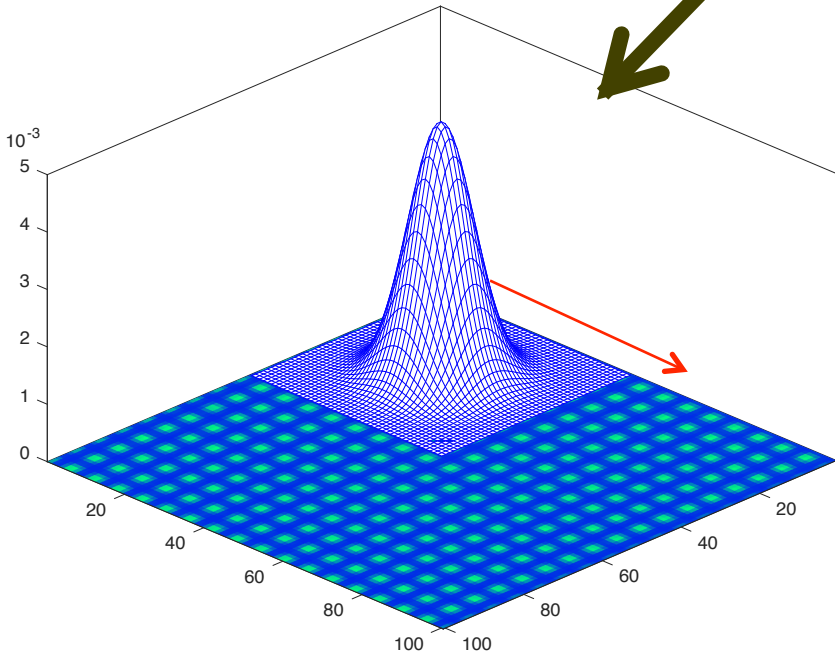
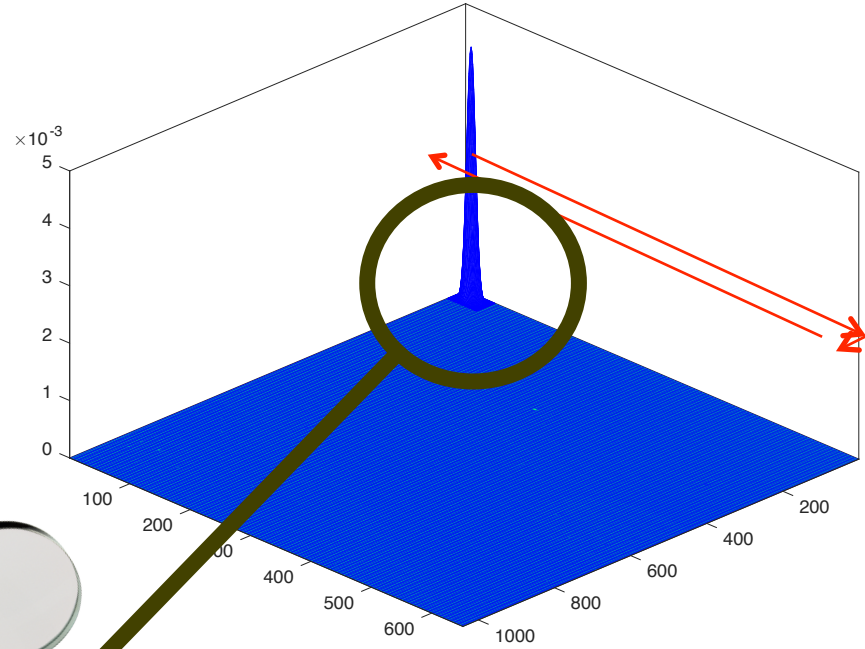
Any questions?



grid image

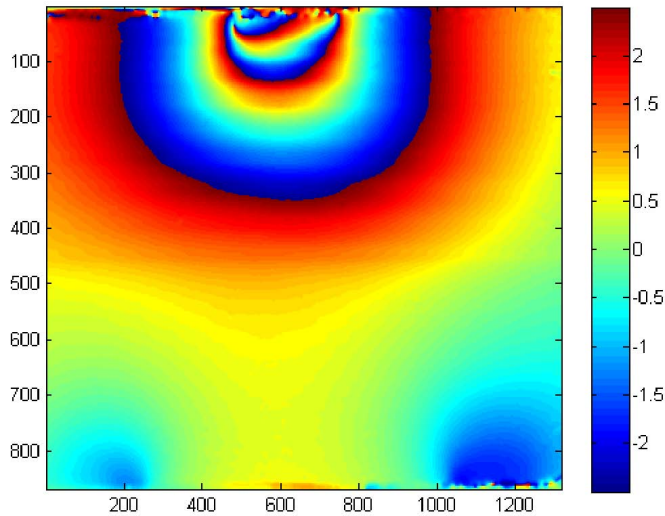


window

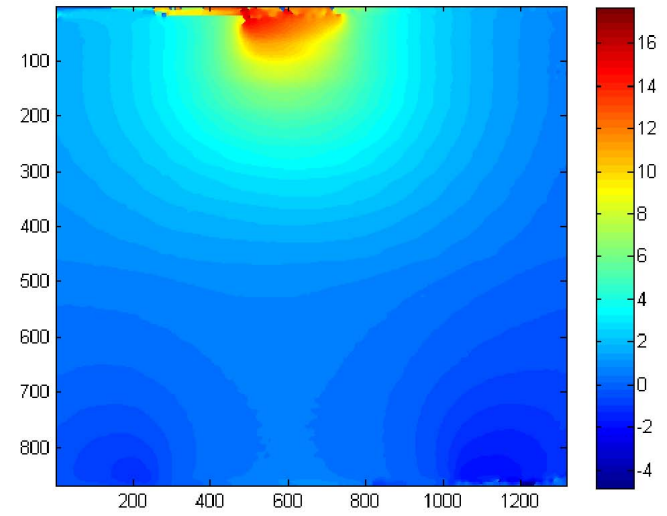


Phase unwrapping:

- argument of a complex number $\rightarrow 2\pi$ phase jumps in phase maps if the amplitude of the phase $> 2\pi$
- map of « wrapped » phases \rightarrow phase maps must be « unwrapped » [1]
- example



before unwrapping



after unwrapping

- $\hat{s}(x, y, 0, f, \alpha)$ and $\hat{s}(x, y, f, 0, \alpha)$: two complex numbers for each image
 → 2 arguments → 2 phases for each image → 2 displacement components

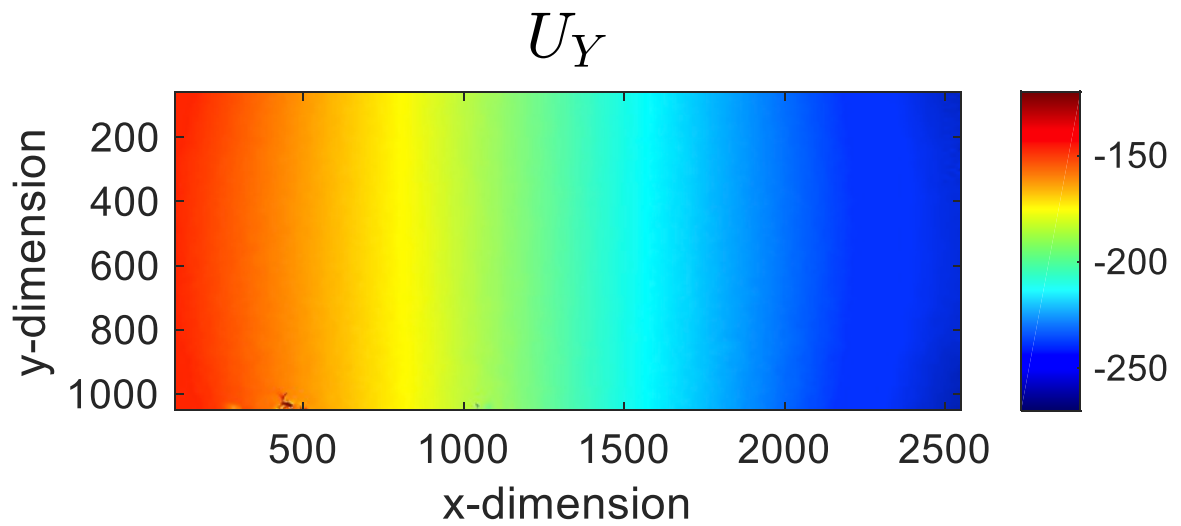
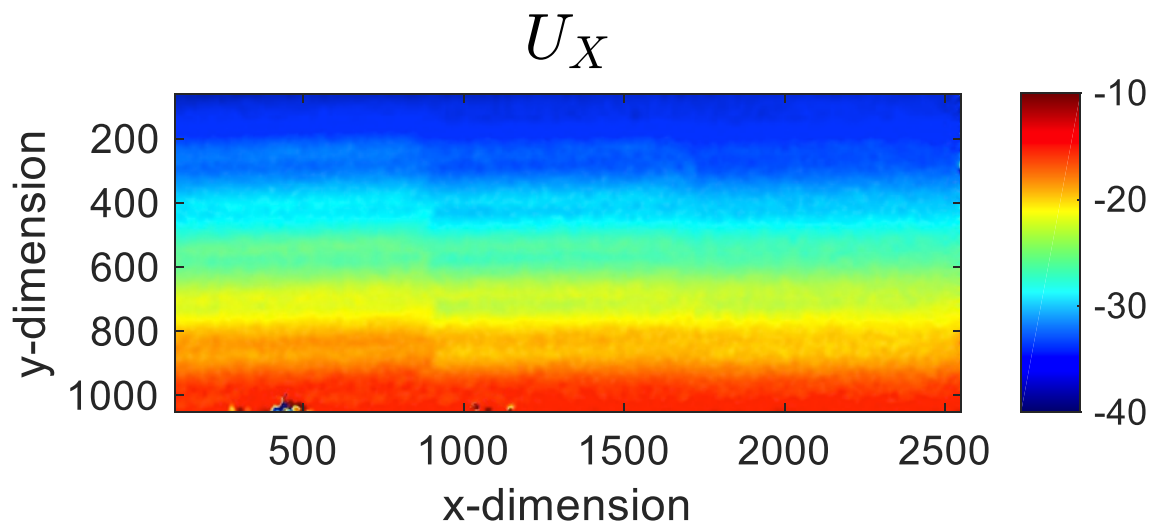
$$\begin{cases} u_x(x, y) = -\frac{p}{2\pi} \Delta \Phi_x \\ u_y(x, y) = -\frac{p}{2\pi} \Delta \Phi_y \end{cases}$$

- fixed-point algorithm to find the displacement:

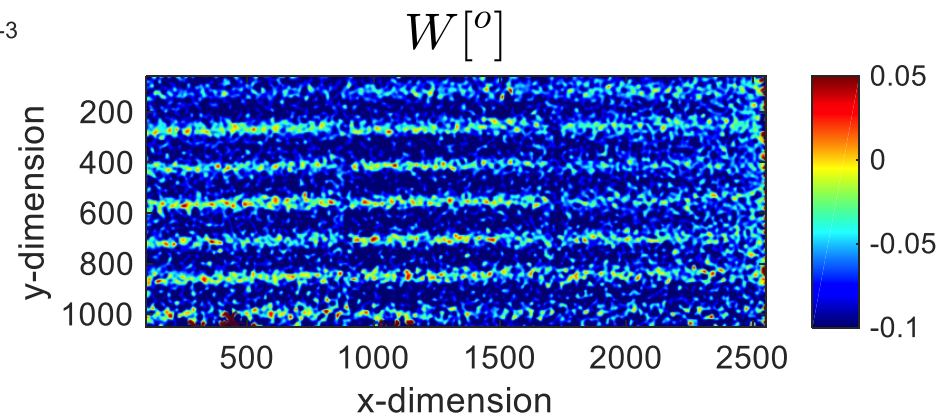
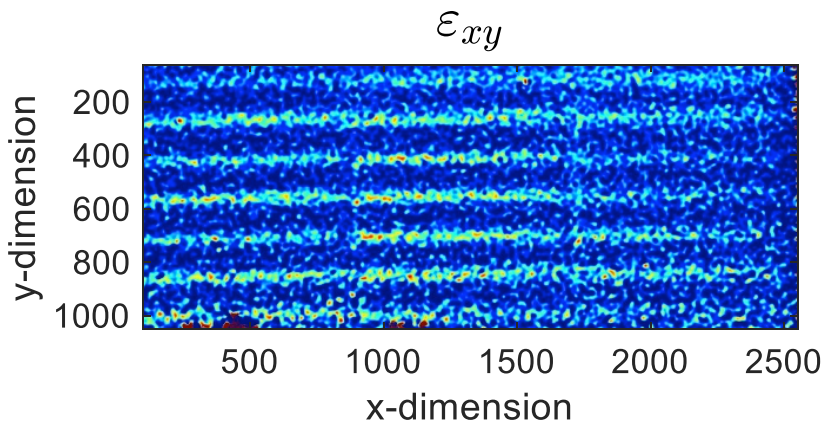
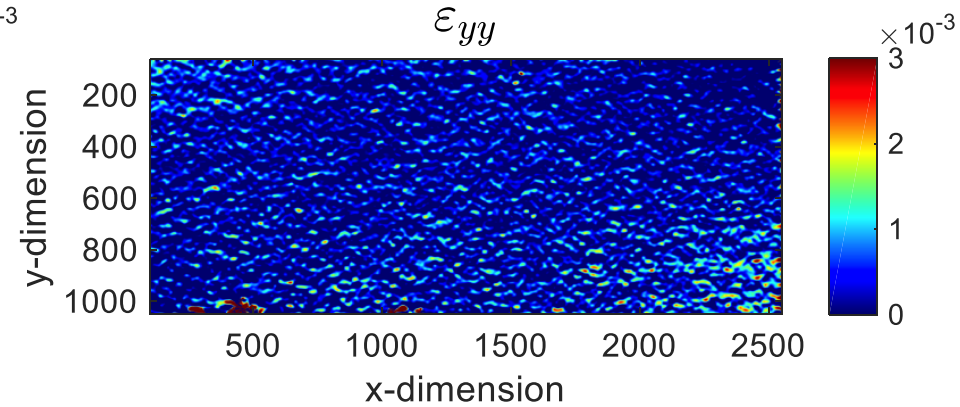
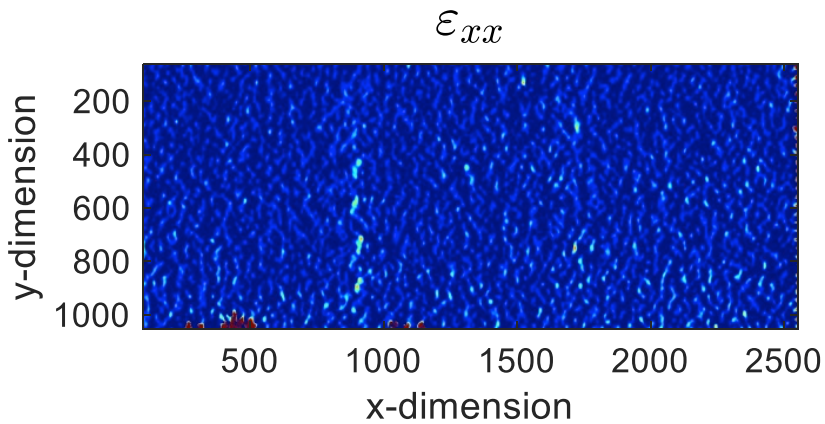
$$\begin{cases} u_x(x, y) = -\frac{p}{2\pi} [\Phi_x^{cur}(x + u_x(x, y), y + u_y(x, y)) - \Phi_x^{ref}(x, y)] \\ u_y(x, y) = -\frac{p}{2\pi} [\Phi_y^{cur}(x + u_x(x, y), y + u_y(x, y)) - \Phi_y^{ref}(x, y)] \end{cases}$$

- with small strains, one iteration to reach convergence

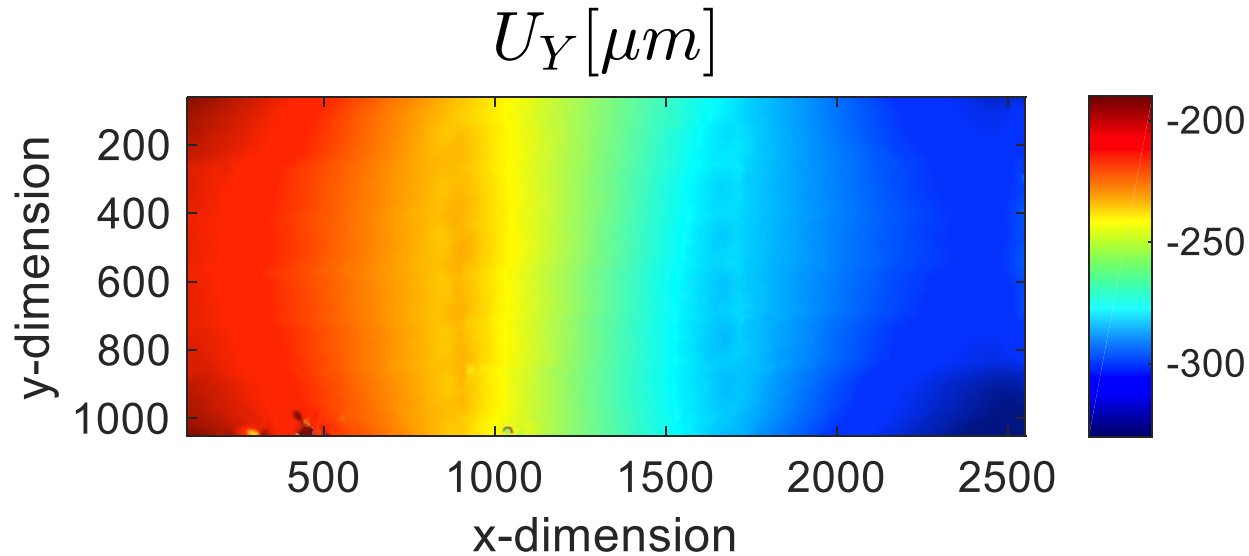
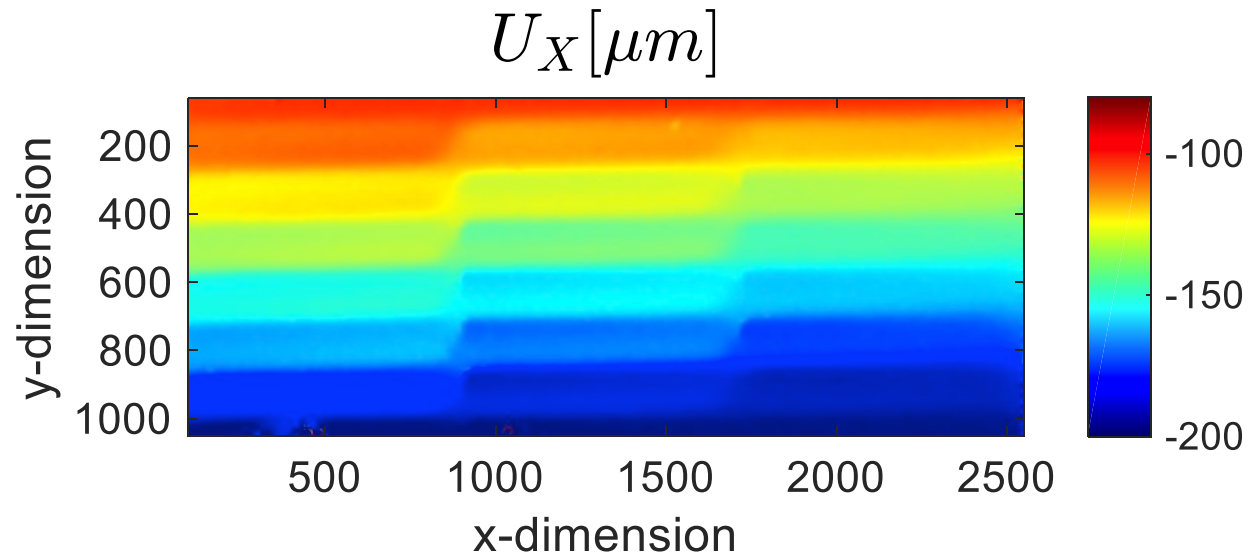
Displacement field at Point C₁



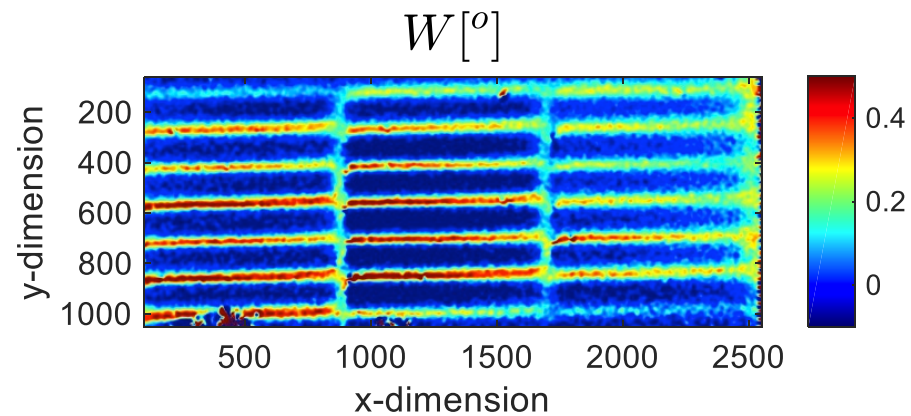
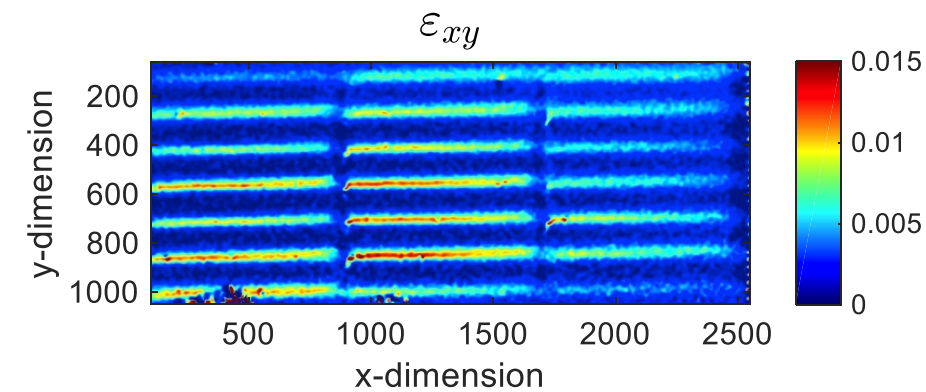
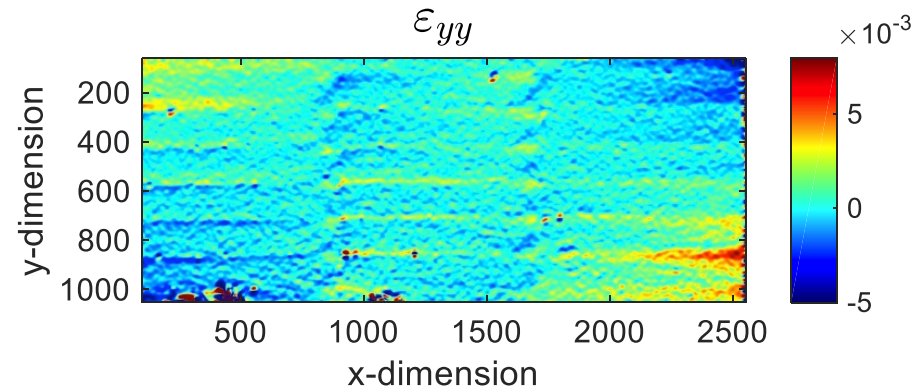
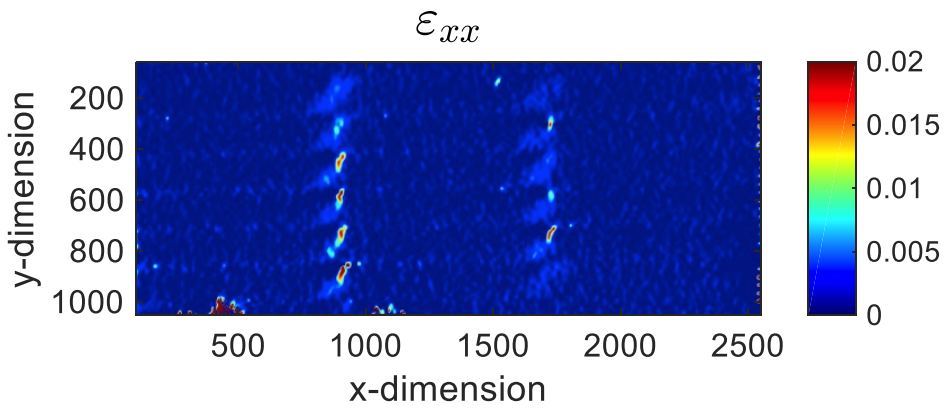
Strain + rotation fields at Point C₁



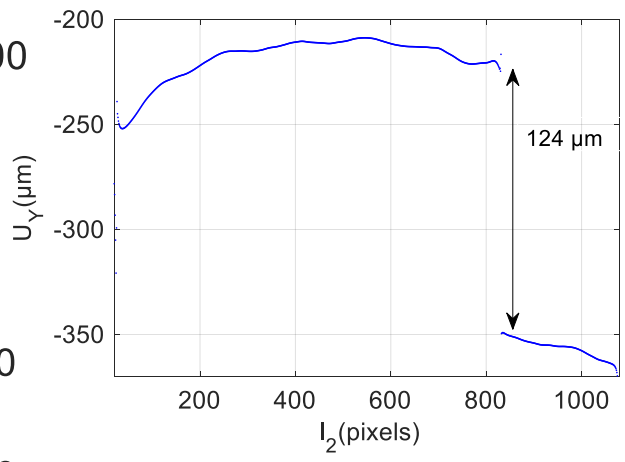
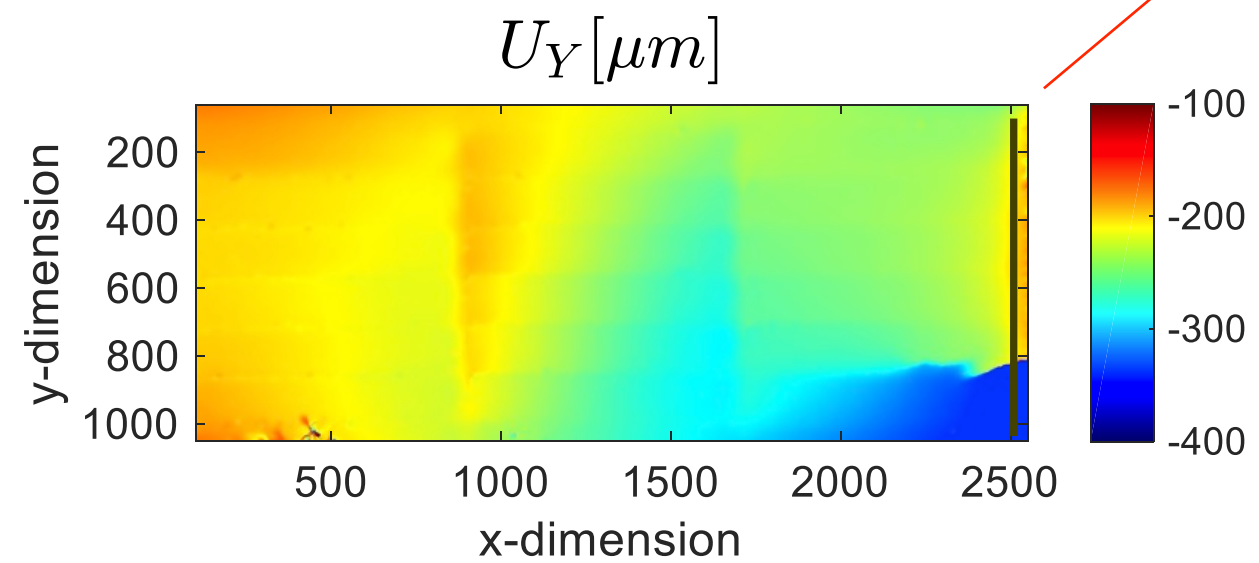
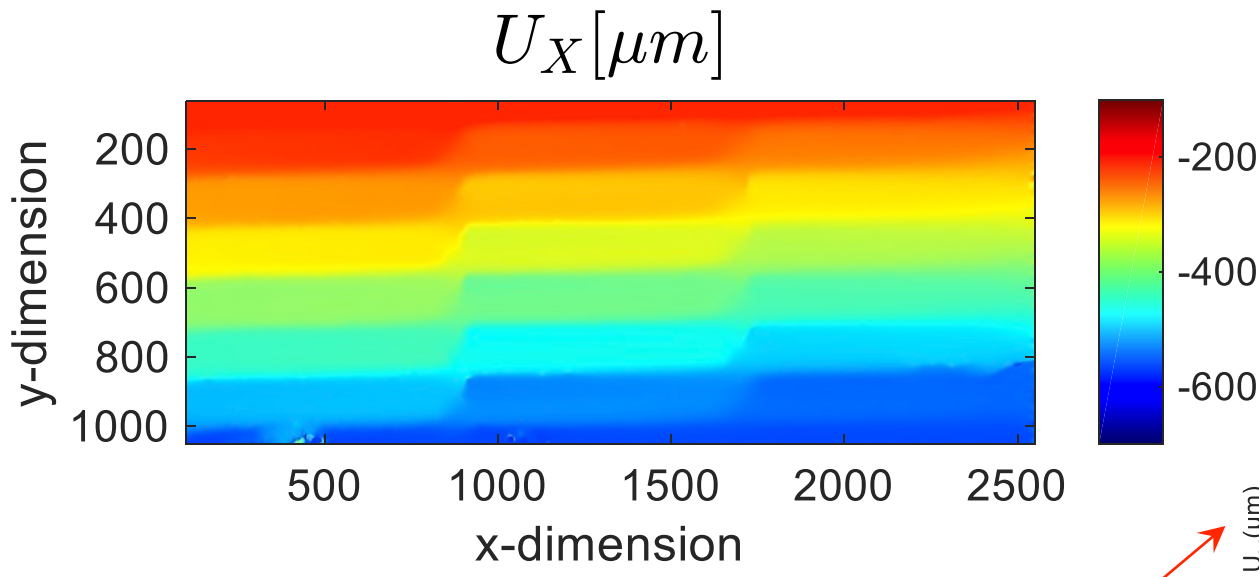
Displacement field at Point C₂



Strain + rotation fields at Point C₂

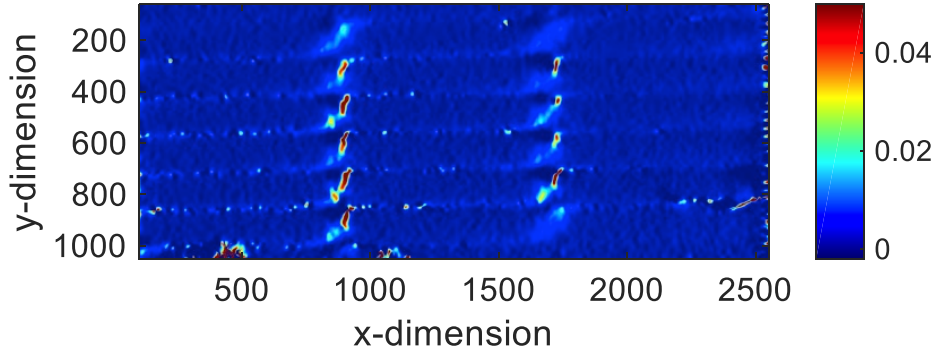


Displacement field at Point C₃

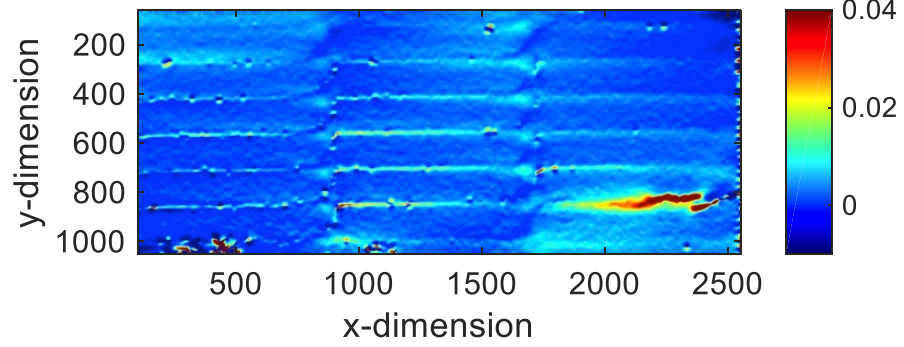


Strain + rotation fields at Point C₃

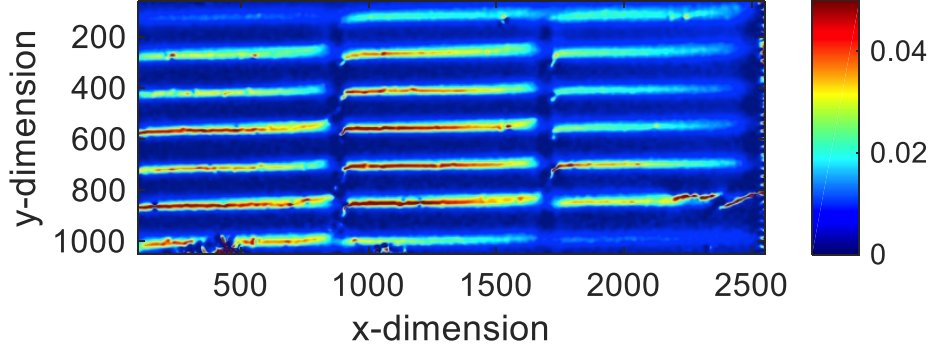
ϵ_{xx}



ϵ_{yy}



ϵ_{xy}



$W [^\circ]$

