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#### D. Teytelman

Dimtel, Inc., San Jose, CA, USA

Next Generation Beam Position Acquisition and Feedback Systems

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#### Leo Tolstoy, "Anna Karenina"

All happy families are alike; each unhappy family is unhappy in its own way.

- Deficiency in any one of a large number factors can lead to failure;
- For success one must avoid all of these deficiencies;
- ► A slight variation in the context of accelerators and feedback:
  - Coupled bunch instabilities are excited by a wide variety of sources:
  - Instabilities exhibit a wide variety of behaviors;
  - Consequently, each storage ring presents unique set of challenges for feedback stabilization;
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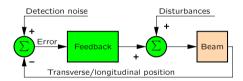
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- Spectrum is determined by feedback channel measurement noise, feedback gain, plus inevitable spur lines;
- Transfer gain from measurement noise to the feedback input is <sup>1</sup>/<sub>1+L(w)</sub>
- Maximum attenuation at the beam resonance produces a notch.

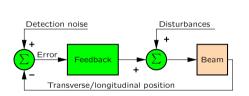
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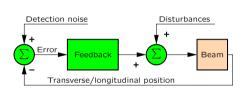
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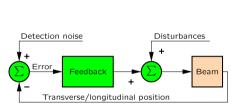
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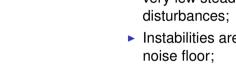
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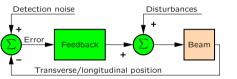
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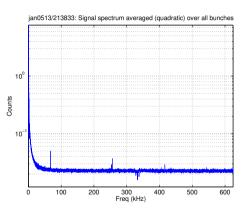
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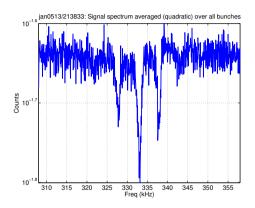
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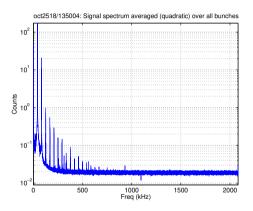
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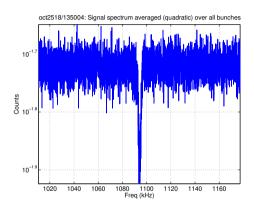
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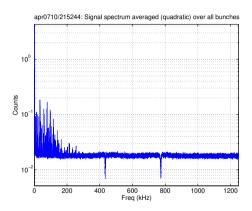
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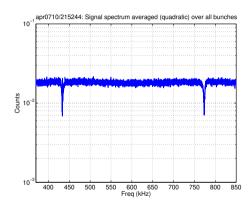
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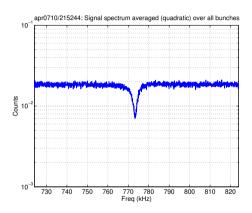
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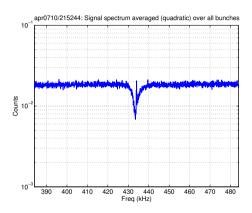
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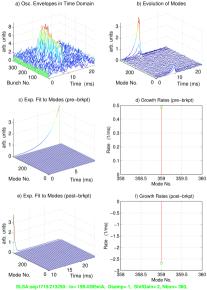
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At Fs: G1= 8.6734, G2= 0, Ph1= -74.4768, Ph2= 0, Brkpt= 13864, Calib= 1.

- Australian Synchrotron has 3 in vacuum undulators (IVUs);
- With IVU gaps open vertical instabilities are dominated by the resistive wall;
- When the gaps are closed, much faster modes appear;
- Scanned vertical growth rates vs.
   IVU gap to quantify the resonance.

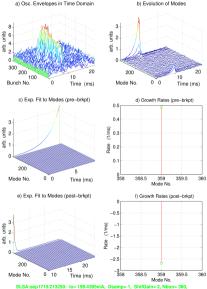
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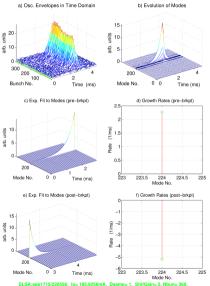
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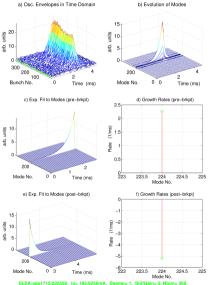
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SLSA:sep1715/220556: lo= 195.9256mA, Dsamp= 1, ShifGain= 5, Nbun= 360 At Fs: G1= 69.3875, G2= 0, Ph1= -74.4768, Ph2= 0, Brkpt= 4148, Calib= 1.

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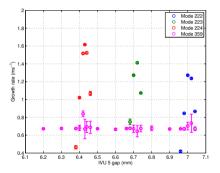
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- Moved the resonance over 3 revolution harmonics;
  - Resistive wall mode is more or less constant;
- Fit second order responses to each mode;
- Consistent results: bandwidth 75–78 μm;
- Impedance seems to increase as we get closer to the beam.

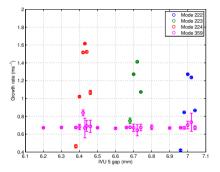
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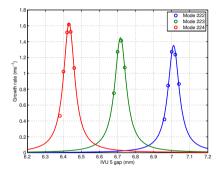
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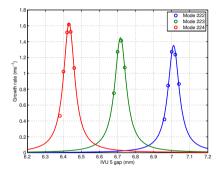
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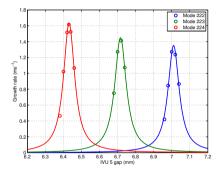
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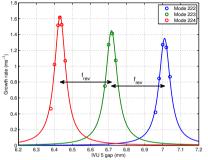
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# **IVU Impedance Conclusions**



- Resonant frequency seems to change linearly with the gap position:
  - Two revolution harmonic distances are within 3%;
- ► Tuning sensitivity 4.8 MHz mm<sup>-1</sup>;
- Bandwidth of 76 μm translates to 365 kHz;

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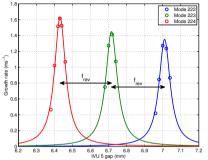
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Parameter	Measurement	Model
Tuning sensitivity, MHz mm <sup>-1</sup>	4.8	4.8
Bandwidth, kHz	360-374	239
CF @ 6 mm gap, MHz	186.4	194.4

# **IVU Impedance Conclusions**



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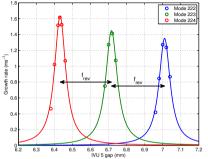
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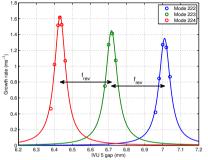
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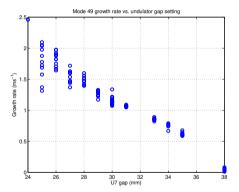
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#### APPLE II undulator;

- Instability threshold at 38 mm gap is 300 mA;
- Growth rates are going up monotonically with decreasing undulator gap;
- Betatron tune moves from 1105 to 1180 kHz during this scan;
- At some point in the range, low frequency (resistive wall?) modes pop up;
- All modes are easily suppressed by feedback, but the mechanism is still unclear.

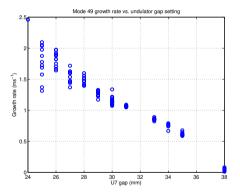
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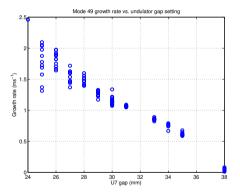
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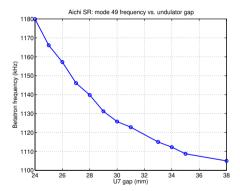
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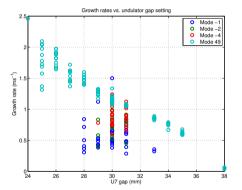
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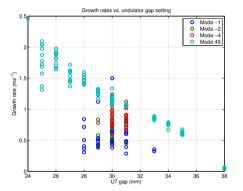
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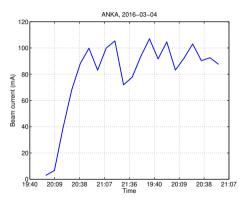
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#### **Initial Assessment**



- A ramping machine, 500 MeV injection, 2.5 GeV operation;
- Historically operated with only transverse feedback, relying on moderate longitudinal instabilities at injection energy to provide sufficient lifetime to accumulate beam;
- After a shutdown had problems injecting more than 100–120 mA, limited by sudden partial beam loss.

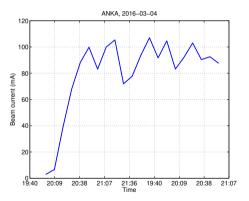
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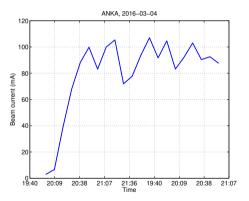
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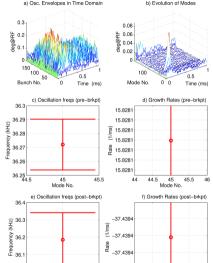
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#### Feedback in All Three Planes



Turned on feedback in the longitudinal plane;

- Still hitting a limit during injection,

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45.5 :mar0516/143809: lo= 138.1967mA, Dsamp= 2, ShifGain= 4, Nbun= 184, At v: G1= 108,2838, G2= 0, Ph1= -59,5791, Ph2= 0, Brkpt= 390, Calib= 34,252

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45

Mode No.

-37 4394

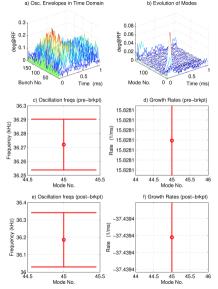
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Mode No.

45.5

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- Turned on feedback in the longitudinal plane;
- Still hitting a limit during injection, with partial beam losses;
  - Feedback tuned near absolute limit, growth time 2.3  $\times$  *T<sub>s</sub>*, damping time *T<sub>s</sub>*;

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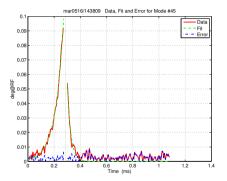
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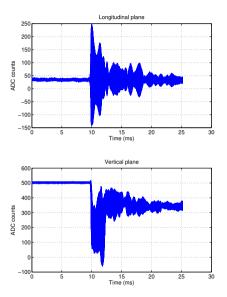
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- Noticed significant activity in the vertical plane during beam loss events;
- Used baseband processor output to trigger acquisition in all planes;
- Vertical correction signals are normally small, only reaching full-scale during beam loss;
- Longitudinal and vertical signals for bunch 140.

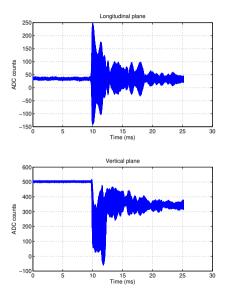
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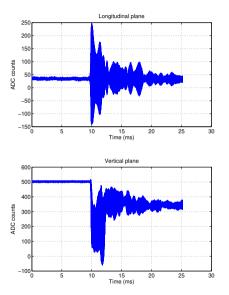
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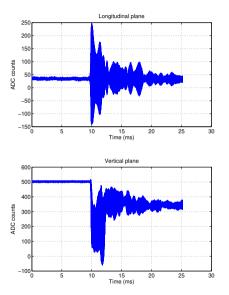
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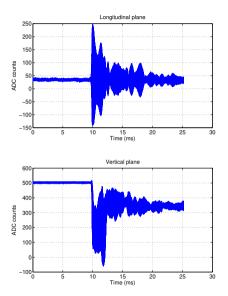
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#### Which plane came first?

- Zoom in, still too close;
- Zoom more looks like longitudinal starts first, but could be trigger error;
- Longitudinal oscillation amplitude exceeds 30°;
- Modal analysis in Z shows mode 46 rapidly running away under full feedback control.

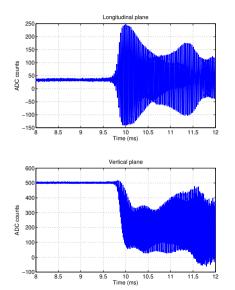
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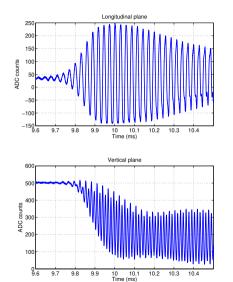
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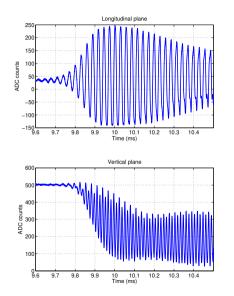
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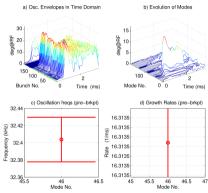
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ANKA:mar0416/015147: lo= 94.1744mA, Dsamp= 1, ShifGain= 4, Nbun= 184, At v: G1= 76.0692, G2= 76.0692, Ph1= 15.1664, Ph2= 15.1664, Brkpt= 1600, Calib= 34.252. Which plane came first?

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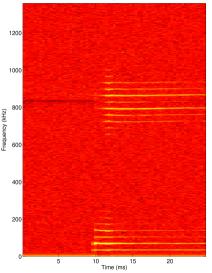
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#### Bunch 140 during beam loss event



#### Spectrogram of vertical bunch signal settles it!

- Longitudinal motion starts first, seen mostly as second harmonic in the amplitude detector channel;
- At beam phase excursions exceeding 90° at detection frequency, vertical feedback gain flips;
- Positive feedback excites vertical motion, causes beam loss.

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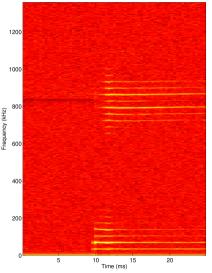
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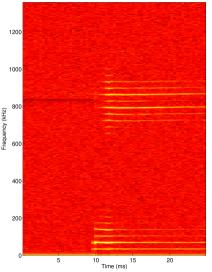
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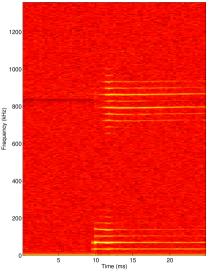
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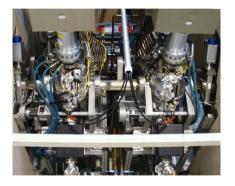
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#### RF cavities in ANKA are compression tuned;

- During injection, LLRF adjusts cavity tuning to compensate for beam loading;
- All cavity HOMs tune at the same time;
- By adjusting cavity temperature we shifted the problematic HOM enough so that synchrotron sideband crossing happened at much lower beam current;
- Growth rates scale with current, feasible to control!

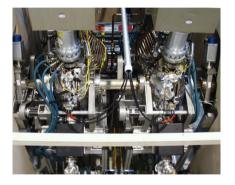
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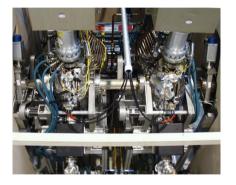
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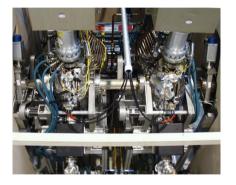
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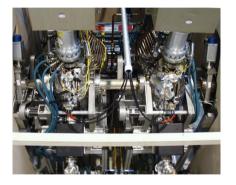
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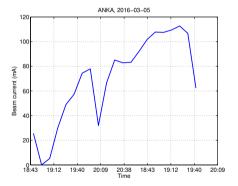
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# The Final Problem



- After adjusting cavity temperature we were able to keep the beam stable in X, Y, and Z;
- New problem with all planes stable, injection saturated around 110 mA due to poor Touschek lifetime;
- Streak camera, stabilized beam;
- Applied quadrupole excitation through the LFB;
- Bunch lengthening leads to Touschek lifetime improvement;
- With both feedback and modulation injected 160 mA and ramped to 2.5 GeV.

Coupled-bunch Instabilities and the Anna Karenina Principle

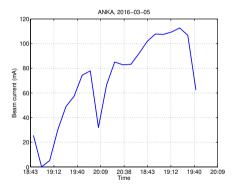
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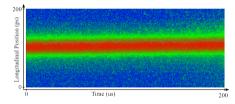
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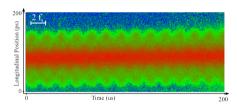
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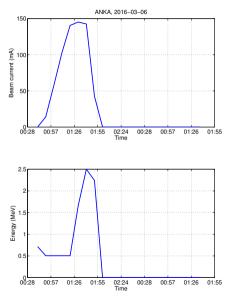
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# **ANKA Summary**

- Historically operated with only transverse feedback, relied on moderate longitudinal instabilities at injection energy to provide sufficient lifetime to accumulate beam;
- Changes during a shutdown prevented injection above 100–120 mA
- Investigation showed:
  - Longitudinal HOM in RF cavity crossed synchrotron sideband around 110 mA;
  - Vertical beam loss mechanism large longitudinal oscillation moved vertical bunch-by-bunch feedback into positive range;
  - Longitudinal growth rates unfeasible to control with feedback;
  - Adjusted cavity temperature to move sideband crossing to lower current, could run with full feedback control in all three planes;
  - With fully stabilized beam, lifetime dropped, injection saturated at 110–115 mA;
  - Used swept quadrupole excitation to control bunch length and lifetime, injected to 160 mA, successfully ramped.

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#### New Machines and Challenges

- Transversely, new light sources and colliders are going become more and more sensitive to residual dipole motion;
  - For low-emittance machines, residual motion should be below 10% of transverse beam size;
  - Usually more critical in the vertical plane;
  - Low-noise techniques in RF front end and digitizer design are required;
  - Most designers do not care about spurs 100 dB below ADC full scale;
  - Since bunch-by-bunch feedback settles to the front end/digitizer noise floor, any spur can ruin performance.
- Longitudinally, harmonic cavities used for lifetime improvement create major difficulties for bunch-by-bunch feedback:
  - Synchrotron tune is pushed down and tune spread increases;
  - Conventional topology can handle tune spread of 2:1 at most.

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#### Transverse Feedback and Noise

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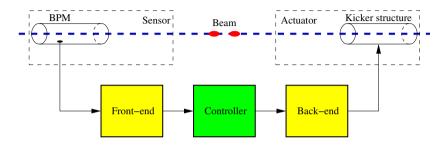
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#### Bunch-by-bunch Feedback



- Sensor (pickup);
- Analog front-end;
- Controller;
- Analog back-end;
- Actuator (kicker).

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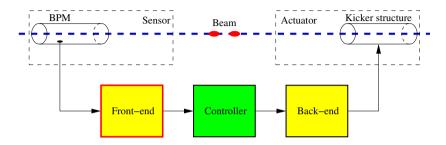
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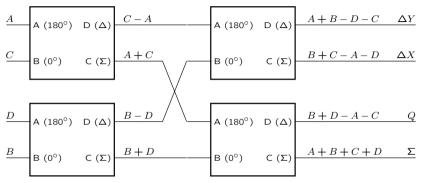
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First stage of BPM signal processing — separating X/Y/Z signals

- Since we are digitizing in the end, why not digitize raw signals?
- ▶ For X and Y we are dealing with small differences of large signals;
- If we can reject the common-mode at 20–30 dB level, that is also the gain of low-noise amplifier we can use to improve sensitivity.

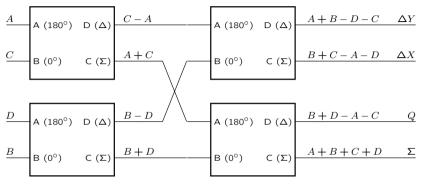
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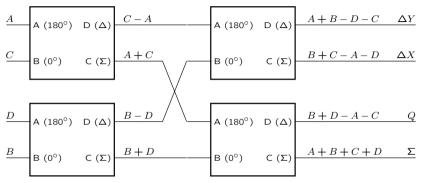
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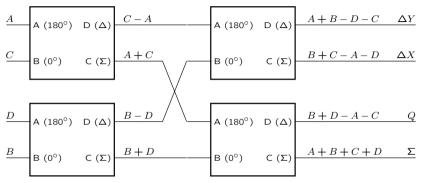
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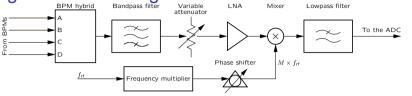
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#### Analog Front-end Design



- Front-end requirements:
  - Low amplitude and phase noise;
  - Wideband to ensure high isolation between neighboring bunches.
- Input bandpass filter is an analog FIR filter that replicates BPM pulse with spacing, matched to detection LO period;
- Detection frequency choice:
  - High frequencies for sensitivity;
  - Must stay below the propagation cut-off frequency of the vacuum chamber.
- Local oscillator adjusted for amplitude (transverse) or phase (longitudinal) detection.

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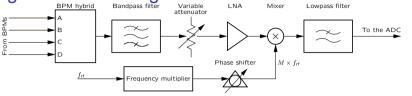
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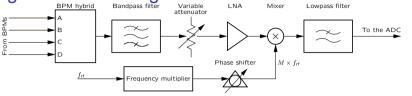
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#### Examples of Front-End Sensitivities Achieved

#### **Vertical Plane**

Machine	Atten.	Calibration	At nominal current
SPEAR3	0 dB	0.54 counts/mA/µm	0.96 counts/µm
MAX IV 3 GeV	0 dB	0.98 counts/mA/µm	2.8 counts/µm
ASLS	2 dB	1.24 counts/mA/µm	0.83 counts/µm

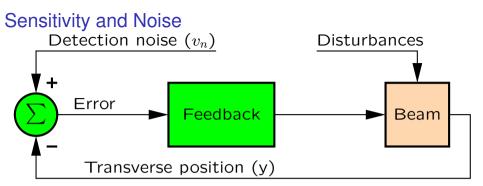
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- Complementary sensitivity S(ω) is the transfer function between noise v<sub>n</sub> and beam motion y;
- Assuming flat spectral density for v<sub>n</sub> can calculate amplification or attenuation of sensing noise;
- $\blacktriangleright$  Qualitatively, faster damping corresponds to wider bandwidth  $\rightarrow$  higher noise sensitivity;
- Rule of thumb: closed loop damping rate should be of the same magnitude as open-loop growth rate.

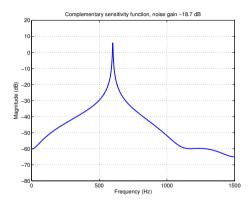
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- Growth and damping times in turns;
- $\tau_{\rm ol} = \tau_{\rm cl} = 300: -18.7 \text{ dB}$
- $\tau_{\rm ol} = \tau_{\rm cl} = 30: -8.1 \text{ dB}$
- ▶  $\tau_{\rm ol} =$  30,  $\tau_{\rm cl} =$  3.2: -6.0 dB
- ▶  $\tau_{\rm ol} = 5.4, \, \tau_{\rm cl} = 5.4$ : 3.8 dB
- Fast growth rates result in higher noise sensitivity.

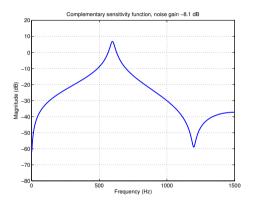
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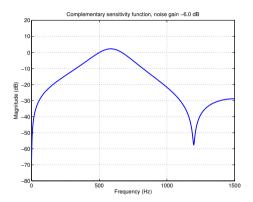
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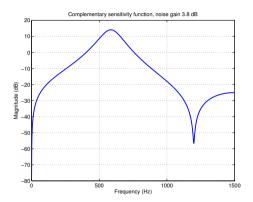
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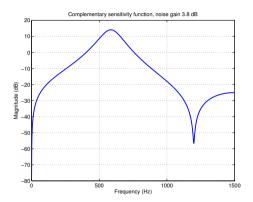
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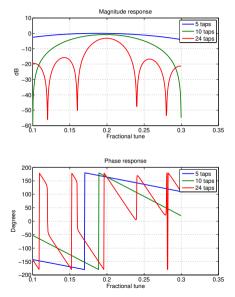
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#### Feedback Filter Design



- Transverse feedback FIR filters, tune of 0.2, adjusted for the same closed-loop damping time (τ<sub>cl</sub> = τ<sub>ol</sub> = 30 turns);
- Conventional wisdom shorter filter can generate faster damping, longer filter is quieter due to narrower bandwidth;
- Let's see what complementary sensitivity function tells us.

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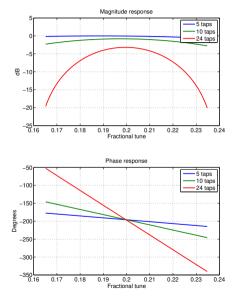
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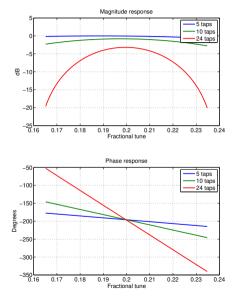
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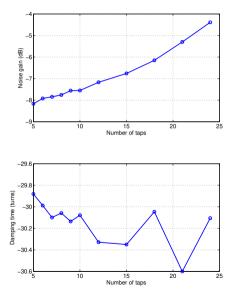
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- Integrated noise gain increases with filter length;
- Effect of the group delay;
- ► S(ω) get more peaked with larger group delay;
- Only applicable in white noise situation, with narrowband spurs/interferers response notches can be helpful.

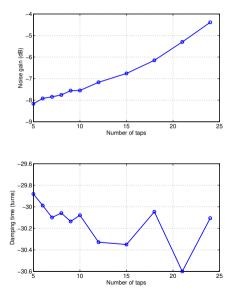
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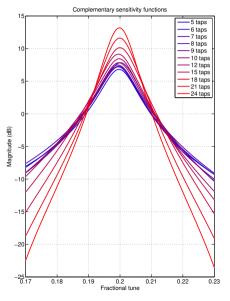
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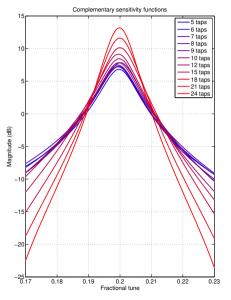
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Summary

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- Basic method: use horizontal signal from a pickup in a high dispersion location to sense energy oscillation directly;
- Eliminates the need to generate a 90° phase shift between longitudinal position measurement and energy kick;
- Feedback filter is just a gain plus two constraints:
  - High-pass transition below the synchrotron frequency band to filter out DC orbit offsets;
  - Low-pass transition above the synchrotron frequency band to remove horizontal signals.
- Can't handle full lengthening, when synchrotron frequency band extends to DC;
- Single pickup setup will respond to injection transients (horizontal) and erroneously drive longitudinal plane;
- Use two pickups with 0° or 180° relative phase advance to eliminate horizontal signals?

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- Can't handle full lengthening, when synchrotron frequency band extends to DC;
- Single pickup setup will respond to injection transients (horizontal) and erroneously drive longitudinal plane;
- Use two pickups with 0° or 180° relative phase advance to eliminate horizontal signals?

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Future Challenges Transverse Feedback and Noise Longitudinal Instabilities and Harmonic Cavities

- Basic method: use horizontal signal from a pickup in a high dispersion location to sense energy oscillation directly;
- Eliminates the need to generate a 90° phase shift between longitudinal position measurement and energy kick;
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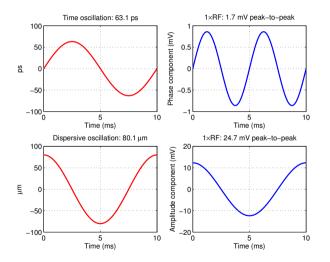
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#### ▶ 352 MHz;

- ▶ 704 MHz;
- ▶ 1056 MHz;
- ▶ 1408 MHz;
- ▶ 1760 MHz;
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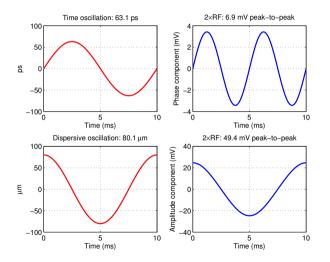
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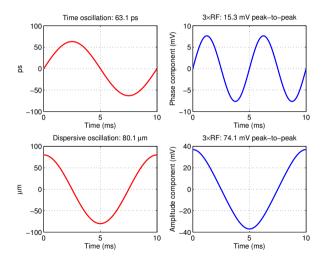
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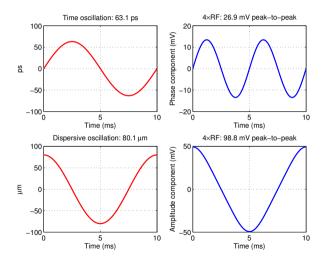
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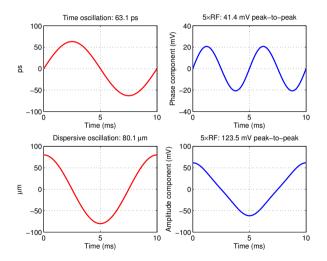
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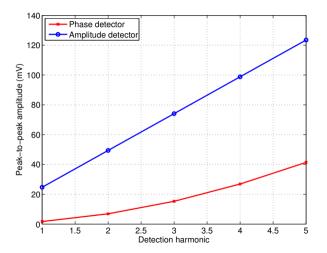
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Future Challenges Transverse Feedback and Noise Longitudinal Instabilities and Harmonic Cavities

- Bunch-by-bunch feedback can make different machines look alike, but it takes good system design and thorough understanding of driving terms;
- Never trust a "mild" instability you never know when it will turn into a showstopper;
- Characterization of instabilities is a definite must for robust feedback operation;
- New low-emittance machines demand noise-figure optimized RF front-ends and digitizers;
- Longitudinal feedback in presence of harmonic cavities is challenging, new (so far untested) energy sensing technique might help.

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