

New layout for alternative ring and wiggler magnet considerations of SPS

20th FCC-e⁺e⁻ Injector Meeting

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For alternative design:

- After FCC week, **new layout study**
- **Phase advance scanning** for optimum selection,
- **Optics functions** and general **parameters**,
- First calculations for DA.

For SPS:

- **Robinson wiggler** for SPS to reduce the emittance.

New Layout

Red: quadrupole magnet Green: sextupole magnet

Different phase advances are chosen in the straight section and in the arcs. Wiggler magnets are located in one of the straight sections.

Phase advance in the arc

h/v emittance is mainly determined by arcs in the ring. Thus, FODO phase advance in the arc is scanned to observe the behavior of some important parameters like emittance, chromaticity, tune shift with amplitude, momentum compaction factor etc.

- Minimum emittance can be obtained with the horizontal phase advance ~ 0.383 .
- Emittance is getting higher slightly while the vertical phase is getting higher.
	- With the experience from CLIC damping ring, 0.1 is chosen for the vertical phase.

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Phase advance in the arc

h/v emittance is mainly determined by arcs in the ring. Thus, FODO phase advance in the arc is scanned to observe the behavior of some important parameters like emittance, chromaticity, tune shift with amplitude, momentum compaction factor etc.

Phase advance in the straight section

Having close to 90 degree phase advance in the straight section provides small beta functions and efficient injection/extraction scheme. But still, phase advance scanning can be done for 80-100 degree; exact phase advance to be decided for working point selection. As expected, emittance, chromaticity, tune shift with

Optic functions and general parameters (0.25/0.25 at straight section)

First, I checked the ideal phase advance for straight section

Phase advances is chosen to be (μ_x, μ_y) = (0.25/2π, 0.25/2π) for the straight section, corresponding to a tune working point of (Q_x, Q_y) = (76.90, 28.75) for the ring.

Dynamic aperture simulations were undertaken, the horizontal versus vertical DA for different momentum deviations using MADX-PTC.

And then, I moved the WP to have better DA.

Phase advances is chosen to be **(μ^x , μ^y) = (0.247/2π, 0.245/2π)** for the straight section, corresponding to a tune working point of (Q_x, Q_y) = (76.76, 28.56) for the ring.

Dynamic aperture simulations were undertaken, the horizontal versus vertical DA for different momentum deviations using MADX-PTC.

Phase advances is chosen to be **(μ^x , μ^y) = (0.237/2π, 0.246/2π)** for the straight section, corresponding to a tune working point of (Q_x, Q_y) = (76.29, 28.67) for the ring.

Dynamic aperture simulations were undertaken, the horizontal versus vertical DA for different momentum deviations using MADX-PTC.

12 **This was an unexpected DA and it gave the idea to check out the higher order resonances.**

Resonance driving terms

Figures shows the dependence of the third order resonance driving terms on the horizontal and vertical phase advances of a FODO cell.

Comparing to the 5 Hamiltonian modes, the (1,0,1,1) mode is excited at low horizontal phase advance.

The non-linear coupling terms (1,0,2,0) mode is excited at low and high vertical phase advance.

And for (1,0,0,2) suppressed area could be selected with horizontal and vertical phase advances.

Resonance driving terms

Because of the strong sextupoles and understanding from DA calculation, higher modes are also checked. Figures shows the dependence of the fourth order resonance driving terms on the horizontal and vertical phase advances of FODO cell.

Hamiltonian modes can be suppressed with around 0.26 horizontal and 0.23 vertical phase advances of FODO cell.

Resonance driving terms

 $1e6$

 0.28

 0.28

 $1e6$

 $1e7$

 2.00
 1.75

1.50

1.25

1.00

 0.75

 0.50
 0.25

 -1.6
 -1.2
 -1.2
 -0.8
 -0.6
 -0.4
 -0.2

5

 $\overline{4}$

3

 $\overline{2}$

15

An optimal choice of phase advances is chosen to be **(μ^x , μ^y) = (0.263/2π, 0.225/2π)** for the straight section, corresponding to a tune working point of (Q_{x} , Q_y) = (77.49, 27.70) for the ring.

An optimal choice of phase advances is chosen to be **(μ^x , μ^y) = (0.263/2π, 0.225/2π)** for the straight section, corresponding to a tune working point of (Q_{x} , Q_y) = (77.49, 27.70) for the ring.

Dynamic aperture simulations were undertaken, the horizontal versus vertical DA for different momentum deviations using MADX-PTC.

17 **better dynamic aperture. DA with errors should still be checked in the After the optimization by checking the resonance driving terms, we have following days.**

SPS (Reminder)

or less

Parameter scaling are done for wiggler magnets in SPS to be able to determine the wiggler magnet characteristics to reduce the emittance to 5nm.rad.

Horizontal emittance, damping time and energy loss per turn are stated in the table with wiggler with the total length of 23 m and 5 T magnetic field.

Can we find another

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Robinson Wiggler for SPS

This is another option that we recently started to discuss after T. Tydecks' recommendation. Here, there are some first estimations for RW.

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\varepsilon_0 = c_q \gamma^2 \frac{I_5}{J_x I_2}
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\varepsilon_0 = c_q \gamma^2 \frac{I_5}{J_x I_2}
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\varepsilon_0 = c_q \gamma^2 \frac{I_5}{J_x I_2}
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\varepsilon_0 = c_q \gamma^2 \frac{I_3}{J_x I_2}
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\varepsilon_0 = c_q \gamma^2 \frac{I_3}{J_z I_2}
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\varepsilon_0 = c_q \gamma^2 \frac{I_3}{J_z I_2}
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I_1 = \oint \frac{\eta_x}{\rho} ds
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I_2 = \oint \frac{1}{\rho^2} ds
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I_3 = \oint \frac{1}{\rho^3} ds
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I_4 = \oint \frac{\eta_x}{\rho^3} (\frac{1}{\rho^2} + 2k_1) ds
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I_5 = \oint \frac{\mathcal{H}_x}{\rho^3} ds
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I_6 = \frac{c_\gamma}{2\pi} E^4 I_2
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$$
I_7 = \int \frac{1}{\rho^3} \frac{1}{\rho^3} ds
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I_8 = \oint \frac{1}{\rho^3} ds
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I_9 = \frac{1}{2\pi} E^4 I_2
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I_1 = \oint \frac{1}{\rho^3} ds
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I_2 = \oint \frac{1}{\rho^3} ds
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I_3 = \oint \frac{1}{\rho^3} ds
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I_4 = \oint \frac{\eta_x}{\rho^3} (1 + 2k_1) ds
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I_5 = \oint \frac{\mathcal{H}_x}{\rho^3} ds
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I_6 = \frac{1}{2\pi} E^4 I_2
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I_7 = \int \frac{1}{\rho^3} ds
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I_8 = \oint \frac{1}{\rho^3} ds
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$$
D = \frac{\rho_0 \eta_x}{\pi (\rho_0 B_0)^2} \left\langle B_w \frac{d B_{w,z}}{dx} \right\rangle L_w
$$

 \boldsymbol{I} .

Robinson Wiggler for SPS

For D=-1.5 9 m normal wiggler for 5 nm.rad emittance

Robinson Wiggler for SPS

Since the emittance reduction is limited with only RW, we are working on a plan to include **both normal wigglers and Robinson wigglers** to the ring. Thus, the emittance can be reduced to 5 nm.rad from 50 nm.rad by keeping the energy loss per turn around 70 MeV. The left plot shows the D without RW, emittance without any wiggler, emittance with wiggler and emittance with RW.

$$
D = \frac{\rho_0 \eta_x}{\pi (\rho_0 B_0)^2} \left\langle B_w \frac{d B_{w,z}}{dx} \right\rangle L_w
$$

After first calculations, the emittance is estimated to reduce to 12 nm.rad from 50 nm.rad by using normal wiggler magnet with 9 m and 5 T, and it is reduced again to 5 nm.rad from 12 nm.rad by using 1-2 m, ̴1 T Robinson wiggler.

Detail studies and simulations should still be done.

Energy Loss per Turn for SPS

Since the emittance reduction is limited with only RW, we are working on a plan to include **both normal wigglers and Robinson wigglers** to the ring. Thus, the emittance can be reduced to 5 nm.rad from 50 nm.rad by keeping the energy loss per turn around 70 MeV.

As it can be seen in the plot, when D is around zero (which means there is no Robinson wiggler), the energy loss per turn is around 160 MeV to be able to have an emittance around 5 nm.rad. However, the energy loss per turn reduces to around 70 MeV when D is around -1.5 (which means there is Robinson wiggler as changing the damping partition to -1.5 from 0).

Wiggler magnets in SPS

Simulations for RW are not done yet for SPS 23

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- New layout for alternative ring is provided;
	- o DA studies with errors should be done,
	- o Frequency map analysis should be done,

- Analytical calculations are done for planned wigglers of SPS;
	- o RW simulations should be done for SPS.